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**EVAPORATION OF A THICKENED AGENT SIMULANT  
FROM OAK AND HICKORY LEAVES**

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**December 1990**

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Diethyl malonate  
Viscosity  
Wind speed  
Vapor recovery  
Spread factor

K125  
Factorial design  
Relative humidity  
Northern red oak  
Shagbark hickory  
Vapor concentration



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## EXECUTIVE SUMMARY

Studies conducted in recent years have resulted in greater importance being attached to chemical defense against attack by thickened agents of intermediate and low volatilities. If the contaminant is a thickened chemical agent, droplets significantly larger than normal will be deposited on a target area, posing a longer term hazard for liquid contact. Further, the droplets constitute an emitting source for the formation of a secondary vapor cloud. Under some conditions, the hazard from the vapor may outweigh that from the liquid. These effects have been modeled in several ways, but selecting the most appropriate formal model and model improvements has been handicapped by a lack of sufficient experimental data to verify the modeling aspects. One of the critical data gaps pertains to the quantity of vapor that becomes airborne and its rate of evolution from droplets of thickened CW agents deposited on various natural-occurring surfaces and common structural materials.

Phase III of a three-phase research program designed to fill part of this data gap has been completed. Basic experimental information has been obtained to characterize the evaporation and sorption losses of thickened liquid droplets deposited on two leaf surfaces (Northern Red Oak and Shagbark Hickory) under a variety of conditions.

To aid in identifying and clarifying the most critical parameters controlling the persistence and evaporation characteristics of thickened liquid droplets deposited on a leaf surface, a bi-level fractional factorial experimental design was followed. The variables treated included the following:

- Liquid viscosity: 100 and 1,000 centipoise (cP); the liquid simulant was thickened with EA K125 copolymer to achieve the specified zero shear viscosities
- Average wind speed over the droplets: 3 and 11 mph
- Leaf surface: either the bottom or top surface of the leaf was contaminated
- Leaf type: oak and hickory leaves collected from the Edgewood Area of Aberdeen Proving Ground
- Leaf condition: green leaves picked in September, and red/yellow/orange leaves gathered in October.

Two bi-level factorial screening experiments were conducted. In all experiments, the leaves were contaminated with 2 mm diameter droplets of thickened diethyl malonate (DEM) and the air temperature was controlled at 60 F. The relative humidity (RH) in the experiments was not controlled. The average RH was 42% +/-8% standard deviation (SD). An area of approximately 4 ft<sup>2</sup> (4 ft by 1 ft) was contaminated in each test. The contamination density was 30 g/m<sup>2</sup>. A previous study showed that there was no significant difference in droplet evaporative behavior at a contamination density of either 30 g/m<sup>2</sup>, or 10 g/m<sup>2</sup> (NATO Standard); therefore, the former was chosen for experimental reasons.

Factorial analysis, as well as analysis of variance (ANOVA), was employed to obtain a clearer understanding of the effects the variables on the evaporation and spreading characteristics of the droplets of thickened DEM deposited on the leaf surface. The following seven droplet evaporation characteristics were studied:

- The percentage of contamination recovered after the 1st, 2d, 3d, and 6th hr from droplets deposited on the leaf surface
- The average droplet evaporation rates (micrograms per minute) based on a 1st, 2d, 3d, and 6th hr after deposition
- The half-life (minutes) of a droplet in the array of droplets deposited on the leaf surface or the time required to recover 50% of the initial (volatile) contaminant
- The average evaporation and recovery rates (micrograms per minute) associated with the half-life of the contaminant
- The total percentage of the contamination recovered as vapor from the droplets deposited on the leaf surface
- The lifetime of the droplet contamination deposited on the leaf surface
- The average evaporation rate (micrograms per minute) over the lifetime of the droplet contamination

In general, the factorial analysis and the ANOVA results are in good agreement. Wind speed is the most dominant factor affecting the amount, the rate of return, and the duration of the 2 mm diameter droplets of thickened DEM deposited on a leaf surface at 60 °F ambient temperature. The effect produced by wind speed is predominantly a direct effect. The wind speed factor alone can explain most of the total variation (80/88%) in the droplet evaporation characteristics that were studied in the two factorial experiments. Only one exception was found. In Experiment 2, the total percentage of contamination recovered was strongly dependent on the viscosity of the deposited liquid droplet and either the condition or age of the oak leaf.

Differences in droplet weathering on contaminated leafy surfaces at 3 and 11 mph are significant. Initially (0-3 hr), the average droplet evaporation rate of the deposited 2 mm diameter droplets at 3 mph is one-half the evaporation rate of the deposited droplets exposed to 11 mph wind speed. However, after 6 hr, the average droplet evaporation rate at 3 mph is nearly two-thirds the droplet evaporation rate at 11 mph. The difference in lifetime of the deposited droplets at 3 and 11 mph is approximately 10 hr, and there is a 3-hr difference in the half-life of the 2 mm diameter droplets.

The leaf surface (top versus bottom) is the second most dominant factor affecting the evaporation behavior of the deposited DEM droplets. The DEM droplets spread substantially more on the top surfaces of the oak and hickory leaves than on the bottom surfaces. This, in turn, affects the initial droplet evaporation characteristics for times, up to 6 hr (the last

time increment in the analysis), after contamination. However, the long-term yields associated with the droplet contamination, such as the total amount of contamination that evolves and surprisingly the lifetime of the deposited droplets, are not dependent on the leaf surface.

The leaf type (Northern Red Oak versus Shagbark Hickory) has only a minor effect on the evaporation of deposited DEM droplets. The measured differences in evaporation behavior for droplets deposited on the oak and hickory leaves are not considered to be operationally significant.

The condition or age of the oak leaf primarily affects the percentage of the liquid droplet contamination that eventually evolves. However, the final amount of liquid agent that is recovered as vapor from the oak leaf is strongly dependent not only on the condition or age of the leaf, but also on the initial viscosity of the liquid droplet.

The spread factor of a thickened DEM droplet deposited on a leaf surface is affected mainly by the leaf surface and the condition or age of the leaf. The leaf surface (top versus bottom) is the most dominant factor, and surprisingly the difference in spreading of a deposited droplet is greater between the top and bottom surfaces of the leaves investigated than between the leaf types. Liquid droplets spread on the top surface to a greater extent than on the bottom surface of both leaf species tested. The average spread factor for a deposited droplet is estimated to be 2.56 ( $\pm 0.236$  SD) on the top surface and 1.88 ( $\pm 0.052$  SD) on the bottom surface, for both the oak and hickory leaves.

However, there is also evidence that the condition or age of the leaf affects the spreading of the droplet on the leaf surface. A significant difference was detected in spreading of droplets deposited on the green September oak leaf and the red October oak leaf. This is manifested by the interaction effect between the leaf surface and the leaf condition in Experiment 2. The average spread factor for a droplet deposited on the top surface of a green oak leaf is 2.47 ( $\pm 0.292$  SD), whereas the average spread factor on the top surface of a red oak leaf is 1.95 ( $\pm 0.062$  SD). However, the average spread factors for the bottom surface of the green and red oak leaves are similar; 1.88 ( $\pm 0.004$  SD) and 1.79 ( $\pm 0.052$  SD), respectively.

The viscosity of thickened DEM (100/1,000 cP) and the wind speed (3/11 mph) over the ranges tested had no detectable effect on the extent of spreading of a droplet deposited on the oak and hickory leaves.

Perhaps one of the most significant results is that a simple first order mathematical expression is shown to be adequate for representing the disappearance of a thickened liquid agent simulant droplet from contaminated leaf foliage surfaces during the evaporation of the thin liquid film that is formed on the leaf surfaces. Droplet half-life is the key and critical parameter for predicting the evaporation of the candidate simulant agent from leaf foliage.

In summary, a clearer understanding has been obtained of the effects of liquid viscosity of deposited droplets, wind speed, and particularly the properties of contaminated foliage leaf, namely leaf surface, leaf type, and condition or age of the leaf on the evaporation and the spreading characteristics of deposited DEM droplets.

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## PREFACE

The work described in this report was authorized under Project No. 1L162706A553, CB Defense and General Investigations, Task 3-1, Chemical Threat Assessment Technology, and Project No. 1C464803DF95, XM135 MLRS Binary Chemical. This work was started in October 1981 and completed in June 1989. The experimental data are stored on an IBM PC/AT computer.

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## EVAPORATION OF A THICKENED AGENT SIMULANT FROM OAK AND HICKORY LEAVES

### 1. OBJECTIVE

This report documents the findings of the fourth in a series of experiments on the liquid droplet evaporation and persistency. This laboratory study was conducted to determine how much vapor contamination occurs, and at what rate the vapor contamination becomes airborne when the thickened agent simulant diethyl malonate (DEM) is dispersed in a uniform array of droplets on foliage, oak and hickory leaves. Once the source of vapors is better defined, the prediction of downwind concentrations can be accomplished with an appropriate model of surface evaporation to ascertain the vapor threat over the given period of evaporation for the threat agent.

### 2. INTRODUCTION

The need and requirements for experimental data to quantify the evaporation and the persistency of thickened liquid agents and simulants dispersed as droplets on various types of natural and structural materials have been outlined in several reports.<sup>1-4</sup> The need includes not only basic evaporation data (i.e., evaporation rates, percent recoveries, etc.) of droplet behavior on the various surfaces, but there is also a requirement to identify the parameters that control the evaporation and persistency of the deposited droplets and determine the extent of their influence over ranges of the parameters that are operationally significant.

An experimental program has been devised to collect the fundamental data needed to more clearly characterize and quantify the evaporation and sorption losses of chemical agents. This program has three related tasks: (1) to quantify the persistency and liquid availability of contamination from nonporous surfaces and determine the principal factors governing liquid persistency, (2) to quantify the evaporation and sorption losses for droplets deposited on porous surfaces of concrete and sand, and (3) to determine the vapor hazards from thickened persistent agents/simulants dispersed on vegetation, turf, and foliage.

In Phase I of this research study, various physical parameters and the extent of their influence on the persistency and liquid availability of deposited droplets on nonporous surfaces of unpainted aluminum and chemically inert Teflon substrates were identified by using two candidate thickened liquid agent simulants, DEM and methyl salicylate (MeS).<sup>2</sup> These two liquid agent simulants have been used extensively in the past as simulants for CW agents TGD and THD, respectively.

In Phase II, basic experimental information was obtained that characterized the evaporation and sorption losses of the candidate thickened MeS and DEM agent simulants deposited as droplets on wet and dry concrete,<sup>3</sup> and of DEM droplets deposited on several compositions of wet and dry sand.<sup>4</sup>

During previous studies, the following five droplet characteristics were quantified for test periods that ranged from 1 to 2 days: (1) the

half-life of the deposited droplet contamination, (2) the average evaporation and recovery rates associated with the half-life, (3) the percent of contamination that is vaporized and recovered from the concrete after 1, 2, and 3 hr, (4) the total percent of contamination from the deposited droplet that is vaporized and recovered from the concrete surface, and (5) the average droplet evaporation rates for 1, 2, and 3 hr after deposition.

In the experiments with concrete surfaces, the primary factors affecting the evaporation characteristics of MeS and DEM were the size of the deposited droplet and the prevailing temperature. Other controlled factors [i.e., viscosity of the thickened agent simulant, moisture content of the concrete, and the relative humidity (RH) of the incident airstream] had little effect on the evaporation characteristics of the deposited droplets for the conditions studied.

The best estimate for the total percent of recoverable contamination from concrete within 1 to 2 days was 75%, which was the extent of the measurement in this study. However, approximately two-thirds of the contamination that eventually evolved from the concrete was recovered within 2 to 3 hr after deposition at temperatures from 60 to 100 °F. Therefore, 3 hr were judged to be the critical period for secondary vapor hazard, following contamination of concrete with thickened agents having intermediate volatility.

The half-life of droplet contamination on concrete, or the time to recover 50% of the mass deposited, was principally affected by the prevailing temperature, the agent simulant characteristics (i.e., vapor pressure, spread factor, etc.), and the incident wind speed for the ranges of the variables tested.

The spread factor of a droplet deposited on concrete was found to be a function of the time after deposition. A maximum spread factor value of 6 [standard deviation (SD) = 1.2] was achieved after approximately 1 hr from an initial spread factor of 5 (SD = 1.27). However, except for the viscosity of the agent simulant, the other factors investigated, most notably the moisture content of the concrete, droplet size, and the liquid agent simulant, did not significantly influence the droplet spread factor in these experiments.

In the experiments with various compositions of wet and dry sand, the primary factors affecting the evaporation characteristics of DEM were the size of the deposited droplet, the ambient temperature, and the incident wind speed. Other controlled factors [i.e., viscosity of the thickened agent simulant, moisture content of the sand, composition of the sand (particle size), and the RH of the incident airstream] had little effect on the evaporation characteristics of the deposited droplet for the conditions studied.

Among the three dominant factors, the ambient temperature is the primary factor controlling the percent of contamination recovered as vapor from the droplets deposited on sand. For the first hour after contamination, wind speed is the second most important factor. However, after the first hour, the size of the droplet deposited on the sand had a slightly greater effect on the percent of contamination recovered than the wind speed. The size of the droplet is the primary factor controlling the evaporation rate of the liquid droplet deposited on sand. The temperature is the second most important factor, and the wind speed is the third most important factor

(parameter) affecting the average evaporation rates of the droplets during the 1-, 2-, 3-, and 6-hr sampling periods. In these experiments, there were interaction effects between the droplet size and the wind speed with the ambient temperature that also affected the evaporation rate of the droplets deposited on sand. Changes in both the ambient temperature and the wind speed had a greater effect on the larger (5 mm diameter) droplets than on the smaller (2 mm diameter) droplets.

The composition of the sand (particle size) had no detectable effect on either the percent of contamination recovered as vapor from the sand or on the average evaporation rate of the droplets deposited on sand during the 1-, 2-, 3-, and 6-hr sampling periods. A slightly greater percent of contamination of DEM droplets deposited on sand was recovered from wet sand than from dry sand for each of the sampling times; however, the differences in recovery were not statistically significant. Evaporation rates from wet sand were consistently greater than the rates for dry sand; however, the differences were within experimental error. Therefore, for all practical purposes, DEM droplets evaporate at the same rate during the first 6 hr whether they are deposited on dry or wet sand. Liquid viscosity [100 per 1,000 centipoise (cP)] of DEM had no detectable effect on either the percent of contamination recovered as vapor or on the average evaporation rates of the droplets deposited on sand during the first 6 hr.

The extent of spreading of a droplet deposited on sand, as measured by the spread factor, varied little for the conditions studied, and none of the six variables investigated in the experiment had a significant effect on the spreading of the droplet. The average spread factor for thickened DEM droplets, 2 and 5 mm diameter, on wet and dry sand was 2.7.

The available half-life data indicated that droplets of thickened DEM deposited on sand at 60 °F have a half-life of 2 to possibly 10 times greater than the half-life of the same droplets deposited on sand at 100 °F.

In this study and during Phase III of the research program, experiments were conducted of the evaporation of thickened DEM deposited as droplets on two species of leaves from oak and hickory trees at the Edgewood Area of Aberdeen Proving Ground. These experiments followed a 2<sup>4</sup> bi-level factorial design. The specific parameters of the experiments investigated included the following:

- Liquid viscosity: 100 and 1,000 cP--the liquid simulant was thickened with EA K125 copolymer to achieve the specified zero shear viscosities
- Average wind speed over the droplets: 3 and 11 mph
- Leaf surface: either the bottom or top surface of the leaf was contaminated
- Leaf type: oak and hickory leaves collected from trees in the Edgewood Area of Aberdeen Proving Ground
- Leaf condition: the green leaf picked in September, and the red/yellow leaf gathered in October.

Two bi-level factorial screening experiments were conducted. In all experiments, the leaves were contaminated with 2 mm diameter droplets of thickened DEM, and the air temperature was controlled at 60 °F. The RH in the experiments was not controlled. The average RH was 42 +/-8% SD.

An area of approximately 4 ft<sup>2</sup> was contaminated in each test. The contamination density was 30 g/m<sup>2</sup>. A previous study showed there was no significant difference in droplet evaporative behavior at a contamination density of either 30 g/m<sup>2</sup> or 10 g/m<sup>2</sup> (NATO Standard); therefore, the former was chosen for experimental reasons.

In keeping with the format established in previous reports and to aid in subsequent modeling efforts, an elaborate set of tables is provided for each test case that completely characterizes the evaporation of the array of uniformly spaced and sized droplets deposited on the leaf. The principal tables include vapor concentration values downstream from the contaminated area, residual droplet mass, cumulative mass recovered, evaporation rates as a function time for a deposited droplet, and total yield from the contaminated area. Data are also given on the extent of spreading of DEM droplets on the two leaf surfaces.

All tests were performed in a specially designed open circuit, low-speed wind tunnel, which are briefly described in this report. This wind tunnel can accommodate surfaces up to 6 ft in length. The primary measurement in each experiment was the time history of the vapor concentration, measured with a Miran IA infrared vapor analyzer. Data analyses and transformations of the spectrometer information were performed with the aid of a Fortran computer program described in a previous report.<sup>3</sup> This program was modified to be more interactive and to run on an IBM PC/AT computer, using a MICROSOFT Fortran Compiler (MICROSOFT, Bellevue, WA). A listing of the modified Fortran program is given in Appendix A.

### 3. EXPERIMENTAL DESIGN

In keeping with the test strategy initiated under Phase 1, a bi-level fractional factorial design was followed to develop a data base for clarifying the most critical physical parameters and the extent of their influence (main effects) on the persistency of liquid droplets on leaf surfaces.

Table 1 lists the variables and the test levels selected for investigation in this initial screening of variables and the experimental test matrix. The design consists of 16 distinct evaporation tests conducted at an ambient temperature of 60 °F. According to convention, a plus sign (+) and a negative sign (-) are used to indicate the high and low levels for each variable in each test. The experiment is a 2<sup>4</sup> factorial design and has a resolution of four (IV); however, because this is a complete factorial design in four variables, there are no confounding of main and interaction effects.

Two experiments were run using the factorial design. Variable 4 is the only variable that differs in these two experiments. In Experiment 1, variable 4 is the type of leaf (hickory versus oak), and in Experiment 2, variable 4 is the condition of the oak leaf (green versus red). The same



Table 1. Design Matrix for Factorial Experiments

| Test | Variables |   |   |    | Contrast |
|------|-----------|---|---|----|----------|
|      | 1         | 2 | 3 | 4* |          |
| 1    | -         | - | - | -  | Mean     |
| 2    | +         | - | - | -  | 1        |
| 3    | -         | + | - | -  | 2        |
| 4    | +         | + | - | -  | 12       |
| 5    | -         | - | + | -  | 3        |
| 6    | +         | - | + | -  | 13       |
| 7    | -         | + | + | -  | 23       |
| 8    | +         | + | + | -  | 123      |
| 9    | -         | - | - | +  | 4        |
| 10   | +         | - | - | +  | 14       |
| 11   | -         | + | - | +  | 24       |
| 12   | +         | + | - | +  | 124      |
| 13   | -         | - | + | +  | 34       |
| 14   | +         | - | + | +  | 134      |
| 15   | -         | + | + | +  | 234      |
| 16   | +         | + | + | +  | 1234     |

Variable Identities/Ranges:

1. Liquid Viscosity      (+) 1,000 cP      (-) 100 cP
2. Wind Speed              (+) 11 mph      (-) 3 mph
3. Leaf Surface            (+) Bottom      (-) Top

Experiment No. 1

4. Leaf Type                      (+) Oak      (-) Hickory

Experiment No. 2

4. Leaf Condition              (+) Green      (-) Red

\* Note: Only Variable 4 differs between experiments 1 and 2.

experimental design was used for both experiments. Thus, half the experiments performed in Experiment 1 pertaining to the oak leaves are also appropriate to Experiment 2. These eight tests (Tests 9-16) from Experiment 1 were not repeated and are used to complete the factorial design for both experiments.

#### 4. EXPERIMENTATION

##### 4.1 Test Materials.

##### 4.1.1 Candidate Chemical Agent Simulant.

Diethyl malonate was the candidate agent simulant used in this study. The physical properties of DEM closely approximates the nerve agent GD. The simulant is made viscoelastic by adding either a copolymer or polymer; in this form, the simulant closely mimics the properties of the thickened agent TGD. However, because the precise nature of the thickened threat agent is unknown, the test strategy was to bracket the operationally significant range of liquid viscosities. Therefore, two liquid viscosities (100 and 1,000 cP) were formulated by adding an appropriate concentration of a copolymer thickener (K125 EA)\* that were experimentally determined to be 2.8 and 4.8% (by weight) per 100 mL of DEM.

The pertinent physical properties of the candidate agent simulant, gathered from various sources, are in Table 2. The data on liquid vapor pressure were derived by performing a linear regression of reported vapor pressure values.<sup>4</sup> The coefficients for the evaporating liquid (in air) are based on the optimized Gilland-type equation. An experimental investigation has been undertaken by the Physical Chemistry Branch, Research Directorate, U.S. Army Chemical Research, Development and Engineering Center, to obtain the vapor pressure values for unthickened DEM in the temperature range of interest and the best fit predictive equation for the vapor pressure of DEM.<sup>5</sup>

##### 4.1.2 Contaminated Surface.

Two species of leaves were selected for this study. The Northern Red Oak (*quercus borealis*) and the Shagbark Hickory (*carya ovata*) were collected from trees at the Edgewood Area of Aberdeen Proving Ground. The oak and hickory leaves identified as green in the experimental design were picked during early September. Those leaves identified as red were actually multi-colored leaves (red/yellow/orange, etc.) that were collected from the same area during October of the same year. The Northern Red Oak measured 5-9 in. long by 4-6 in. wide, and had 5-11 unequal bristle-tipped lobes. The top surface of the leaf was a dark green, and the bottom surface was a paler green. The leaves appear in late spring, turn to either deep red or orange by fall, and hang on until late fall or winter. The hickory leaf is from the Shagbark Hickory, which is the most widespread type of hickory tree on the American continent. The compound leaves of the hickory are alternately

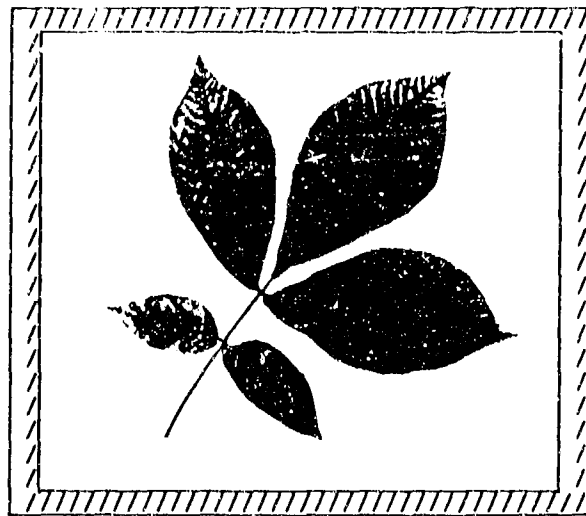
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\*Manufactured by Rohm and Haas, Philadelphia, PA. Copolymer EA K125 is 80% PMMA, 7% ethyl, and 13% butyl acrylate, with an MW of  $2.5 \times 10^6$ .

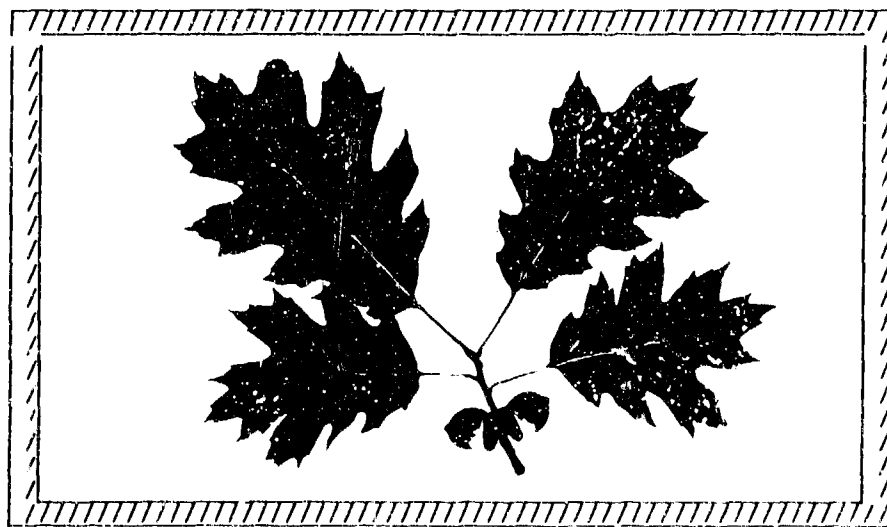
Table 2. Physical Properties of Chemical Agent Simulant

| Properties                        | Diethyl Malonate           |
|-----------------------------------|----------------------------|
| Molecular weight, gm/mole         | 160.17                     |
| Density, gm/cm <sup>3</sup>       | 1.055 @ 25 °C              |
| Surface Tension, dynes/cm         | 32.3 @ 25 °C               |
| Vapor Pressure, mm Hg             |                            |
| 60 °F                             | 0.195 (0.101) <sup>6</sup> |
| 80 °F                             | 0.427 (0.255)              |
| 100 °F                            | 0.885 (0.592)              |
| Diffusivity, cm <sup>2</sup> /sec |                            |
| 60 °F                             | 0.060                      |
| 80 °F                             | 0.0646                     |
| 100 °F                            | 0.0689                     |
| Volatility, µg/cm <sup>3</sup>    |                            |
| 60 °F                             | 1.739 (0.897)              |
| 80 °F                             | 3.659 (2.181)              |
| 100 °F                            | 7.310 (4.882)              |

arranged on a stem with five or seven leaflets. The narrow base of each leaflet is attached to the leaf stem. The three outer leaves are 4 to 6 in. long, while the lower (inner) ones are much smaller. Narrow at the base and wide at the top, the margin of each leaflet is toothed and the shape is described as obovate. Photos of the oak and hickory leaves are shown in Figure 1.



(a)



(b)

Figure 1. (a) Hickory Leaves (Carya Ovata), and  
(b) Oak Leaves (Quercus Borealis)

At the most, 1 to 2 weeks may have transpired between the time the leaves were collected and used in an evaporation experiment. To reduce the deterioration of the leaves during this period, the leaves were stored in sealed polyethylene bags and refrigerated. There was no discernible difference in the appearances of most of the leaves after 2 weeks of storage. The leaves that appeared to have changed were not used. No attempt was made in these initial screening experiments to investigate the effect of storage time of the leaves on the evaporation characteristics of droplets deposited on the leaves.

#### 4.2 Experimental Wind Tunnel Facility.

An overall view of the experimental Plexiglas wind tunnel facility that was designed for controlled large-scale evaporation studies is shown in Figure 2. Room air enters the wind tunnel through the inlet filter and the evaporator of a high-volume 27,000 BTU, water-cooled air conditioning unit (Koldwave Model K26DF) and exits into a laboratory fume hood. A large test section can accommodate contaminated materials up to 75 in. long. The walls of the wind tunnel downstream from the test section are lined with Bytac,\* a Teflon overlay, to prevent adsorption of vapors on the walls and to facilitate cleaning. The wind tunnel offers a wind speed range of approximately 1-15 mph, a temperature range of 10-40 °C, and a RH of 15-85%. Details of this facility have been described in an earlier report.<sup>2</sup>

#### 4.3 Procedures.

All the evaporation experiments were conducted, using approximately 4 ft<sup>2</sup> of exposed leaf surface. This leaf surface was contaminated with a uniform array of 2 mm diameter droplets to a deposition level of 30 g/m<sup>2</sup> (nominal values). The test leaf samples were supported and held in place horizontally 2 in. above the wind tunnel's floor by a specially designed wire rack, which had a mesh size of approximately 2 in. Two wire racks (25 in. long by 10.5 in. wide) were used in each evaporation experiment. The leaves were carefully positioned on the wire racks to form a continuous layer of overlapped leaves, without any large voids. This facilitated contaminating the leaves with a uniform array of test droplets and prevented the loss of any test droplets. A similar wire rack was also laid over the leaves. This prevented the leaves from flapping in the wind during the test.

The test droplets of the thickened DEM were expeditiously produced by simply immersing a rod into a liquid reservoir to a predetermined depth and then transferring the adherent liquid to the leaves by allowing the droplets to drip off the rod. This technique, which has been successfully employed in previous droplet evaporation experiments, makes use of a transfer block, with an array of uniformly spaced rods of the appropriate size, to expedite the contamination process and facilitate producing an array of droplets with the desired spacing. With this method, contaminating the two racks with droplets of DEM was accomplished in approximately 10-15 min. The total liquid mass contamination on each rack of leaves was determined gravimetrically with a standard laboratory beam balance. This provided a reliable

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\*Distributed by Bolab, Incorporated, Derry, NY

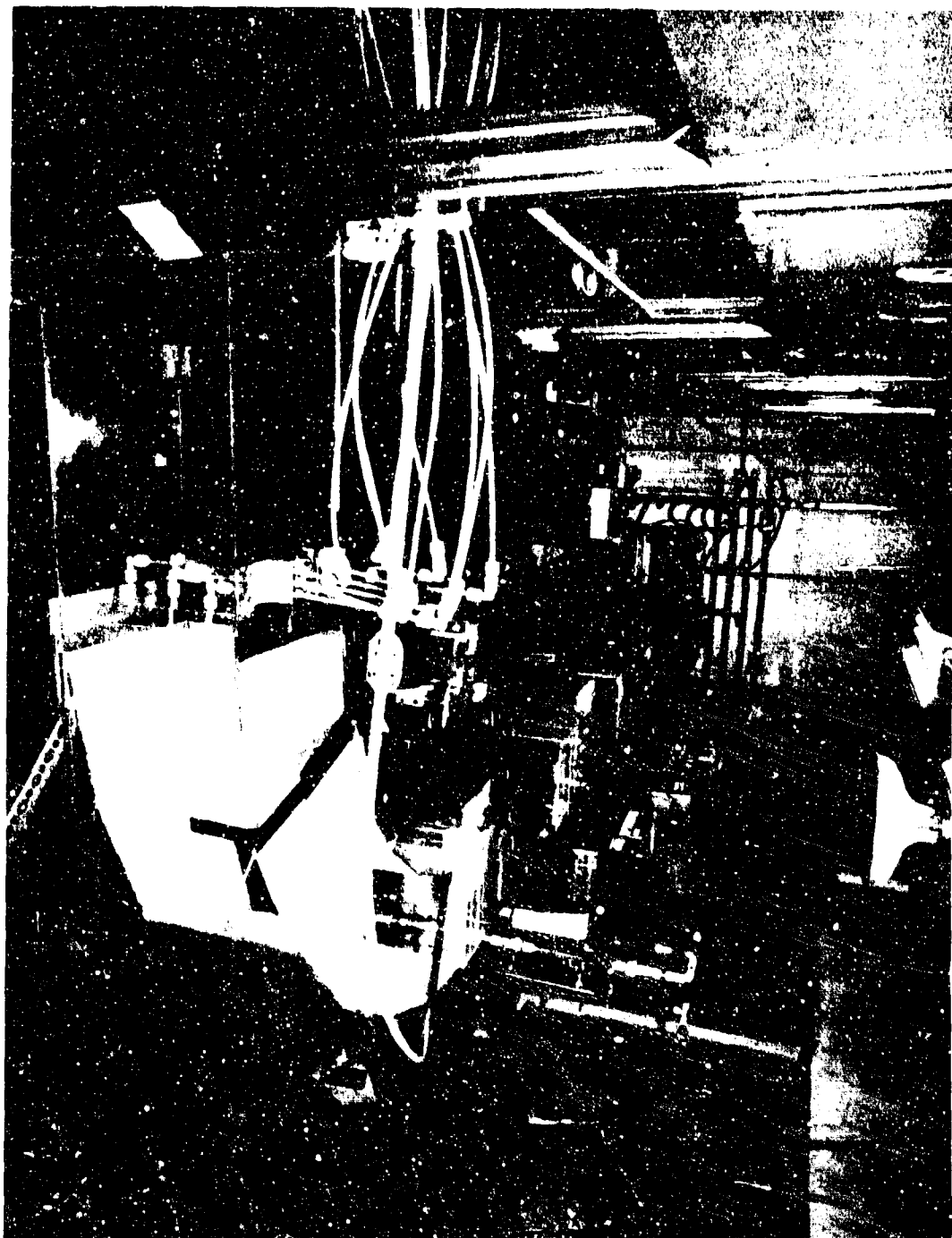


Figure 2. Experimental Wind Tunnel Facility

means of estimating the average droplet size per rack. The measurements of contamination mass had an accuracy of  $\pm 0.1$  g. Two contaminated racks of leaves were placed in the test section of the wind tunnel. These were butted together to form a continuous contaminated area (patch) 50 in. long by 10.5 in. wide.

During the course of an experiment, the incident air temperature and RH were measured with a Humitemp instrument\* and associated electro-humidity temperature sensors in a probe that was projected into the airstream ahead of the test section. The data were recorded on a standard two-channel strip chart recorder. The accuracy of the RH measurements is  $\pm 2.5\%$ , and the accuracy of the temperature measurement is  $\pm 0.5$  °C. The wind speed [feet per minute (fpm)] was measured with a direct reading, electronic anemometer,\*\* with a rotating vane that was also installed ahead of the test section. The stated meter accuracy was  $\pm 2\%$  of full-scale deflection. The surface temperature of the contaminated leaves was measured with copper constantan thermocouples and a multipoint digital/recording thermometer (Omega Model 2176A\*\*\*).

A measurement of the simulant vapor concentration in the airstream was made continuously at a location approximately 9 ft downstream from the contaminated area with a Miran IA analyzer† and recorded on a Linear Strip Chart recorder.†† The Miran IA is a single beam spectrometer variable filter that is capable of scanning the infrared spectral range between 2.5 and 14.5  $\mu\text{m}$ .

The vapor samples were obtained from a multipoint probe. The probe is a grid of nine symmetrically arranged sampling tubes located at a position downstream from the test section where a uniform vapor concentration profile was established (see Figure 2). During the course of the experiment, the gas analyzer was periodically purged with an automatic zero gas purging system (Model 063-5751) to enhance the long-term stability of the instrument. The accuracy of the zero gas purging system is reported as  $\pm 1$  millivolt (mv).

At the end of the test, the analog records of vapor concentration/time information were manually converted into a representative series of data points (maximum - 40) and stored in assigned computer files for detailed computer analysis. The resolution of these data conversions is limited to 1 mv [approximately 0.02 parts per million (ppm)] which is equivalent to the background noise level of the Miran IA vapor analyzer system.

A special purpose Fortran computer program was written to perform the cumbersome tasks of reducing all the digitized voltage readings from the Miran IA analyzer time plot into an equivalent time history of vapor concentration values and transforming the basic vapor concentrations to dosage values, mass transfer rates, and the deposited droplet mass remaining as

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\*Manufactured by Phys-Chemical Research Corporation, New York, NY

\*\*Manufactured by Davis Instrument Manufacturing Company, Inc., Baltimore, MD

\*\*\*Omega Engineering, Inc., Stamford, CT

†Wilks Scientific Corporation, Norwalk, CT

††Linear Instruments Corporation, Irvine, CA

a function of time, etc. This enabled us to extract as much information as possible for an in-depth analysis of the experimental results and to also tabulate the mass of information with a consistent style and notation to facilitate further reference. A discussion of the computer program is given in the Phase I and II reports.<sup>2,3</sup> The original Fortran program was slightly modified to handle the analyses of tests on an IBM PC/AT computer for this study. A listing of the IBM PC/AT computer version for this study is in Appendix A.

## 5. RESULTS

### 5.1 Evaporation and Recovery.

In this preliminary screening, an experimental data base was developed to quantify the evaporation and persistency of thickened DEM deposited on foliage, which consisted of the Northern Red Oak and the Shagbark Hickory leaves. For purposes of this experiment, distinctions were made between the top and bottom surfaces of both species of leaves, and additionally for the oak leaves, distinctions between the condition or age of the leaf, identified as green and red leaves. All the evaporation results are based on tests with one candidate agent simulant, DEM. The physical properties of DEM closely resembles those of the nerve agents having intermediate volatility. When thickened with a polymeric additive, this simulant becomes more viscous and closely mimics the properties of a thickened CW agent, such as TGD.

The primary purpose of these controlled wind tunnel experiments was to quantify as a function of time and under a variety of conditions the amount of agent and the rate at which it becomes airborne. An extensive number of tables and figures are provided in Appendixes B-I. With this information on liquid droplet persistency/evaporation, prediction of downwind concentrations can be accomplished using an appropriate surface evaporation model to determine the vapor threat to personnel over the given period of evaporation.

A bi-level factorial experiment was followed to aid in clarifying and identifying the most critical parameters controlling the persistency and evaporation characteristics of thickened viscoelastic liquid droplets deposited on a porous surface, such as a leaf. The variables treated in this initial screening included: (a) liquid viscosity of DEM, (b) wind speed, (c) leaf surface, (d) type of leaf (Experiment 1), and (e) condition of leaf (Experiment 2). By design, 16 distinct tests, in Experiment 1, and 8 complementary tests, in Experiment 2, were investigated. These 24 tests were conducted at one ambient temperature of 60 °F and with an average RH of 42%.

The results of experimental evaporation are given in detail in Tables 1-24 of Appendixes B-L. Tables 1-16 contain the results for the tests performed in Experiment 1 with oak and hickory leaves, and Tables 17-24 contain the test results in Experiment 2 pertaining only to oak leaves.

Appendix B provides the absorbance (volts) data measured by the Miran IA vapor analyzer, on which all subsequent tabulations were based. The absorbance voltage readings were derived from continuous strip chart recordings, using a fixed sampling period that was chosen based on the length of



the experiment and how quickly the readings changed during any given test. The sampling period ranged from 10 to 45 min, but was predominantly 15 min for the high wind speed condition and 30 min for the low wind speed. An integration of the absorbance volts and time data was performed using Simpson's rule. The area (volt minute) is proportional to the cumulative vapor mass recovered under the steady state test conditions. The fractional (normalized) values given in the last column of Appendix B are based on the total initial liquid contamination for two contaminated racks of leaves. The last value in this column is a measure of the total fractional mass recovered from the leaves.

Appendix C presents the vapor contamination levels developed from the uniform array of droplets covering an area of approximately 4 ft<sup>2</sup> of leaf surface. The vapor concentration is given as a function of time in terms of parts per million in Column 2 and equivalently as micrograms per cubic meter in Column 3. Columns 4 and 5 indicate the vapor contamination (micrograms per cubic meter) developed per unit area and per unit contamination mass. The sixth and seventh columns present the vapor concentration attributed to an average size deposited droplet, in terms of parts per million and micrograms per cubic meter, respectively.

Appendix D contains the data on the evaporation history for a typical test droplet in the array and the results of a simple half-life model fitted to the residual droplet mass. The elapsed time is given in Column 1 of the tables. The residual droplet mass, in terms of milligrams, and the fractional mass remaining are shown in Columns 2 and 3, respectively. Alternately, Columns 4 and 5 in the table indicate the cumulative mass recovered in terms of milligrams of mass and fractional amount. The right half of this table provides the predictions for a simple half-life model. The half-life is estimated by a linear interpolation of the fractional mass recovered.

A summary of the half-life values for each experiment are given in Table 4 and are analyzed in the Section 6, Analysis, of this report.

Columns 6 and 7 of the tables in Appendix D indicate the residual contamination mass in terms of milligrams and fractional amount derived from the half-life model. Columns 8 and 9 show two alternate ways of indicating the elapsed time in the evaporation experiment. Column 9 gives the elapsed time in terms of half-lives and is perhaps more meaningful and useful.

Appendix E contains the evaporation rates of the residual droplet deposited on leaf surfaces; Columns 1, 2, and 3 depict the elapsed time in terms of minutes, fractional values, and half-lives. Column 4 gives the corresponding droplet evaporation rates in micrograms per minute. Column 5 indicates the normalized evaporation rates. The normalization was obtained by dividing the measured evaporation rate by the fraction of liquid droplet remaining.

Information defining the experimental contamination levels achieved for each rack of leaves in the experiment are in Appendix F [e.g., grams of contamination, number of droplets, grams of contamination per area (square meter), and grams of contamination per droplet]. In most instances, the level of contamination of one rack of leaves is identical to the level of contamination of another rack; therefore, the estimated mean droplet mass for

the experiment is the same as that determined for the individual racks of leaves. In these cases, the indicated equivalent droplet diameter (millimeter) is also the same.

Graphs depicting the evaporation behavior of a droplet on a leaf surface are shown in Appendixes G through I. Plots of the residual droplet mass (milligram) versus time are in Appendix G. Appendix H depicts the corresponding droplet evaporation rates (micrograms per minute) as a function of time. The rates are given as negative values in keeping with the concept of vapor mass lost by the deposited droplet. Appendix I gives a combined plot showing the fractional mass remaining and the complimentary plot of fractional mass recovered as a function of time, normalized by dividing time by the droplet half-life. Additionally, a first order half-life model fit to data, given the fractional droplet mass remaining is indicated.

## 5.2 Droplet Spread Factors.

The extent of spreading of a liquid droplet deposited on leaf surface was determined from measurements of the minimum and maximum diameter of the copolymer residue, which was visible on the leaf surface after the liquid droplet had evaporated. The residual of 40 of 1,472 total droplets in the uniform array were examined for each test case. These values, as well as the average spread diameter for the sample of droplets, are in Appendix J. The appropriate spread factor information, derived from the ratio of the average spread diameter of the deposited droplet and the equivalent mass diameter of the droplets (Appendix F), is summarized in Table 3.

## 6. ANALYSIS

### 6.1 Evaporation and Vapor Recovery.

In keeping with the procedure established in Phase I, seven droplet evaporation characteristics were selected from the pool of empirical information cited above to describe the persistency/evaporation of a droplet deposited on a leafy surface. Information of this type provides the responses required for detailed statistical analysis of the experimental data and is extremely useful in identifying the conditions/critical parameters that contribute to the vapor hazard produced by contaminated surfaces. The seven evaporation characteristics that seem most pertinent are as follows:

- The percent of contamination recovered after the 1st, 2d, 3d, and 6th hr from droplets deposited on leafy surfaces
- The average droplet evaporation rates (micrograms per minute) based on a 1st, 2d, 3d, and 6th hr following deposition on the leaf surfaces
- The half-life (minutes) for a droplet in the uniform array of droplets deposited on the leaf surfaces or the time required to recover 50% of the initial (volatile) contaminant
- The average evaporation and recovery rates (micrograms per minute) associated with the half-life of the contaminant

Table 3. Average Spread Factor of 2 mm Diameter Droplets of Thickened Diethyl Malonate on Leaf Surface at 60 °F Air Temperature and 42% Average Relative Humidity

| Leaf Type<br>(Condition) | Leaf<br>Surface | Liquid Viscosity            |                              |                             |                              |
|--------------------------|-----------------|-----------------------------|------------------------------|-----------------------------|------------------------------|
|                          |                 | 100 cP                      |                              | 1,000 cP                    |                              |
|                          |                 | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph |
| Hickory<br>(Green)       | Top             | 2.47                        | 2.72                         | 2.67                        | 2.80                         |
|                          | Bottom          | 1.89                        | 1.91                         | 1.91                        | 1.85                         |
| Oak<br>(Green)           | Top             | 2.90                        | 2.36                         | 2.39                        | 2.24                         |
|                          | Bottom          | 1.94                        | 1.94*                        | 1.83                        | 1.80                         |
| Oak<br>(Red)             | Top             | 1.97                        | 1.86                         | 1.99                        | 1.99                         |
|                          | Bottom          | 1.77                        | 1.87                         | 1.76                        | 1.77                         |

\* Estimate based on rearest

- The total percent of the contamination recovered as vapor from the droplets deposited on the leaf surfaces
- The lifetime of the droplet contamination deposited on the leaf surfaces
- The average evaporation rate (micrograms per minute) over the lifetime of the droplet contamination

These seven droplet evaporation characteristics are given in Tables 4-16 for each of the tests in the two,  $2^4$  factorial experiments.

A factorial analysis (Yates' method), half normal probability plots (HNPP) analysis of the magnitude of the effects, and an analysis of variance (ANOVA) were performed to statistically examine the evaporation characteristics in Tables 4-16. The results of the factorial analysis and the studies of the magnitude of the effects in the two factorial experiments via HNPP, which depict the most significant factors and the 0.40, 0.20 and 0.05 confidence bars for Experiments 1 and 2, respectively, are in Appendixes K and L. The ANOVA results for both experiments are in Appendix M. In performing the ANOVA, it was arbitrarily assumed that all interactions of order, three and higher, were really zero, and the five corresponding sums of squares are used to estimate the residual variance (mean square term) in each case. The "F" statistic corresponding to confidence levels of 99.9, 99, 95, 90 and 75% for each case is indicated in Tables M1-M26. Because at times there is a question as to which effects can reasonably be pooled together into the residual sum of squares (which interactions will be assumed to be either zero or at least negligible), the probability plots of the magnitude of the effects in each experiment also serve to confirm the more formal ANOVA table. Adopting a significance level of either 0.10 or 0.20 or a confidence bar of 0.20, as used in HNPP (or correspondingly, a confidence level of 90 or 80%), seems appropriate in examining the significance of the main effects and interactions in this experiment.

In general, the factorial analysis and the ANOVA results are in good agreement. Tables 17 through 19 summarize the findings of the ANOVA for each of the droplet evaporation characteristics. Table 17 provides a summary of the analysis on the half-life and lifetime of the deposited droplet, the total percent of contamination recovered as vapor, and the average evaporation rates based on droplet half-life and lifetime values. Table 18 provides a summary of the most significant factors affecting the percent of contamination recovered as vapor after the 1st, 2d, 3d, and 6th hr. Table 19 indicates the most significant factors affecting the average droplet evaporation rates for the same time periods after deposition of the droplets on the leaf surfaces.

#### 6.1.1 Wind Speed (Factor 2).

Inspecting the summarized ANOVA results in Tables 17 through 19 clearly indicates that wind speed [Factor 2 (11 mph versus 3 mph)] in these experiments is the most dominant factor in both droplet evaporation

Text continued on page 47.

Table 4. Half-Life (Minutes) of Droplet Contamination of 2 mm Diameter Droplets of Thickened Diethyl Malonate Deposited on Leaf Surface at 60 °F Air Temperature and 42% Average Relative Humidity

| Leaf Type<br>(Condition) | Leaf<br>Surface | Liquid Viscosity            |                              |                             |                              |
|--------------------------|-----------------|-----------------------------|------------------------------|-----------------------------|------------------------------|
|                          |                 | 100 cP                      |                              | 1,000 cP                    |                              |
|                          |                 | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph |
| Hickory<br>(Green)       | Top             | 246                         | 84                           | 264                         | 98                           |
|                          | Bottom          | 320                         | 148                          | 332                         | 156                          |
| Oak<br>(Green)           | Top             | 245                         | 100                          | 287                         | 136                          |
|                          | Bottom          | 367                         | 150                          | 404                         | 162                          |
| Oak<br>(Red)             | Top             | 339                         | 142                          | 315                         | 137                          |
|                          | Bottom          | 341                         | 145                          | 315                         | 150                          |

Table 5. Average Evaporation Rate (Micrograms per Minute) over Droplet Half-Life of 2 mm Diameter Droplets of Thickened Diethyl Malonate Deposited on Leaf Surface at 60 °F Air Temperature and 42% Average Relative Humidity

| Leaf Type<br>(Condition) | Leaf<br>Surface | Liquid Viscosity            |                      |                             |                      |
|--------------------------|-----------------|-----------------------------|----------------------|-----------------------------|----------------------|
|                          |                 | 100 cP                      |                      | 1,000 cP                    |                      |
|                          |                 | Nominal Wind Speed<br>3 mph | Wind Speed<br>11 mph | Nominal Wind Speed<br>3 mph | Wind Speed<br>11 mph |
| Hickory<br>(Green)       | Top             | 12.6                        | 33.1                 | 12.2                        | 32.9                 |
|                          | Bottom          | 8.7                         | 20.5                 | 9.1                         | 20.8                 |
| Oak<br>(Green)           | Top             | 10.5                        | 28.4                 | 11.3                        | 23.7                 |
|                          | Bottom          | 7.4                         | 19.0                 | 8.0                         | 19.1                 |
| Oak<br>(Red)             | Top             | 9.3                         | 22.3                 | 10.3                        | 24.4                 |
|                          | Bottom          | 8.9                         | 20.0                 | 10.1                        | 22.0                 |

Table 6. Total Percent of Contamination Recovered as Vapor from  
2 mm Diameter Droplets of Thickened Diethyl Malonate  
Deposited on Leaf Surface at 60 °F Air Temperature and  
42% Average Relative Humidity

| Leaf Type<br>(Condition) | Leaf<br>Surface | Liquid Viscosity            |                              |                             |                              |
|--------------------------|-----------------|-----------------------------|------------------------------|-----------------------------|------------------------------|
|                          |                 | 100 cP                      |                              | 1,000 cP                    |                              |
|                          |                 | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph |
| Hickory<br>(Green)       | Top             | 76                          | 84                           | 84                          | 94                           |
|                          | Bottom          | 75                          | 87                           | 77                          | 89                           |
| Oak<br>(Green)           | Top             | 80                          | 88                           | 83                          | 89                           |
|                          | Bottom          | 83                          | 87                           | 83                          | 86                           |
| Oak<br>(Red)             | Top             | 81                          | 86                           | 98                          | 98                           |
|                          | Bottom          | 83                          | 88                           | 93                          | 96                           |

Table 7. Time (Minutes) for Complete Evaporation of 2 mm Diameter Droplets of Thickened Diethyl Malonate Deposited on Leaf Surface at 60 °F Air Temperature and 42% Average Relative Humidity

| Leaf Type<br>(Condition) | Leaf<br>Surface | Liquid Viscosity            |                              |                             |                              |
|--------------------------|-----------------|-----------------------------|------------------------------|-----------------------------|------------------------------|
|                          |                 | 100 cP                      |                              | 1,000 cP                    |                              |
|                          |                 | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph |
| Hickory<br>(Green)       | Top             | 870                         | 360                          | 1,020                       | 370                          |
|                          | Bottom          | 870                         | 480                          | 900                         | 480                          |
| Oak<br>(Green)           | Top             | 780                         | 360                          | 960                         | 390                          |
|                          | Bottom          | 1,280                       | 465                          | 1,160                       | 435                          |
| Oak<br>(Red)             | Top             | 1,215                       | 450                          | 1,280                       | 560                          |
|                          | Bottom          | 1,140                       | 510                          | 1,240                       | 480                          |



Table 8. Average Evaporation Rate (Micrograms per Minute) over Lifetime of 2 mm Diameter Droplets of Thickened Diethyl Malonate Deposited on Leaf Surface at 60 °F Air Temperature and 42% Average Relative Humidity

| Leaf Type<br>(Condition) | Leaf<br>Surface | Liquid Viscosity            |                              |                             |                              |
|--------------------------|-----------------|-----------------------------|------------------------------|-----------------------------|------------------------------|
|                          |                 | 100 cP                      |                              | 1,000 cP                    |                              |
|                          |                 | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph |
| Hickory<br>(Green)       | Top             | 5.4                         | 13.0                         | 5.3                         | 16.4                         |
|                          | Bottom          | 4.8                         | 11.0                         | 5.2                         | 12.0                         |
| Oak<br>(Green)           | Top             | 5.3                         | 13.8                         | 5.6                         | 14.8                         |
|                          | Bottom          | 3.5                         | 10.6                         | 4.6                         | 12.2                         |
| Oak<br>(Red)             | Top             | 4.2                         | 12.2                         | 4.9                         | 11.8                         |
|                          | Bottom          | 4.4                         | 10.0                         | 4.7                         | 13.1                         |

Table 9. Percent of Contamination Recovered as Vapor 1 hr After Deposition of 2 mm Diameter Droplets of Thickened Diethyl Malonate on Leaf Surface at 60 °F Air Temperature and 42% Average Relative Humidity

| Leaf Type<br>(Condition) | Leaf<br>Surface | Liquid Viscosity            |                              |                             |                              |
|--------------------------|-----------------|-----------------------------|------------------------------|-----------------------------|------------------------------|
|                          |                 | 100 cP                      |                              | 1,000 cP                    |                              |
|                          |                 | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph |
| Hickory<br>(Green)       | Top             | 16                          | 39                           | 14                          | 33                           |
|                          | Bottom          | 12                          | 23                           | 11                          | 22                           |
| Oak<br>(Green)           | Top             | 16                          | 33                           | 13                          | 24                           |
|                          | Bottom          | 10                          | 22                           | 9                           | 21                           |
| Oak<br>(Red)             | Top             | 10                          | 24                           | 11                          | 24                           |
|                          | Bottom          | 10                          | 23                           | 11                          | 22                           |

Table 10. Percent of Contamination Recovered as Vapor 2 hr  
After Deposition of 2 mm Diameter Droplets of  
Thickened Diethyl Malonate on Leaf Surface at  
60 °F Air Temperature and 42% Average Relative Humidity

| Leaf Type<br>(Condition) | Leaf<br>Surface | Liquid Viscosity            |                              |                             |                              |
|--------------------------|-----------------|-----------------------------|------------------------------|-----------------------------|------------------------------|
|                          |                 | 100 cP                      |                              | 1,000 cP                    |                              |
|                          |                 | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph |
| Hickory<br>(Green)       | Top             | 29                          | 63                           | 27                          | 58                           |
|                          | Bottom          | 22                          | 42                           | 21                          | 40                           |
| Oak<br>(Green)           | Top             | 29                          | 57                           | 24                          | 45                           |
|                          | Bottom          | 19                          | 42                           | 17                          | 39                           |
| Oak<br>(Red)             | Top             | 20                          | 44                           | 21                          | 44                           |
|                          | Bottom          | 20                          | 43                           | 21                          | 41                           |

Table 11. Percent of Contamination Recovered as Vapor 3 hr  
After Deposition of 2 mm Diameter Droplets of  
Thickened Diethyl Malonate on Leaf Surface at  
60 °F Air Temperature and 42% Average Relative Humidity

| Leaf Type<br>(Condition) | Leaf<br>Surface | Liquid Viscosity            |        |                             |        |
|--------------------------|-----------------|-----------------------------|--------|-----------------------------|--------|
|                          |                 | 100 cP                      |        | 1,000 cP                    |        |
|                          |                 | Nominal Wind Speed<br>3 mph | 11 mph | Nominal Wind Speed<br>3 mph | 11 mph |
| Hickory<br>(Green)       | Top             | 40                          | 76     | 37                          | 75     |
|                          | Bottom          | 32                          | 58     | 30                          | 56     |
| Oak<br>(Green)           | Top             | 40                          | 74     | 34                          | 62     |
|                          | Bottom          | 27                          | 58     | 23                          | 54     |
| Oak<br>(Red)             | Top             | 29                          | 60     | 31                          | 62     |
|                          | Bottom          | 29                          | 59     | 30                          | 58     |

Table 12. Percent of Contamination Recovered as Vapor 6 hr  
After Deposition of 2 mm Diameter Droplets of  
Thickened Diethyl Malonate on Leaf Surface at  
60 °F Air Temperature and 42% Average Relative Humidity

| Leaf Type<br>(Condition) | Leaf<br>Surface | Liquid Viscosity            |                              |                             |                              |
|--------------------------|-----------------|-----------------------------|------------------------------|-----------------------------|------------------------------|
|                          |                 | 100 cP                      |                              | 1,000 cP                    |                              |
|                          |                 | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph |
| Hickory<br>(Green)       | Top             | 62                          | 84                           | 61                          | 94                           |
|                          | Bottom          | 54                          | 84                           | 53                          | 85                           |
| Oak<br>(Green)           | Top             | 64                          | 88                           | 59                          | 89                           |
|                          | Bottom          | 49                          | 85                           | 46                          | 84                           |
| Oak<br>(Red)             | Top             | 54                          | 85                           | 56                          | 94                           |
|                          | Bottom          | 52                          | 84                           | 56                          | 92                           |

Table 13. Average Droplet Evaporation Rate (Micrograms per Minute) for the First Hour After Deposition of 2 mm Diameter Droplets of Thickened Diethyl Malonate on Leaf Surface at 60 °F Air Temperature and 42% Average Relative Humidity

| Leaf Type<br>(Condition) | Leaf<br>Surface | Liquid Viscosity            |                              |                             |                              |
|--------------------------|-----------------|-----------------------------|------------------------------|-----------------------------|------------------------------|
|                          |                 | 100 cP                      |                              | 1,000 cP                    |                              |
|                          |                 | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph |
| Hickory<br>(Green)       | Top             | 16.9                        | 36.2                         | 15.4                        | 35.9                         |
|                          | Bottom          | 10.9                        | 23.1                         | 10.8                        | 23.3                         |
| Oak<br>(Green)           | Top             | 13.7                        | 31.0                         | 14.4                        | 26.4                         |
|                          | Bottom          | 8.6                         | 21.5                         | 9.4                         | 21.6                         |
| Oak<br>(Red)             | Top             | 10.9                        | 25.2                         | 11.7                        | 26.3                         |
|                          | Bottom          | 10.6                        | 22.3                         | 11.3                        | 24.4                         |

Table 14. Average Droplet Evaporation Rate (Micrograms per Minute) for the First 2 hr After Deposition of 2 mm Diameter Droplets of Thickened Diethyl Malonate on Leaf Surface at 60 °F Air Temperature and 42% Average Relative Humidity

| Leaf Type<br>(Condition) | Leaf<br>Surface | Liquid Viscosity            |                              |                             |                              |
|--------------------------|-----------------|-----------------------------|------------------------------|-----------------------------|------------------------------|
|                          |                 | 100 cP                      |                              | 1,000 cP                    |                              |
|                          |                 | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph |
| Hickory<br>(Green)       | Top             | 15.2                        | 29.2                         | 14.3                        | 31.3                         |
|                          | Bottom          | 10.4                        | 21.3                         | 10.5                        | 21.7                         |
| Oak<br>(Green)           | Top             | 12.3                        | 27.1                         | 13.1                        | 24.3                         |
|                          | Bottom          | 8.4                         | 19.7                         | 9.1                         | 20.0                         |
| Oak<br>(Red)             | Top             | 10.5                        | 23.0                         | 11.3                        | 24.9                         |
|                          | Bottom          | 10.1                        | 20.7                         | 11.0                        | 22.7                         |

Table 15. Average Droplet Evaporation Rate (Micrograms per Minute) for the First 3 hr After Deposition of 2 mm Diameter Droplets of Thickened Diethyl Malonate on Leaf Surface at 60 °F Air Temperature and 42% Average Relative Humidity

| Leaf Type<br>(Condition) | Leaf<br>Surface | Liquid Viscosity            |                              |                             |                              |
|--------------------------|-----------------|-----------------------------|------------------------------|-----------------------------|------------------------------|
|                          |                 | 100 cP                      |                              | 1,000 cP                    |                              |
|                          |                 | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph |
| Hickory<br>(Green)       | Top             | 13.9                        | 23.4                         | 13.4                        | 27.0                         |
|                          | Bottom          | 9.8                         | 19.6                         | 10.1                        | 20.2                         |
| Oak<br>(Green)           | Top             | 11.4                        | 23.2                         | 12.4                        | 22.3                         |
|                          | Bottom          | 8.1                         | 18.2                         | 8.9                         | 18.7                         |
| Oak<br>(Red)             | Top             | 10.2                        | 21.2                         | 11.0                        | 23.2                         |
|                          | Bottom          | 9.7                         | 19.1                         | 10.7                        | 21.3                         |



Table 16. Average Droplet Evaporation Rate (Micrograms per Minute) for the First 6 hr After Deposition of 2 mm Diameter Droplets of Thickened Diethyl Malonate on Leaf Surface at 60 °F Air Temperature and 42% Average Relative Humidity

| Leaf Type<br>(Condition) | Leaf<br>Surface | Liquid Viscosity            |                              |                             |                              |
|--------------------------|-----------------|-----------------------------|------------------------------|-----------------------------|------------------------------|
|                          |                 | 100 cP                      |                              | 1,000 cP                    |                              |
|                          |                 | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph | Nominal Wind Speed<br>3 mph | Nominal Wind Speed<br>11 mph |
| Hickory<br>(Green)       | Top             | 10.7                        | 13.0                         | 11.0                        | 16.8                         |
|                          | Bottom          | 8.3                         | 14.1                         | 9.0                         | 15.3                         |
| Oak<br>(Green)           | Top             | 9.2                         | 13.8                         | 10.6                        | 15.9                         |
|                          | Bottom          | 7.4                         | 13.4                         | 8.2                         | 14.5                         |
| Oak<br>(Red)             | Top             | 9.2                         | 15.0                         | 10.0                        | 17.5                         |
|                          | Bottom          | 8.8                         | 13.6                         | 9.8                         | 16.8                         |

Table 17. Summary of ANOVA of 24 Experiments 1 and 2: 2 mm Diameter Droplets of DEM Deposited on Leaf Surfaces at 60 °F Air Temperature and 42% Average Relative Humidity

| Source                | (A)   |       | (B)   |       | (C)   |       | (D)   |       | (E)   |       |
|-----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
|                       | Exp 1 | Exp 2 | Exp 1 | Exp 2 | Exp 1 | Exp 2 | Exp 1 | Exp 2 | Exp 1 | Exp 2 |
| 1 Liquid Viscosity    | **    |       |       |       | **    | ****  |       |       | **    | **    |
| 2 Wind Speed          | ****  | ****  | ****  | ****  | ****  | ****  | ****  | ****  | ****  | ****  |
| 3 Leaf Surface        | ****  | **    | *     |       |       |       | ****  | ***   | ***   | ***   |
| 4 Leaf Type/Condition | **    |       | **    |       | ****  |       | **    |       | *     | *     |
| <u>Interactions</u>   |       |       |       |       |       |       |       |       |       |       |
| 1x2                   |       |       |       |       |       |       |       |       |       |       |
| 1x3                   |       |       |       |       |       |       |       |       |       |       |
| 1x4                   |       |       |       |       |       |       |       |       |       |       |
| 2x3                   |       |       |       |       | *     | **    |       |       |       |       |
| 2x4                   | **    |       |       | 44    | *     | ****  | ***   | *     | **    |       |
| 3x4                   |       | **    | **    | **    | **    | ****  | **    | **    | *     | *     |

Keys:

(A) Half-Life of Droplet

(B) Lifetime of Droplet

(C) Total Percent of Contamination Recovered as Vapor

(D) Average Evaporation Rate of Droplet Over Half-Life

(E) Average Evaporation Rate Over Lifetime of Droplet

Critical Values for F-Statistic:

\*\*\*\*  $F_{1,5,0.999} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*  $F_{1,5,0.90} = 4.06$

Table 18. Summary of ANOVA of 24 Experiments 1 and 2 on Percent of Contamination Recovered as Vapor After Specified Time from 2 mm Diameter Droplets of DEM Deposited on Leaf Surface at 60 °F Air Temperature and 42% Average Relative Humidity

| Source                | 1 hr  |       | 2 hr  |       | 3 hr  |       | 6 hr  |       |
|-----------------------|-------|-------|-------|-------|-------|-------|-------|-------|
|                       | Exp 1 | Exp 2 | Exp 1 | Exp 2 | Exp 1 | Exp 2 | Exp 1 | Exp 2 |
| 1 Liquid Viscosity    | **    | *     | **    | **    | **    | **    |       |       |
| 2 Wind Speed          | ***   | ***   | ***   | ***   | ***   | ***   | ***   | ***   |
| 3 Leaf Surface        | ***   | ***   | ***   | ***   | ***   | ***   | ***   | ***   |
| 4 Leaf Type/Condition | *     | *     | **    | *     | **    |       |       |       |
| <u>Interactions</u>   |       |       |       |       |       |       |       |       |
| 1x2                   |       |       |       |       |       |       |       |       |
| 1x3                   |       |       |       |       |       |       |       |       |
| 1x4                   |       |       |       |       |       |       |       |       |
| 2x3                   |       | *     |       | **    |       | **    |       | **    |
| 2x4                   | **    |       | **    |       |       |       | **    |       |
| 3x4                   |       | **    |       | **    |       | ***   |       | ***   |

Critical Values for F-Statistic:

\*\*\*  $F_{1,5,0.999} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*  $F_{1,5,0.90} = 4.06$

Table 19. Summary of ANOVA of 24 Experiments 1 and 2 on Average Evaporation Rate over Specified Time for 2 mm Diameter Droplets of DEM Deposited on Leaf Surfaces at 60 °F Air Temperature and 42% Relative Humidity.

| Source              |                     | 1 hr  |       | 2 hr  |       | 3 hr  |       | 6 hr  |       |
|---------------------|---------------------|-------|-------|-------|-------|-------|-------|-------|-------|
|                     |                     | Exp 1 | Exp 2 | Exp 1 | Exp 2 | Exp 1 | Exp 2 | Exp 1 | Exp 2 |
| 1                   | Liquid Viscosity    | ****  | ****  | ****  | ****  | ****  | ****  | **    | ***   |
| 2                   | Wind Speed          | ****  | ****  | ****  | ****  | ****  | ****  | ****  | ****  |
| 3                   | Leaf Surface        | ****  | ***   | ****  | ***   | ****  | ****  | ***   | ***   |
| 4                   | Leaf Type/Condition | **    |       | **    |       | **    |       |       | ***   |
| <u>Interactions</u> |                     |       |       |       |       |       |       |       |       |
| 1x2                 |                     |       |       |       |       |       |       |       |       |
| 1x3                 |                     |       |       |       |       |       |       |       |       |
| 1x4                 |                     |       |       |       |       |       |       |       |       |
| 2x3                 |                     |       |       |       |       |       |       |       |       |
| 2x4                 |                     | *     |       | *     |       | *     |       |       |       |
| 3x4                 |                     |       | **    |       | **    |       | **    |       | *     |

Critical Values for F-Statistic:

\*\*\*\*  $F_{1,5,0.999} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*  $F_{1,5,0.90} = 4.06$

experiments. The "F" statistic associated with the wind speed effect is significant at 0.1% level for all evaporation characteristics examined in both of the factorial experiments. The effect produced by the wind speed is predominantly a direct effect. There is only one notable interaction effect (Factor 23) between the wind speed and the leaf surface, which is significant at 5% level in these experiments. For each of the droplet evaporation characteristic examined, except for the total contamination recovered from the DEM droplets deposited on the leaf surfaces, wind speed alone can explain most of the variation in the responses, 80 and 88% in Experiments 1 and 2, respectively. The total percent of contamination recovered was strongly dependent on the viscosity of the deposited liquid droplet and condition or age of the leaf surface, especially in Experiment 2. These effects are discussed in Sections 6.1.2 and 6.1.3. On the average, the initial (0-3 hr) average droplet evaporation rate of a droplet deposited on the leaf surface at 3 mph is one-half the evaporation rate of the droplet exposed to a wind speed of 11 mph. Correspondingly, the percent of contamination recovered as vapor from the contaminated surface at 3 mph when compared to 11 mph is one-half. However, the average droplet evaporation rate for 6 hr at 3 mph is nearly two-thirds the evaporation rate at 11 mph (9.3  $\mu\text{g}/\text{min}$  versus 14.6  $\mu\text{g}/\text{min}$  and 9.2  $\mu\text{g}/\text{min}$  versus 15.1  $\mu\text{g}/\text{min}$ ) in Experiments 1 and 2. The evaporation rate averaged over the lifetime of the droplet on the leaf surface at 3 mph is 38% of that for droplets at 11 mph in Experiments 1 and 2 (5.0  $\mu\text{g}/\text{min}$  versus 13.0  $\mu\text{g}/\text{min}$  and 4.6  $\mu\text{g}/\text{min}$  versus 12.3  $\mu\text{g}/\text{min}$ ), respectively. The difference in the lifetime of the deposited droplets at 3 mph and 11 mph, 9.3 hr in Experiment 1 (980 min versus 418 min) and 10.8 hr (1,106 min versus 456 min in Experiment 2), is significant, both statistically and operationally. Additionally, the 3-hr difference in the half-life of the deposited droplets evaporating at 3 mph versus 11 mph, which is attributable mainly to the difference in the wind speed, in both experiments, is also of operational significance.

In summary, the variation in the evaporation characteristics of the DEM droplets deposited on leaf surfaces at a constant temperature is due primarily to the difference in wind speed (3-11 mph) in these experiments. The increase in droplet evaporation rates, the percent of contamination recovered during evaporation, and the decrease in persistency of the droplets deposited on the leaf surfaces exposed to wind speed of 11 mph, when compared to 3 mph, are both statistically and operationally significant.

#### 6.1.2 Leaf Surface (Factor 3).

The leaf surface [Factor 3 (top versus bottom)] in Experiments 1 and 2 is also highly significant at 0.1 and 1.0% levels, respectively, for all the droplet evaporation characteristics examined, except for the lifetime of the droplet deposited on the leaf surfaces and for the total percent of contamination recovered as vapor from the evaporating droplets. Apparently, for short times (0-3 hr), whether the top or bottom surfaces of the oak and hickory leaves are contaminated, has a direct effect on the amount and rate at which the droplet contamination evaporates. However, the leaf surface does not have a direct effect on the long-term yields in the evaporation experiment (i.e., the total amount of contamination that evolves or the total time required for evaporation of the deposited droplet). There is evidence of an interaction effect between the top and bottom surfaces and condition or

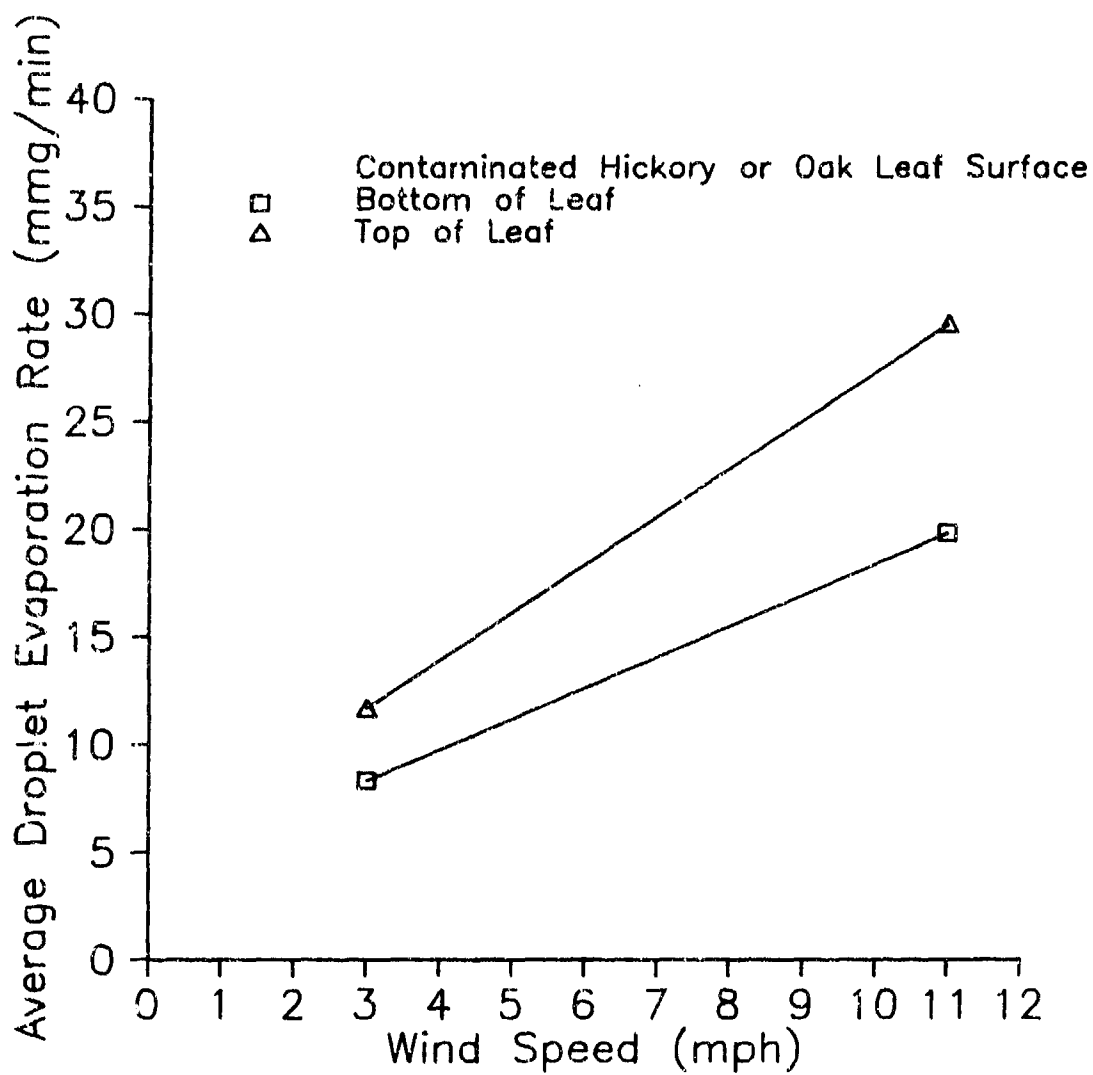


Figure 3. Effect of Interaction Between Wind Speed and Leaf Surface on the Average Droplet Evaporation Rate for Droplet Half-Life (Factor 23) in Experiment 1

interaction is evident with the hickory and oak leaves in Experiment 1. There is however evidence of an interaction between the leaf surface and the wind speed (Factor 23) that has an effect on the initial evaporation rate of the droplets in both the ANOVA and HNPP analysis. While there is only a small difference in the evaporation rate of the droplets deposited on the top and bottom surfaces at the 3 mph wind speed (approximately 3  $\mu\text{g}/\text{min}$ ), a two-way comparison (Figure 3) shows that this interaction arises because there is a substantial difference in the evaporation rates (10.4  $\mu\text{g}/\text{min}$ ) between droplets deposited on the top and bottom leaf surfaces at 11 mph. This is probably related to the finding that droplets deposited on the top surfaces of the oak and hickory leaves spread substantially more than droplets deposited on the bottom surfaces of these leaves. With a larger exposed droplet surface, an increase in the incident wind speed can be expected to have a greater effect on the droplet evaporation rates, etc. It is noteworthy that the differences in the percent of contamination recovered from the top and bottom leaf surfaces in Experiments 1 and 2 are negligible, approximately 10 and 5%, respectively. These differences are not considered to be operationally significant to warrant making the distinction between the top and bottom surfaces of the leaf in modeling downwind vapor hazards. In addition, the leaf surface does not have to be considered to predict the persistency of the hazard because droplet lifetime and the total percent of vapor recovered are not affected by the leaf surface.

#### 6.1.3 Leaf Types and Leaf Conditions (Factor 4).

In comparison with the wind speed and leaf surface effects, the type of leaf (hickory versus oak), Factor 4 in Experiment 1, has a minor effect on the evaporative behavior of the deposited thickened DEM droplets. Most notably, the type of leaf that is contaminated has a direct effect on the rate of evaporation and the half-life of the droplet, which are significant at the 5% level. According to the HNPP analysis, there are no two factor interactions that are significant at the 5% level. Therefore, the interaction (Factor 24) in Table 17 is suspect. The difference in the half-life of DEM droplets deposited on hickory and oak leaves (206/231 min) is <30 min and is not statistically significant by the HNPP standard. Moreover, a difference of 30 min in droplet half-life is not believed to be operationally significant. For the first 3 hr after deposit, the significant increase (2-3  $\mu\text{g}/\text{min}$ ) in the average evaporation rate for droplets deposited on hickory versus oak leaves, which is judged to be significant, cannot be attributed to a difference in spreading of the droplet on the leaf surfaces. Therefore, the difference in evaporative behavior of the droplets, cannot be directly attributed to the species of leaf. Because this increase in evaporation rate corresponds to <5% increase in the amount of contamination recovered from the hickory when compared to the oak leaf, it is not considered to be operationally significant. This raises the hope that leaf species does not have to be included to model the evaporative behavior of the droplets deposited on foliage in the field.

With regards to Factor 4 in Experiment 2, the condition of the oak leaf (red October leaf versus green September leaf), the statistical analysis indicates only the total percent of contamination recovered is directly affected by the condition or age of the leaf. Factor 4 is significant at the 0.1% level; however, there is also a large interaction (Factor 14) between the liquid viscosity and the leaf condition, which is also significant at 0.1%. The two-way plot of Factor 14 in Figure 4 shows that this interaction

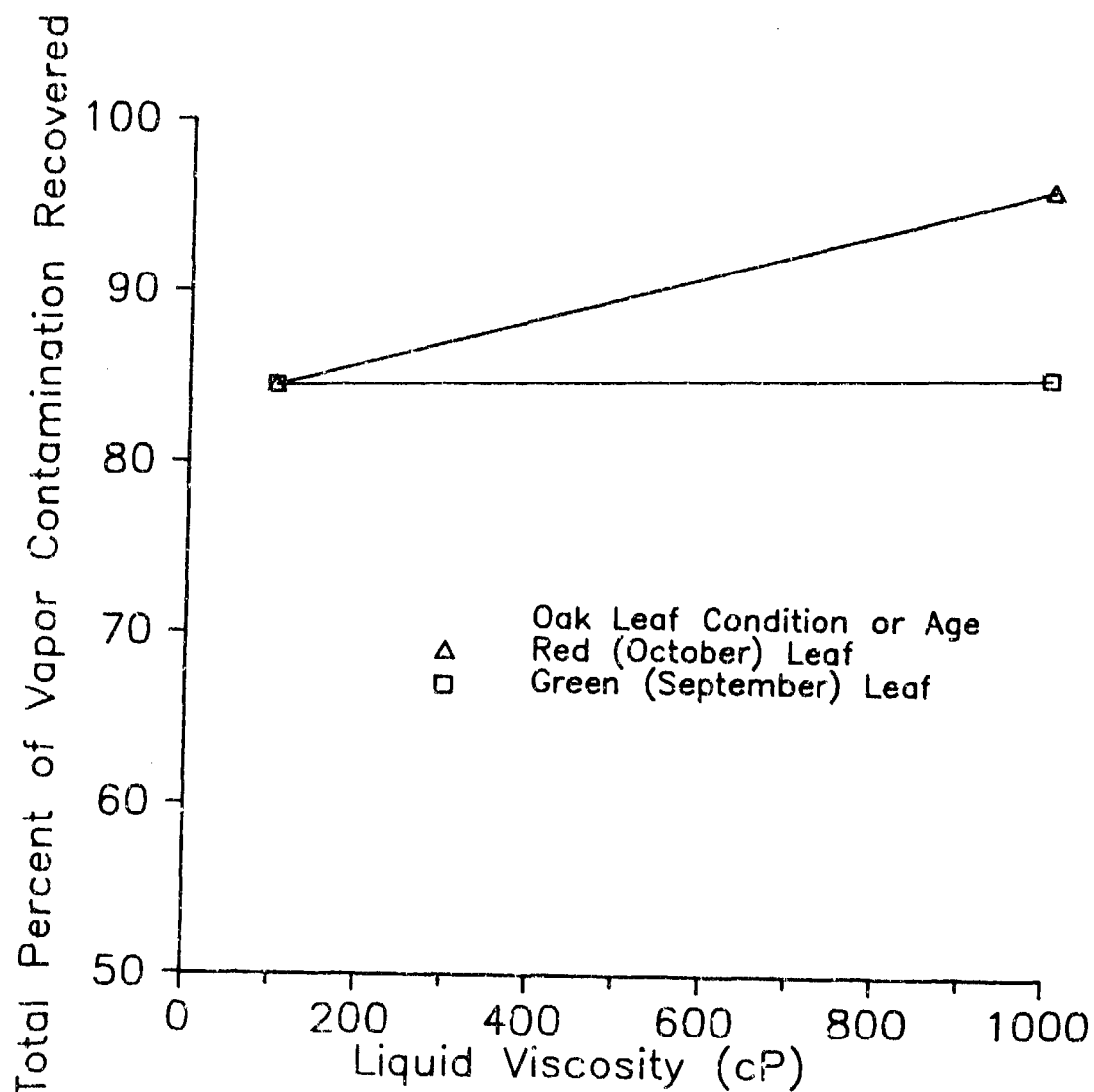


Figure 4. Effect of Interaction Between Liquid Viscosity and the Oak Leaf Condition/Age on the Total Percentage of Vapor Contamination Recovered (Factor 14) in Experiment 2



arises because there is a significant increase (11%) increase in the percent of vapor recovered from the 1,000 cP viscosity DEM droplets deposited on the red oak leaf over the green oak leaf (96 versus 85%), but there is no difference in the percent of vapor recovery of the 100 cP viscosity DEM droplets on the red and green oak leaves. There is also some evidence of this interaction effect on the percent of vapor recovered after 3 and 6 hr, because Factor 14 is significant at 5% in both the ANOVA and HNPP analysis. The only other noteworthy interaction involving the condition of the oak leaf is Factor 34 in Experiment 2. This interaction between the leaf condition and the leaf surface was discussed previously in this report.

In summary, the primary effect that Factor 4 (leaf condition or age) has in this evaporation experiment is on the percent of contamination that is eventually recovered as vapor from the leaves. However, the final amount of agent recovered from the oak leaf surfaces is strongly dependent on the initial viscosity of the liquid droplet, as well as the condition or age of the oak leaf.

#### 6.1.4 Liquid Viscosity (Factor 1).

Although the factorial analysis results of the two statistical analysis methods are in general agreement, there is a major difference between the two in judging the significance of Factor 1, the liquid viscosity of the deposited droplets in these experiments. According to the results of the HNPP of the standardized effects, the liquid viscosity is not as dominant a factor in these experiments as the ANOVA results in Tables 17 to 19 indicate. This was substantiated by a one-way ANOVA on this data.

According to the ANOVA (Factor 1), the liquid viscosity (1,000 cP versus 100 cP) has a significant effect on the percent of contamination recovered as vapor from the leaf surfaces in both experiments (Table 18). After the first hour, there is a significant interaction between the liquid viscosity and the condition of the oak leaf in Experiment 2. This is indicated by the interaction (Factor 14) in the Tables, which is judged to be significant at the 5% level. This interaction effect is also highly significant (0.1% level) for the total percent of contamination recovered from the deposited droplets in Experiment 2. Surprisingly, no such interaction is manifested in Experiment 1. Apparently, the interaction of liquid viscosity with leaf condition (green versus red oak leaves), as examined in Experiment 2, is greater than the interaction of liquid viscosity with leaf type (oak versus hickory) in Experiment 1.

However, according to the HNPP of standardized effects, the liquid viscosity does not have a significant effect on the percent of contamination recovered as vapor from the leaf surfaces in either Experiment 1 or 2 for the 0-6 hr time period. The interaction effect (Factor 14) corresponding to the interaction between the liquid viscosity and the oak leaf condition in Experiment 2 is significant only after evaporation times of 3 hr and longer. Interaction of liquid viscosity with leaf condition is not evident for short evaporation periods (0 to 2 hr) after droplet deposit.

According to ANOVA, the viscosity of the liquid contamination has a significant effect on the half-life of the droplets deposited on the oak and hickory leaf surfaces in Experiment 1 (5% level); however, it has little

effect on the half-life of the droplets deposited on the green and red oak leaves in Experiment 2. The HNPPs of the factorial analysis for the same results indicate there is no significant difference in the half-life of the 100 and 1,000 cP droplets deposited on leaf surfaces in Experiment 1 (208/217 min) and in Experiment 2 (229/225 min).

The HNPP and the ANOVA indicate that the differences in total percentage of contamination recovered from the deposited droplets, with initial viscosities of 100 and 1,000 cP (82.5/85.6%) and (84.5/90.8%) in Experiments 1 and 2, as indicated in Table 17, are significant at the 5% level. The actual differences, approximately 3 and 6%, in the total percent of contamination recovered between the 100 and 1,000 cP viscosity droplets are probably not operationally significant.

The ANOVA and HNPP results indicate that the viscosity of the liquid contamination does not significantly effect the lifetime of the droplet contamination in these experiments. Although the 100 cP droplets consistently exhibited a lifetime that is less than the lifetime of 1,000 cP droplets in both Experiment 1 (69 min) and Experiment 2 (38 min), these differences cannot be judged to be significant at the 5% level in the HNPP.

The ANOVA and the HNPP results also indicate that the average evaporation rates of the 100 and 1,000 cP viscosity droplets are not significantly different in the early stage (0 to 2 hr) of the evaporation process in Experiments 1 and 2. However, in the later stage of the process, a statistically significant difference in the average evaporation rate for the 100 and 1,000 cP droplets is evident [e.g., after 6 hr in Experiment 1 (11.2  $\mu\text{g}/\text{min}$  and 12.6  $\mu\text{g}/\text{min}$ ) and in Experiment 2 (11.3  $\mu\text{g}/\text{min}$  and 12.9  $\mu\text{g}/\text{min}$ )]. It is noteworthy that the average evaporation for the 6-hr period is greater for the 1,000 cP droplets than for the 100 cP droplets. The difference of approximately 1  $\mu\text{g}/\text{min}$  amounts to a difference of 10% in the rates, which is probably of little operational significance.

## 6.2 Droplet Spread Factors.

A factorial analysis was performed on the average spread factor results that were derived for the droplets deposited on the leaf surfaces (Table 3). The results of the Yates' factorial analysis and HNPP of the magnitude of the effects are in Appendix N. The ANOVA tables for the droplet spread factors are in Appendix O. Both the HNPP and the ANOVA indicate that the leaf surface [Factor 3 (top versus bottom surface)] is the most dominant factor affecting the extent of spreading of the liquid droplets on the leaf surface. The droplet spread factors in Experiment 2 are also influenced to some extent by the condition of the leaf surface. Factor 4 is significant at the 1% level, and the interaction between the surface and condition of the oak leaf (Factor 34), which is significant at the 5% level, seems plausible. The other variables in these experiments, over the ranges tested, had no significant effect on the extent of spreading of the droplets on the leaf surfaces. Most important in Experiment 1, the results indicate there was no significant difference in spreading of the droplets deposited on the leaves of the Northern Red Oak and the Skagbark Hickory.

The principal finding in Experiment 1 is that the liquid droplets spread more on the top surface of the leaf than on the bottom surface for

both leaf species (2.66/1.89 and 2.47/1.88 for the top/bottom surfaces of the hickory and oak leaves, respectively). The average spread factor for droplets on the top and bottom surfaces of these leaves are estimated to be 2.56 ( $\pm 0.236$  SD) and 1.88 ( $\pm 0.052$  SD), respectively.

In addition to the difference in spreading of the droplets on the top and bottom leaf surfaces in Experiment 2, it is also evident there is a difference in spreading of droplets deposited on the green September oak and the red October oak leaves. Moreover, this difference in spreading is greater for the top surfaces than for the bottom surfaces of these leaves, which explains the interaction effect (Factor 34) between the oak leaf surface and the condition of the oak leaf. This is evident in the two-way plot shown in Figure 5. The average spread factor for droplets on the top surface of the green oak leaf is 2.47 ( $\pm 0.292$  SD), compared to a spread factor of 1.95 ( $\pm 0.062$  SD) for the top surface of red oak leaf. However, the average spread factors for the bottom surfaces of the green and red oak leaves are quite similar (1.88 ( $\pm 0.004$  SD) and 1.79 ( $\pm 0.052$  SD), respectively). Evidently, this interaction arises because there is apparently little difference in spreading of the droplets on the bottom surfaces of the green and red oak leaves; however, there is a significant difference in spreading of the droplets deposited on the top surfaces of the green and red oak leaves.

The viscosity of the thickened liquid droplet and the wind speed, over the ranges tested, did not affect the spreading of the deposited droplets in these experiments.

In summary, the analyses of the droplet spread factor results indicate first that there is a greater difference between the top and bottom surfaces of the oak and hickory leaves investigated than between the oak and hickory species. Secondly, the spread factor for a leaf can be expected to vary with the condition of the leaf or its age, as indicated by the difference in spreading on the oak leaves in September and October. In general, these droplet spread factor findings correlate well with the evaporative behavior of the deposited droplets.

## 7. DISCUSSION

Graphs depicting the experimental residual mass and fractional mass of the evaporating droplets deposited on leaf foliage and the predictions of a first order model are in Appendixes G and H. The simple first order expression defined as

$$-dm/dt = Km$$

or

$$m(t) = M(0)e^{-Kt}$$

is described by the initial droplet mass,  $M(0)$ , and an empirical constant  $K$ , the specific rate or velocity constant of the process. Recognizing that at  $t = t_{1/2}$ ,  $m(t) = M(0)/2$ , this velocity content can then be defined in terms of the half-life of the deposited droplet

$$K = \ln 2/t_{1/2}$$

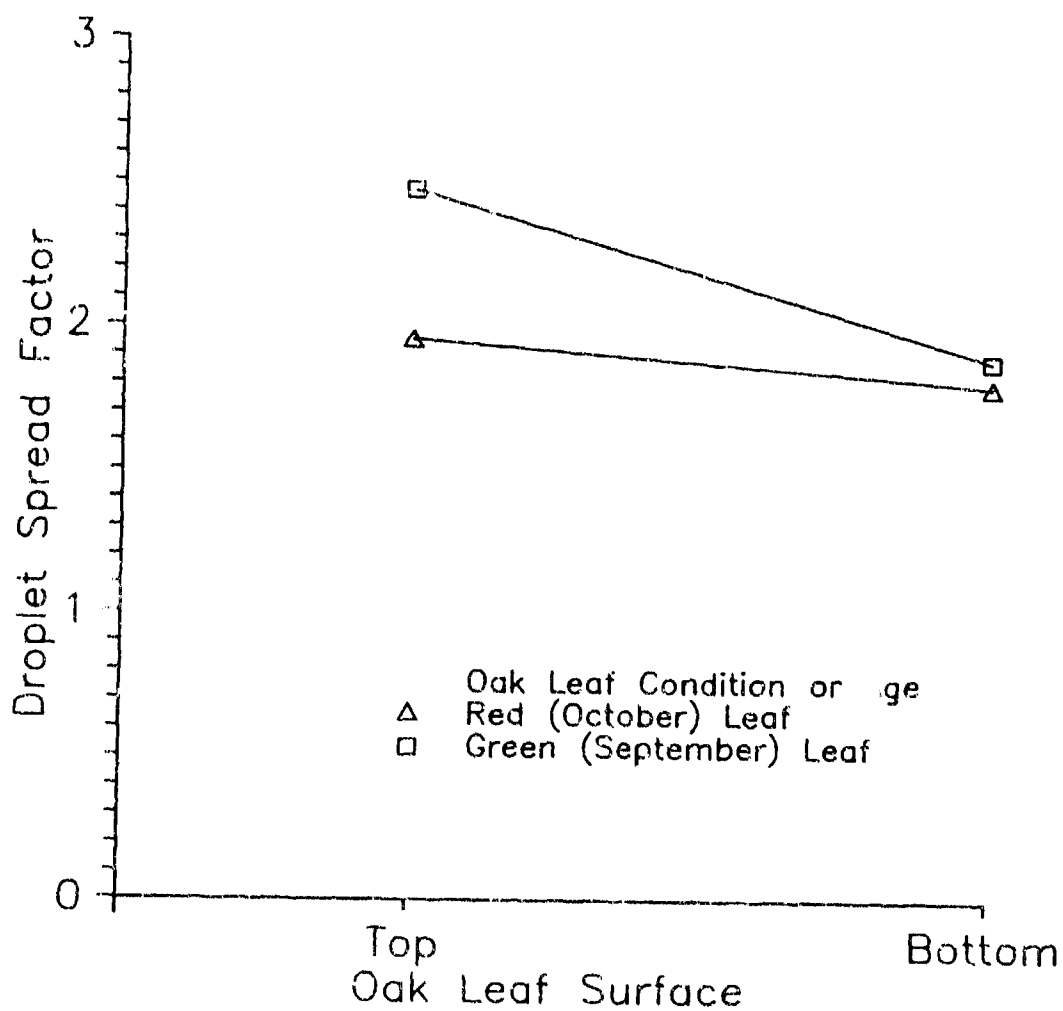


Figure 5. Effect of Interaction Between the Oak Leaf Surface and the Condition/Age on the Leaf Spread Factor (Factor 34) in Experiment 2

This simple expression fits reasonably well the experimental droplet evaporation data obtained in Experiments 1 and 2 during the most significant part of the volatilization period, as shown in Figure 6. This raises the possibility that the evaporation of droplets deposited on leaf foliage can be reasonably well predicted, in general, from the characteristic half-life of the contamination.

The utility of the half-life model in expressing the evaporative behavior of agent droplets on surfaces is not without precedence. For example, in 1928, Walker et al. issued a lengthy report on HD evaporation from soil in field tests conducted between 1922 and 1926 at the Edgewood Arsenal. The evaporation of large H droplets was found to follow a first order decay for about 2 to 3 hr, at temperatures ranging between about 18 and 28 °C.<sup>7</sup> In 1956, Trick showed that the evaporation of GB droplet contamination from wet and dry grounds also followed the first order relationship.<sup>8</sup> In 1986, Podoll et al. found that GD, TGD, VX, and HD droplets deposited on soil and vegetation had similar curves of volatilization. Generally, a slight maximum rise in the volatilization, which they believed corresponded to the initial spreading of the droplet, was followed by a first order decline in the volatilization rate.<sup>9</sup>

The summary of the ANOVA (Table 17) for droplet evaporation Experiments 1 and 2 indicate that the droplet half-life depends principally on two or three factors in these experiments, wherein the temperature was held constant. It seems plausible that the half-life of the simulant agent droplet evaporating at constant ambient temperature might be reasonably well predicted by a simple linear model involving two or three terms; wind speed, leaf surface, and perhaps leaf age or condition. The results of fitting three regression models (Models 1 and 1B--Experiment 1, and Model 2--Experiment 2) to the experimental half-life data obtained in these two experiments are in Appendix P, Tables 1 through 3. In Model 1, the droplet half-life is estimated by the two terms of wind speed ( $B = -89.4375$ ), the leaf surface factor ( $C = 36.1875$ ), and the constant 218.6875. In Model 1B, a slightly better estimate of droplet half-life over Model 1 is provided by including the effects due to the liquid viscosity of the droplet ( $A = 11.1875$ ), the type of leaf ( $D = -12.6875$ ), and an interaction factor ( $BC = -11.4375$ ). The multiple correlation factor and standard error of the estimate for Model 1B are 0.9921 and 15.744, when compared to 0.9706 and 26.530 for Model 1. In Model 2, the droplet half-life is estimated by three terms; wind speed ( $B = -93.1875$ ), leaf surface ( $C = 20.8175$ ) and an interaction factor ( $CD = 18.5625$ ) between leaf surface and leaf condition or age, and the constant 233.4375. The multiple correlation for this model is 0.9796, and the standard error of the estimate is 23.047. A comparison of the three model predictions is also shown in Figure P-1, which gives a plot of the experimental droplet half-life versus the predicted droplet half-life. In addition, the best fit linear curve for each of the model predictions is also shown. It is evident from these curves that there is little difference between the predictions of the models on the data in Experiments 1 and 2. This is further exemplified by comparing model predictions for the same droplet half-life in Table P-4. Figure 7 shows a two-way plot of the predictions of droplet half-life based on the wind speed and leaf foliage surface parameters of the most simple model (Model 1). If the leaf surface effect is compared to spreadability of the droplet on the leaf foliage, it is evident that the droplet half-life is inversely proportional to the wind speed and spread

# Droplet Evaporation on Northern Red Oak and Shagbark Hickory Leaf Foliage

- Diethyl Malonate Droplets - 2 mm Diameter
- Liquid Viscosity - 100 and 1,000 cP
- Nominal Contamination Density - 30 g/m<sup>2</sup> on the Top and Bottom Leaf Surfaces
- Wind Speeds - 3 and 11 mph
- Air Temperature - 60 °F
- Average Relative Humidity - 42%

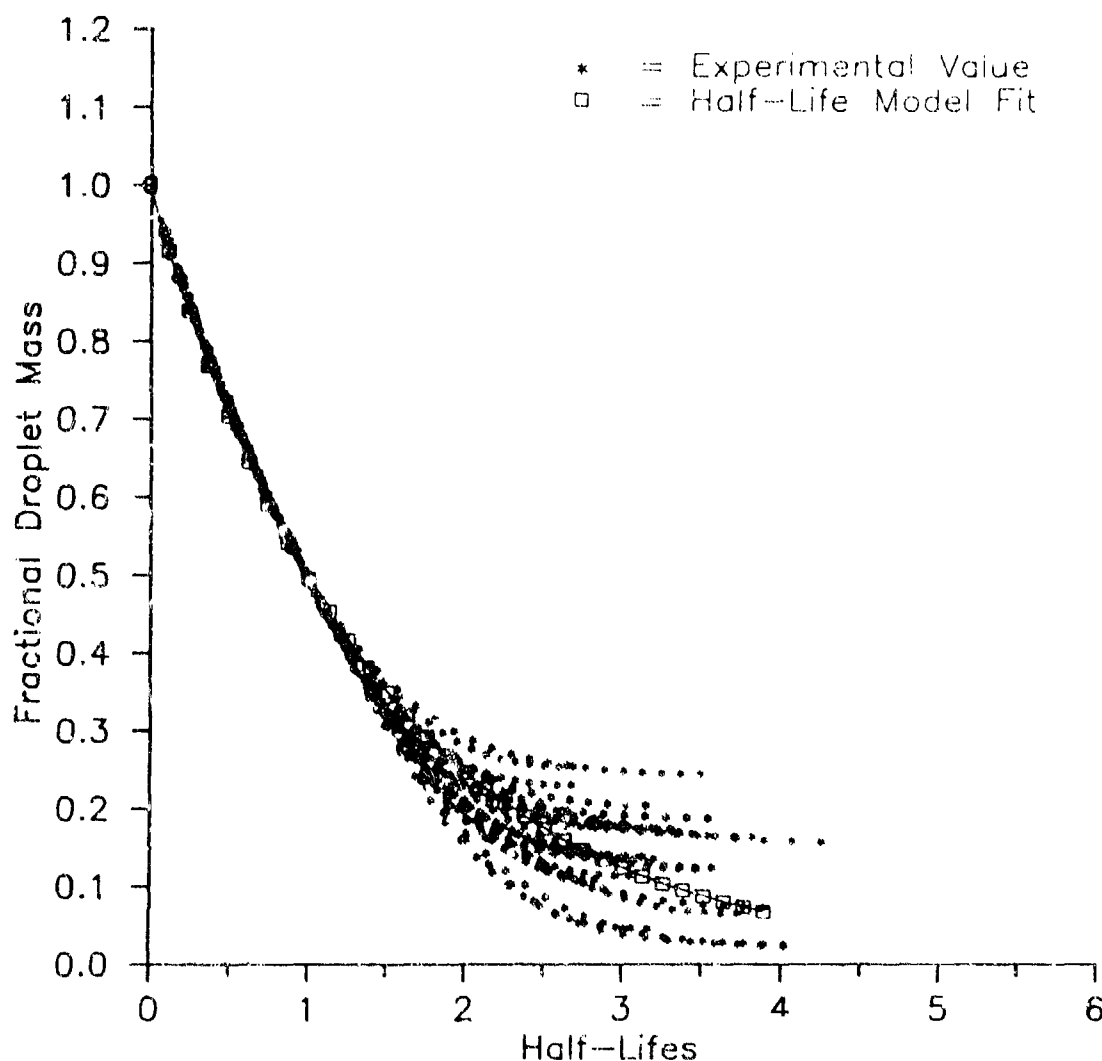


Figure 6. Comparison of Droplet Half-Life Model Predictions with Experimental Leaf Foliage Results (Normalized)

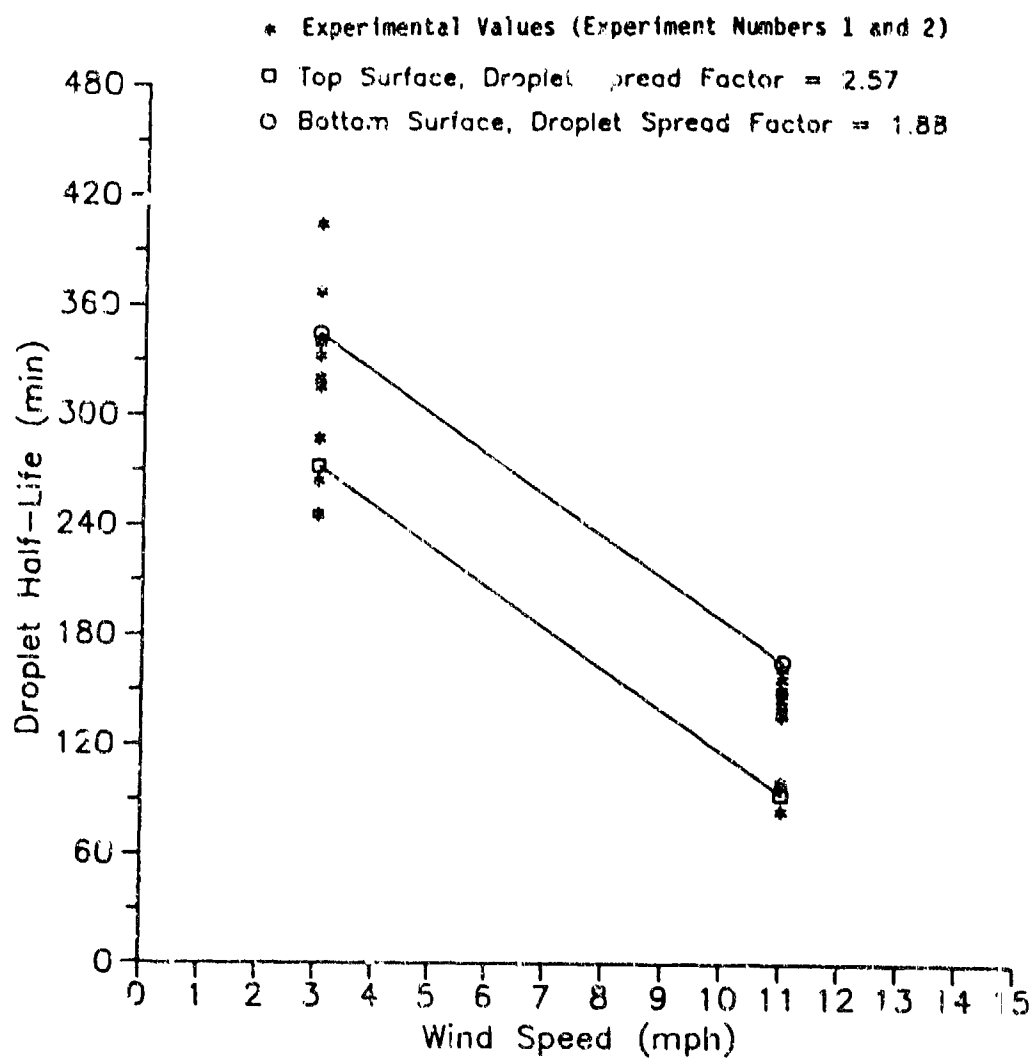


Figure 7. Model 1 Predictions of the Half-Life of a 2 mm Diameter DEM Droplet Deposited on Leaf Foliage

factor of the droplet. At a constant wind speed, the difference in droplet half-life estimates between the top and bottom surfaces of the leaf is explained reasonably well by the difference in droplet spread factor. For example, at 3 mph, the ratio of the estimate droplet half-life on the top leaf surface to the bottom leaf surface is 0.79 and the ratio of the droplet spread factors is 0.73.

In Figure 8, a similar two-way plot for droplet half-life predictions based on Model 2 indicates that droplet half-life prediction may be complicated by some other chemical/physical leaf properties that are not completely related to the droplet spread factor. For a given month (September/October), the ratio of droplet half-life estimates for the top and bottom leaf surfaces is predicted reasonably well by the inverse ratio of the droplet spread factors. However, even though the spread factors of the green September oak leaf are larger than those of the red October oak leaf for both surfaces, the estimated half-lives of the green September oak leaf are also greater than that of the red October oak leaf. This explains the need for the interaction term between leaf surface and leaf condition or age in predicting droplet half-life. Figure 8 also indicates that the half-life for droplets deposited on the top surface of the red September oak leaf, with a spread factor of 2.27, is practically the same as for droplets deposited on the bottom surface of the green October oak leaf, with a spread factor of 1.79. Obviously, the similarities and differences in droplet evaporation on leaf foliage cannot be explained by the droplet spread factor alone.

Figures 9 and 10 show a comparison of the experimental and Model 1B predictions of simulant agent droplet half-life for thickened simulant droplets of 100 and 1,000 cP deposited on the top and bottom surfaces of the Northern Red Oak and Shagbark Hickory. Model 1B is an extension of Model 1 and includes the effects attributed to liquid viscosity ( $A = +11.1875$ ), the leaf species ( $D = +12.6875$ ), and an interaction effect ( $BC = -11.4375$ ) between the wind speed and the leaf surface. Depending on the wind speed, droplet half-life estimates from this model indicate that droplet half-life is approximately 60-90 min longer on the bottom leaf surface than on the top leaf surface for both leaf types. There is also a slight increase in half-life expectancy for droplets with a viscosity of 1,000 cP (30 min) and for droplets deposited on the oak leaf (30 min) as well. However, the increased sensitivity of Model 1B is based on a limited amount of evaporation and spread factor data. The increase in droplet half-life expectancy does not appear to be warranted by small differences in droplet spread factors for 100 and 1,000 cP liquid droplets deposited on both the oak and hickory leaf surfaces (Figures 9 and 10). Additional droplet evaporation and spread factor data are needed to corroborate these findings. A 30-60 min refinement in predicting the half-life of droplets is probably not important to military operations in the field. Therefore, the more simple model for estimating droplet half-life is probably satisfactory for predicting the persistency of droplets on leaf foliage when corrected for temperature and droplet size.

In summary, the simple first order mathematical expression is adequate for representing the disappearance of a thickened liquid agent simulant droplet from a contaminated leaf foliage surface during the evaporation of the thin liquid film formed on the leaf surface. Although the comparison of experimental data and model predictions are somewhat limited due to the



# Northern Red Oak Leaf

- ◊ Top, September Leaf -- Spread Factor = 2.47
- △ Bottom, September Leaf -- Spread Factor = 1.88
- Top, October Leaf -- Spread Factor = 1.95
- Bottom, October Leaf -- Spread Factor = 1.79

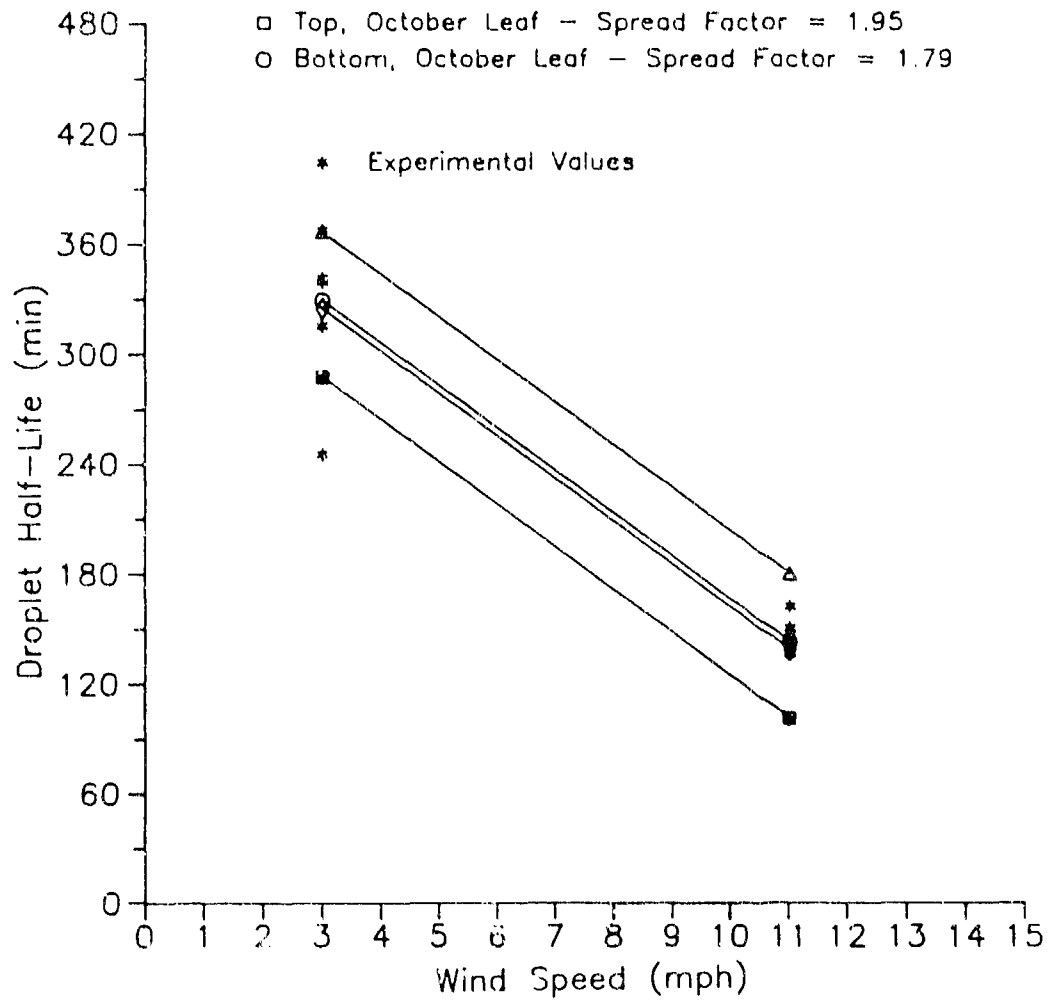


Figure 8. Model 2 Predictions of the Half-Life of a 2 mm Diameter DEM Droplet Deposited on Leaf Foliage

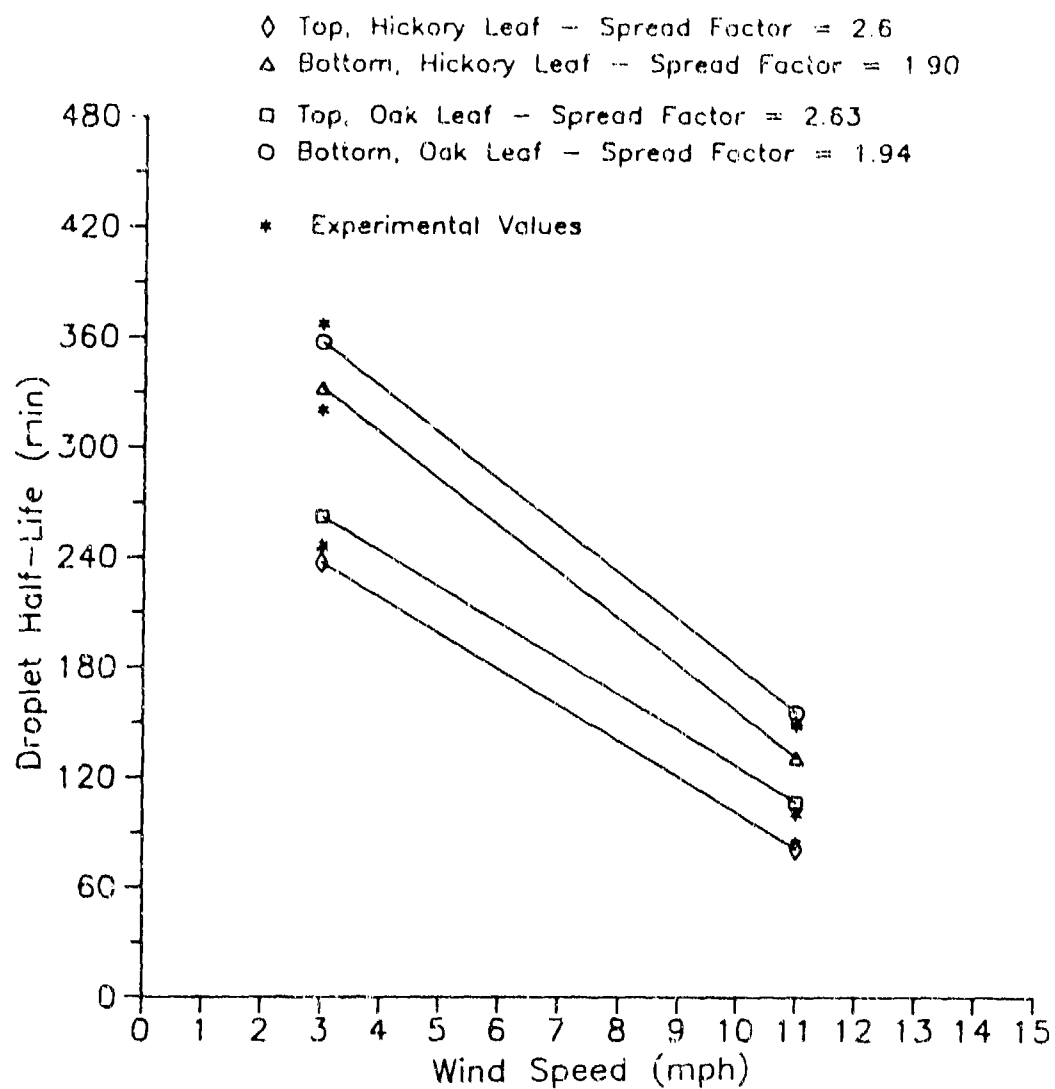


Figure 9. Model 1B Predictions of the Half-Life of a 100 cP, 2 mm Diameter DEM Droplet Deposited on Leaf Foliage

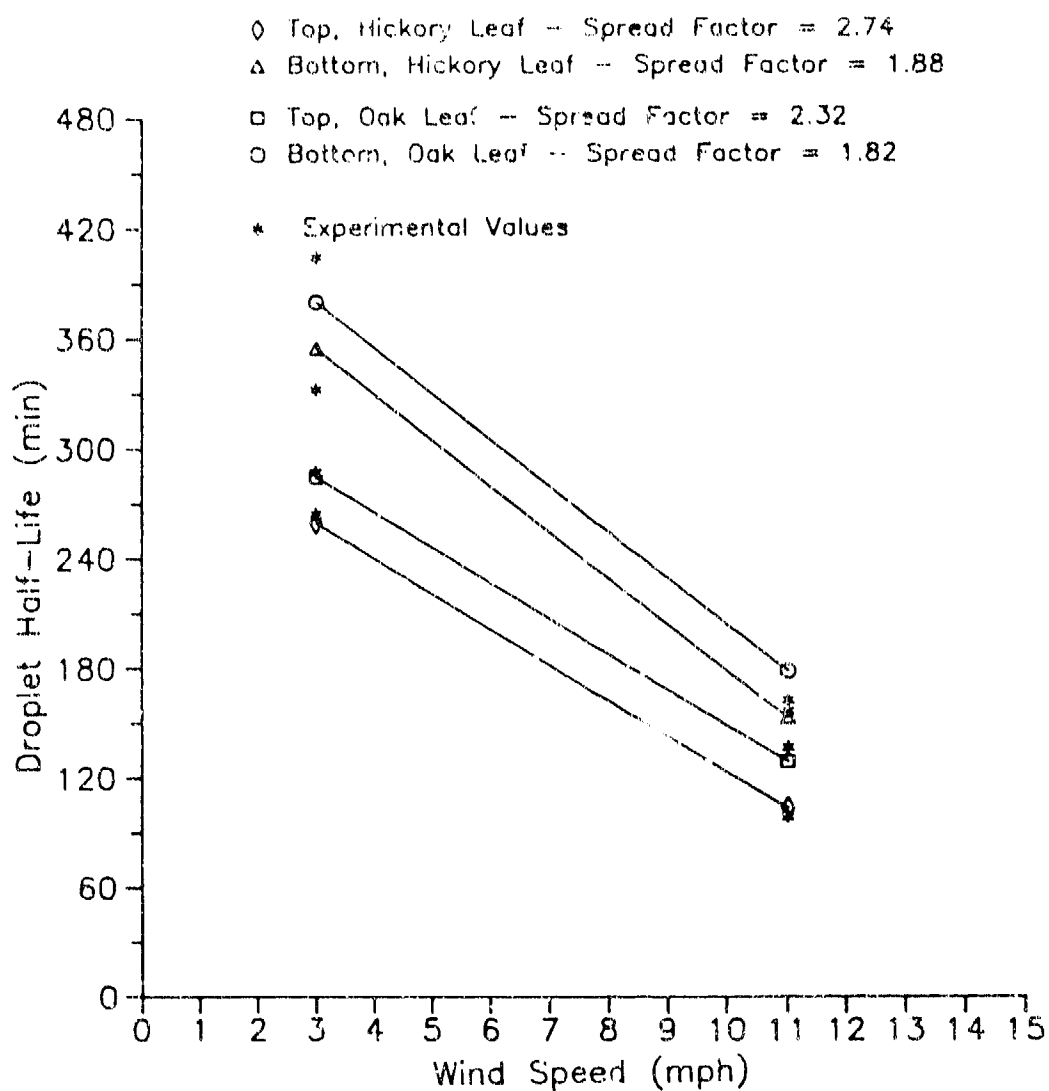


Figure 10. Model 1B Predictions of the Half-Life of a 1000 cP, 2 mm Diameter DEM Droplet Deposited on Leaf Foliage

limited scope of this study [2 mm diameter droplet of 100 and 1,000 cP thickened DEM deposited on only two varieties of leaf surfaces (Northern Red Oak and Shagbark Hickory) at only one ambient temperature, 60 °F], it is expected that the half-life model will also hold for other conditions (i.e., droplet size, ambient temperature, etc.) where evaporation is occurring from a thin shrinking film of liquid on a relatively nonabsorbing surface. Predictions of the half-life of deposited droplets on leaf foliage in these experiments depend primarily on the wind speed and the leaf surface (top/bottom) and, to a lesser extent, on type of the leaf (oak/hickory) and leaf condition or age (September oak/October oak). The influence of the leaf foliage is manifested to a large extent by the spreading of the deposited liquid droplet mass and the liquid surface area assumed. Unfortunately, the spreading of agents on surfaces is difficult to predict because of the sensitivity of spreading on the chemical and the physical state of the leaf foliage. In general, of the most critical factors that affect agent droplet volatilization (i.e. wind speed, droplet size, and droplet spreadability), the spreadability of the deposited droplets on surfaces is the one that is largely unknown. This is an area that needs to be explored further because the rate of sorption and biotransformation of the liquid agent droplets are probably also affected by the spreadability of the deposited droplet.

## 8. CONCLUSIONS

A clearer understanding of the effects of liquid viscosity of deposited droplets (100 cP versus 1,000 cP), the wind speed (3 mph versus 11 mph), and particularly the properties of contaminated leaf foliage (namely leaf surface top versus bottom), leaf type (oak versus hickory) and the condition or age (green September leaf versus red October leaf) on the evaporation and spreading characteristics of deposited droplets of thickened diethyl malonate (DEM) has been obtained.

A simple first order mathematical expression is adequate for representing the disappearance of a thickened liquid agent simulant droplet from contaminated leaf foliage surface during the evaporation of the thin liquid film that is formed on the leaf surface.

Wind speed is the most dominant factor affecting the amount, rate of return, and duration of the hazard for 2 mm diameter droplets of thickened DEM deposited on a leaf surface at 60 °F ambient temperature. The effect produced by wind speed is predominantly a direct effect, and the wind speed factor alone can explain most of the total variation (80 and 88%) in the droplet evaporation characteristics studied in the two factorial experiments. Only one exception was found. In Experiment 2, the the total percentage of contamination recovered is also strongly dependent on the viscosity of the deposited liquid droplet and the condition or age of the oak leaf.

The differences in droplet weathering on contaminated leafy surfaces at 3 and 11 mph are significant. Initially (0-3 hr), the average droplet evaporation rate of the deposited 2 mm diameter droplets at 3 mph is one-half the evaporation rate of the deposited droplets exposed to 11 mph wind speed. However, after 6 hr, the average droplet evaporation rate at 3 mph is nearly two-thirds the droplet evaporation rate at 11 mph. The difference in life-time of the deposited droplets at 3 and 11 mph is approximately 10 hr, and there is a 3-hr difference in the half-life of the 2-mm droplets.

The leaf surface (top versus bottom) is the second most important factor affecting the evaporation behavior of the deposited DEM droplets. The DEM droplets spread substantially more on the top surfaces of the oak and hickory leaves than on the bottom surfaces. This in turn affects the initial rate of evaporation of the deposited droplet, especially at the higher wind speed, up to 6 hr (the last time increment in the analysis) after contamination. However, the differences in the percent of contamination recovered from the top and bottom leaf surfaces are negligible (approximately 10 and 5%) in Experiments 1 and 2. The long-term yields associated with the droplet contamination (i.e., the total amount of contamination that evolves and, surprisingly, the lifetime of the deposited droplets) are not dependent on the leaf surface. Thus, the leaf surface does not have to be considered to predict the persistency of the hazard in these experiments.

The leaf type (Northern Red Oak versus Shagbark Hickory) has only a minor effect on the evaporation of deposited DEM droplets. The differences in droplet evaporation behavior for droplets deposited on oak and hickory leaves are not considered to be operationally significant.

The condition or age of the oak leaf primarily affects the percent of the liquid droplet contamination that eventually evolves. However, the final amount of liquid agent that is recovered as vapor from the oak leaf is strongly dependent on the initial viscosity of the liquid droplet, as well as the condition or age of the leaf.

The spread factor of a thickened DEM droplet deposited on a leaf surface is affected mainly by the leaf surface and the condition or age of the leaf. The leaf surface (top versus bottom) is the most dominant factor. Surprisingly, the difference in spreading of a deposited droplet is greater between the top and bottom surfaces of the leaves investigated than between the leaf types. Liquid droplets spread to a greater extent on the top surface than on the bottom surface of both leaf species that were tested. The average spread factor for a deposited droplet is estimated to be 2.56 ( $\pm 0.236$  SD) on the top surface and 1.88 ( $\pm 0.052$  SD) on the bottom surfaces of both the oak and hickory leaves.

However, there is also evidence that the condition or age of the leaf affects the the spreading of the droplet on the leaf surface. A significant difference in spreading of droplets deposited on the green September oak leaf and the red October oak leaf was detected. This is revealed by the interaction effect between leaf surface and leaf condition in Experiment 2. The average spread factor for a droplet deposited on the top surface of a green September oak leaf is 2.47 ( $\pm 0.292$  SD) compared to 1.95 ( $\pm 0.062$  SD) on the top surface of a red October oak leaf. However, the average spread factors for the bottom surface of the green and red oak leaves are similar [1.88 ( $\pm 0.004$  SD) and 1.79 ( $\pm 0.052$  SD)].

The viscosity of thickened DEM (100/1,000 cP) and the wind speed (3-11 mph) over the ranges tested had no detectable effect on the extent of spreading of a droplet deposited on the oak and hickory leaves.

9. RECOMMENDATION

Experimental droplet evaporation and spread factor studies should be continued with DEM and other persistent liquid CW agent/simulants deposited on other natural and man-made surfaces that have not been investigated in this research project to better quantify their spreadability, volatilization, persistency, and expected recoveries. These studies should be accomplished in order to ascertain and classify the liquid/vapor threats posed by droplets of the agent on these surfaces under a variety of atmospheric and surface conditions.

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APPENDIX A  
A COMPUTER PROGRAM  
FOR TRANSFORMING MIRAN IA VAPOR ANALYZER VOLTAGE READINGS  
ON AN IBM PC/AT

```

D Line# 1      7      Microsoft FORTRAN77 V3.31 August 1985
1      PROGRAM MIRAN
2 C      ***** PROGRAM TO ANALYZE MIRAN VAPOR ANALYZER DATA *****
3 C      ***** FROM WINDTUNNEL DROPLET EVAPORATION EXPERIMENTS *****
4 C
5 C
6 C      WINDTUNNEL CONDITION:
7 C      DYNAMIC AREA = 10.25 X 3.75 SQ INCHES (NOMINAL)
8 C      AREA=10.5 X 4.0 SQ INCHES (UPPER BOUND)
9 C      AREAL=10.0 X 3.0 SQ INCHES (LOWER BOUND)
10 C
11 C
12 C
13 C      PROGRAM OUTPUT REPORT:
14 C
15 C      (1)  OUTPUT VOLTAGE DATA FROM MIRAN 1A ANALYZER.
16 C
17 C      (2)  VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED
18 C      DROPLETS, (PPM/AB BASED ON MIRAN MASS BALANCE).
19 C
20 C      (3)  VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED
21 C      DROPLETS, (PPM/AB BASED ON MIRAN CALIBRATION DATA).
22 C
23 C      (4)  CUMULATIVE DOSAGE DERIVED FROM A UNIFORM ARRAY OF DEPOSITED,
24 C      (PPM/AB BASED ON MASS BALANCE).
25 C
26 C      (5)  CUMULATIVE DOSAGE DERIVED FROM A UNIFORM ARRAY OF DEPOSITED,
27 C      (PPM/AB BASED ON MIRAN CALIBRATION DATA).
28 C
29 C      (6)  EVAPORATION HISTORY OF TEST DROPLET MEASURED & THEORETICAL.
30 C
31 C      (7)  EVAPORATION HISTORY OF DEPOSITED TEST DROPLET.
32 C
33 C      (8)  SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION.C
34 C
35 C      (9)  EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY.
36 C
37 C      (10) CHECK OF INPUT AND OUTPUT PARAMETER VALUES.
38 C
39 C      (11) EFFECTIVE WINDSPEEDS FOR TEST TO ACHIEVE PPM/AB OF MIRAN
40 C      CALIBRATION FOR ASSUMED WINDTUNNEL DYNAMIC CROSS-SECTIONAL AREAS.
41 C
42 C
43 C
44 C      CHARACTER*1 ANSWER,DASH
45 C      CHARACTER*14 FNAME
46 C      CHARACTER*72 LL1,LL2,LL3,LL4
47 C      INTEGER NQ,NSLT,HTBL,DISPLAY,NOPTS
48 C      REAL ENDV,ENDVT
49 C
50 C      DIMENSION VOLT(45),TMEAC(40),VPPMT(40),VCDT(40),VPPMD(40),
51 C      JVCDD(40),CPMT(40),CCDT(40),CPMD(40),CCDD(40),CUMDT(40),CUMDD(40),
52 C      &CCUMT(40),CCUMD(40),SUMVS(40),EVAPN(40),EVAPM(40),IVOL(45),
53 C      &VOLTN(40),EVPN5(40),EVPMS(40),EVPRN(40),EVPRM(40),TIMER(40),
54 C      &XSQMT(40),XGSQM(40),CSQMT(40),CGSQM(40),FRMT(40),FRYM(40)
55 C
56 C

```

```

D Line# 1      7
57 1  CONTINUE
58      DATA VOLT,TMEAC,VPPMT,VCDT,VPPMD,
59      &VCCD,CPMT,CCDT,CPMD,CCDD,CUMDT,CUMDD,
60      &CCUMT,CCUMD,SUMVS,EVAPN,EVAPM,
61      &VOLYN,EVPNS,EVPM5,EVPRN,EVPRM,TIMER,
62      &FRMT,XSQMT,XGSQM,CSQMT,CGSQM,FRHT,IVOL/1165*0.0,45*0/
63 C
64      DASH = '-'
65 C
66 C      READ EXPERIMENTAL CONDITIONS AND VALUES FROM DATA FILE ON DRIVE B
67 C
68      WRITE(*,1500)
69      WRITE(*,1510)
70      WRITE(*,1515)
71      WRITE(*,1520)
72      READ(*,30) FNAME
73 C
74 1519 WRITE(*,1521)
75      WRITE(*,1522)
76      WRITE(*,1523)
77      WRITE(*,1524)
78      WRITE(*,1525)
79      WRITE(*,1526)
80      READ(*,1529) NSLT
81      IF((NSLT.NE. 1) .AND. (NSLT.NE. 2) .AND. (NSLT.NE. 3) .AND. (N
82      &SLT.NE. 4)) GOTO 1519
83 C
84      WRITE(*,1531)
85      WRITE(*,1532)
86      WRITE(*,1533)
87      READ(*,1529) DISPLAY
88 C
89 C      READ FILE USES UNIT 5
90 C
91      OPEN(5,FILE=FNAME,STATUS='OLD')
92      READ(5,30) LL1
93      READ(5,30) LL2
94      READ(5,30) LL3
95      READ(5,30) LL4
96 C
97      READ(5,35) GM1TP,GM2TP,GM3TP,DPPT,NCODE,CODEL,AIRSP,CAL
98 C
99 C      ENTER TEST INFORMATION PERTAINING TO MIRAN ANALYZER RECORD TO BE
100 C      ANALYZED:
101 C
102      READ(5,40) ABPV,IMINV,NOPTS,ENDVT
103      ENDV = ENDVT
104 C
105 C      ENTER VALUES FROM VOLT VERSUS TIME CURVE **AS MILLIVOLT**
106 C
107      READ(5,45) (IVOL(I),I=1,NOPTS)
108      CLOSE(5)
109 C
110 C      CONVERT INPUT COLUMN MATRIX IVOL (MILLIVOLTS) TO COLUMN MATRIX
111 C      VOLV (VOLTS) E.G. 40 TO .040
112 C

```

```

D Line# 1      7
113          DO 50 I = 1,NOPTS
114          VOLT(I) = IVOL(I)/1000.0
115          50 CONTINUE
116          WRITE(*,51)
117          DO 60 I = 1,15
118          WRITE(*,52) I,IVOL(I),VOLT(I),I+15,IVOL(I+15),VOLT(I+15),I+30,IVOL
119          &(I+30),VOLT(I+30)
120          60 CONTINUE
121          WRITE(*,53)
122          WRITE(*,55)
123          WRITE(*,57)
124          70 READ(*,30) ANSWER
125          IF((ANSWER.NE.'Y').AND.(ANSWER.NE.'y').AND.(ANSWER.NE.'N
126          &') .AND. (ANSWER.NE.'n')) GOTO 70
127          IF((ANSWER.EQ.'N') .OR. (ANSWER.EQ.'n')) GOTO 1550
128          IF((ANSWER.EQ.'Y') .OR. (ANSWER.EQ.'y')) CONTINUE
129 C
130 C      COMPUTE CONTAMINANT ION DENSITY LEVEL PER TRAY (GRAMS/SQ METER)
131 C
132          GPM21 = (GM1TP/.169) + .00
133          GPM22 = (GM2TP/.169) + .05
134          GPM23 = (GM3TP/.169) + .05
135          GPM24 = ((GM2TP + GM3TP)/.3387) + .05
136 C
137 C      ASSIGN LIQUID DENSITY TO LIQUIDS (DIBENZOYL MALONATE = 1.05
138 C      METHYL SALICYLATE = 1.18 G/CC)
139 C
140          DENL1 = 1.05
141          DENL2 = 1.18
142 C
143 C      ASSIGN PERCENT COPOLYMER THICKENER
144 C
145          CPD1L = 2.8
146          CPD1H = 4.8
147          CPM2L = 2.0
148          CPM2H = 4.5
149 C
150 C      ASSIGN LIQUID CONVERSION FACTOR FOR CONVERTING PPM TO MICROGRAMS
151 C      PER CUBIC METER FOR MIRAN OPERATING TEMPERATURE OF 100 DEG F.
152 C
153          COVL1 = 6.278E3
154          COVL2 = 5.963E3
155 C
156 C      CALIBRATION INFORMATION FOR MIRAN RELATING PPM TO ABSORBANCE
157 C      VALUE
158 C
159          IF(CODEL.EQ.100.) GO TO 100
160          IF(CODEL.EQ.1000.) GO TO 110
161          IF(CODEL.EQ.200.) GO TO 120
162          IF(CODEL.EQ.2000.) GO TO 130
163          100 PERCP = CPD1L
164          105 DENLQ = DENL1
165          COVLQ = COVL1
166          PRPAB = CAL
167          GO TO 150
168          110 PERCP = CPD1H

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D Line# 1      7      Microsoft FORTRAN77 V3.31 August 1985
169      GO TO 105
170 120 PERCP = CPM2L
171 125 DENLQ = DENL2
172      COVLQ = COVL2
173      PRPAB = CAL
174      GO TO 150
175 130 PERCP = CPM2H
176      GO TO 125
177 150 CONTINUE
178 C
179 C      COMPUTE DROPLET MASS FROM LIQUID MASS AND NUMBER OF DROPLETS
180 C      ON EACH TRAY (GRAMS)
181 C
182      TM1 = GM1TP/DPPT
183      TM2 = GM2TP/DPPT
184      TM3 = GM3TP/DPPT
185      TTMT = TM1 + TM2 + TM3
186 C
187 C      COMPUTE AVERAGE VALUE OF TEST DROPLET MASS (GRAMS)
188 C
189      IF(NCODE .GE. 6) GO TO 160
190      ETDPM = TTMT/3.0
191 C
192 C      COMPUTE STANDARD DEVIATION OF TEST DROPLET MASS
193 C
194      SDMAS = (((TM1-ETDPM)**2+(TM2-ETDPM)**2+(TM3-ETDPM)**2)/2.0)**.5
195 C
196 C
197 C      COMPUTE STANDARD ERROR OF MEAN TEST DROP MASS
198 C
199      SEMAS = SDMAS/1.73205
200 C
201 C      COMPUTE EQUIVALENT DROPLET DIAMETER FOR MEAN MASS (MM)
202 C
203      EQDPD = (((1.90985*ETDPM)/DENLQ)**.33333)*10
204 C
205 C      DETERMINE THE APPROPRIATE CONVERSION FACTOR FOR SUBSTRATE
206 C      ANALYZED CORRESPONDING TO VOLT MATRIX... INFORMATION
207 C
208      IF(NCODE .LT. 6) GO TO 165
209 160 ETDPM = TTMT/2.0
210      SDMAS = (((TM2-ETDPM)**2+(TM3-ETDPM)**2)/1.0)**.5
211      EQDPD = (((1.90985*ETDPM)/DENLQ)**.33333)*10
212 165 IF(NCODE .EQ. 1) GO TO 200
213      IF(NCODE .EQ. 2) GO TO 220
214      IF(NCODE .EQ. 3) GO TO 240
215      IF(NCODE .EQ. 4) GO TO 260
216      IF(NCODE .EQ. 5) GO TO 280
217      IF(NCODE .EQ. 6) GO TO 285
218 C
219 C      DATA FROM THREE SUBSTRATES REDUCED TO SINGLE TRAY EQUIVALENT
220 C
221 200 TVCF3 = GM3TP/(GM1TP + GM2TP + GM3TP)
222      VGPT = GPM23
223      NTRAY = 3
224      TRAYM = GM3TP

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D Line# 1      7      Microsoft FORTRAN77 V3.31 August 1985
225      NSET = 3
226      EXPGM = GM1TP + GM2TP + GM3TP
227      GO TO 290
228 C
229 C      VGPT IS A CONVERSION FACTOR USED TO CONVERT DATA TO GRAM/SQ METER
230 C      BASIS.
231 C      NTRAY IS ID NUMBER BY POSITION IN WINDTUNNEL TEST 1 UPSTREAM ETC.
232 C      NSET IS NUMBER OF SUBSTRATES USED FOR VOLT INPUT DATA.
233 C
234 C      DATA INPUT CORRESPONDS TO 2 AND 3 SUBSTRATES REDUCED TO SINGLE
235 C      TRAY EQUIVALENT
236 C
237 220 TVCF3 = GM3TP/(GM3TP + GM2TP)
238      VGPT = GPM23
239      NTRAY = 3
240      TRAYM = GM3TP
241      NSET = 2
242      EXPGM = GM3TP + GM2TP
243      GO TO 290
244 C
245 C      DATA INPUT CORRESPONDS TO 3 AND 1 SUBSTRATES REDUCED TO SINGLE
246 C      TRAY EQUIVALENT
247 C
248 240 TVCF3 = GM3TP/(GM3TP + GM1TP)
249      VGPT = GPM23
250      NTRAY = 3
251      TRAYM = GM3TP
252      NSET = 2
253      EXPGM = GM3TP + GM1TP
254      GO TO 290
255 C
256 C      DATA INPUT CORRESPONDS TO 1 SUBSTRATE AT POSITION 3 IN TUNNEL
257 C
258 260 TVCF3 = 1.0
259      VGPT = GPM23
260      NTRAY = 3
261      TRAYM = GM3TP
262      NSET = 1
263      EXPGM = GM3TP
264      GO TO 290
265 C
266 C      DATA INPUT CORRESPONDS TO 1 SUBSTRATE AT POSITION 1 IN TUNNEL
267 C
268 280 TVCF3 = 1.0
269      VGPT = GPM21
270      NTRAY = 1
271      TRAYM = GM1TP
272      NSET = 1
273      EXPGM = GM1TP
274      GO TO 290
275 C
276 C      DATA INPUT CORRESPONDS TO TWO SUBSTRATES AT POSITIONS 2 & 3
277 C
278 285 TVCF3 = 1.0
279      VGPT = GPM24
280      NTRAY = 4

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D Line# 1      7      Microsoft FORTRAN77 V3.31 August 1985
281      TRAYM = GM3TP + GM2TP
282      NSET = 6
283      EXPGM = TRAYM
284      DPPT = DPPT*2
285      GO TO 290
286 C
287 C      SELECT APPROPRIATE TEST MASS
288 C
289 290 CONTINUE
290 C
291      IF(NTRAY - 2) 300,310,315
292 300 TMASS = TM1
293      GOTO 330
294 310 TMASS = TM2
295      GOTO 330
296 315 IF(NTRAY - 4) 320,325,325
297 320 TMASS = TM3
298      GOTO 330
299 325 TMASS = (TM2 + TM3)/2
300 C
301 C      CORRECT THE LIQUID DROP MASS ON SUBSTRATE TO ACCOUNT FOR PERCENT
302 C      POLYMER THICKENER WHICH IS ASSUMED TO BE NON-VOLATILE INGREDIENT
303 C
304 330 CMASS = TMASS*(100. - PERCP)/100.0
305 C
306 C      DETERMINE THE CUMULATIVE DISTRIBUTION (VOLT.MIN) FOR SINGLE
307 C      SUBSTRATE USING TRAPEZOIDAL RULE
308 C
309      SUMVS(1) = 0.0
310      VOLTM = 0.0
311      DO 400 I = 2,NOPTS
1 312 C
1 313 C      TVCF3 PRODUCES THE OUTPUT DATA EQUIVALENT TO A SINGLE SUBSTRATE
1 314 C
1 315      VOLTM = ((VOLT(I)+VOLT(I-1))/2)*TMINV*TVCF3
1 316      SUMVS(I) = SUMVS(I-1) + VOLTM
1 317 C
1 318 C      TIME INCREMENT FOR CORRESPONDING CUMULATIVE VOLT.MIN FOR
1 319 C      TABULATING
1 320 C
1 321      TMEAC(I) = (TMINV * I) - TMINV
1 322 400 CONTINUE
323 C
324 C      ASSIGN THE TOTAL VALUE OF CUMULATIVE DISYRIBUTION
325 C
326      IF((NCODE .GE. 6) .AND. (ENDVT .EQ. 1.0)) GOTO 654
327      GOTO 420
328 405 CONTINUE
329 C
330 C      ASSIGN A VALUE TO TOTAL CUMULATIVE VOLT.MIN FOR MIRAN VOLTAGE DAT
331 C
332      ACVTM = (((100.-PERCP)/100.)*EXPGM*1E6)/(ABPV*PRPAB*COVLQ*Y)
333      IF((NCODE .GE. 6) .OR. (ENDVT .EQ. 1.0)) GOTO 422
334 420 ACVTM = SUMVS(NOPTS)
335 422 CONTINUE
336 C

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```

D Line# 1      7
337      NSET = 7
338      ENDVT = 0.0
339 C
340 C      CALCULATE THE HALF-LIFE FOR EVAPORATION USING CUMULATIVE VOLTAGE
341 C      READINGS, SUMVS(I)
342 C
343      N = NOPTS - 1
344      DO 500 I = 1,N
1 345      HAFVT = SUMVS(I)/ACVTM
1 346      IF (HAFVT .LT. .5) GO TO 500
1 347      IF (HAFVT .EQ. .5) GO TO 520
1 348      T2 = TMEAC(I)
1 349      T1 = TMEAC(I-1)
1 350      V2 = SUMVS(I)/ACVTM
1 351      V1 = SUMVS(I-1)/ACVTM
1 352 C
1 353 C      COMPUTE TIME VALUE BY LINEAR INTERPOLATION METHOD
1 354 C
1 355      HAFTM = (((T2 - T1) * (.5 - V1))/(V2 - V1)) + T1
1 356      GO TO 530
1 357 500  CONTINUE
1 358 520  HAFTM = TMEAC(I)
1 359 530  CONTINUE
360 C
361 C      EVAPORATION RATE AVERAGED OVER ONE HALF-LIFE (MICROGRAMS/MIN)
362 C
363      ERHLF = ((CMASS/(-2.))/HAFTM)*1E6
364 C
365 C      CALCULATE NORMALIZED EVAPORATION CURVE FOR SINGLE DROPLET OF
366 C      SPECIFIED SIZE
367 C
368      DO 550 I = 1,NOPTS
1 369      VOLTN(I) = SUMVS(I)/ACVTM
1 370      EVAPN(I) = 1 - VOLTN(I)
1 371 C
1 372 C      CALCULATE THE MASS OF DROPLET REMAINING AS A FUNCTION OF
1 373 C      EVAPORATION TIME, EXCLUDING NON-VOLATILE POLYMER CONTENT
1 374 C
1 375      EVAPM(I) = EVAPN(I)*CMASS
1 376 550  CONTINUE
377 C
378 C      CALCULATE THE EVAPORATION HISTORY OF THE TEST DROPLET ASSUMING
379 C      FIRST ORDER MODEL USING HALF-LIFE TIME
380 C
381      CK = ALOG(2.0)/HAFTM
382      DO 600 I = 1,NOPTS
1 383      TK = CK*TMEAC(I)
1 384 C
1 385 C      NORMALIZED VALUES
1 386 C
1 387      EVPN5(I) = EXP(-TK)*1.0
1 388 C
1 389 C      LIQUID MASS REMAINING (GRAMS)
1 390 C
1 391      EVPM5(I) = EVPN5(I)*CMASS
1 392 600  CONTINUE

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D Line# 1      7      Microsoft FORTRAN77 V3.31 August 1985
393 C          PRINTOUT MIRAN ANALYZER VALUES
394 C          //////////// TABLE 1 ////////////
395 C
396           NTBL=1
397           DO 610 IT=1,NSLT
1 398           IF(IT .EQ. 1) THEN
1 399           OPEN(6,FILE='CON')
1 400           ELSEIF((IT .EQ. 2) .AND. ((NSLT .EQ. 2) .OR. (NSLT .EQ. 3))) THEN
1 401           OPEN(6,FILE='TABLE.1',STATUS='NEW')
1 402           ELSEIF((IT .EQ. 2) .AND. ((NSLT .NE. 2) .OR. (NSLT .NE. 3))) THEN
1 403           GOTO 610
1 404           ELSEIF((IT .EQ. 3) .AND. (NSLT .EQ. 3)) THEN
1 405           OPEN(6,FILE='PRN')
1 406           ELSEIF((IT .EQ. 3) .AND. (NSLT .NE. 3)) THEN
1 407           GOTO 610
1 408           ELSEIF((IT .EQ. 4) .AND. (NSLT .EQ. 4)) THEN
1 409           OPEN(6,FILE='PRN')
1 410           ENDIF
1 411           IF(IT .EQ. 1) THEN
1 412           WRITE(6,804) NTBL
1 413           ELSE
1 414           WRITE(6,805)
1 415           ENDIF
1 416           IF(IT .EQ. 1) THEN
1 417           WRITE(6,30) LL1
1 418           WRITE(6,30) LL2
1 419           WRITE(6,30) LL3
1 420           WRITE(6,30) LL4
1 421           ELSE
1 422           WRITE(6,810) LL1
1 423           WRITE(6,810) LL2
1 424           WRITE(6,810) LL3
1 425           WRITE(6,811) LL4
1 426           ENDIF
1 427           IF(IT .EQ. 1) THEN
1 428           WRITE(6,919)
1 429           WRITE(6,923)
1 430           WRITE(6,931)
1 431           WRITE(6,936)
1 432           ELSE
1 433           WRITE(6,918)
1 434           WRITE(6,922)
1 435           WRITE(6,930)
1 436           WRITE(6,935)
1 437           ENDIF
1 438           DO 650 I = 1,NOPTS
2 439           TIM = ((TMINV*I) - TMINV)
2 440           V = VOLT(I)
2 441           CV = SUMVS(I)
2 442           VN = VOLTN(I)
2 443           IF(IT .EQ. 1) THEN
2 444           WRITE(6,941) TIM,V,TIM,CV,VN
2 445           ELSE
2 446           WRITE(6,940) TIM,V,TIM,CV,VN
2 447           ENDIF
2 448 650 CONTINUE

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D Line# 1      7
1 449      IF(IT.EQ. 1) THEN
1 450      WRITE(6,921) ABPV
1 451      ELSE
1 452      WRITE(6,920) ABPV
1 453      ENDIF
1 454      CLOSE(6)
1 455      IF((IT.EQ. 1).AND. (DISPLAY.EQ. 1)) PAUSE
1 456 610    CONTINUE
457 C
458 C      COMPUTE CONVERSION FACTOR **CPMAG** PPM/AB TO FIT ANALYZED DATA
459 C      ABPV EQUALS ABSORBANCE PER VOLT AND COVLQ IS LIQUID CONVERSION
460 C      FACTOR IN MG PER CUBIC METER
461 C
462      X = ACVTM * ABPV * COVLQ * 1E-6
463 C
464 C      AIRSP EQUALS WINDSPEED FOR TEST RUN IN MPH FOR 10.25 INCHES
465 C      (TUNNEL WIDTH) AND 3.75 INCHES (TUNNEL HEIGHT)
466 C
467 654      CONTINUE
468 C
469      IF (AIRSP.LT. 5.0) GO TO 655
470      DARTN = 10.25 * 3.75
471      WDTUN = AIRSP
472      GO TO 660
473 655      DARTN = 10.25 * 3.75
474      WDTUN = AIRSP
475 660      Y = AIRSP * DARTN * .02832 * 88/144
476 C
477      IF ((NSET.EQ. 6).OR. (ENDVT.EQ. 1.0)) GO TO 405
478 C
479      Z = X * Y
480 C
481      CPMAB = (TRAYM * (100. - PERCP)/100.)/Z
482      CCVR1 = ABPV * CPMAB * TVCF3
483 C
484 C      COMPUTE VAPOR CONCENTRATION PRODUCED BY DEPOSITED DROPLETS
485 C      ON ONE SUBSTRATE
486 C
487 C      CONVERSION USING CALCULATED PPM/AB FROM MASS BALANCE OF
488 C      WINDTUNNEL DATA
489 C      //////////// TABLE 2 ////////////
490 C
491      NTBL=2
492      DO 676 IT=1,NSLT
1 493      IF(IT.EQ. 1) THEN
1 494      OPEN(6,FILE='CON')
1 495      ELSEIF((IT.EQ. 2).AND. ((NSLT.EQ. 2).OR. (NSLT.EQ. 3))) THEN
1 496      OPEN(6,FILE='TABLE.2',STATUS='NEW')
1 497      ELSEIF((IT.EQ. 2).AND. ((NSLT.NE. 2).OR. (NSLT.NE. 3))) THEN
1 498      GOTO 676
1 499      ELSEIF((IT.EQ. 3).AND. (NSLT.EQ. 3)) THEN
1 500      OPEN(6,FILE='PRN')
1 501      ELSEIF((IT.EQ. 3).AND. (NSLT.NE. 3)) THEN
1 502      GOTO 676
1 503      ELSEIF((IT.EQ. 4).AND. (NSLT.EQ. 4)) THEN
1 504      OPEN(6,FILE='PRN')

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D Line# 1      7
1 505      ENDIF
1 506      IF(IT .EQ. 1) THEN
1 507      WRITE(6,804) NTBL
1 508      ELSE
1 509      WRITE(6,805)
1 510      ENDIF
1 511      IF(IT .EQ. 1) THEN
1 512      WRITE(6,30) LL1
1 513      WRITE(6,30) LL2
1 514      WRITE(6,30) LL3
1 515      WRITE(6,30) LL4
1 516      ELSE
1 517      WRITE(6,810) LL1
1 518      WRITE(6,810) LL2
1 519      WRITE(6,810) LL3
1 520      WRITE(6,811) LL4
1 521      ENDIF
1 522      IF(IT .EQ. 1) THEN
1 523      WRITE(6,944)
1 524      WRITE(6,951)
1 525      WRITE(6,971)
1 526      WRITE(6,981)
1 527      WRITE(6,991)
1 528      WRITE(6,1001)
1 529      ELSE
1 530      WRITE(6,945)
1 531      WRITE(6,950)
1 532      WRITE(6,970)
1 533      WRITE(6,980)
1 534      WRITE(6,990)
1 535      WRITE(6,1000)
1 536      ENDIF
1 537      DO 675 I = 1,NOPTS
2 538 C
2 539 C      CONCENTRATION IN PPM
2 540 C
2 541      VPPMT(I) = VOLT(I) * CCVR1
2 542 C
2 543 C      CONCENTRATION IN MICROGRAM/CUBIC METER OR PANOGRAMS PER CC
2 544 C
2 545      VCDT(I) = VPPMT(I) * COVLQ
2 546 C
2 547 C      MICROGRAMS PER CUBIC METER PER METERED SQAURED
2 548 C
2 549      VCPMS = VCDT(I)/.3387
2 550 C
2 551 C      MICROGRAMS PER CUBIC METER PER GRAM/METER SQAURED
2 552 C
2 553      VCPGM = VCDT(I)/VGPT
2 554 C
2 555 C      VAPOR CONCENTRATION PRODUCED BY SINGLE DROPLET EVAPORATING
2 556 C      FROM THE SUBSTRATE (PPM)
2 557 C
2 558      VPPMD(I) = VPPMT(I)/DEPT
2 559 C
2 560 C      VAPOR CONCENTRATION PRODUCED BY SINGLE DROPLET EVAPORATING

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D Line# 1      7      Microsoft FORTRAN77 V3.31 August 1985
2 561 C      FROM THE SUBSTRATE (MICROGRAMS PER CUBIC METER)
2 562 C
2 563      VCDD(1) = VCDT(1)/DPPT
2 564      TIM = ((TMINV * I) - TMINV)
2 565      A = VPPMT(1)
2 566      B = VCDT(1)
2 567      C = VPPMD(1)
2 568      D = VCDD(1)
2 569      IF(IT .EQ. 1) THEN
2 570      WRITE(6,1041) TIM,A,B,VCPMS,VCPGM,C,D
2 571      ELSE
2 572      WRITE(6,1040) TIM,A,B,VCPMS,VCPGM,C,D
2 573      ENDIF
2 574 675 CONTINUE
1 575      IF(IT .EQ. 1) THEN
1 576      WRITE(6,1889)
1 577      ELSE
1 578      WRITE(6,1888)
1 579      ENDIF
1 580      CLOSE(6)
1 581      IF((IT .EQ. 1) .AND. (DISPLAY .EQ. 1)) PAUSE
1 582 676 CONTINUE
583 C
584 C      VAPOR CONCENTRATION PRODUCED BY DEPOSITED DROPS ON SUBSTRATE
585 C      USES THE MIRAN CALIBRATION FACTOR FOR CONVERSION TO PPM/AB
586 C      //////////// TABLE 3 ////////////
587 C
588      NTBL=3
589      DO 691 IT=1,NSLT
1 590      IF(IT .EQ. 1) THEN
1 591      OPEN(6,FILE='CON')
1 592      ELSEIF((IT .EQ. 2) .AND. ((NSLT .EQ. 2) .OR. (NSLT .EQ. 3))) THEN
1 593      OPEN(6,FILE='TABLE.3',STATUS='NEW')
1 594      ELSEIF((IT .EQ. 2) .AND. ((NSLT .NE. 2) .OR. (NSLT .NE. 3))) THEN
1 595      GOTO 691
1 596      ELSEIF((IT .EQ. 3) .AND. (NSLT .EQ. 3)) THEN
1 597      OPEN(6,FILE='PRN')
1 598      ELSEIF((IT .EQ. 3) .AND. (NSLT .NE. 3)) THEN
1 599      GOTO 69
1 600      ELSEIF((IT .EQ. 4) .AND. (NSLT .EQ. 4)) THEN
1 601      OPEN(6,FILE='PRN')
1 602      ENDIF
1 603      IF(IT .EQ. 1) THEN
1 604      WRITE(6,804) NTBL
1 605      ELSE
1 606      WRITE(6,805)
1 607      ENDIF
1 608      IF(IT .EQ. 1) THEN
1 609      WRITE(6,30) LL1
1 610      WRITE(6,30) LL2
1 611      WRITE(6,30) LL3
1 612      WRITE(6,30) LL4
1 613      ELSE
1 614      WRITE(6,810) LL1
1 615      WRITE(6,810) LL2
1 616      WRITE(6,810) LL3

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D Line# 1      7
1 617      WRITE(6,811) LL4
1 618      ENDIF
1 619      IF(IT .EQ. 1) THEN
1 620      WRITE(6,944)
1 621      WRITE(6,956)
1 622      WRITE(6,971)
1 623      WRITE(6,981)
1 624      WRITE(6,991)
1 625      WRITE(6,1001)
1 626      ELSE
1 627 680    WRITE(6,945)
1 628      WRITE(6,955)
1 629      WRITE(6,970)
1 630      WRITE(6,980)
1 631      WRITE(6,990)
1 632      WRITE(6,1000)
1 633      ENDIF
1 634      DO 690 I = 1,NOPTS
2 635 C
2 636 C      ANSWER (PPM)
2 637 C
2 638      CPMT(I) = VOLT(I) * ABPV * PRPAB * TVCF3
2 639 C
2 640 C      ANSWER (MICROGRAMS PER CUBIC METER OR NANOGRAMS PER CC)
2 641 C
2 642      CCDT(I) = CPMT(I) * COVLQ
2 643 C
2 644 C      (MICROGRAMS PER CUBIC METER PER METER SQUARED)
2 645 C
2 646      VCPMS = CCDT(I)/.3387
2 647 C
2 648 C      (MICROGRAMS PER CUBIC METER PER GRAM METER SQUARED)
2 649 C
2 650      VCPGM = CCDT(I)/VGPT
2 651 C
2 652 C      VAPOR CONCENTRATION PRODUCED BY SINGLE DROPLET EVAPORATING
2 653 C      FROM THE SUBSTRATE (PPM)
2 654 C
2 655      CPMD(I) = CPMT(I)/DPPT
2 656 C
2 657 C      ANSWER (MICROGRAMS PER CUBIC METER)
2 658 C
2 659      CCDD(I) = CCDT(I)/DPPT
2 660      TIM = ((TMINV * I) - TMINV)
2 661      A = CPMT(I)
2 662      B = CCDT(I)
2 663      C = CPMD(I)
2 664      D = CCDD(I)
2 665      IF(IT .EQ. 1) THEN
2 666      WRITE(6,1041) TIM,A,B,VCPMS,VCPGM,C,D,
2 667      ELSE
2 668      WRITE(6,1040) TIM,A,B,VCPMS,VCPGM,C,D,
2 669      ENDIF
2 670 690    CONTINUE
1 671      IF(IT .EQ. 1) THEN
1 672      WRITE(6,1889)

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D Line# 1      7
1 673      ELSE
1 674      WRITE(6,1888)
1 675      ENDDIF
1 676      CLOSE(6)
1 677      IF((IT.EQ. 1) .AND. (DISPLAY.EQ.1)) PAUSE
1 678 691    CONTINUE
1 679 C
1 680 C      COMPUTE CUMULATIVE MASS DISTRIBUTION
1 681 C      ////////// TABLE 4 //////////
1 682 C
1 683      NTBL=4
1 684      DO 756 IT=1,NSLT
1 685      IF(IT.EQ. 1) THEN
1 686      OPEN(6,FILE='CON')
1 687      ELSEIF((IT.EQ. 2) .AND. ((NSLT.EQ. 2) .OR. (NSLT.EQ. 3))) THEN
1 688      OPEN(6,FILE='TABLE.4',STATUS='NEW')
1 689      ELSEIF((IT.EQ. 2) .AND. ((NSLT.NE. 2) .OR. (NSLT.NE. 3))) THEN
1 690      GOTO 756
1 691      ELSEIF((IT.EQ. 3) .AND. (NSLT.EQ. 3)) THEN
1 692      OPEN(6,FILE='PRN')
1 693      ELSEIF((IT.EQ. 3) .AND. (NSLT.NE. 3)) THEN
1 694      GOTO 756
1 695      ELSEIF((IT.EQ. 4) .AND. (NSLT.EQ. 4)) THEN
1 696      OPEN(6,FILE='PRN')
1 697      ENDDIF
1 698      IF(IT.EQ. 1) THEN
1 699      WRITE(6,804) NTBL
1 700      ELSE
1 701      WRITE(6,805)
1 702      ENDDIF
1 703      IF(IT.EQ. 1) THEN
1 704      WRITE(6,30) LL1
1 705      WRITE(6,30) LL2
1 706      WRITE(6,30) LL3
1 707      WRITE(6,30) LL4
1 708      ELSE
1 709      WRITE(6,810) LL1
1 710      WRITE(6,810) LL2
1 711      WRITE(6,810) LL3
1 712      WRITE(6,811) LL4
1 713      ENDDIF
1 714      IF(IT.EQ. 1) THEN
1 715      WRITE(6,947)
1 716      WRITE(6,951)
1 717      WRITE(6,976)
1 718      WRITE(6,1051)
1 719      ELSE
1 720      WRITE(6,946)
1 721      WRITE(6,950)
1 722      WRITE(6,975)
1 723      WRITE(6,1050)
1 724      ENDDIF
1 725 C
1 726      CUMDT(1) = 0.0
1 727      CSQMT(1) = 0.0
1 728      CGSQM(1) = 0.0

```

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D Line# 1      7
1 729          CUMDD(1) = 0.0
1 730 C
1 731          DO 750 I = 1,NOPTS
2 732 C
2 733 C          CALCULATE DOSAGE USING PPM/AB FROM MASS BALANCE FOR A
2 734 C          SINGLE SUBSTRATE (MILLIGRAM MINUTES PER CUBIC METER)
2 735 C
2 736          DOSGT = (((VCDT(1) + VCDT(I-1))/2.0) * TMINV/1000.0)
2 737          CUMDT(I) = CUMDT(I-1) + DOSGT
2 738 C
2 739 C          DOSAGE ANSWER PER SQUARE METER
2 740 C
2 741          CSQMT(I) = CUMDT(I)/.3387
2 742 C
2 743 C          DOSAGE ANSWER PER GRAM PER SQUARE METER
2 744 C
2 745          CGSQM(I) = CUMDT(I)/VGPT
2 746 C
2 747 C          DOSAGE ANSWER PER DROPLET
2 748 C
2 749          DOSGD = (((VCDD(1) + VCDD(I-1))/2.0) * TMINV/1000.0)
2 750          CUMDD(I) = CUMDD(I-1) + DOSGD
2 751 750      CONTINUE
1 752 C
1 753          DO 755 I = 1,NOPTS
2 754          A = CUMDT(I)
2 755          B = CSQMT(I)
2 756          C = CGSQM(I)
2 757          D = CUMDD(I)
2 758          TIM = TMEAC(I)
2 759          IF(IT .EQ. 1) THEN
2 760          WRITE(6,1061) TIM,A,B,C,D
2 761          ELSE
2 762          WRITE(6,1060) TIM,A,B,C,D
2 763          ENDIF
2 764 755      CONTINUE
1 765          TIMT = TMEAC(NOPTS)
1 766          CLOSE(6)
1 767          IF((IT .EQ. 1) .AND. (DISPLAY .EQ. 1)) PAUSE
1 768 756      CONTINUE
2 769 C
2 770 C          PRINTOUT CUMULATIVE DISTRIBUTION BASED ON PPM/AB CONVERSION FACTOR
2 771 C          OBTAINED FROM CALIBRATION OF MIRAN ANALYZER
2 772 C          //////////// TABLE 5 ////////////
2 773 C
2 774          NTBL=5
2 775          DO 771 IT=1,NSIT
1 776          IF(IT .EQ. 1) THEN
1 777          OPEN(6,FILE='CON')
1 778          ELSEIF((IT .EQ. 2) .AND. ((NSLT .EQ. 2) .OR. (NSLT .EQ. 3))) THEN
1 779          OPEN(6,FILE='TABLE.5',STATUS='NEW')
1 780          ELSEIF((IT .EQ. 2) .AND. ((NSLT .NE. 2) .OR. (NSLT .NE. 3))) THEN
1 781          GOTO 771
1 782          ELSEIF((IT .EQ. 3) .AND. (NSLT .EQ. 3)) THEN
1 783          OPEN(6,FILE='PRN')
1 784          ELSEIF((IT .EQ. 3) .AND. (NSLT .NE. 3)) THEN

```

```

D Line# 1      7
1 785      GOTO 771
1 786      ELSEIF((IT .EQ. 4) .AND. (NSLY .EQ. 4)) THEN
1 787      OPEN(4,FILE='PRN')
1 788      ENDIF
1 789      IF(IT .EQ. 1) THEN
1 790      WRITE(6,804) NISL
1 791      ELSE
1 792      WRITE(6,805)
1 793      ENDIF
1 794      IF(IT .EQ. 1) THEN
1 795      WRITE(6,30) LL1
1 796      WRITE(6,30) LL2
1 797      WRITE(6,30) LL3
1 798      WRITE(6,30) LL4
1 799      ELSE
1 800      WRITE(6,810) LL1
1 801      WRITE(6,810) LL2
1 802      WRITE(6,810) LL3
1 803      WRITE(6,811) LL4
1 804      ENDIF
1 805      IF(IT .EQ. 1) THEN
1 806      WRITE(6,947)
1 807      WRITE(6,956)
1 808      WRITE(6,976)
1 809      WRITE(6,1051)
1 810      ELSE
1 811      WRITE(6,946)
1 812      WRITE(6,955)
1 813      WRITE(6,975)
1 814      WRITE(6,1050)
1 815      ENDIF
1 816 C
1 817      CCUMT(1) = 0.0
1 818      XSQMT(1) = 0.0
1 819      XGSQM(1) = 0.0
1 820      CCUMD(1) = 0.0
1 821 C
1 822      DO 770 I = 2,NOPTS
2 823 C
2 824 C      CALCULATE DOASAGE USING PPM/AB FROM CALIBRATION OF MIRAN ANALYZER
2 825 C      (MILLIGRAM MINUTES PER CUBIC METER)
2 826 C
2 827      DOSXT = ((CCDT(I) + CCDT(I-1))/2.0) * TMINV/1000.0
2 828      CCUMT(I) = CCUMT(I-1) + DOSXT
2 829 C
2 830 C      DOASAGE ANSWER PER SQUARE METER OF CONTAMINATION
2 831 C
2 832      XSQMT(I) = CCUMT(I)/.3387
2 833 C
2 834 C      DOASAGE ANSWER PER GRAM PER SQUARE METER OF CONTAMINATION
2 835 C
2 836      XGSQM(I) = CCUMT(I)/VGPT
2 837 C
2 838 C      DOASAGE ANSWER PER DROPLET
2 839 C
2 840      DOSXD = ((CCDD(I) + CCDD(I-1))/2.0) * TMINV/1000.0

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0 Line# 1      7      Microsoft FORTRAN77 V3.31 August 1985
2 841      CCUMD(I) = CCUMD(I-1) + DOSXD
2 842 770 CONTINUE
1 843 C
1 844      DO 775 I = 1,NOPTS
2 845      A = CCUMT(I)
2 846      B = XSQMT(I)
2 847      C = XGSQM(I)
2 848      D = CCUMD(I)
2 849      TIM = TMEAC(I)
2 850      IF(IT .EQ. 1) THEN
2 851      WRITE(6,1061) TIM,A,B,C,D
2 852      ELSE
2 853      WRITE(6,1060) TIM,A,B,C,D
2 854      ENDIF
2 855 775 CONTINUE
1 856      CLOSE(6)
1 857      IF((IT .EQ. 1) .AND. (DISPLAY .EQ. 1)) PAUSE
1 858 771 CONTINUE
859 C
860 C      CALCULATE AND PRINTOUT DROPLET EVAPORATION HISTORY
861 C      CONVERT MASS OF DROPLET IN GRAMS TO MILLIGRAMS
862 C      //////////// TABLE 6 ////////////
863 C
864      NTBL=6
865      XMASD = CMAS * 1000.0
866      DO 772 IT=1,NSLT
1 867      IF(IT .EQ. 1) THEN
1 868      OPEN(6,FILE='CON')
1 869      ELSEIF((IT .EQ. 2) .AND. ((NSLT .EQ. 2) .OR. (NSLT .EQ. 3))) THEN
1 870      OPEN(6,FILE='TABLE.6',STATUS='NEW')
1 871      ELSEIF((IT .EQ. 2) .AND. ((NSLT .NE. 2) .OR. (NSLT .NE. 3))) THEN
1 872      GOTO 772
1 873      ELSEIF((IT .EQ. 3) .AND. (NSLT .EQ. 3)) THEN
1 874      OPEN(6,FILE='PRN')
1 875      ELSEIF((IT .EQ. 3) .AND. (NSLT .NE. 3)) THEN
1 876      GOTO 772
1 877      ELSEIF((IT .EQ. 4) .AND. (NSLT .EQ. 4)) THEN
1 878      OPEN(6,FILE='PRN')
1 879      ENDIF
1 880      IF(IT .EQ. 1) THEN
1 881      WRITE(6,804) NTBL
1 882      ELSE
1 883      WRITE(6,805)
1 884      ENDIF
1 885      IF(IT .EQ. 1) THEN
1 886      WRITE(6,30) LL1
1 887      WRITE(6,30) LL2
1 888      WRITE(6,30) LL3
1 889      WRITE(6,30) LL4
1 890      ELSE
1 891      WRITE(6,810) LL1
1 892      WRITE(6,810) LL2
1 893      WRITE(6,810) LL3
1 894      WRITE(6,811) LL4
1 895      ENDIF
1 896      IF(IT .EQ. 1) THEN

```

```

D Line# 1      7
1 897      WRITE(6,1111)
1 898      WRITE(6,1121)
1 899      WRITE(6,1141)
1 900      WRITE(6,1151)
1 901      ELSE
1 902      WRITE(6,1110)
1 903      WRITE(6,1120)
1 904      WRITE(6,1140)
1 905      WRITE(6,1150)
1 906      ENDIF
1 907      DO 785 I = 1,NOPTS
2 908 C
2 909      TIM = TMEAC(I)
2 910      AX = EVAPM(I)
2 911      ACDMG = (EVAPM(1) - EVAPM(I)) * 1000.0
2 912      ACDMF = EVAPM(1) - EVAPM(I)
2 913      BX = EVAPM(I) * 1000.0
2 914      CX = EVPMS(I) * 1000.0
2 915      DY = EVPNS(I)
2 916      FRT = TMEAC(I)/TIMT
2 917      FRHT(I) = TMEAC(I)/HAFTM
2 918      FHL = FRHT(I)
2 919 C
2 920      IF((VOLTN(NOPTS) .GE. .5) .AND. (IT .EQ. 1)) THEN
2 921      WRITE(6,1169) TIM,BX,AX,ACDMG,ACDMF,CX,DY,FRT,FHL
2 922      ELSEIF((VOLTN(NOPTS) .GE. .5) .AND. (IT .NE. 1)) THEN
2 923      WRITE(6,1170) TIM,BX,AX,ACDMG,ACDMF,CX,DY,FRT,FHL
2 924      ELSEIF((VOLTN(NOPTS) .LT. .5) .AND. (IT .EQ. 1)) THEN
2 925      WRITE(6,1172) TIM,BX,AX,ACDMG,ACDMF,CX,DY,FRT,DASH
2 926      ELSEIF((VOLTN(NOPTS) .LT. .5) .AND. (IT .NE. 1)) THEN
2 927      WRITE(6,1171) TIM,BX,AX,ACDMG,ACDMF,CX,DY,FRT,DASH
2 928      ENDIF
2 929 785 CONTINUE
1 930      CLOSE(6)
1 931      IF((IT .EQ. 1) .AND. (DISPLAY .EQ. 1)) PAUSE
1 932 772 CONTINUE
933 C
934 C      PRINTOUT EVAPORATION HISTORY OF DEPOSITED DROPLET
935 C      //////////// TABLE 7 ////////////
936 C
937      NTBL=7
938      DO 778 IT=1,NSLT
1 939      IF(IT .EQ. 1) THEN
1 940      OPEN(6,FILE='CON')
1 941      ELSEIF((IT .EQ. 2) .AND. ((NSLT .EQ. 2) .OR. (NSLT .EQ. 3))) THEN
1 942      OPEN(6,FILE='TABLE.7',STATUS='NEW')
1 943      ELSEIF((IT .EQ. 2) .AND. ((NSLT .NE. 2) .OR. (NSLT .NE. 3))) THEN
1 944      GOTO 778
1 945      ELSEIF((IT .EQ. 3) .AND. (NSLT .EQ. 3)) THEN
1 946      OPEN(6,FILE='PRN')
1 947      ELSEIF((IT .EQ. 3) .AND. (NSLT .NE. 3)) THEN
1 948      GOTO 778
1 949      ELSEIF((IT .EQ. 4) .AND. (NSLT .EQ. 4)) THEN
1 950      OPEN(6,FILE='PRN')
1 951      ENDIF
1 952      IF(IT .EQ. 1) THEN

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D Line# 1      7
1  953      WRITE(6,804) NTBL
1  954      ELSE
1  955      WRITE(6,805)
1  956      ENDIF
1  957      IF(IT .EQ. 1) THEN
1  958      WRITE(6,30) LL1
1  959      WRITE(6,30) LL2
1  960      WRITE(6,30) LL3
1  961      WRITE(6,30) LL4
1  962      ELSE
1  963      WRITE(6,810) LL1
1  964      WRITE(6,810) LL2
1  965      WRITE(6,810) LL3
1  966      WRITE(6,811) LL4
1  967      ENDIF
1  968      IF(IT .EQ.1) THEN
1  969      WRITE(6,1114)
1  970      WRITE(6,1126)
1  971      WRITE(6,1117)
1  972      ELSE
1  973      WRITE(6,1115)
1  974      WRITE(6,1125)
1  975      WRITE(6,1116)
1  976      ENDIF
1  977      DO 777 I = 1,NOPTS
2  978 C
2  979      TIM = TMEAC(I)
2  980      AX = EVAPN(I)
2  981      BX = EVAPN(I) * 1000.0
2  982      ACDMG = (EVAPN(I) - EVAPN(I)) * 1000.0
2  983      ACDMF = EVAPN(I) - EVAPN(I)
2  984      ACDMN = ACDMF/(1 - EVAPN(NOPTS))
2  985      FRT = TMEAC(I)/TIMT
2  986      FRHT(I) = TMEAC(I)/HAFTH
2  987      FHL = FRHT(I)
2  988 C
2  989      IF((VOLTN(NOPTS) .GE. .5) .AND. (IT .EQ. 1)) THEN
2  990      WRITE(6,1174) TIM,FRT,FHL,BX,AX,ACDMG,ACDMF,ACDMN
2  991      ELSEIF((VOLTN(NOPTS) .GE. .5) .AND. (IT .NE. 1)) THEN
2  992      WRITE(6,1175) TIM,FRT,FHL,BX,AX,ACDMG,ACDMF,ACDMN
2  993      ELSEIF((VOLTN(NOPTS) .LT. .5) .AND. (IT .EQ. 1)) THEN
2  994      WRITE(6,1177) TIM,FRT,DASH,BX,AX,ACDMG,ACDMF,ACDMN
2  995      ELSEIF((VOLTN(NOPTS) .LT. .5) .AND. (IT .NE. 1)) THEN
2  996      WRITE(6,1176) TIM,FRT,DASH,BX,AX,ACDMG,ACDMF,ACDMN
2  997      ENDIF
2  998 777 CONTINUE
1  999      IF(IT .EQ.1) THEN
1 1000      WRITE(6,1213)
1 1001      ELSE
1 1002      WRITE(6,1212)
1 1003      ENDIF
1 1004      CLOSE(6)
1 1005      IF((IT .EQ. 1) .AND. (DISPLAY .EQ. 1)) PAUSE
1 1006 778 CONTINUE
1007 C
1008 C

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D Line# 1      7      Microsoft FORTRAN77 V3.31 August 1985
1009 C      PRINTOUT DROPLET MASS INFORMATION FROM TRAY MASS LOADING
1010 C      AND NUMBER OF DROPLETS ON EACH SUBSTRATE
1011 C      //////////// TABLE B ////////////
1012 C
1013      NTBL=8
1014      DPPO = 0.0000
1015      DO 788 IT=1,NSLT
1016      IF(IT .EQ. 1) THEN
1017      OPEN(6,FILE='CON')
1018      ELSEIF((IT .EQ. 2) .AND. ((NSLT .EQ. 2) .OR. (NSLT .EQ. 3))) THEN
1019      OPEN(6,FILE='TABLE.8',STATUS='NEW')
1020      ELSEIF((IT .EQ. 2) .AND. ((NSLT .NE. 2) .OR. (NSLT .NE. 3))) THEN
1021      GOTO 788
1022      ELSEIF((IT .EQ. 3) .AND. (NSLT .EQ. 3)) THEN
1023      OPEN(6,FILE='PRN')
1024      ELSEIF((IT .EQ. 3) .AND. (NSLT .NE. 3)) THEN
1025      GOTO 788
1026      ELSEIF((IT .EQ. 4) .AND. (NSLT .EQ. 4)) THEN
1027      OPEN(6,FILE='PRN')
1028      ENDIF
1029      IF(IT .EQ. 1) THEN
1030      WRITE(6,804) NTBL
1031      ELSE
1032      WRITE(6,805)
1033      ENDIF
1034      IF(IT .EQ. 1) THEN
1035      WRITE(6,30) LL1
1036      WRITE(6,30) LL2
1037      WRITE(6,30) LL3
1038      WRITE(6,30) LL4
1039      ELSE
1040      WRITE(6,810) LL1
1041      WRITE(6,810) LL2
1042      WRITE(6,810) LL3
1043      WRITE(6,811) LL4
1044      ENDIF
1045      IF(IT .EQ. 1) THEN
1046      WRITE(6,821)
1047      WRITE(6,831)
1048      WRITE(6,841) GM1TP,GM2TP,GM3TP
1049      ELSE
1050      WRITE(6,820)
1051      WRITE(6,830)
1052      WRITE(6,840) GM1TP,GM2TP,GM3TP
1053      ENDIF
1054 C
1055      IF (NCODE .GE. 6) GOTO 786
1056 C
1057      IF(IT .EQ. 1) THEN
1058      WRITE(6,851) DPPO,DPPT,DPPT
1059      ELSE
1060      WRITE(6,850) DPPO,DPPT,DPPT
1061      ENDIF
1062 C
1063      IF (NCODE .LT. 6) GOTO 787
1064 C

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D Line# 1      7
1 1065 786 CONTINUE
1 1066      DPP3 = DPPT/2.0
1 1067      DPP2 = DPP3
1 1068      IF(IT .EQ. 1) THEN
1 1069      WRITE(6,851) DPPO,DPP2,DPP3
1 1070      ELSE
1 1071      WRITE(6,850) DPPO,DPP2,DPP3
1 1072      ENDIF
1 1073 C
1 1074 787 CONTINUE
1 1075      IF(IT .EQ. 1) THEN
1 1076      WRITE(6,861) GPM21,GPM22,GPM23
1 1077      WRITE(6,871) TM1,TM2,TM3
1 1078      WRITE(6,881) ETDPM
1 1079      WRITE(6,891) SDMAS
1 1080      WRITE(6,901) SEMAS
1 1081      WRITE(6,911) EQDPO
1 1082      ELSE
1 1083      WRITE(6,860) GPM21,GPM22,GPM23
1 1084      WRITE(6,870) TM1,TM2,TM3
1 1085      WRITE(6,880) ETDPM
1 1086      WRITE(6,890) SDMAS
1 1087      WRITE(6,900) SEMAS
1 1088      WRITE(6,910) EQDPO
1 1089      ENDIF
1 1090 C
1 1091 C      CALCUALTE MASS SAMPLED BY MIRAN ON SUBSTRATE BASIS
1 1092 C
1 1093      SMAS = CUMDT(NOPTS) * 7.5E-5
1 1094      XSMAS = CCUMT(NOPTS) * 7.5E-5
1 1095 C
1 1096 C      COMPARE WITH SUBSTRATE MASS ANS EXPRESS AS PERCENT
1 1097 C
1 1098      RMAS = (SMAS/(CHASS * DPPT)) * 100.0
1 1099      XRMAS = (XSMAS/(CHASS * DPPT)) * 100.0
1 1100 C
1 1101 C      CALCULATE THE DIFFERENCE BETWEEN MIRAN SAMPLED MASS FOR
1 1102 C      CALCUALTED AND CALIBRATED PPM/AB CONVERSION FACTOR
1 1103 C
1 1104      DIFMS = SMAS - XSMAS
1 1105      IF(IT .EQ. 1) THEN
1 1106      WRITE(6,1101) DIFMS
1 1107      WRITE(6,1081) CPMAB
1 1108      WRITE(6,1091) PRPAB
1 1109      WRITE(6,1071)
1 1110      WRITE(6,1073) RMAS
1 1111      WRITE(6,1075) XRMAS
1 1112      ELSE
1 1113      WRITE(6,1100) DIFMS
1 1114      WRITE(6,1080) CPMAB
1 1115      WRITE(6,1090) PRPAB
1 1116      WRITE(6,1070)
1 1117      WRITE(6,1072) RMAS
1 1118      WRITE(6,1074) XRMAS
1 1119      ENDIF
1 1120      CLOSE(6)

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D Line# 1      7      Microsoft FORTRAN77 V3.31 August 1985
1 1121      IF((IT.EQ. 1) .AND. (DISPLAY.EQ. 1)) PAUSE
1 1122 788    CONTINUE
1123 C
1124 C      FORMAT STATEMENTS FOR INPUT DATA
1125 C
1126 C
1127 C
1128 C      CALCULATE EVAPORATION RATE FOR SINGLE DROPLET
1129 C
1130      N = NOPTS - 1
1131 C
1132 C      ANSWER MICROGRAMS PER MINUTE
1133 C
1134      EVPRM(1) = (EVAPM(1) - CMASS)/TMINV
1135 C
1136 C      ANSWER FRACTIONAL AMOUNT PER MINUTE
1137 C
1138      EVPRN(1) = EVPRM(1) * CMASS/EVAPM(1)
1139      TIMER(1) = TMEAC(1)
1140      FRTM(1) = TIMER(1)/TIMT
1141 C
1142      DO 790 I = 2,NOPTS
1 1143 C
1 1144 C      ANSWER MICROGRAMS PER MINUTE
1 1145 C
1 1146      EVPRM(I) = (EVAPM(I) - EVAPM(I-1))/TMINV
1 1147 C
1 1148 C      ANSWER FRACTIONAL AMOUNT PER MINUTE
1 1149 C
1 1150      EVPRN(I) = EVPRM(I) * CMASS/EVAPM(I)
1 1151 C
1 1152      TIMER(I) = TMEAC(I)
1 1153      FRTM(I) = TIMER(I)/TIMT
1 1154 790    CONTINUE
1155 C
1156 C      EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY
1157 C      //////////// TABLE 9 ////////////
1158 C
1159      NTBL=9
1160      DO 796 IT=1,NSLT
1 1161      IF(IT.EQ. 1) THEN
1 1162      OPEN(6,FILE='CON')
1 1163      ELSEIF((IT.EQ. 2) .AND. ((NSLT.EQ. 1) .OR. (NSLT.EQ. 3))) THEN
1 1164      OPEN(6,FILE='TABLE.9',STATUS='NEW')
1 1165      ELSEIF((IT.EQ. 2) .AND. ((NSLT.NE. 2) .OR. (NSLT.NE. 3))) THEN
1 1166      GOTO 796
1 1167      ELSEIF((IT.EQ. 3) .AND. (NSLT.EQ. 3)) THEN
1 1168      OPEN(6,FILE='PRN')
1 1169      ELSEIF((IT.EQ. 3) .AND. (NSLT.NE. 3)) THEN
1 1170      GOTO 796
1 1171      ELSEIF((IT.EQ. 4) .AND. (NSLT.EQ. 4)) THEN
1 1172      OPEN(6,FILE='PRN')
1 1173      ENDIF
1 1174      IF(IT.EQ. 1) THEN
1 1175      WRITE(6,804) NTBL
1 1176      ELSE

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D Line# 1      7
1 1177      WRITE(6,805)
1 1178      ENDIF
1 1179      IF(IT .EQ. 1) THEN
1 1180      WRITE(6,30) LL1
1 1181      WRITE(6,30) LL2
1 1182      WRITE(6,30) LL3
1 1183      WRITE(6,30) LL4
1 1184      ELSE
1 1185      WRITE(6,810) LL1
1 1186      WRITE(6,810) LL2
1 1187      WRITE(6,810) LL3
1 1188      WRITE(6,811) LL4
1 1189      ENDIF
1 1190      IF(IT .EQ. 1) THEN
1 1191      WRITE(6,1181)
1 1192      WRITE(6,1191)
1 1193      WRITE(6,1201)
1 1194      ELSE
1 1195      WRITE(6,1180)
1 1196      WRITE(6,1190)
1 1197      WRITE(6,1200)
1 1198      ENDIF
1 1199 C
1 1200      SUMEV = 0.0
1 1201 C
1 1202      DO 795 I = 1,NOPTS
2 1203      TIM = TIMER(I)
2 1204      FRT = FRTM(I)
2 1205      FHL = FRHT(I)
2 1206      XX = EVPRN(I) * 1E6
2 1207      YY = EVPRM(I) * 1E6
2 1208      SUMEV = SUMEV + YY
2 1209 C
2 1210      IF((VOLTN(NOPTS) .GE. .5) .AND. (IT .EQ. 1)) THEN
2 1211      WRITE(6,1209) TIM,FRT,FHL,YY,XX
2 1212      ELSEIF((VOLTN(NOPTS) .GE. .5) .AND. (IT .NE. 1)) THEN
2 1213      WRITE(6,1210) TIM,FRT,FHL,YY,XX
2 1214      ELSEIF((VOLTN(NOPTS) .LT. .5) .AND. (IT .EQ. 1)) THEN
2 1215      WRITE(6,1214) TIM,FRT,DASH,YY,XX
2 1216      ELSEIF((VOLTN(NOPTS) .LT. .5) .AND. (IT .NE. 1)) THEN
2 1217      WRITE(6,1211) TIM,FRT,DASH,YY,XX
2 1218      ENDIF
2 1219 C
2 1220 795 CONTINUE
1 1221      IF(IT .EQ. 1) THEN
1 1222      WRITE(6,1213)
1 1223      ELSE
1 1224      WRITE(6,1212)
1 1225      ENDIF
1 1226      CLOSE(6)
1 1227 C
1 1228 C      EVAPORATION RATE AVERGED OVER DURATION OF TEST, MICROGRAMS/MIN
1 1229 C
1 1230      ERTMX =SUMEV/NOPTS
1 1231 C
1 1232      IF((IT .EQ. 1) .AND. (DISPLAY .EQ. 1)) PAUSE

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D Line# 1      7
1 1233 796 CONTINUE
1234 C
1235 C
1236 C      CHECK OF INPUT AND OUTPUT PARAMETER VALUES
1237 C      ////////// TABLE 10 //////////
1238 C
1239      NTBL=10
1240      DO 792 IT=1,NSLY
1 1241      IF(IT .EQ. 1) THEN
1 1242      OPEN(6,FILE='CON')
1 1243      ELSEIF((IT .EQ. 2) .AND. ((NSLT .EQ. 2) .OR. (NSLT .EQ. 3))) THEN
1 1244      OPEN(6,FILE='TABLE.10',STATUS='NEW')
1 1245      ELSEIF((IT .EQ. 2) .AND. ((NSLT .NE. 2) .OR. (NSLT .NE. 3))) THEN
1 1246      GOTO 792
1 1247      ELSEIF((IT .EQ. 3) .AND. (NSLT .EQ. 3)) THEN
1 1248      OPEN(6,FILE='PRN')
1 1249      ELSEIF((IT .EQ. 3) .AND. (NSLT .NE. 3)) THEN
1 1250      GOTO 792
1 1251      ELSEIF((IT .EQ. 4) .AND. (NSLT .EQ. 4)) THEN
1 1252      OPEN(6,FILE='PRN')
1 1253      ENDIF
1 1254      IF(IT .EQ. 1) THEN
1 1255      WRITE(6,804) NTBL
1 1256      ELSE
1 1257      WRITE(6,805)
1 1258      ENDIF
1 1259      IF(IT .EQ. 1) THEN
1 1260      WRITE(6,30) LL1
1 1261      WRITE(6,30) LL2
1 1262      WRITE(6,30) LL3
1 1263      WRITE(6,30) LL4
1 1264      ELSE
1 1265      WRITE(6,810) LL1
1 1266      WRITE(6,810) LL2
1 1267      WRITE(6,810) LL3
1 1268      WRITE(6,811) LL4
1 1269      ENDIF
1 1270      IF(IT .EQ. 1) THEN
1 1271      WRITE(6,1218)
1 1272      WRITE(6,1202) PRPAB
1 1273      WRITE(6,1204) COVLQ
1 1274      WRITE(6,1206) PERCP
1 1275      WRITE(6,1216) Z
1 1276      WRITE(6,1221) X
1 1277      WRITE(6,1231) Y
1 1278      WRITE(6,1237) DARTN
1 1279      WRITE(6,1241) TRAYH
1 1280      WRITE(6,1243) NCLOS
1 1281      WRITE(6,1245) CODEI
1 1282      WRITE(6,1247) TMASS
1 1283      WRITE(6,1249) CMASH
1 1284      WRITE(6,1251) CK
1 1285      WRITE(6,1253) GPMAN
1 1286      WRITE(6,1255) IVCEL
1 1287      WRITE(6,1257) CCVET
1 1288      WRITE(6,1259) ACVEN

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D Line# 1      7
1 1289      ELSE
1 1290      WRITE(6,1217)
1 1291      WRITE(6,1207) PRPAB
1 1292      WRITE(6,1203) COVLQ
1 1293      WRITE(6,1205) PERCP
1 1294      WRITE(6,1215) Z
1 1295      WRITE(6,1220) X
1 1296      WRITE(6,1230) Y
1 1297      WRITE(6,1236) DARTN
1 1298      WRITE(6,1240) TRAYM
1 1299      WRITE(6,1242) NCODE
1 1300      WRITE(6,1244) CODEL
1 1301      WRITE(6,1246) TMASS
1 1302      WRITE(6,1248) CMASS
1 1303      WRITE(6,1292) CK
1 1304      WRITE(6,1250) CPMAB
1 1305      WRITE(6,1260) TVCF3
1 1306      WRITE(6,1270) CCVR1
1 1307      WRITE(6,1280) ACVTM
1 1308      ENDIF
1 1309 C
1 1310      IF((VOLTN(NOPTS) .GE. .5) .AND. (IT .EQ. 1)) THEN
1 1311      WRITE(6,1289) HAFTM
1 1312      ELSEIF((VOLTN(NOPTS) .GE. .5) .AND. (IT .NE. 1)) THEN
1 1313      WRITE(6,1290) HAFTM
1 1314      ELSEIF((VOLTN(NOPTS) .LT. .5) .AND. (IT .EQ. 1)) THEN
1 1315      WRITE(6,1288) DASH
1 1316      ELSEIF((VOLTN(NOPTS) .LT. .5) .AND. (IT .NE. 1)) THEN
1 1317      WRITE(6,1291) DASH
1 1318      ENDIF
1 1319 C
1 1320      IF(IT .EQ. 1) THEN
1 1321      WRITE(6,1301) T2
1 1322      WRITE(6,1311) T1
1 1323      WRITE(6,1321) V2
1 1324      WRITE(6,1329) V1
1 1325      ELSE
1 1326      WRITE(6,1300) T2
1 1327      WRITE(6,1310) T1
1 1328      WRITE(6,1320) V2
1 1329      WRITE(6,1330) V1
1 1330      ENDIF
1 1331 C
1 1332      IF((VOLTN(NOPTS) .GE. .5) .AND. (IT .EQ. 1)) THEN
1 1333      WRITE(6,1328) ERHLF
1 1334      WRITE(6,1327) ERTMX
1 1335      ELSEIF((VOLTN(NOPTS) .GE. .5) .AND. (IT .NE. 1)) THEN
1 1336      WRITE(6,1331) ERHLF
1 1337      WRITE(6,1332) ERTMX
1 1338      ELSEIF((VOLTN(NOPTS) .LT. .5) .AND. (IT .EQ. 1)) THEN
1 1339      WRITE(6,1326) DASH
1 1340      WRITE(6,1336) DASH
1 1341      ELSEIF((VOLTN(NOPTS) .LT. .5) .AND. (IT .NE. 1)) THEN
1 1342      WRITE(6,1333) DASH
1 1343      WRITE(6,1335) DASH
1 1344      ENDIF

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D Line# 1      7
1 1345 C
1 1346 C      IF((VOLTN(NOPTS) .GE. .5) .AND. (IT .EQ. 1)) THEN
1 1347 C      WRITE(6,1327) ERTMX
1 1348 C      ELSEIF((VOLTN(NOPTS) .GE. .5) .AND. (IT .NE. 1)) THEN
1 1349 C      WRITE(6,1332) ERTMX
1 1350 C      ELSEIF((VOLTN(NOPTS) .LT. .5) .AND. (IT .EQ. 1)) THEN
1 1351 C      WRITE(6,1336) DASH
1 1352 C      ELSEIF((VOLTN(NOPTS) .LT. .5) .AND. (IT .NE. 1)) THEN
1 1353 C      WRITE(6,1335) DASH
1 1354 C      ENDIF
1 1355 C
1 1356 C      IF(IT .EQ. 1) THEN
1 1357 C      WRITE(6,1325) ENOV
1 1358 C      ELSE
1 1359 C      WRITE(6,1334) ENOV
1 1360 C      ENDIF
1 1361 C      CLOSE(6)
1 1362 C      IF((IT .EQ. 1) .AND. (DISPLAY .EQ. 1)) PAUSE
1 1363 792 CONTINUE
1364 C
1365 C      CALCULATE THE EFFECTIVE WINDSPEEDS TO ACHIEVE PPM/AB CALIBRATION
1366 C      VALUE PRPAB FROM TEST DATA
1367 C
1368 C      IF (WDTUN .LT. 5.0) GO TO 798
1369 C      FOR HIGH WIND SPEED TESTS
1370 C      AREAH = 10.5 * 4.0
1371 C      AREAL = 10.0 * 3.5
1372 C      GO TO 799
1373 C      FOR LOW WIND SPEED TESTS
1374 798 AREAH = 10.5 * 4.0
1375 AREAL = 10.0 * 3.5
1376 799 ARCR1 = DARTN/AREAH
1377 ARCR2 = DARTN/AREAL
1378 C
1379 C      ASSUME DYNAMIC CROSS-SECTIONAL AREA OF 10.25 BY 3.75 SQ INCHES
1380 C      WINDSPEED IN MPH
1381 C
1382 C      WMPH1 = (CPM/AB/PRPAB) * AIRSP
1383 C
1384 C      EQUIVALENT WINDSPEED IN FPM
1385 C
1386 C      WFPH1 = WMPH1 * 88.0 + .5
1387 C
1388 C      ASSUME DYNAMIC CROSS-SECTIONAL AREA OF 10.5 BY 4.0 SQ INCHES
1389 C      WINDSPEED IN MPH
1390 C
1391 C      WMPH2 = WMPH1 * ARCR1
1392 C
1393 C      EQUIVALENT WINDSPEED IN FPM
1394 C
1395 C      WFPH2 = WMPH2 * 88.0 + .5
1396 C
1397 C      ASSUME DYNAMIC CROSS-SECTIONAL AREA OF 10.0 BY 3.5 SQUARE INCHES
1398 C      WINDSPEED IN MPH
1399 C
1400 C      WMPH3 = WMPH1 * ARCR2

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C Line# 1      7      Microsoft FORTRAN77 V3.31 August 1985
1401 C
1402 C      EQUIVALENT WINDSPEED IN FPM
1403 C
1404 C      WFP3 = WMP3 * 88.0 + .5
1405 C
1406 C
1407 C      CALCULATE THE EFFECTIVE WINDSPEEDS TO ACHIEVE PPM/AB CALIBRATION
1408 C      VALUE = PRPAB + 3 SIGMA
1409 C      ASSUME DYNAMIC CROSS-SECTIONAL AREA OF 10.25 BY 3.75 SQ INCHES
1410 C
1411 C      AHPRA = PRPAB + 7.5
1412 C
1413 C      WINDSPEED IN MPH
1414 C
1415 C      SMPH1 = (WMPH1 * PRPAB)/AHPRA
1416 C
1417 C      EQUIVALENT WINDSPEED IN FPM
1418 C
1419 C      SFPM1 = SMPH1 * 88.0 + .5
1420 C
1421 C      ASSUME DYNAMIC CROSS-SECTIONAL AREA OF 10.5 BY 4.0
1422 C      WINDSPEED IN MPH
1423 C
1424 C      SMPH2 = SMPH1 * ARCR1
1425 C
1426 C      EQUIVALENT WINDSPEED IN FPM
1427 C
1428 C      SFPM2 = SMPH2 * 88.0 + .5
1429 C
1430 C      ASSUME DYNAMIC CROSS-SECTIONAL AREA OF 10.0 BY 3.5 SQ INCHES
1431 C      WINDSPEED IN MPH
1432 C
1433 C      SMPH3 = SMPH1 * ARCR2
1434 C
1435 C      EQUIVALENT WINDSPEED IN FPM
1436 C
1437 C      SFPM3 = SMPH3 * 88.0 + .5
1438 C
1439 C      CALCULATE THE EFFECTIVE WINDSPEEDS TO ACHIEVE PPM/AB CALIBRATION
1440 C      VALUE = PRPAB - 3 SIGMA
1441 C
1442 C      ALPRA = PRPAB - 7.5
1443 C
1444 C      ASSUME DYNAMIC CROSS-SECTIONAL AREA OF 10.25 BY 3.75 SQ INCHES
1445 C      WINDSPEED IN MPH
1446 C
1447 C      AMPH1 = (WMPH1 * PRPAB)/ALPRA
1448 C
1449 C      EQUIVALENT WINDSPEED IN FPM
1450 C
1451 C      AFPM1 = AMPH1 * 88.0 + .5
1452 C
1453 C      ASSUME DYNAMIC CROSS-SECTIONAL AREA OF 10.0 BY 4.0 SQ INCHES
1454 C      WINDSPEED IN MPH
1455 C
1456 C      AMPH2 = AMPH1 * ARCR1

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D Line# 1      7
1457 C
1458 C      EQUIVALENT WINDSPEED IN FPM
1459 C
1460 C      AFPM2 = AMPH2 * 88.0 + .5
1461 C
1462 C      ASSUME DYNAMIC CROSS-SECTIONAL AREA OF 10.0 BY 3.5 SQ INCHES
1463 C      WINDSPEED IN MPH
1464 C
1465 C      AMPH3 = AMPH1 * ARCR2
1466 C
1467 C      EQUIVALENT IN FPM
1468 C
1469 C      AFPM3 = AMPH3 * 88.0 + .5
1470 C
1471 C      EFFECTIVE WINDSPEEDS FOR TEST TO ACHIEVE PPM/AB OF MIRAN
1472 C      CALIBRATION FOR THE TEST DATA
1473 C      //////////// TABLE 11 ////////////
1474 C
1475 C      NTBL=11
1476 C      DO 793 IT=1,NSLT
1 1477 C      IF(IT .EQ. 1) THEN
1 1478 C      OPEN(6,FILE='CON')
1 1479 C      ELSEIF((IT .EQ. 2) .AND. ((NSLT .EQ. 2) .OR. (NSLT .EQ. 3))) THEN
1 1480 C      OPEN(6,FILE='TABLE.11',STATUS='NEW')
1 1481 C      ELSEIF((IT .EQ. 2) .AND. ((NSLT .NE. 2) .OR. (NSLT .NE. 3))) THEN
1 1482 C      GOTO 793
1 1483 C      ELSEIF((IT .EQ. 3) .AND. (NSLT .EQ. 3)) THEN
1 1484 C      OPEN(6,FILE='PRN')
1 1485 C      ELSEIF((IT .EQ. 3) .AND. (NSLT .NE. 3)) THEN
1 1486 C      GOTO 793
1 1487 C      ELSEIF((IT .EQ. 4) .AND. (NSLT .EQ. 4)) THEN
1 1488 C      OPEN(6,FILE='PRN')
1 1489 C      ENDIF
1 1490 C      IF(IT .EQ. 1) THEN
1 1491 C      WRITE(6,804) NTBL
1 1492 C      ELSE
1 1493 C      WRITE(6,805)
1 1494 C      ENDIF
1 1495 C      IF(IT .EQ. 1) THEN
1 1496 C      WRITE(6,30) LL1
1 1497 C      WRITE(6,30) LL2
1 1498 C      WRITE(6,30) LL3
1 1499 C      WRITE(6,30) LL4
1 1500 C      ELSE
1 1501 C      WRITE(6,810) LL1
1 1502 C      WRITE(6,810) LL2
1 1503 C      WRITE(6,810) LL3
1 1504 C      WRITE(6,811) LL4
1 1505 C      ENDIF
1 1506 C      IF(IT .EQ. 1) THEN
1 1507 C      WRITE(6,1401)
1 1508 C      WRITE(5,1411)
1 1509 C      ELSE
1 1510 C      WRITE(6,1400)
1 1511 C      WRITE(6,1410)
1 1512 C      ENDIF

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D Line# 1      7
1 1513 C
1 1514      IF(WTOTW .GT. 5.0) GO TO 7000
1 1515 C
1 1516      IF(IT .EQ. 1) THEN
1 1517      WRITE(6,1421)
1 1518      ELSE
1 1519      WRITE(6,1420)
1 1520      ENDIF
1 1521      GO TO 7050
1 1522 7000 CONTINUE
1 1523      IF(IT .EQ. 1) THEN
1 1524      WRITE(6,1426)
1 1525      ELSE
1 1526      WRITE(6,1425)
1 1527      ENDIF
1 1528 7050 CONTINUE
1 1529      IF(IT .EQ. 1) THEN
1 1530      WRITE(6,1431)
1 1531      WRITE(6,1441) ALPRA,AMPH2,AFPM2,AMPH1,AFPM1,AMPH3,AFPM3
1 1532      WRITE(6,1441) PRPAB,WMPH2,WFPM2,WMPH1,WFP1,WMPH3,WFPM3
1 1533      WRITE(6,1441) AHPRA,SMPH2,SFPM2,SMPH1,SFPM1,SMPH3,SFPM3
1 1534      ELSE
1 1535      WRITE(6,1430)
1 1536      WRITE(6,1440) ALPRA,AMPH2,AFPM2,AMPH1,AFPM1,AMPH3,AFPM3
1 1537      WRITE(6,1440) PRPAB,WMPH2,WFPM2,WMPH1,WFP1,WMPH3,WFPM3
1 1538      WRITE(6,1440) AHPRA,SMPH2,SFPM2,SMPH1,SFPM1,SMPH3,SFPM3
1 1539      ENDIF
1 1540      WRITE(6,2000)
1 1541      CLOSE(6)
1 1542      IF((IT .EQ. 1) .AND. (DISPLAY .EQ. 1)) PAUSE
1 1543 793 CONTINUE
1544 C
1545 C
1546
1547 C
1548 C      OPTION TO RUN THE PROGRAM AGAIN WITH ANOTHER DATA FILE
1549 C
1550 1550 ANSWER=' '
1551      WRITE(*,1500)
1552      WRITE(*,1530)
1553      WRITE(*,1540)
1554      READ(*,30) ANSWER
1555      IF((ANSWER .NE. 'Y') .AND. (ANSWER .NE. 'y') .AND. (ANSWER .NE. 'N
1556      &' ) .AND. (ANSWER .NE. 'n')) GOTO 1550
1557      IF((ANSWER .EQ. 'Y') .OR. (ANSWER .EQ. 'y')) GOTO 1
1558      IF((ANSWER .EQ. 'N') .OR. (ANSWER .EQ. 'n')) GOTO 9999
1559 C
1560 C      FORMAT STATEMENTS FOR PROGRAM
1561 C
1562 30  FORMAT(A)
1563 35  FORMAT(F7.2,F7.2,F7.2,F8.1,15,F8.1,F7.2,F8.2)
1564 40  FORMAT(F7.3,F7.1,15,F7.2)
1565 45  FORMAT(14)
1566 51  FORMAT(1H0,'INDEX MILLIVOLT  VOLT      INDEX MILLIVOLT  VOLT
1567      &  INDEX MILLIVOLT  VOLT')
1568 52  FORMAT(1H ,14,3X,14,3X,F8.4,7X,14,3X,14,2X,F8.4,7X,14,2X,14,2X,F8.

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D Line# 1      7      Microsoft FORTRAN77 V3 31 August 1985
1569      &4)
1570 53      FORMAT(/1X,'THIS IS THE MIRAN VOLTAGE DATA IN THE SELECTED FILE')
1571 55      FORMAT(1H,'DO YOU WISH TO CONTINUE WITH THE ANALYSIS USING THIS D
1572      &ATA?')
1573 57      FORMAT(1H0,'ANSWER Y FOR YES OR N FOR NO.....THEN PRESS ENTER')
1574 804     FORMAT(1H1//,37X,'TABLE',13/)
1575 805     FORMAT(1H1//,61X,'TABLE'//)
1576 810     FORMAT(28X,A)
1577 811     FORMAT(28X,A//)
1578 820     FORMAT(1H,37X,'SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSIT
1579      &ION')
1580 821     FORMAT(8X,'SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION')
1581 830     FORMAT(/49X,'SUBSTRATE 1',8X,'SUBSTRATE 2',8X,'SUBSTRATE 3'//)
1582 831     FORMAT(/29X,'SUBSTRATE 1',8X,'SUBSTRATE 2',8X,'SUBSTRATE 3'//)
1583 840     FORMAT(1H,25X,'CONTAMINATION, GRAMS',4X,F7.3,4X,F5.3,14X,F5.3,
1584 841     FORMAT(1H,25X,'CONTAMINATION, GRAMS',4X,F14.6,5X,F14.6,5X,F14.6)
1585 850     FORMAT(1H,25X,'NUMBER OF DROPLETS',5X,F8.3,11X,F8.3,11X,F8.3)
1586 851     FORMAT(1H,25X,'NUMBER OF DROPLETS',6X,F14.6,5X,F14.6,5X,F14.6)
1587 860     FORMAT(1H,25X,'GRAMS PER SQ METER',5X,F8.3,11X,F8.3,11X,F8.3)
1588 861     FORMAT(1H,25X,'GRAMS PER SQ METER',6X,F14.6,5X,F14.6,5X,F14.6)
1589 870     FORMAT(1H,25X,'GRAMS PER DROPLET',10X,F6.5,13X,F6.5,13X,F6.5//)
1590 871     FORMAT(1H,25X,'GRAMS PER DROPLET',7X,F14.6,5X,F14.6,5X,F14.6//)
1591 880     FORMAT(1H,25X,'ESTIMATED MEAN DROPLET MASS',12X,F8.5,'GRAMS')
1592 881     FORMAT(1H,25X,'ESTIMATED MEAN DROPLET MASS',12X,F8.5,'GRAMS')
1593 890     FORMAT(1H,25X,'STANDARD DEVIATION OF TEST DROPLET MASS',8.5,'G
1594      &RAMS')
1595 891     FORMAT(1H,25X,'STANDARD DEVIATION OF TEST DROPLET MASS',8.5,'G
1596      &RAMS')
1597 900     FORMAT(1H,25X,'STANDARD ERROR OF MEAN MASS ESTIMANT',3X,F8.5,'G
1598      &RAMS'//)
1599 901     FORMAT(1H,25X,'STANDARD ERROR OF MEAN MASS ESTIMANT',3X,F8.5,'G
1600      &RAMS'//)
1601 910     FORMAT(1H,26X,'EQUIVALENT DROPLET DIAMETER',11X,F6.2,'MILLIMETER
1602      &S'//)
1603 911     FORMAT(1H,26X,'EQUIVALENT DROPLET DIAMETER',12X,F6.2,'MILLIMETERS
1604      &S'//)
1605 918     FORMAT(1H,40X,'OUTPUT VOLTAGE DATA FROM MIRAN IA VAPOR ANALYZER'/
1606      &)
1607 919     FORMAT(1H0,16X,'OUTPUT VOLTAGE DATA FROM MIRAN IA VAPOR ANALYZER'/
1608      &)
1609 920     FORMAT(/30X,'MIRAN VAPOR ANALYZER',F6.2,2X,'ABSORBANCE UNITS PER V
1610      &OLT')
1611 921     FORMAT(6X,'MIRAN VAPOR ANALYZER',F6.2,2X,'ABSORBANCE UNITS PER VO
1612      &LT')
1613 922     FORMAT(31X,'ANALYZER',4X,'OUTPUT',12X,'CUMULATIVE DISTRIBUTION FOR
1614      & TWO SUBSTRATES')
1615 923     FORMAT(6X,'ANALYZER',5X,'OUTPUT',12X,'CUMULATIVE DISTRIBUTION F
1616      & TWO SUBSTRATES')
1617 930     FORMAT(1H,32X,'TIME',4X,'ABSORBANCE',10X,'ELAPSED TIME',6X,'TOTAL
1618      &,8X,'TOTAL')
1619 931     FORMAT(1H,32X,'TIME',4X,'ABSORBANCE',10X,'ELAPSED TIME',4X,'TOTAL
1620      &,8X,'TOTAL')
1621 935     FORMAT(1H,31X,'MINUTES',4X,'VOLTS',15X,'MINUTES',7X,'VOLT.MIN',5X
1622      &,'NORMALIZED'//)
1623 936     FORMAT(1H,31X,'MINUTES',4X,'VOLTS',15X,'MINUTES',5X,'VOLT.MIN',5X
1624      &,'NORMALIZED'//)

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D Line# 1      7      Microsoft FORTRAN77 V3.31 August 1985
1625 940 FORMAT(29X,F8.1,5X,F6.4,15X,F7.1,8X,F6.3,6X,F8.6)
1626 941 FORMAT(6X,F8.1,3X,F8.4,13X,F7.1,8X,F6.3,6X,F8.6)
1627 944 FORMAT(1H,6X,'VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSIT
1628      &ED DROPLETS')
1629 945 FORMAT(1H,37X,'VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSIT
1630      &ED DROPLETS')
1631 946 FORMAT(1H,29X,'CUMULATIVE DOSAGE DERIVED FROM UNIFORM ARRAY OF DE
1632      &POSITED DROPLETS')
1633 947 FORMAT(1H,2X,'CUMULATIVE DOSAGE DERIVED FROM UNIFORM ARRAY OF DEP
1634      &OSITED DROPLETS')
1635 950 FORMAT(1H,49X,'(PPM/AB BASED ON MASS BALANCE)')
1636 951 FORMAT(1H,17X,'(PPM/AB BASED ON MASS BALANCE)')
1637 955 FORMAT(1H,47X,'(PPM/AB BASED ON MIRAN CALIBRATION DATA)')
1638 956 FORMAT(1H,17X,'(PPM/AB BASED ON MIRAN CALIBRATION DATA)')
1639 970 FORMAT(27X,'ELAPSED',4X,'PPM',6X,'MICROGRAMS',8X,'*',13X,'*',10X,
1640      &'PPM',6X,'MICROGRAMS')
1641 971 FORMAT(1X,'ELAPSED',4X,'PPM',3X,'MICROGRAMS',6X,'*',12X,'*',8X,'PP
1642      &'M',6X,'MICROGRAMS')
1643 975 FORMAT(1H,28X,'TIME',3X,'***** MILLIGRAM.MINUTES PER CUBIC
1644      & METER *****')
1645 976 FORMAT(1H,4X,'TIME',3X,'***** MILLIGRAM.MINUTES PER CUBIC
1646      & METER *****')
1647 980 FORMAT(28X,'TIME',18X,'PER',11X,'PER',11X,'PER',22X,'PER')
1648 981 FORMAT(2X,'TIME',15X,'PER',9X,'PER',10X,'PER',19X,'PER')
1649 990 FORMAT(49X,'CUBIC',9X,'METER',10X,'GRAM/',10X,'PER',4X,'CUBIC METER
1650      &'R')
1651 991 FORMAT(20X,'CUBIC',7X,'METER',7X,'GRAM/',7X,'PER',5X,'CUBIC METER
1652      &')
1653 1000 FORMAT(27X,'MINUTES',15X,'METER',8X,'SQUARED',6X,'METER SQD',5X,'
1654      &DROP',6X,'PER DROP')
1655 1001 FORMAT(1X,'MINUTES',12X,'METER',6X,'SQUARED',4X,'METER SQD',3X,'
1656      &DROP',6X,'PER DROP')
1657 1030 FORMAT(1H,98X,'METER')
1658 1040 FORMAT(27X,F6.1,3X,F8.1,3X,F10.3,5X,F10.3,3X,F10.3,4X,F8.5,4X,
1659      &F8.3)
1660 1041 FORMAT(1X,F7.1,F7.3,F11.2,1X,F12.3,F10.3,3X,F10.6,F11.3)
1661 1050 FORMAT(1H,27X,'MINUTES',3X,'DOSAGE',4X,'PER SQUARE METER',2X,
1662      &'PER GRAM/SQ METER',6X,'PER DROPLET')
1663 1051 FORMAT(1H,3X,'MINUTES',3X,'DOSAGE',4X,'PER SQUARE METER',2X,
1664      &'PER GRAM/SQ METER',6X,'PER DROPLET')
1665 1060 FORMAT(27X,F6.1,3X,F8.3,8X,F10.3,8X,F9.5,11X,F9.5)
1666 1061 FORMAT(3X,F6.1,3X,F8.3,6X,F10.3,6X,F12.4,9X,F12.4)
1667 1070 FORMAT(1H,26X,'RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT
1668      & 75 LITER PER MINUTE TO TOTAL MASS')
1669 1071 FORMAT(1H,1X,'RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT
1670      & 75 L/MIN TO TOTAL MASS')
1671 1072 FORMAT(1H,26X,'BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) ',
1672      &F10.5,2X,'PERCENT')
1673 1073 FORMAT(1H,1X,'BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) ',
1674      &F10.5,2X,'PERCENT')
1675 1074 FORMAT(1H,26X,'BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) ',
1676      &F10.5,2X,'PERCENT')
1677 1075 FORMAT(1H,1X,'BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) ',
1678      &F10.5,2X,'PERCENT')
1679 1080 FORMAT(1H,26X,'FOR CONVERSION FACTOR PPM/AB * CALCULATION * ',
1680      &F8.3)

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1681 1081 FORMAT(1H,1X,'FOR CONVERSION FACTOR PPM/AB * CALCULATION * ',
1682      &F8.3/)
1683 1090 FORMAT(1H,26X,'FOR CONVERSION FACTOR PPM/AB * CALIBRATION * ',
1684      &F8.3/)
1685 1091 FORMAT(1H,1X,'FOR CONVERSION FACTOR PPM/AB * CALIBRATION * ',
1686      &F8.3/)
1687 1100 FORMAT(1H,26X,'DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES',F10.7,
1688      &2X,'GRAMS'/)
1689 1101 FORMAT(1H,1X,'DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES',F10.7,2X
1690      &,'GRAMS'/)
1691 1110 FORMAT(1H,32X,'EVAPORATION HISTORY OF TEST DROPLET MEASURED AND T
1692      &HEORETICAL'/)
1693 1111 FORMAT(1H0,6X,'EVAPORATION HISTORY OF TEST DROP MEASURED AND THEOR
1694      &ETICAL')
1695 1114 FORMAT(1H0,16X,'EVAPORATION HISTORY OF DEPOSITED TEST DROPLET')
1696 1115 FORMAT(1H,40X,'EVAPORATION HISTORY OF DEPOSITED TEST DROPLET')
1697 1116 FORMAT(1H,14X,'MINUTES',3X,'FRACTION',3X,'HALF-LIFES',5X,'MILLIGR
1698      &AMS',3X,'FRACTIONAL',5X,'MILLIGRAMS',3X,'FRACTIONAL'3X,
1699      &'NORMALIZED'/)
1700 1117 FORMAT(1H,1X,'MINUTES',4X,'FRACTION',2X,'HALF-LIFES',3X,'MG',5X
1701      &,'FRACTION',5X,'MG',3X,'FRACTION',2X,'NORMALIZED'/)
1702 1120 FORMAT(1H0,25X,'EXPERIMENTAL EVAPORATION DATA',18X,'THEORETICAL',
1703      &1X,'HALF LIFE MODEL DATA')
1704 1121 FORMAT(1H0,1X,'EXPERIMENTAL EVAPORATION DATA',15X,'THEORETICAL',
1705      &1X,'HALF LIFE MODEL DATA')
1706 1125 FORMAT(1H,14X,'***** TIME *****',5X,
1707      &'***** RESIDUAL MASS *****',5X,'***** CUMULATIVE MASS *****
1708      &')
1709 1126 FORMAT(1H,1X,'***** TIME *****',1X,'RESIDUAL MASS
1710      &'*****',5X,'CUMULATIVE MASS *****')
1711 1140 FORMAT(1H,9X,'TIME',9X,'RESIDUAL MASS',12X,'CUMULATIVE MASS',9X,
1712      &'MASS',9X,'MASS',8X,'TIME',8X,'TIME')
1713 1141 FORMAT(1H,3X,'TIME',2X,'RESIDUAL MASS',5X,'CUMULATIVE MASS',2X,
1714      &'RESIDUAL MASS',4X,'***** TIME *****')
1715 1150 FORMAT(1H,9X,'MINUTES',3X,'MILLIGRAMS',2X,'FRACTIONAL',2X,'MILLIG
1716      &RAMS',3X,'FRACTIONAL',3X,'MILLIGRAMS',3X,'FRACTIONAL',3X,'FRACTION
1717      &AL',3X,'HALF-LIFES'/)
1718 1151 FORMAT(1H,2X,'MIN',5X,'MG',5X,'FRACTION',3X,'MG',5X,'FRACTION',2X
1719      &,'MG',3X,'FRACTION',2X,'FRACTION',2X,'HALF-LIFES'/)
1720 1169 FORMAT(1X,F7.1,2X,F6.3,3X,F6.3,2X,F6.3,1X,F6.3,4X,F7.3,2X,F6.3,2X,
1721      &F6.3,4X,F6.3)
1722 1170 FORMAT(9X,F7.1,3X,F10.5,4X,F8.6,3X,F10.6,3X,F9.5,1X,F11.5,5X,
1723      &F8.6,4X,F6.4,5X,F9.5)
1724 1171 FORMAT(9X,F7.1,3X,F10.5,4X,F8.6,3X,F10.6,3X,F9.5,1X,F11.5,5X,
1725      &F8.6,4X,F6.4,10X,A)
1726 1172 FORMAT(1X,F7.1,2X,F6.3,3X,F6.3,2X,F6.3,1X,F6.3,4X,F7.3,2X,F6.3,2X,
1727      &F6.3,4X,A)
1728 1174 FORMAT(1X,F7.1,4X,F6.3,4X,F6.3,7X,F6.3,2X,F6.3,5X,F6.3,3X,F6.3,3X,
1729      &F6.3)
1730 1175 FORMAT(15X,F7.1,5X,F6.4,5X,F9.4,3X,F13.5,4X,F8.5,6X,F10.5,3X,F10.4
1731      &,3X,F10.4)
1732 1176 FORMAT(15X,F7.1,5X,F6.4,10X,A6,6X,F13.5,4X,F8.5,6X,F10.5,3X,F10.4,
1733      &3X,F10.4)
1734 1177 FORMAT(1X,F7.1,4X,F6.3,4X,A,12X,F6.3,2X,F6.3,5X,F6.3,3X,F6.3,3X,F6
1735      &.3)
1736 1180 FORMAT(1H,40X,'EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

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1737      &'/)
1738 1181 FORMAT(1H0,16X,'EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY
1739      &')
1740 1190 FORMAT(1H ,25X,'***** TIME *****',12X,' ***** EVA
1741      &PORATION RATE *****')
1742 1191 FORMAT(1H0,1X,'***** TIME *****',9X,' ***** EVAPO
1743      &RATION RATE *****')
1744 1200 FORMAT(26X,'MINUTES',3X,'FRACTIONAL',3X,'HALF-LIFES',5X,'MICROGRAM
1745      &S PER MINUTE',6X,'NORMALIZED')
1746 1201 FORMAT(2X,'MINUTES',3X,'FRACTIONAL',3X,'HALF-LIFES',10X,'MMG PER M
1747      &IN',6X,'NORMALIZED')
1748 1202 FORMAT(1H ,2X,'PRPAB = CONVERSION FACTOR, CALIBRATION PPM/AB',15X,
1749      &F12.5)
1750 1203 FORMAT(1H ,26X,'COVLQ = CONVERSION FACTOR, CALIBRATION MICROGRAMS/
1751      &PPM',7X,F14.5/)
1752 1204 FORMAT(1H ,2X,'COVLQ = CONVERSION FACTOR, CALIBRATION MICROGRAMS/P
1753      &PM',7X,F12.5)
1754 1205 FORMAT(1H ,26X,'PERCP = PERCENT COPOLYMER THICKENER IN LIQUID SIMU
1755      &LANT',6X,F14.5/)
1756 1206 FORMAT(1H ,2X,'PERCP = PERCENT COPOLYMER THICKENER IN LIQUID SIMUL
1757      &ANT',6X,F12.5)
1758 1207 FORMAT(1H ,26X,'PRPAB = CONVERSION FACTOR, CALIBRATION PP/AB',15X,
1759      &F14.5/)
1760 1209 FORMAT(1X,F7.1,5X,F6.3,6X,F6.3,14X,F9.3,8X,F9.3)
1761 1210 FORMAT(26X,F6.1,5X,F6.4,5X,F9.5,10X,F14.5,8X,F12.5)
1762 1211 FORMAT(26X,F6.1,5X,F6.4,8X,A6,10X,F14.5,8X,F12.5)
1763 1212 FORMAT(/26X,'NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQ
1764      &UID CONTAMINATION REMAINING.')
1765 1213 FORMAT(1H0,1X,'NORMALIZED: MMG PER MIN PER FRACTION OF LIQUID DROP
1766      &LET CONTAMINATION REMAINING')
1767 1214 FORMAT(2X,F6.1,5X,F6.3,8X,A,14X,F9.3,8X,F9.3)
1768 1215 FORMAT(1H ,26X,'Z = X*Y',53X,F14.5/)
1769 1216 FORMAT(1H ,2X,'Z = X*Y',53X,F12.5)
1770 1217 FORMAT(1H ,52X,'PARAMETERS')
1771 1218 FORMAT(1H0,28X,'PARAMETERS')
1772 1220 FORMAT(1H ,26X,'X = ACVTM*ABPV*COVLQ*1E-6',32X,F14.5/)
1773 1221 FORMAT(1H ,2X,'X = ACVTM*ABPV*COVLQ*1E-6',31X,F12.5)
1774 1230 FORMAT(1H ,26X,'Y = AIRSP*DARTN*.02832*88/144',28X,F14.5/)
1775 1231 FORMAT(1H ,2X,'Y = AIRSP*DARTN*.02832*88/144',27X,F12.5)
1776 1236 FORMAT(1H ,26X,'DARTN = ASSUMED DYNAMIC CROSS-SECTIONAL AREA OF TU
1777      &NNEL SQIN',1X,F14.5/)
1778 1237 FORMAT(1H ,2X,'DARTN = ASSUMED DYNAMIC CROSS-SECTIONAL AREA OF TUN
1779      &NEL SQIN',1X,F12.5)
1780 1240 FORMAT(1H ,26X,'TRAYM = TOTAL MASS ON TEST SUBSTRATES, GRAMS',16X,
1781      &F14.5/)
1782 1241 FORMAT(1H ,2X,'TRAYM = TOTAL MASS ON TEST SUBSTRATES, GRAHS',16X,F
1783      &12.5)
1784 1242 FORMAT(1H ,26X,'NCODE = TEST CONFIGURATION OF SUBSTRATES',23X,15/)
1785 1243 FORMAT(1H ,2X,'NCODE = TEST CONFIGURATION OF SUBSTRATES',21X,15)
1786 1244 FORMAT(1H ,26X,'CODEL = LIQUID SIMULANT CODE',32X,F14.5/)
1787 1245 FORMAT(1H ,2X,'CODEL = LIQUID SIMULANT CODE',32X,F12.5)
1788 1246 FORMAT(1H ,26X,'TMASS = TEST DROPLET MASS, GRAMS',28X,F14.5/)
1789 1247 FORMAT(1H ,2X,'TMASS = TEST DROPLET MASS, GRAMS',28X,F12.5)
1790 1248 FORMAT(1H ,26X,'CMASS = TEST DROPLET MASS CORRECTED FOR COPLOYMER,
1791      & GRAMS',4X,F14.5/)
1792 1249 FORMAT(1H ,2X,'CMASS = TEST DROPLET MASS CORRECTED FOR COPLOYMER,

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1793      &GRAMS',4X,F12.5)
1794 1250 FORMAT(1H ,26X,'CPMAB = CONVERSION FACTOR, MASS BALANCE PPM/AB',14
1795      &X,F14.5/)
1796 1251 FORMAT(1H ,2X,'CPMAB = CONVERSION FACTOR, MASS BALANCE PPM/AB',F1
1797      &2.5)
1798 1260 FORMAT(1H ,26X,'TVCF3 = CORRECTION FACTOR FOR NUMBER OF SUBSTRATES
1799      &',10X,F14.5/)
1800 1261 FORMAT(1H ,2X,'TVCF3 = CORRECTION FACTOR FOR NUMBER OF SUBSTRATES'
1801      &,10X,F12.5)
1802 1270 FORMAT(1H ,26X,'CCVR1 = ABPV*CPMAB*TVCF3, PPM/VOLT',26X,F14.5/)
1803 1271 FORMAT(1H ,2X,'CCVR1 = ABPV*CPMAB*TVCF3, PPM/VOLT',26X,F12.5)
1804 1280 FORMAT(1H ,26X,'ACVTM = TOTAL ACCUMULATIVE VOLT.MIN',25X,F14.5/)
1805 1281 FORMAT(1H ,2X,'ACVTM = TOTAL ACCUMULATIVE VOLT.MIN',25X,F12.5)
1806 1288 FORMAT(1H ,2X,'HAFTM = HALF-LIFE OF DROPLET, MINUTES',30X,A)
1807 1289 FORMAT(1H ,2X,'HAFTM = HALF-LIFE OF DROPLET, MINUTES',23X,F12.5)
1808 1290 FORMAT(1H ,26X,'HAFTM = HALF-LIFE OF DROPLET, MINUTES',23X,F14.5)
1809 1291 FORMAT(1H ,26X,'HAFTM = HALF-LIFE OF DROPLET, MINUTES',30X,A)
1810 1292 FORMAT(1H ,26X,'CK' = LN2/HAFTM, USED IN DEFINING TK',22X,F14.5/
1811      &)
1812 1293 FORMAT(1H ,2X,'CK' = LN2/HAFTM, USED IN DEFINING TK',22X,F12.5)
1813 1300 FORMAT(1H ,26X,'T2' = VALUE USED IN INTERPOLATION FOR HALF-LIFE
1814      &, MIN',5X,F14.5)
1815 1301 FORMAT(1H ,5X,'T2 = VALUE USED IN INTERPOLATION FOR HALF-LIFE, MIN
1816      &',6X,F12.5)
1817 1310 FORMAT(1H ,26X,'T' = VALUE USED IN INTERPOLATION FOR HALF-LIFE
1818      &, MIN',5X,F14.5)
1819 1311 FORMAT(1H ,5X,'T1 = VALUE USED IN INTERPOLATION FOR HALF-LIFE, MIN
1820      &',6X,F12.5)
1821 1320 FORMAT(1H ,26X,'V' = VALUE USED IN INTERPOLATION FOR HALF-LIFE'
1822      &,11X,F14.5)
1823 1321 FORMAT(1H ,5X,'V2 = VALUE USED IN INTERPOLATION FOR HALF-LIFE',11X
1824      &,F12.5)
1825 1325 FORMAT(1H ,2X,'ENDVT MONITORS WHETHER EVAPORATION IS COMPLETE (0.0
1826      &) OR NOT (1.0):',2X,F3.1)
1827 1326 FORMAT(1H ,2X,'ERHLF = EVAPORATION RATE AVERAGED OVER ONE-HALF-LIFE,
1828      &MMG/MIN',7X,A)
1829 1327 FORMAT(1H ,2X,'ERTMX = EVAPORATION RATE AVERAGED OVER DURATION OF
1830      &TEST:MMG/MIN',F9.5)
1831 1328 FORMAT(3X,'ERHLF = EVAPORATION RATE AVERAGED OVER ONE-HALF-LIFE,
1832      &MMG/MIN',F10.5)
1833 1329 FORMAT(1H ,5X,'V1 = VALUE USED IN INTERPOLATION FOR HALF-LIFE',11X
1834      &,F12.5)
1835 1330 FORMAT(1H ,26X,'V1' = VALUE USED IN INTERPOLATION FOR HALF-LIFE'
1836      &,11X,F14.5/)
1837 1331 FORMAT(1H ,26X,'ERHLF = EVAPORATION RATE AVERAGED OVER ONE-HALF-LI
1838      &FE, MMG/MIN',F13.5/)
1839 1332 FORMAT(1H ,26X,'ERTMX = EVAPORATION RATE AVERAGED OVER DURATION OF
1840      &TEST:MMG/MIN',F11.5/)
1841 1333 FORMAT(1H ,26X,'ERHLF = EVAPORATION RATE AVERAGED OVER ONE-HALF-
1842      &LIFE, MMG/MIN',9X,A/)
1843 1334 FORMAT(1H ,26X,'ENDVT=MONITORS WHETHER EVAPORATION IS COMPLETE (0.
1844      &0) OR NOT (1.0):',2X,F3.1)
1845 1335 FORMAT(1H ,26X,'ERTMX = EVAPORATION RATE AVERAGED OVER DURATION OF
1846      &TEST:MMG/MIN',6X,A/)
1847 1336 FORMAT(1H ,2X,'ERTMX = EVAPORATION RATE AVERAGED OVER DURATION OF
1848      &TEST MMG/MIN',6X,A)

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1849 1400 FORMAT(1H ,27X,'EFFECTIVE WINDSPEED FOR TEST TO ACHIEVE PPM/AB OF
1850      &CALIBRATION FOR TEST DATA'/)
1851 1401 FORMAT(1X,'EFFECTIVE WINDSPEED FOR TEST TO ACHIEVE PPM/AB OF CALIB
1852      &RATION FOR TEST DATA'/)
1853 1410 FORMAT(1H ,37X,'ASSUMED WINDSPEED FOR DYNAMIC CROSS-SECTIONAL AREA
1854      & SQ INCHES'/)
1855 1411 FORMAT(1H0,8X,'ASSUMED WINDSPEED FOR DYNAMIC CROSS SECTIONAL AREA
1856      &SQ INCHES')
1857 1420 FORMAT(1H ,28X,'PPM/AB',5X,'10.5 X 4.0 SQ IN',6X,'10.25 X 3.75 SQ
1858      & IN',6X,'10.0 X 3.5 SQ IN'/)
1859 1421 FORMAT(1H0,3X,'PPM/AB',5X,'10.5 X 4.0 SQ IN',6X,'10.25 X 3.75 SQ I
1860      &N',5X,'10.0 X 3.5 SQ IN')
1861 1425 FORMAT(1H ,28X,'PPM/AB',5X,'10.5 X 4.0 SQ IN',6X,'10.25 X 3.75 SQ
1862      & IN',6X,'10.0 X 3.5 SQ IN'/)
1863 1426 FORMAT(1H0,3X,'PPM/AB',5X,'10.5 X 4.0 SQ IN',6X,'10.25 X 3.75 SQ I
1864      &N',5X,'10.0 X 3.5 SQ IN')
1865 1430 FORMAT(1H ,30X,'+/-',8X,'MPH',7X,'FPM',9X,'MPH',9X,'FPM',10X,'MPH'
1866      &,7X,'FPM'/)
1867 1431 FORMAT(1H0,4X,'+/-',9X,'MPH',6X,'FPM',9X,'MPH',8X,'FPM',9X,'MPH',8
1868      &X,'FPM')
1869 1440 FORMAT(1H ,28X,F6.1,3X,F8.2,F10.0,4X,F8.2,4X,F8.0,5X,F8.2,F10.0/)
1870 1441 FORMAT(1H0,2X,F6.1,4X,F8.2,1X,F8.0,4X,F8.2,3X,F8.0,4X,F8.2,F11.0)
1871 1500 FORMAT(1H1,/////////////////)
1872 1510 FORMAT(1H1,////,3X,'THE DATA FILE TO BE READ MUST BE IN DRIVE B')
1873 1515 FORMAT(1H ,2X,'DATA FILES HAVE ASSIGNED NAMES SUCH AS - GLF1.DAT')
1874 1520 FORMAT(1H ,2X,'INPUT - NAME OF DATA FILE TO READ'/)
1875 1521 FORMAT(1H0,'***** TABLE PRINT OPTIONS *****')
1876      &*****')
1877 1522 FORMAT(1H ,3X,'FOUR OPTIONS ARE AVAILABLE FOR VIEWING OR PRINTING
1878      &THE TABLES')
1879 1523 FORMAT(1H ,10X,'PRINT TABLES ON SCREEN, ONLY              -OPTION
1880      & -1?')
1881 1524 FORMAT(1H ,10X,'PRINT TABLES ON SCREEN & IN A FILE        -OPTION
1882      & -2?')
1883 1525 FORMAT(1H ,10X,'PRINT TABLES ON SCREEN, IN FILE & PRINTER -OPTION
1884      & -3?')
1885 1526 FORMAT(1H ,10X,'PRINT TABLES ON SCREEN & ON THE PRINTER  -OPTION
1886      & -4?')
1887 1529 FORMAT(11)
1888 1530 FORMAT(1H0,20X,'DO YOU WISH TO RUN THE PROGRAM AGAIN?')
1889 1531 FORMAT(1H0,'PAUSE AFTER DISPLAYING EACH TABLE ON THE SCREEN?')
1890 1532 FORMAT(1H ,'FOR A PAUSE              ENTER OPTION - 1 -')
1891 1533 FORMAT(1H ,'FOR CONTINUOUS DISPLAY ENTER OPTION - 2 -')
1892 1540 FORMAT(1H0,13X,'ANSWER Y FOR YES OR N FOR NO...THEN PRESS ENTER')
1893 1548 FORMAT(1H ,F10.2)
1894 1888 FORMAT(/27X,'* MICROGRAMS PER CUBIC METER')
1895 1889 FORMAT(1H0,3X,'* MICROGRAMS PER CUBIC METER')
1896 2000 FORMAT(1H1)
1897 9900 FORMAT(1H1,'DATA ERROR IN INPUT')
1898 C
1899 9000 WRITE(*,9900)
1900      STOP
1901 9999 CONTINUE
1902      END

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D Line# 1 7

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| Name   | Type   | Offset | P Class   |
|--------|--------|--------|-----------|
| A      | REAL   | 5506   |           |
| ABPV   | REAL   | 5204   |           |
| ACDMF  | REAL   | 5594   |           |
| ACDMG  | REAL   | 5590   |           |
| ACDMN  | REAL   | 5626   |           |
| ACVTM  | REAL   | 5374   |           |
| AFPM1  | REAL   | 5774   |           |
| AFPM2  | REAL   | 5782   |           |
| AFPM3  | REAL   | 5790   |           |
| AHPRA  | REAL   | 5738   |           |
| AIRSP  | REAL   | 5196   |           |
| ALOG   |        |        |           |
| ALPRA  | REAL   | 5766   | INTRINSIC |
| AMPH1  | REAL   | 5770   |           |
| AMPH2  | REAL   | 5778   |           |
| AMPH3  | REAL   | 5786   |           |
| ANSWER | CHAR*1 | 5236   |           |
| ARCR1  | REAL   | 5706   |           |
| ARCR2  | REAL   | 5710   |           |
| AREAH  | REAL   | 5698   |           |
| AREAL  | REAL   | 5702   |           |
| AX     | REAL   | 5586   |           |
| B      | REAL   | 5510   |           |
| BX     | REAL   | 5598   |           |
| C      | REAL   | 5514   |           |
| CAL    | REAL   | 5200   |           |
| CCDD   | REAL   | 4700   |           |
| CCDT   | REAL   | 3900   |           |
| CCUMD  | REAL   | 4540   |           |
| CCUMT  | REAL   | 4220   |           |
| CCVR1  | REAL   | 5486   |           |
| CGSQM  | REAL   | 4380   |           |
| CK     | REAL   | 5422   |           |
| CMASS  | REAL   | 5362   |           |
| CODEL  | REAL   | 5192   |           |
| COVL1  | REAL   | 5278   |           |
| COVL2  | REAL   | 5282   |           |
| COVLQ  | REAL   | 5294   |           |
| CPD1H  | REAL   | 5266   |           |
| CPD1L  | REAL   | 5262   |           |
| CPM2H  | REAL   | 5274   |           |
| CPM2L  | REAL   | 5270   |           |
| CPMAB  | REAL   | 5482   |           |
| CPMD   | REAL   | 4060   |           |
| CPMT   | REAL   | 3260   |           |
| CSQMT  | REAL   | 3740   |           |
| CUMDD  | REAL   | 3580   |           |
| CUMDT  | REAL   | 3420   |           |
| CV     | REAL   | 5458   |           |
| CX     | REAL   | 5602   |           |
| D      | REAL   | 5518   |           |
| DARTH  | REAL   | 5470   |           |
| DASH   | CHAR*1 | 4860   |           |

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D Line# 1      7
DENL1 REAL      5254
DENL2 REAL      5258
DENLQ REAL      5290
DIFMS REAL      5362
DISPLA INTEGER*4 4880
DOSGD REAL      5542
DOSGT REAL      5538
DOSXD REAL      5566
DOSXT REAL      5562
DPP2 REAL      5642
DPP3 REAL      5638
DPPO REAL      5630
DPPT REAL      5184
DY REAL      5606
ENDV REAL      5220
ENDVT REAL      5216
EODPD REAL      5330
ERHLF REAL      5414
ERTMX REAL      5690
ETDPM REAL      5318
EVAPM REAL      3100
EVAPN REAL      2300
EVPMS REAL      2940
EVPNS REAL      2460
EVPRM REAL      2780
EVPRN REAL      2620
EXP
EXPGM REAL      5354
FHL REAL      5614
FNAME CHAR*14    4861
FRHT REAL      1980
FRT REAL      5610
FRTH REAL      2140
GM1TP REAL      5172
GM2TP REAL      5176
GM3TP REAL      5180
GPM21 REAL      5238
GPM22 REAL      5242
GPM23 REAL      5246
GPM24 REAL      5250
HAFTM REAL      5410
HAFV7 REAL      5390
HTBL INTEGER*4    *****
I INTEGER*4      5224
IT INTEGER*4      5438
IVOL INTEGER*4    1800
LL1 CHAR*72      4884
LL2 CHAR*72      4956
LL3 CHAR*72      5028
LL4 CHAR*72      5100
N INTEGER*4      5382
NCODE INTEGER*4    5188
NOPTS INTEGER*4    5212
NQ INTEGER*4      *****
NSET INTEGER*4    5350
NOIT INTEGER*4    4876

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INTRINSIC

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D Line# 1      7
NTBL  INTEGER*4  5434
NTRAY INTEGER*4  5342
PERCP  REAL      5286
PRPAB  REAL      5298
RMA5   REAL      5654
SDMAS  REAL      5322
SEMAS  REAL      5326
SFPM1  REAL      5746
SFPM2  REAL      5754
SFPH3  REAL      5762
SMAS   REAL      5646
SMPH1  REAL      5742
SMPH2  REAL      5750
SMPH3  REAL      5758
SUMEV  REAL      5674
SUMVS  REAL      1480
T1     REAL      5398
T2     REAL      5394
TIM    REAL      5450
TIMER  REAL      1640
TIMT   REAL      5550
TK     REAL      5430
TM1    REAL      5302
TM2    REAL      5306
TM3    REAL      5310
TMASS  REAL      5358
TMEAC  REAL      1000
TMINV  REAL      5208
TRAYM  REAL      5346
TTMT   REAL      5314
TVCF3  REAL      5334
V       REAL      5454
V1     REAL      5406
V2     REAL      5402
VCDD   REAL      1320
VCDT   REAL      1160
VCPGM  REAL      5502
VCPMS  REAL      5498
VGPT   REAL      5338
VN     REAL      5462
VOLT   REAL      20
VOLT1  REAL      5366
VOLT2  REAL      840
VPPMD  REAL      5750
VPPMT  REAL      5700
WDTUN  REAL      5474
WFFM1  REAL      5718
WFFM2  REAL      5726
WFFM3  REAL      5734
WMPH1  REAL      5714
WMPH2  REAL      5722
WMPH3  REAL      5730
X       REAL      5466
XGSOM  REAL      520
XMASD  REAL      5574
XRMA5  REAL      5658

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|           |      |      |
|-----------|------|------|
| D Line# 1 | 7    |      |
| XSMAS     | REAL | 5650 |
| XSQMT     | REAL | 360  |
| XX        | REAL | 5682 |
| Y         | REAL | 5378 |
| YY        | REAL | 5686 |
| Z         | REAL | 5478 |

| Name  | Type | Size | Class   |
|-------|------|------|---------|
| MIRAN |      |      | PROGRAM |

Pass One    No Errors Detected  
            1902 Source Lines

Blank



APPENDIX B

OUTPUT VOLTAGE DATA FROM A MIRAN 1A VAPOR ANALYZER

TABLE B-1

EVAPORATION EXPERIMENT NO. GLE1 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 3G GMS/SQ METER ON HICKORY/TOP SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 45%

## OUTPUT VOLTAGE DATA FROM MIRAN 1A VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES |                   |                     |
|-----------------------------|-------------------------------|--|-------------------|---------------------|
|                             |                               | ELAPSED TIME<br>MINUTES                    | TOTAL<br>VOLT-MIN | TOTAL<br>NORMALIZED |
| .0                          | .1289                         | .0   | .000              | .000000             |
| 30.0                        | .1160                         | 30.0                                       | 3.660             | .086574             |
| 60.0                        | .1040                         | 60.0                                       | 6.915             | .163568             |
| 90.0                        | .0920                         | 90.0                                       | 9.810             | .232047             |
| 120.0                       | .0840                         | 120.0                                      | 12.450            | .294493             |
| 150.0                       | .0770                         | 150.0                                      | 14.865            | .351618             |
| 180.0                       | .0680                         | 180.0                                      | 17.040            | .403066             |
| 210.0                       | .0630                         | 210.0                                      | 19.005            | .449546             |
| 240.0                       | .0570                         | 240.0                                      | 20.805            | .492123             |
| 270.0                       | .0519                         | 270.0                                      | 22.425            | .530443             |
| 300.0                       | .0460                         | 300.0                                      | 23.880            | .564859             |
| 330.0                       | .0410                         | 330.0                                      | 25.185            | .595728             |
| 360.0                       | .0360                         | 360.0                                      | 26.340            | .623049             |
| 390.0                       | .0320                         | 390.0                                      | 27.360            | .647176             |
| 420.0                       | .0280                         | 420.0                                      | 28.260            | .668464             |
| 450.0                       | .0230                         | 450.0                                      | 29.025            | .686560             |
| 480.0                       | .0190                         | 480.0                                      | 29.655            | .701462             |
| 510.0                       | .0150                         | 510.0                                      | 30.165            | .713525             |
| 540.0                       | .0120                         | 540.0                                      | 30.570            | .723105             |
| 570.0                       | .0100                         | 570.0                                      | 30.900            | .730911             |
| 600.0                       | .0080                         | 600.0                                      | 31.170            | .737298             |
| 630.0                       | .0060                         | 630.0                                      | 31.380            | .742265             |
| 660.0                       | .0050                         | 660.0                                      | 31.545            | .746168             |
| 690.0                       | .0040                         | 690.0                                      | 31.680            | .749361             |
| 720.0                       | .0030                         | 720.0                                      | 31.785            | .751845             |
| 750.0                       | .0020                         | 750.0                                      | 31.860            | .753619             |
| 780.0                       | .0020                         | 780.0                                      | 31.920            | .755038             |
| 810.0                       | .0010                         | 810.0                                      | 31.965            | .756103             |
| 840.0                       | .0010                         | 840.0                                      | 31.995            | .756812             |
| 870.0                       | .0000                         | 870.0                                      | 32.010            | .757167             |

MIRAN VAPOR ANALYZER .25 ABSORBANCE UNITS PER VOLT

TABLE B-2

EVAPORATION EXPERIMENT NO. GUE2 SERIES ID 244 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/TOP SURFACE  
 WIND SPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 39%

## OUTPUT VOLTAGE DATA FROM MIRAN 1A VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES |                   |                     |
|-----------------------------|-------------------------------|--|-------------------|---------------------|
|                             |                               | ELAPSED TIME<br>MINUTES                    | TOTAL<br>VOLT.MIN | TOTAL<br>NORMALIZED |
| 0.0                         | .1130                         | 0.0  | .000              | .000000             |
| 30.0                        | .1050                         | 30.0                                       | 3.270             | .074235             |
| 60.0                        | .0970                         | 60.0                                       | 6.300             | .143022             |
| 90.0                        | .0900                         | 90.0                                       | 9.105             | .205701             |
| 120.0                       | .0840                         | 120.0                                      | 11.715            | .265953             |
| 150.0                       | .0790                         | 150.0                                      | 14.160            | .321460             |
| 180.0                       | .0730                         | 180.0                                      | 16.440            | .373220             |
| 210.0                       | .0680                         | 210.0                                      | 18.555            | .421235             |
| 240.0                       | .0640                         | 240.0                                      | 20.535            | .466185             |
| 270.0                       | .0590                         | 270.0                                      | 22.380            | .508070             |
| 300.0                       | .0540                         | 300.0                                      | 24.075            | .546550             |
| 330.0                       | .0500                         | 330.0                                      | 25.635            | .581965             |
| 360.0                       | .0460                         | 360.0                                      | 27.075            | .614655             |
| 390.0                       | .0420                         | 390.0                                      | 28.395            | .644622             |
| 420.0                       | .0380                         | 420.0                                      | 29.595            | .671864             |
| 450.0                       | .0340                         | 450.0                                      | 30.675            | .696382             |
| 480.0                       | .0300                         | 480.0                                      | 31.635            | .718176             |
| 510.0                       | .0260                         | 510.0                                      | 32.475            | .737246             |
| 540.0                       | .0220                         | 540.0                                      | 33.195            | .753591             |
| 570.0                       | .0190                         | 570.0                                      | 33.810            | .767553             |
| 600.0                       | .0160                         | 600.0                                      | 34.335            | .779472             |
| 630.0                       | .0130                         | 630.0                                      | 34.770            | .789347             |
| 660.0                       | .0110                         | 660.0                                      | 35.130            | .797520             |
| 690.0                       | .0100                         | 690.0                                      | 35.445            | .804671             |
| 720.0                       | .0080                         | 720.0                                      | 35.715            | .810800             |
| 750.0                       | .0070                         | 750.0                                      | 35.940            | .815903             |
| 780.0                       | .0070                         | 780.0                                      | 36.150            | .820676             |
| 810.0                       | .0060                         | 810.0                                      | 36.345            | .825103             |
| 840.0                       | .0050                         | 840.0                                      | 36.510            | .828848             |
| 870.0                       | .0040                         | 870.0                                      | 36.645            | .831913             |
| 900.0                       | .0030                         | 900.0                                      | 36.750            | .834297             |
| 930.0                       | .0020                         | 930.0                                      | 36.825            | .836000             |
| 960.0                       | .0010                         | 960.0                                      | 36.870            | .837021             |
| 990.0                       | .0010                         | 990.0                                      | 36.900            | .837702             |
| 1020.0                      | .0000                         | 1020.0                                     | 36.915            | .838043             |

MIRAN VAPOR ANALYZER .025 ABSORBANCE UNITS PER VOLT

TABLE B-3

EVAPORATION EXPERIMENT NO. 613 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 40%

## OUTPUT VOLTAGE DATA FROM MIRAN IA VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES |                   |                     |
|-----------------------------|-------------------------------|--|-------------------|---------------------|
|                             |                               | ELAPSED TIME<br>MINUTES                    | TOTAL<br>VOLT.MIN | TOTAL<br>NORMALIZED |
| .0                          | .0860                         | .0   | .000              | .000000             |
| 15.0                        | .0750                         | 15.0                                       | 1.208             | .117196             |
| 30.0                        | .0660                         | 30.0                                       | 2.265             | .219834             |
| 45.0                        | .0590                         | 45.0                                       | 3.203             | .310825             |
| 60.0                        | .0520                         | 60.0                                       | 4.035             | .391624             |
| 75.0                        | .0460                         | 75.0                                       | 4.770             | .462961             |
| 90.0                        | .0410                         | 90.0                                       | 5.423             | .526291             |
| 105.0                       | .0360                         | 105.0                                      | 6.000             | .582341             |
| 120.0                       | .0310                         | 120.0                                      | 6.503             | .631112             |
| 135.0                       | .0260                         | 135.0                                      | 6.930             | .672604             |
| 150.0                       | .0210                         | 150.0                                      | 7.283             | .706816             |
| 165.0                       | .0180                         | 165.0                                      | 7.575             | .735206             |
| 180.0                       | .0150                         | 180.0                                      | 7.823             | .759227             |
| 195.0                       | .0120                         | 195.0                                      | 8.025             | .778881             |
| 210.0                       | .0090                         | 210.0                                      | 8.183             | .794168             |
| 225.0                       | .0070                         | 225.0                                      | 8.303             | .805814             |
| 240.0                       | .0050                         | 240.0                                      | 8.393             | .814550             |
| 255.0                       | .0040                         | 255.0                                      | 8.460             | .821101             |
| 270.0                       | .0040                         | 270.0                                      | 8.520             | .826524             |
| 285.0                       | .0030                         | 285.0                                      | 8.573             | .832020             |
| 300.0                       | .0030                         | 300.0                                      | 8.618             | .836387             |
| 315.0                       | .0020                         | 315.0                                      | 8.655             | .840027             |
| 330.0                       | .0010                         | 330.0                                      | 8.678             | .842211             |
| 345.0                       | .0010                         | 345.0                                      | 8.693             | .843667             |
| 360.0                       | .0000                         | 360.0                                      | 8.700             | .844395             |

MIRAN VAPOR ANALYZER .25 ABSORBANCE UNITS PER VOLT

TABLE B-4

EVAPORATION EXPERIMENT NO. GLF4 SERIES 10 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

## OUTPUT VOLTAGE DATA FROM MIRAN 1A VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES |                   |                     |
|-----------------------------|-------------------------------|--|-------------------|---------------------|
|                             |                               | ELAPSED TIME<br>MINUTES                    | TOTAL<br>VOLT-MIN | TOTAL<br>NORMALIZED |
| 0.0                         | .0730                         | 0.0  | .000              | .000000             |
| 10.0                        | .0720                         | 10.0                                       | .725              | .060349             |
| 20.0                        | .0710                         | 20.0                                       | 1.440             | .119866             |
| 30.0                        | .0680                         | 30.0                                       | 2.35              | .177718             |
| 40.0                        | .0640                         | 40.0                                       | 2.795             | .232657             |
| 50.0                        | .0600                         | 50.0                                       | 3.415             | .284266             |
| 60.0                        | .0580                         | 60.0                                       | 4.005             | .333378             |
| 70.0                        | .0550                         | 70.0                                       | 4.570             | .380409             |
| 80.0                        | .0520                         | 80.0                                       | 5.105             | .424943             |
| 90.0                        | .0490                         | 90.0                                       | 5.610             | .466979             |
| 100.0                       | .0470                         | 100.0                                      | 6.090             | .506935             |
| 110.0                       | .0440                         | 110.0                                      | 6.545             | .544809             |
| 120.0                       | .0410                         | 120.0                                      | 6.970             | .580186             |
| 130.0                       | .0390                         | 130.0                                      | 7.370             | .613483             |
| 140.0                       | .0370                         | 140.0                                      | 7.750             | .645114             |
| 150.0                       | .0340                         | 150.0                                      | 8.105             | .674664             |
| 160.0                       | .0320                         | 160.0                                      | 8.435             | .702134             |
| 170.0                       | .0300                         | 170.0                                      | 8.745             | .727938             |
| 180.0                       | .0280                         | 180.0                                      | 9.035             | .752078             |
| 190.0                       | .0260                         | 190.0                                      | 9.305             | .774553             |
| 200.0                       | .0240                         | 200.0                                      | 9.555             | .795363             |
| 210.0                       | .0220                         | 210.0                                      | 9.785             | .814508             |
| 220.0                       | .0200                         | 220.0                                      | 9.995             | .831989             |
| 230.0                       | .0180                         | 230.0                                      | 10.185            | .847805             |
| 240.0                       | .0160                         | 240.0                                      | 10.355            | .861955             |
| 250.0                       | .0140                         | 250.0                                      | 10.505            | .874442             |
| 260.0                       | .0130                         | 260.0                                      | 10.640            | .885679             |
| 270.0                       | .0110                         | 270.0                                      | 10.760            | .895668             |
| 280.0                       | .0090                         | 280.0                                      | 10.860            | .903992             |
| 290.0                       | .0080                         | 290.0                                      | 10.945            | .911067             |
| 300.0                       | .0070                         | 300.0                                      | 11.020            | .917310             |
| 310.0                       | .0060                         | 310.0                                      | 11.085            | .922721             |
| 320.0                       | .0050                         | 320.0                                      | 11.140            | .927299             |
| 330.0                       | .0040                         | 330.0                                      | 11.185            | .931045             |
| 340.0                       | .0020                         | 340.0                                      | 11.215            | .933542             |
| 350.0                       | .0020                         | 350.0                                      | 11.235            | .935207             |
| 360.0                       | .0010                         | 360.0                                      | 11.250            | .936456             |
| 370.0                       | .0000                         | 370.0                                      | 11.255            | .936872             |

MIRAN VAPOR ANALYZER .25 ABSORBANCE UNITS PER VOLT

TABLE B-5

EVAPORATION EXPERIMENT NO. GLF5 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/BOTTOM SURFACE  
 WINDSPEED 10 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 58%

OUTPUT VOLTAGE DATA FROM MIRAN IA VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES |                   |                     |
|-----------------------------|-------------------------------|--|-------------------|---------------------|
|                             |                               | ELAPSED TIME<br>MINUTES                    | TOTAL<br>VOLT-MIN | TOTAL<br>NORMALIZED |
| .0                          | .0780                         | .0   | .000              | .000000             |
| 30.0                        | .0740                         | 30.0                                       | 2.280             | .060352             |
| 60.0                        | .0710                         | 60.0                                       | 4.455             | .117924             |
| 90.0                        | .0670                         | 90.0                                       | 6.525             | .172717             |
| 120.0                       | .0630                         | 120.0                                      | 8.475             | .224334             |
| 150.0                       | .0600                         | 150.0                                      | 10.320            | .273171             |
| 180.0                       | .0560                         | 180.0                                      | 12.060            | .319229             |
| 210.0                       | .0530                         | 210.0                                      | 13.695            | .362507             |
| 240.0                       | .0500                         | 240.0                                      | 15.240            | .403404             |
| 270.0                       | .0470                         | 270.0                                      | 16.695            | .441917             |
| 300.0                       | .0440                         | 300.0                                      | 18.060            | .478049             |
| 330.0                       | .0400                         | 330.0                                      | 19.320            | .511401             |
| 360.0                       | .0360                         | 360.0                                      | 20.460            | .541577             |
| 390.0                       | .0330                         | 390.0                                      | 21.495            | .568974             |
| 420.0                       | .0300                         | 420.0                                      | 22.440            | .593988             |
| 450.0                       | .0280                         | 450.0                                      | 23.310            | .617017             |
| 480.0                       | .0250                         | 480.0                                      | 24.105            | .638060             |
| 510.0                       | .0230                         | 510.0                                      | 24.825            | .657119             |
| 540.0                       | .0210                         | 540.0                                      | 25.485            | .674589             |
| 570.0                       | .0180                         | 570.0                                      | 26.070            | .690074             |
| 600.0                       | .0160                         | 600.0                                      | 26.580            | .703574             |
| 630.0                       | .0130                         | 630.0                                      | 27.015            | .715088             |
| 660.0                       | .0110                         | 660.0                                      | 27.375            | .724617             |
| 690.0                       | .0080                         | 690.0                                      | 27.660            | .732161             |
| 720.0                       | .0060                         | 720.0                                      | 27.870            | .737720             |
| 750.0                       | .0040                         | 750.0                                      | 28.020            | .741691             |
| 780.0                       | .0030                         | 780.0                                      | 28.125            | .744470             |
| 810.0                       | .0020                         | 810.0                                      | 28.200            | .746455             |
| 840.0                       | .0010                         | 840.0                                      | 28.245            | .747646             |
| 870.0                       | .0000                         | 870.0                                      | 28.260            | .748043             |

MIRAN VAPOR ANALYZER .25 ABSORBANCE UNITS PER VOLT

TABLE B-6

EVAPORATION EXPERIMENT NO. GLF6 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/BOTTOM SURFACE  
 WINDSPEED 5.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 55%

## OUTPUT VOLTAGE DATA FROM MIRAN 1A VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES |                   |                     |
|-----------------------------|-------------------------------|--|-------------------|---------------------|
|                             |                               | ELAPSED TIME<br>MINUTES                    | TOTAL<br>VOLT.MIN | TOTAL<br>NORMALIZED |
| .0                          | .0750                         | .0   | .000              | .000000             |
| 30.0                        | .0740                         | 30.0                                       | 2.250             | .054340             |
| 60.0                        | .0710                         | 60.0                                       | 4.425             | .106868             |
| 90.0                        | .0700                         | 90.0                                       | 6.540             | .157948             |
| 120.0                       | .0660                         | 120.0                                      | 8.580             | .207216             |
| 150.0                       | .0640                         | 150.0                                      | 10.530            | .254310             |
| 180.0                       | .0620                         | 180.0                                      | 12.420            | .299956             |
| 210.0                       | .0590                         | 210.0                                      | 14.235            | .343790             |
| 240.0                       | .0560                         | 240.0                                      | 15.960            | .385450             |
| 270.0                       | .0530                         | 270.0                                      | 17.595            | .424937             |
| 300.0                       | .0500                         | 300.0                                      | 19.140            | .462250             |
| 330.0                       | .0470                         | 330.0                                      | 20.595            | .497390             |
| 360.0                       | .0440                         | 360.0                                      | 21.960            | .530356             |
| 390.0                       | .0410                         | 390.0                                      | 23.235            | .561149             |
| 420.0                       | .0380                         | 420.0                                      | 24.420            | .589768             |
| 450.0                       | .0350                         | 450.0                                      | 25.515            | .616213             |
| 480.0                       | .0320                         | 480.0                                      | 26.520            | .640485             |
| 510.0                       | .0290                         | 510.0                                      | 27.435            | .662583             |
| 540.0                       | .0260                         | 540.0                                      | 28.260            | .682508             |
| 570.0                       | .0230                         | 570.0                                      | 28.995            | .700259             |
| 600.0                       | .0200                         | 600.0                                      | 29.640            | .715836             |
| 630.0                       | .0170                         | 630.0                                      | 30.195            | .729240             |
| 660.0                       | .0140                         | 660.0                                      | 30.660            | .740470             |
| 690.0                       | .0110                         | 690.0                                      | 31.035            | .749527             |
| 720.0                       | .0080                         | 720.0                                      | 31.320            | .756410             |
| 750.0                       | .0060                         | 750.0                                      | 31.530            | .761482             |
| 780.0                       | .0050                         | 780.0                                      | 31.695            | .765466             |
| 810.0                       | .0030                         | 810.0                                      | 31.815            | .768365             |
| 840.0                       | .0020                         | 840.0                                      | 31.890            | .770176             |
| 870.0                       | .0010                         | 870.0                                      | 31.935            | .771265             |
| 900.0                       | .0000                         | 900.0                                      | 31.950            | .771665             |

MIRAN VAPOR ANALYZER .25 ABSORBANCE UNITS PER VOLT

TABLE B-7

EVAPORATION EXPERIMENT NO. GLF7 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/BOTTOM SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

## OUTPUT VOLTAGE DATA FROM MIRAN IA VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES |                   |                     |
|-----------------------------|-------------------------------|--|-------------------|---------------------|
|                             |                               | ELAPSED TIME<br>MINUTES                    | TOTAL<br>VOLT.MIN | TOTAL<br>NORMALIZED |
| .0                          | .0480                         | .0   | .000              | .000000             |
| 15.0                        | .0450                         | 15.0                                       | .697              | .060915             |
| 30.0                        | .0430                         | 30.0                                       | 1.358             | .118554             |
| 45.0                        | .0420                         | 45.0                                       | 1.995             | .174229             |
| 60.0                        | .0400                         | 60.0                                       | 2.610             | .227939             |
| 75.0                        | .0380                         | 75.0                                       | 3.195             | .279028             |
| 90.0                        | .0370                         | 90.0                                       | 3.758             | .328153             |
| 105.0                       | .0350                         | 105.0                                      | 4.298             | .375313             |
| 120.0                       | .0340                         | 120.0                                      | 4.815             | .420507             |
| 135.0                       | .0320                         | 135.0                                      | 5.310             | .463737             |
| 150.0                       | .0310                         | 150.0                                      | 5.782             | .505002             |
| 165.0                       | .0290                         | 165.0                                      | 6.232             | .544302             |
| 180.0                       | .0270                         | 180.0                                      | 6.652             | .580981             |
| 195.0                       | .0260                         | 195.0                                      | 7.050             | .615696             |
| 210.0                       | .0240                         | 210.0                                      | 7.425             | .648446             |
| 225.0                       | .0220                         | 225.0                                      | 7.770             | .678576             |
| 240.0                       | .0200                         | 240.0                                      | 8.085             | .706086             |
| 255.0                       | .0180                         | 255.0                                      | 8.370             | .730975             |
| 270.0                       | .0160                         | 270.0                                      | 8.625             | .753245             |
| 285.0                       | .0140                         | 285.0                                      | 8.850             | .772895             |
| 300.0                       | .0130                         | 300.0                                      | 9.052             | .790580             |
| 315.0                       | .0110                         | 315.0                                      | 9.233             | .806300             |
| 330.0                       | .0090                         | 330.0                                      | 9.382             | .819400             |
| 345.0                       | .0070                         | 345.0                                      | 9.502             | .829880             |
| 360.0                       | .0060                         | 360.0                                      | 9.600             | .838395             |
| 375.0                       | .0050                         | 375.0                                      | 9.682             | .845609             |
| 390.0                       | .0040                         | 390.0                                      | 9.750             | .851495             |
| 405.0                       | .0030                         | 405.0                                      | 9.802             | .856080             |
| 420.0                       | .0020                         | 420.0                                      | 9.840             | .859355             |
| 435.0                       | .0020                         | 435.0                                      | 9.870             | .861975             |
| 450.0                       | .0010                         | 450.0                                      | 9.892             | .863941             |
| 465.0                       | .0010                         | 465.0                                      | 9.908             | .865250             |
| 480.0                       | .0000                         | 480.0                                      | 9.915             | .865905             |

MIRAN VAPOR ANALYZER .25 ABSORBANCE UNITS PER VOLT



TABLE B-8

EVAPORATION EXPERIMENT NO. GLF8 SERIES 1D 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/BOTTOM SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 50%

## OUTPUT VOLTAGE DATA FROM MIRAN 1A VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES |                   |                     |
|-----------------------------|-------------------------------|--|-------------------|---------------------|
|                             |                               | ELAPSED TIME<br>MINUTES                    | TOTAL<br>VOLT-MIN | TOTAL<br>NORMALIZED |
| .0                          | .0450                         | .0   | .000              | .000000             |
| 15.0                        | .0430                         | 15.0                                       | .660              | .056531             |
| 30.0                        | .0420                         | 30.0                                       | 1.298             | .111135             |
| 45.0                        | .0410                         | 45.0                                       | 1.920             | .164454             |
| 60.0                        | .0390                         | 60.0                                       | 2.520             | .215846             |
| 75.0                        | .0380                         | 75.0                                       | 3.097             | .265311             |
| 90.0                        | .0360                         | 90.0                                       | 3.652             | .312849             |
| 105.0                       | .0350                         | 105.0                                      | 4.185             | .358459             |
| 120.0                       | .0340                         | 120.0                                      | 4.702             | .402784             |
| 135.0                       | .0320                         | 135.0                                      | 5.197             | .445183             |
| 150.0                       | .0310                         | 150.0                                      | 5.670             | .485614             |
| 165.0                       | .0290                         | 165.0                                      | 6.120             | .524198             |
| 180.0                       | .0280                         | 180.0                                      | 6.547             | .560815             |
| 195.0                       | .0260                         | 195.0                                      | 6.952             | .595504             |
| 210.0                       | .0250                         | 210.0                                      | 7.335             | .628257             |
| 225.0                       | .0230                         | 225.0                                      | 7.695             | .659102             |
| 240.0                       | .0220                         | 240.0                                      | 8.033             | .688010             |
| 255.0                       | .0200                         | 255.0                                      | 8.347             | .714991             |
| 270.0                       | .0190                         | 270.0                                      | 8.640             | .740044             |
| 285.0                       | .0170                         | 285.0                                      | 8.910             | .763171             |
| 300.0                       | .0160                         | 300.0                                      | 9.158             | .784370             |
| 315.0                       | .0140                         | 315.0                                      | 9.383             | .803642             |
| 330.0                       | .0130                         | 330.0                                      | 9.585             | .820987             |
| 345.0                       | .0110                         | 345.0                                      | 9.765             | .836404             |
| 360.0                       | .0090                         | 360.0                                      | 9.915             | .849252             |
| 375.0                       | .0080                         | 375.0                                      | 10.043            | .860173             |
| 390.0                       | .0060                         | 390.0                                      | 10.148            | .869167             |
| 405.0                       | .0050                         | 405.0                                      | 10.230            | .876233             |
| 420.0                       | .0030                         | 420.0                                      | 10.290            | .881372             |
| 435.0                       | .0020                         | 435.0                                      | 10.328            | .884584             |
| 450.0                       | .0010                         | 450.0                                      | 10.350            | .886511             |
| 465.0                       | .0010                         | 465.0                                      | 10.365            | .887796             |
| 480.0                       | .0000                         | 480.0                                      | 10.373            | .888439             |

MIRAN VAPOR ANALYZER .25 ABSORBANCE UNITS PER VOLT

TABLE B-9

EVAPORATION EXPERIMENT NO. GLF9 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 44%

## OUTPUT VOLTAGE DATA FROM MIRAN IA VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES |                   |                     |
|-----------------------------|-------------------------------|--|-------------------|---------------------|
|                             |                               | ELAPSED TIME<br>MINUTES                    | TOTAL<br>VOLT.MIN | TOTAL<br>NORMALIZED |
| .0                          | .1410                         | .0   | .000              | .000000             |
| 30.0                        | .0900                         | 30.0                                       | 3.465             | .090853             |
| 60.0                        | .0840                         | 60.0                                       | 6.075             | .159288             |
| 90.0                        | .0820                         | 90.0                                       | 8.565             | .224576             |
| 120.0                       | .0750                         | 120.0                                      | 10.920            | .286325             |
| 150.0                       | .0700                         | 150.0                                      | 13.095            | .343353             |
| 180.0                       | .0660                         | 180.0                                      | 15.135            | .396843             |
| 210.0                       | .0610                         | 210.0                                      | 17.040            | .446792             |
| 240.0                       | .0570                         | 240.0                                      | 18.810            | .493202             |
| 270.0                       | .0520                         | 270.0                                      | 20.445            | .536072             |
| 300.0                       | .0480                         | 300.0                                      | 21.945            | .575402             |
| 330.0                       | .0430                         | 330.0                                      | 23.310            | .611193             |
| 360.0                       | .0390                         | 360.0                                      | 24.540            | .643444             |
| 390.0                       | .0340                         | 390.0                                      | 25.635            | .672155             |
| 420.0                       | .0300                         | 420.0                                      | 26.575            | .697326             |
| 450.0                       | .0250                         | 450.0                                      | 27.420            | .718958             |
| 480.0                       | .0210                         | 480.0                                      | 28.110            | .737050             |
| 510.0                       | .0170                         | 510.0                                      | 28.680            | .751995             |
| 540.0                       | .0140                         | 540.0                                      | 29.145            | .764188             |
| 570.0                       | .0110                         | 570.0                                      | 29.520            | .774020             |
| 600.0                       | .0080                         | 600.0                                      | 29.805            | .781793             |
| 630.0                       | .0060                         | 630.0                                      | 30.015            | .786999             |
| 660.0                       | .0040                         | 660.0                                      | 30.165            | .790932             |
| 690.0                       | .0030                         | 690.0                                      | 30.270            | .793525             |
| 720.0                       | .0020                         | 720.0                                      | 30.345            | .795652             |
| 750.0                       | .0010                         | 750.0                                      | 30.390            | .796832             |
| 780.0                       | .0000                         | 780.0                                      | 30.405            | .797225             |

MIRAN VAPOR ANALYZER .25 ABSORBANCE UNITS PER VOLT

TABLE B-10

EVAPORATION EXPERIMENT NO. GLF10 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 M.M DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 52%

## OUTPUT VOLTAGE DATA FROM MIRAN 1A VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES |                   |                     |
|-----------------------------|-------------------------------|--|-------------------|---------------------|
|                             |                               | ELAPSED TIME<br>MINUTES                    | TOTAL<br>VOLT.MIN | TOTAL<br>NORMALIZED |
| .0                          | .1350                         | .0   | .000              | .000000             |
| 30.0                        | .0970                         | 30.0                                       | 3.480             | .073736             |
| 60.0                        | .0910                         | 60.0                                       | 6.300             | .133488             |
| 90.0                        | .0860                         | 90.0                                       | 8.955             | .189743             |
| 120.0                       | .0830                         | 120.0                                      | 11.490            | .243456             |
| 150.0                       | .0790                         | 150.0                                      | 13.920            | .294944             |
| 180.0                       | .0750                         | 180.0                                      | 16.230            | .343889             |
| 210.0                       | .0720                         | 210.0                                      | 18.435            | .390610             |
| 240.0                       | .0680                         | 240.0                                      | 20.535            | .435106             |
| 270.0                       | .0650                         | 270.0                                      | 22.530            | .477377             |
| 300.0                       | .0600                         | 300.0                                      | 24.405            | .517105             |
| 330.0                       | .0570                         | 330.0                                      | 26.160            | .554291             |
| 360.0                       | .0530                         | 360.0                                      | 27.810            | .589252             |
| 390.0                       | .0490                         | 390.0                                      | 29.340            | .621670             |
| 420.0                       | .0450                         | 420.0                                      | 30.750            | .651546             |
| 450.0                       | .0400                         | 450.0                                      | 32.025            | .678562             |
| 480.0                       | .0350                         | 480.0                                      | 33.150            | .702399             |
| 510.0                       | .0310                         | 510.0                                      | 34.140            | .723375             |
| 540.0                       | .0270                         | 540.0                                      | 35.010            | .741909             |
| 570.0                       | .0230                         | 570.0                                      | 35.760            | .757701             |
| 600.0                       | .0200                         | 600.0                                      | 36.405            | .771367             |
| 630.0                       | .0160                         | 630.0                                      | 36.945            | .782809             |
| 660.0                       | .0140                         | 660.0                                      | 37.395            | .792344             |
| 690.0                       | .0120                         | 690.0                                      | 37.785            | .800607             |
| 720.0                       | .0100                         | 720.0                                      | 38.115            | .807599             |
| 750.0                       | .0080                         | 750.0                                      | 38.385            | .813320             |
| 780.0                       | .0060                         | 780.0                                      | 38.595            | .817770             |
| 810.0                       | .0050                         | 810.0                                      | 38.760            | .821266             |
| 840.0                       | .0040                         | 840.0                                      | 38.895            | .824126             |
| 870.0                       | .0030                         | 870.0                                      | 39.000            | .826351             |
| 900.0                       | .0010                         | 900.0                                      | 39.060            | .827623             |
| 930.0                       | .0010                         | 930.0                                      | 39.090            | .828258             |
| 960.0                       | .0000                         | 960.0                                      | 39.105            | .828576             |

MIRAN VAPOR ANALYZER .25 ABSORBANCE UNITS PER VOLT

TABLE B-11

EVAPORATION EXPERIMENT NO. GLF11 SERIES 10 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 50 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 55%

## OUTPUT VOLTAGE DATA FROM MIRAN IA VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES |          |            |
|-----------------------------|-------------------------------|--|----------|------------|
|                             |                               | ELAPSED TIME                               | TOTAL    | TOTAL      |
|                             |                               | MINUTES                                    | VOLT MIN | NORMALIZED |
| .0                          | .0650                         | .0   | .000     | .000000    |
| 10.0                        | .0620                         | 10.0                                       | .635     | .061070    |
| 20.0                        | .0590                         | 20.0                                       | 1.240    | .119255    |
| 30.0                        | .0570                         | 30.0                                       | 1.820    | .175036    |
| 40.0                        | .0540                         | 40.0                                       | 2.375    | .228412    |
| 50.0                        | .0520                         | 50.0                                       | 2.905    | .279384    |
| 60.0                        | .0490                         | 60.0                                       | 3.410    | .327952    |
| 70.0                        | .0470                         | 70.0                                       | 3.890    | .374115    |
| 80.0                        | .0450                         | 80.0                                       | 4.350    | .418555    |
| 90.0                        | .0430                         | 90.0                                       | 4.790    | .460672    |
| 100.0                       | .0400                         | 100.0                                      | 5.205    | .500584    |
| 110.0                       | .0380                         | 110.0                                      | 5.595    | .538091    |
| 120.0                       | .0350                         | 120.0                                      | 5.960    | .573195    |
| 130.0                       | .0330                         | 130.0                                      | 6.300    | .605894    |
| 140.0                       | .0310                         | 140.0                                      | 6.620    | .636669    |
| 150.0                       | .0280                         | 150.0                                      | 6.915    | .665040    |
| 160.0                       | .0260                         | 160.0                                      | 7.185    | .691007    |
| 170.0                       | .0240                         | 170.0                                      | 7.435    | .715051    |
| 180.0                       | .0220                         | 180.0                                      | 7.665    | .737171    |
| 190.0                       | .0190                         | 190.0                                      | 7.870    | .756886    |
| 200.0                       | .0170                         | 200.0                                      | 8.050    | .774197    |
| 210.0                       | .0150                         | 210.0                                      | 8.210    | .789585    |
| 220.0                       | .0130                         | 220.0                                      | 8.350    | .803050    |
| 230.0                       | .0120                         | 230.0                                      | 8.475    | .815071    |
| 240.0                       | .0100                         | 240.0                                      | 8.585    | .825650    |
| 250.0                       | .0090                         | 250.0                                      | 8.680    | .834787    |
| 260.0                       | .0080                         | 260.0                                      | 8.765    | .842962    |
| 270.0                       | .0070                         | 270.0                                      | 8.840    | .850175    |
| 280.0                       | .0060                         | 280.0                                      | 8.905    | .856426    |
| 290.0                       | .0050                         | 290.0                                      | 8.960    | .861715    |
| 300.0                       | .0040                         | 300.0                                      | 9.005    | .866043    |
| 310.0                       | .0030                         | 310.0                                      | 9.040    | .869409    |
| 320.0                       | .0030                         | 320.0                                      | 9.070    | .872294    |
| 330.0                       | .0020                         | 330.0                                      | 9.095    | .874699    |
| 340.0                       | .0010                         | 340.0                                      | 9.110    | .876143    |
| 350.0                       | .0010                         | 350.0                                      | 9.120    | .877103    |
| 360.0                       | .0000                         | 360.0                                      | 9.125    | .877584    |

MIRAN VAPOR ANALYZER .01% ABSORBANCE UNITS PER VOLT

TABLE B-12

EVAPORATION EXPERIMENT NO. GLF12 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOX SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 40%

## OUTPUT VOLTAGE DATA FROM MIRAN IA VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES |                   |                     |
|-----------------------------|-------------------------------|--|-------------------|---------------------|
|                             |                               | ELAPSED TIME<br>MINUTES                    | TOTAL<br>VOLT.MIN | TOTAL<br>NORMALIZED |
| .0                          | .0540                         | .0   | .000              | .000000             |
| 10.0                        | .0520                         | 10.0                                       | .530              | .044117             |
| 20.0                        | .0510                         | 20.0                                       | 1.045             | .086986             |
| 30.0                        | .0490                         | 30.0                                       | 1.545             | .128607             |
| 40.0                        | .0470                         | 40.0                                       | 2.025             | .168562             |
| 50.0                        | .0460                         | 50.0                                       | 2.490             | .207269             |
| 60.0                        | .0450                         | 60.0                                       | 2.945             | .245143             |
| 70.0                        | .0430                         | 70.0                                       | 3.385             | .281769             |
| 80.0                        | .0420                         | 80.0                                       | 3.810             | .317146             |
| 90.0                        | .0410                         | 90.0                                       | 4.225             | .351691             |
| 100.0                       | .0400                         | 100.0                                      | 4.630             | .385404             |
| 110.0                       | .0390                         | 110.0                                      | 5.025             | .418284             |
| 120.0                       | .0380                         | 120.0                                      | 5.410             | .450331             |
| 130.0                       | .0360                         | 130.0                                      | 5.780             | .481130             |
| 140.0                       | .0350                         | 140.0                                      | 6.135             | .510680             |
| 150.0                       | .0340                         | 150.0                                      | 6.480             | .539398             |
| 160.0                       | .0330                         | 160.0                                      | 6.815             | .567284             |
| 170.0                       | .0320                         | 170.0                                      | 7.140             | .594337             |
| 180.0                       | .0300                         | 180.0                                      | 7.450             | .620142             |
| 190.0                       | .0290                         | 190.0                                      | 7.745             | .644698             |
| 200.0                       | .0280                         | 200.0                                      | 8.030             | .668421             |
| 210.0                       | .0270                         | 210.0                                      | 8.305             | .691312             |
| 220.0                       | .0250                         | 220.0                                      | 8.565             | .712955             |
| 230.0                       | .0240                         | 230.0                                      | 8.810             | .733369             |
| 240.0                       | .0220                         | 240.0                                      | 9.040             | .752494             |
| 250.0                       | .0210                         | 250.0                                      | 9.255             | .770391             |
| 260.0                       | .0190                         | 260.0                                      | 9.455             | .787039             |
| 270.0                       | .0180                         | 270.0                                      | 9.640             | .802438             |
| 280.0                       | .0170                         | 280.0                                      | 9.815             | .817006             |
| 290.0                       | .0150                         | 290.0                                      | 9.975             | .830324             |
| 300.0                       | .0140                         | 300.0                                      | 10.120            | .842394             |
| 310.0                       | .0120                         | 310.0                                      | 10.250            | .853215             |
| 320.0                       | .0100                         | 320.0                                      | 10.360            | .862372             |
| 330.0                       | .0090                         | 330.0                                      | 10.455            | .870279             |
| 340.0                       | .0080                         | 340.0                                      | 10.540            | .877355             |
| 350.0                       | .0060                         | 350.0                                      | 10.610            | .883182             |
| 360.0                       | .0050                         | 360.0                                      | 10.665            | .887766             |
| 370.0                       | .0030                         | 370.0                                      | 10.705            | .891090             |
| 380.0                       | .0020                         | 380.0                                      | 10.730            | .893171             |
| 390.0                       | .0000                         | 390.0                                      | 10.740            | .894003             |

MIRAN VAPOR ANALYZER 25 ABSORBANCE UNITS PER VOLT

TABLE B-13

EVAPORATION EXPERIMENT NO. GLF13 SERIES ID 2\*\*4 FAC ORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 44%

## CUTPUT VOLTAGE DATA FROM MIRAN 1A VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES<br>ELAPSED TIME<br>MINUTES | TOTAL<br>VOLT/MIN | TOTAL<br>NORMALIZED |
|-----------------------------|-------------------------------|---|-------------------|---------------------|
| 0.0                         | .0700                         | 0.0   | .000              | .000000             |
| 40.0                        | .0630                         | 40.0  | 2.660             | .066343             |
| 80.0                        | .0600                         | 80.0  | 5.120             | .127699             |
| 120.0                       | .0580                         | 120.0   | 7.480             | .186560             |
| 160.0                       | .0550                         | 160.0   | 9.740             | .242227             |
| 200.0                       | .0530                         | 200.0   | 11.900            | .296800             |
| 240.0                       | .0510                         | 240.0   | 13.980            | .348677             |
| 280.0                       | .0490                         | 280.0   | 15.980            | .396560             |
| 320.0                       | .0470                         | 320.0   | 17.900            | .445447             |
| 360.0                       | .0450                         | 360.0   | 19.740            | .492339             |
| 400.0                       | .0410                         | 400.0   | 21.480            | .535237             |
| 440.0                       | .0390                         | 440.0   | 23.060            | .575143             |
| 480.0                       | .0360                         | 480.0   | 24.560            | .612555             |
| 520.0                       | .0330                         | 520.0   | 25.940            | .646974             |
| 560.0                       | .0290                         | 560.0   | 27.180            | .677901             |
| 600.0                       | .0250                         | 600.0   | 28.260            | .704837             |
| 640.0                       | .0210                         | 640.0   | 29.180            | .727783             |
| 680.0                       | .0180                         | 680.0   | 29.960            | .747237             |
| 720.0                       | .0150                         | 720.0   | 30.620            | .763698             |
| 760.0                       | .0120                         | 760.0   | 31.160            | .777167             |
| 800.0                       | .0100                         | 800.0   | 31.600            | .788141             |
| 840.0                       | .0080                         | 840.0   | 31.960            | .797120             |
| 880.0                       | .0070                         | 880.0   | 32.260            | .804602             |
| 920.0                       | .0060                         | 920.0   | 32.520            | .811087             |
| 960.0                       | .0050                         | 960.0   | 32.740            | .816574             |
| 1000.0                      | .0040                         | 1000.0  | 32.920            | .821063             |
| 1040.0                      | .0030                         | 1040.0  | 33.060            | .824555             |
| 1080.0                      | .0020                         | 1080.0  | 33.160            | .827049             |
| 1120.0                      | .0020                         | 1120.0  | 33.240            | .829044             |
| 1160.0                      | .0020                         | 1160.0  | 33.320            | .831040             |
| 1200.0                      | .0010                         | 1200.0  | 33.380            | .832536             |
| 1240.0                      | .0010                         | 1240.0  | 33.420            | .833534             |
| 1280.0                      | .0000                         | 1280.0  | 33.440            | .834033             |

MIRAN VAPOR ANALYZER .01% ABSORBANCE UNITS PER VOLT

TABLE B-14

EVAPORATION EXPERIMENT NO. GLF14 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLNALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 43%

## OUTPUT VOLTAGE DATA FROM MIRAN 1A VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES |                    |                     |
|-----------------------------|-------------------------------|--|--------------------|---------------------|
|                             |                               | ELAPSED TIME<br>MINUTES                    | TOTAL<br>VOL.T.MIN | TOTAL<br>NORMALIZED |
| .0                          | .0700                         | .0   | .000               | .000000             |
| 40.0                        | .0670                         | 40.0                                       | 2.740              | .058898             |
| 80.0                        | .0640                         | 80.0                                       | 5.360              | .115216             |
| 120.0                       | .0620                         | 120.0                                      | 7.880              | .169385             |
| 160.0                       | .0600                         | 160.0                                      | 10.320             | .221834             |
| 200.0                       | .0580                         | 200.0                                      | 12.680             | .272564             |
| 240.0                       | .0550                         | 240.0                                      | 14.940             | .321144             |
| 280.0                       | .0530                         | 280.0                                      | 17.100             | .367574             |
| 320.0                       | .0510                         | 320.0                                      | 19.180             | .412285             |
| 360.0                       | .0490                         | 360.0                                      | 21.180             | .455276             |
| 400.0                       | .0460                         | 400.0                                      | 23.080             | .496118             |
| 440.0                       | .0440                         | 440.0                                      | 24.880             | .534810             |
| 480.0                       | .0410                         | 480.0                                      | 26.580             | .571352             |
| 520.0                       | .0380                         | 520.0                                      | 28.160             | .605315             |
| 560.0                       | .0350                         | 560.0                                      | 29.620             | .636699             |
| 600.0                       | .0320                         | 600.0                                      | 30.960             | .665503             |
| 640.0                       | .0290                         | 640.0                                      | 32.180             | .691727             |
| 680.0                       | .0250                         | 680.0                                      | 33.260             | .714943             |
| 720.0                       | .0220                         | 720.0                                      | 34.200             | .735148             |
| 760.0                       | .0200                         | 760.0                                      | 35.040             | .753205             |
| 800.0                       | .0170                         | 800.0                                      | 35.780             | .769112             |
| 840.0                       | .0150                         | 840.0                                      | 36.420             | .782869             |
| 880.0                       | .0130                         | 880.0                                      | 36.980             | .794906             |
| 920.0                       | .0090                         | 920.0                                      | 37.420             | .804364             |
| 960.0                       | .0060                         | 960.0                                      | 37.720             | .810813             |
| 1000.0                      | .0050                         | 1000.0                                     | 37.940             | .815542             |
| 1040.0                      | .0050                         | 1040.0                                     | 38.140             | .819841             |
| 1080.0                      | .0030                         | 1080.0                                     | 38.300             | .823280             |
| 1120.0                      | .0020                         | 1120.0                                     | 38.400             | .825430             |
| 1160.0                      | .0000                         | 1160.0                                     | 38.440             | .826290             |

MIRAN VAPOR ANALYZER .25 ABSORBANCE UNITS PER VOLT

TABLE B-15

EVAPORATION EXPERIMENT NO. GLF15 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 11.3 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 33%

## OUTPUT VOLTAGE DATA FROM MIRAN 1A VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES |                   |                     |
|-----------------------------|-------------------------------|--|-------------------|---------------------|
|                             |                               | ELAPSED TIME<br>MINUTES                    | TOTAL<br>VOLT.MIN | TOTAL<br>NORMALIZED |
| .0                          | .0430                         | .0   | .000              | .900000             |
| 15.0                        | .0410                         | 15.0                                       | .630              | .059574             |
| 30.0                        | .0390                         | 30.0                                       | 1.230             | .116312             |
| 45.0                        | .0380                         | 45.0                                       | 1.808             | .170922             |
| 60.0                        | .0360                         | 60.0                                       | 2.362             | .223404             |
| 75.0                        | .0350                         | 75.0                                       | 2.895             | .273758             |
| 90.0                        | .0340                         | 90.0                                       | 3.412             | .322694             |
| 105.0                       | .0330                         | 105.0                                      | 3.915             | .370212             |
| 120.0                       | .0310                         | 120.0                                      | 4.395             | .415602             |
| 135.0                       | .0300                         | 135.0                                      | 4.852             | .458864             |
| 150.0                       | .0290                         | 150.0                                      | 5.295             | .500708             |
| 165.0                       | .0270                         | 165.0                                      | 5.715             | .540424             |
| 180.0                       | .0260                         | 180.0                                      | 6.113             | .578013             |
| 195.0                       | .0250                         | 195.0                                      | 6.495             | .614183             |
| 210.0                       | .0240                         | 210.0                                      | 6.863             | .648934             |
| 225.0                       | .0220                         | 225.0                                      | 7.207             | .681558             |
| 240.0                       | .0200                         | 240.0                                      | 7.523             | .711346             |
| 255.0                       | .0180                         | 255.0                                      | 7.807             | .738296             |
| 270.0                       | .0160                         | 270.0                                      | 8.063             | .762409             |
| 285.0                       | .0140                         | 285.0                                      | 8.288             | .783686             |
| 300.0                       | .0120                         | 300.0                                      | 8.483             | .802125             |
| 315.0                       | .0100                         | 315.0                                      | 8.648             | .817728             |
| 330.0                       | .0080                         | 330.0                                      | 8.783             | .830494             |
| 345.0                       | .0060                         | 345.0                                      | 8.897             | .840423             |
| 360.0                       | .0050                         | 360.0                                      | 8.970             | .848225             |
| 375.0                       | .0040                         | 375.0                                      | 9.038             | .854608             |
| 390.0                       | .0030                         | 390.0                                      | 9.090             | .859572             |
| 405.0                       | .0020                         | 405.0                                      | 9.128             | .863118             |
| 420.0                       | .0010                         | 420.0                                      | 9.150             | .865246             |
| 435.0                       | .0010                         | 435.0                                      | 9.165             | .866664             |
| 450.0                       | .0010                         | 450.0                                      | 9.180             | .868083             |
| 465.0                       | .0000                         | 465.0                                      | 9.188             | .868792             |

MIRAN VAPOR ANALYZER .25 ABSORBANCE UNITS PER VOLT



TABLE B-16

EVAPORATION EXPERIMENT NO. GLF16 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 11.3 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 30%

## OUTPUT VOLTAGE DATA FROM MIRAN IA VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES |                   |                     |
|-----------------------------|-------------------------------|--|-------------------|---------------------|
|                             |                               | ELAPSED TIME<br>MINUTES                    | TOTAL<br>VOLT.MIN | TOTAL<br>NORMALIZED |
| .0                          | .0430                         | .0   | .000              | .000000             |
| 15.0                        | .0410                         | 15.0                                       | .630              | .055303             |
| 30.0                        | .0390                         | 30.0                                       | 1.230             | .107973             |
| 45.0                        | .0380                         | 45.0                                       | 1.808             | .158667             |
| 60.0                        | .0360                         | 60.0                                       | 2.362             | .207387             |
| 75.0                        | .0350                         | 75.0                                       | 2.895             | .254131             |
| 90.0                        | .0340                         | 90.0                                       | 3.412             | .299559             |
| 105.0                       | .0330                         | 105.0                                      | 3.915             | .343669             |
| 120.0                       | .0320                         | 120.0                                      | 4.403             | .386463             |
| 135.0                       | .0310                         | 135.0                                      | 4.875             | .427941             |
| 150.0                       | .0300                         | 150.0                                      | 5.332             | .468101             |
| 165.0                       | .0280                         | 165.0                                      | 5.767             | .506287             |
| 180.0                       | .0280                         | 180.0                                      | 6.188             | .543156             |
| 195.0                       | .0260                         | 195.0                                      | 6.593             | .578708             |
| 210.0                       | .0250                         | 210.0                                      | 6.975             | .612284             |
| 225.0                       | .0240                         | 225.0                                      | 7.343             | .644545             |
| 240.0                       | .0220                         | 240.0                                      | 7.688             | .674830             |
| 255.0                       | .0210                         | 255.0                                      | 8.010             | .703140             |
| 270.0                       | .0200                         | 270.0                                      | 8.318             | .730133             |
| 285.0                       | .0180                         | 285.0                                      | 8.602             | .755151             |
| 300.0                       | .0160                         | 300.0                                      | 8.858             | .777535             |
| 315.0                       | .0140                         | 315.0                                      | 9.083             | .797287             |
| 330.0                       | .0120                         | 330.0                                      | 9.278             | .814404             |
| 345.0                       | .0090                         | 345.0                                      | 9.435             | .828230             |
| 360.0                       | .0070                         | 360.0                                      | 9.555             | .838764             |
| 375.0                       | .0050                         | 375.0                                      | 9.645             | .846664             |
| 390.0                       | .0030                         | 390.0                                      | 9.705             | .851931             |
| 405.0                       | .0020                         | 405.0                                      | 9.743             | .855223             |
| 420.0                       | .0010                         | 420.0                                      | 9.765             | .857198             |
| 435.0                       | .0000                         | 435.0                                      | 9.773             | .857857             |

MIRAN VAPOR ANALYZER .25 ABSORBANCE UNITS PER VOLT

TABLE B-17

EVAPORATION EXPERIMENT NO. BLF1 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SG METER ON OAK/10P SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 39%

## OUTPUT VOLTAGE DATA FROM MIRAN LA VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES |                   |                     |
|-----------------------------|-------------------------------|--|-------------------|---------------------|
|                             |                               | ELAPSED TIME<br>MINUTES                    | TOTAL<br>VOLT/HIN | TOTAL<br>NORMALIZED |
| .0                          | .0780                         | .0   | .000              | .000000             |
| 45.0                        | .0730                         | 45.0                                       | 3.398             | .078690             |
| 90.0                        | .0690                         | 90.0                                       | 6.592             | .152691             |
| 135.0                       | .0660                         | 135.0                                      | 9.630             | .223043             |
| 180.0                       | .0630                         | 180.0                                      | 12.532            | .290269             |
| 225.0                       | .0600                         | 225.0                                      | 15.360            | .354368             |
| 270.0                       | .0560                         | 270.0                                      | 17.910            | .414819             |
| 315.0                       | .0530                         | 315.0                                      | 20.362            | .471622             |
| 360.0                       | .0480                         | 360.0                                      | 22.635            | .524256             |
| 405.0                       | .0440                         | 405.0                                      | 24.705            | .572200             |
| 450.0                       | .0390                         | 450.0                                      | 26.572            | .615453             |
| 495.0                       | .0350                         | 495.0                                      | 28.237            | .654017             |
| 540.0                       | .0300                         | 540.0                                      | 29.700            | .687890             |
| 585.0                       | .0250                         | 585.0                                      | 30.937            | .716552             |
| 630.0                       | .0210                         | 630.0                                      | 31.972            | .740524             |
| 675.0                       | .0160                         | 675.0                                      | 32.805            | .759806             |
| 720.0                       | .0130                         | 720.0                                      | 33.457            | .774919             |
| 765.0                       | .0090                         | 765.0                                      | 33.952            | .786384             |
| 810.0                       | .0070                         | 810.0                                      | 34.312            | .794722             |
| 855.0                       | .0040                         | 855.0                                      | 34.560            | .800454             |
| 900.0                       | .0030                         | 900.0                                      | 34.717            | .804102             |
| 945.0                       | .0020                         | 945.0                                      | 34.830            | .806708             |
| 990.0                       | .0020                         | 990.0                                      | 34.920            | .808702             |
| 1035.0                      | .0010                         | 1035.0                                     | 34.987            | .810356             |
| 1080.0                      | .0010                         | 1080.0                                     | 35.032            | .811398             |
| 1125.0                      | .0010                         | 1125.0                                     | 35.077            | .812440             |
| 1170.0                      | .0010                         | 1170.0                                     | 35.122            | .813482             |
| 1215.0                      | .0000                         | 1215.0                                     | 35.145            | .814003             |

MIRAN VAPOR ANALYZER .25 ABSORBANCE UNITS PER VOLT

TABLE B-18

EVAPORATION EXPERIMENT NO. BLEZ SERIES ID 2454 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOB SURFACE  
 WINDSPEED 2.9 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 39%

## OUTPUT VOLTAGE DATA FROM MIRAN 1A VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES |          |            |
|-----------------------------|-------------------------------|--|----------|------------|
|                             |                               | ELAPSED TIME                               | TOTAL    | TOTAL      |
|                             |                               | MINUTES                                    | VOLT.MIN | NORMALIZED |
| .0                          | .0890                         | .0   | .000     | .000000    |
| 40.0                        | .0840                         | 40.0                                       | 3.460    | .073730    |
| 80.0                        | .0800                         | 80.0                                       | 6.740    | .143624    |
| 120.0                       | .0770                         | 120.0                                      | 9.880    | .210534    |
| 160.0                       | .0740                         | 160.0                                      | 12.900   | .274888    |
| 200.0                       | .0710                         | 200.0                                      | 15.800   | .335684    |
| 240.0                       | .0680                         | 240.0                                      | 18.580   | .395924    |
| 280.0                       | .0650                         | 280.0                                      | 21.240   | .452006    |
| 320.0                       | .0620                         | 320.0                                      | 23.780   | .506731    |
| 360.0                       | .0590                         | 360.0                                      | 26.200   | .558299    |
| 400.0                       | .0560                         | 400.0                                      | 28.500   | .607310    |
| 440.0                       | .0520                         | 440.0                                      | 30.660   | .653338    |
| 480.0                       | .0490                         | 480.0                                      | 32.680   | .696382    |
| 520.0                       | .0450                         | 520.0                                      | 34.560   | .736443    |
| 560.0                       | .0400                         | 560.0                                      | 36.260   | .772669    |
| 600.0                       | .0360                         | 600.0                                      | 37.780   | .805059    |
| 640.0                       | .0320                         | 640.0                                      | 39.140   | .834039    |
| 680.0                       | .0280                         | 680.0                                      | 40.340   | .859610    |
| 720.0                       | .0240                         | 720.0                                      | 41.380   | .881772    |
| 760.0                       | .0200                         | 760.0                                      | 42.260   | .900524    |
| 800.0                       | .0170                         | 800.0                                      | 43.000   | .916293    |
| 840.0                       | .0140                         | 840.0                                      | 43.620   | .929504    |
| 880.0                       | .0120                         | 880.0                                      | 44.140   | .940585    |
| 920.0                       | .0090                         | 920.0                                      | 44.560   | .949555    |
| 960.0                       | .0080                         | 960.0                                      | 44.900   | .956780    |
| 1000.0                      | .0060                         | 1000.0                                     | 45.180   | .962747    |
| 1040.0                      | .0040                         | 1040.0                                     | 45.380   | .967608    |
| 1080.0                      | .0030                         | 1080.0                                     | 45.520   | .971992    |
| 1120.0                      | .0020                         | 1120.0                                     | 45.620   | .975122    |
| 1160.0                      | .0020                         | 1160.0                                     | 45.700   | .977327    |
| 1200.0                      | .0010                         | 1200.0                                     | 45.760   | .978106    |
| 1240.0                      | .0010                         | 1240.0                                     | 45.800   | .978558    |
| 1280.0                      | .0000                         | 1280.0                                     | 45.820   | .978884    |

MIRAN VAPOR ANALYZER .25 ABSORBANCE UNITS PER VOLT

TABLE B-19

EVAPORATION EXPERIMENT NO. BLF3 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

## OUTPUT VOLTAGE DATA FROM MIRAN IA VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES |                   |                     |
|-----------------------------|-------------------------------|--|-------------------|---------------------|
|                             |                               | ELAPSED TIME<br>MINUTES                    | TOTAL<br>VOLT.MIN | TOTAL<br>NORMALIZED |
| .0                          | .0520                         | .0   | .000              | .000000             |
| 15.0                        | .0490                         | 15.0                                       | .757              | .064330             |
| 30.0                        | .0470                         | 30.0                                       | 1.477             | .125476             |
| 45.0                        | .0440                         | 45.0                                       | 2.160             | .183437             |
| 60.0                        | .0420                         | 60.0                                       | 2.805             | .238214             |
| 75.0                        | .0410                         | 75.0                                       | 3.427             | .291079             |
| 90.0                        | .0390                         | 90.0                                       | 4.027             | .342034             |
| 105.0                       | .0370                         | 105.0                                      | 4.597             | .390441             |
| 120.0                       | .0350                         | 120.0                                      | 5.137             | .436301             |
| 135.0                       | .0340                         | 135.0                                      | 5.655             | .480249             |
| 150.0                       | .0320                         | 150.0                                      | 6.150             | .522287             |
| 165.0                       | .0310                         | 165.0                                      | 6.622             | .562414             |
| 180.0                       | .0290                         | 180.0                                      | 7.072             | .600630             |
| 195.0                       | .0270                         | 195.0                                      | 7.492             | .636298             |
| 210.0                       | .0250                         | 210.0                                      | 7.882             | .669419             |
| 225.0                       | .0230                         | 225.0                                      | 8.242             | .699992             |
| 240.0                       | .0200                         | 240.0                                      | 8.565             | .727380             |
| 255.0                       | .0180                         | 255.0                                      | 8.850             | .751584             |
| 270.0                       | .0160                         | 270.0                                      | 9.105             | .773240             |
| 285.0                       | .0140                         | 285.0                                      | 9.330             | .792348             |
| 300.0                       | .0120                         | 300.0                                      | 9.525             | .808908             |
| 315.0                       | .0100                         | 315.0                                      | 9.690             | .822921             |
| 330.0                       | .0080                         | 330.0                                      | 9.825             | .834385             |
| 345.0                       | .0060                         | 345.0                                      | 9.930             | .843302             |
| 360.0                       | .0040                         | 360.0                                      | 10.005            | .849672             |
| 375.0                       | .0030                         | 375.0                                      | 10.057            | .854130             |
| 390.0                       | .0020                         | 390.0                                      | 10.095            | .857315             |
| 405.0                       | .0020                         | 405.0                                      | 10.125            | .859863             |
| 420.0                       | .0010                         | 420.0                                      | 10.147            | .861774             |
| 435.0                       | .0010                         | 435.0                                      | 10.162            | .863047             |
| 450.0                       | .0000                         | 450.0                                      | 10.170            | .863684             |

MIRAN VAPOR ANALYZER .25 ABSORBANCE UNITS PER VOLT

TABLE B-20

EVAPORATION EXPERIMENT NO. BLF4 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 20%

## OUTPUT VOLTAGE DATA FROM MIRAN 1A VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES |                   |                     |
|-----------------------------|-------------------------------|--|-------------------|---------------------|
|                             |                               | ELAPSED TIME<br>MINUTES                    | TOTAL<br>VOLT.MIN | TOTAL<br>NORMALIZED |
| .0                          | .0510                         | .0   | .000              | .000000             |
| 20.0                        | .0500                         | 20.0                                       | 1.010             | .080839             |
| 40.0                        | .0480                         | 40.0                                       | 1.990             | .159277             |
| 60.0                        | .0460                         | 60.0                                       | 2.930             | .234514             |
| 80.0                        | .0450                         | 80.0                                       | 3.840             | .307350             |
| 100.0                       | .0430                         | 100.0                                      | 4.720             | .377784             |
| 120.0                       | .0400                         | 120.0                                      | 5.550             | .444216             |
| 140.0                       | .0380                         | 140.0                                      | 6.330             | .506647             |
| 160.0                       | .0360                         | 160.0                                      | 7.070             | .565875             |
| 180.0                       | .0340                         | 180.0                                      | 7.770             | .621903             |
| 200.0                       | .0310                         | 200.0                                      | 8.420             | .673928             |
| 220.0                       | .0290                         | 220.0                                      | 9.020             | .721951             |
| 240.0                       | .0260                         | 240.0                                      | 9.570             | .765973             |
| 260.0                       | .0240                         | 260.0                                      | 10.070            | .805992             |
| 280.0                       | .0210                         | 280.0                                      | 10.520            | .842010             |
| 300.0                       | .0180                         | 300.0                                      | 10.910            | .873225             |
| 320.0                       | .0150                         | 320.0                                      | 11.240            | .899638             |
| 340.0                       | .0120                         | 340.0                                      | 11.510            | .921248             |
| 360.0                       | .0090                         | 360.0                                      | 11.720            | .938056             |
| 380.0                       | .0060                         | 380.0                                      | 11.870            | .950062             |
| 400.0                       | .0040                         | 400.0                                      | 11.970            | .958066             |
| 420.0                       | .0030                         | 420.0                                      | 12.040            | .963669             |
| 440.0                       | .0020                         | 440.0                                      | 12.090            | .967671             |
| 460.0                       | .0020                         | 460.0                                      | 12.130            | .970872             |
| 480.0                       | .0010                         | 480.0                                      | 12.160            | .973274             |
| 500.0                       | .0010                         | 500.0                                      | 12.180            | .974874             |
| 520.0                       | .0010                         | 520.0                                      | 12.200            | .976475             |
| 540.0                       | .0010                         | 540.0                                      | 12.220            | .978076             |
| 560.0                       | .0000                         | 560.0                                      | 12.230            | .978876             |

MIRAN VAPOR ANALYZER .25 ABSORBANCE UNITS PER VOLT

TABLE B-21

EVAPORATION EXPERIMENT NO. BLF5 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

## OUTPUT VOLTAGE DATA FROM MIRAN IA VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES |                   |                     |
|-----------------------------|-------------------------------|--|-------------------|---------------------|
|                             |                               | ELAPSED TIME<br>MINUTES                    | TOTAL<br>VOLT.MIN | TOTAL<br>NORMALIZED |
| .0                          | .0790                         | .0   | .000              | .000000             |
| 30.0                        | .0720                         | 30.0                                       | 2.265             | .054741             |
| 60.0                        | .0670                         | 60.0                                       | 4.350             | .105132             |
| 90.0                        | .0650                         | 90.0                                       | 6.330             | .152985             |
| 120.0                       | .0630                         | 120.0                                      | 8.250             | .199388             |
| 150.0                       | .0610                         | 150.0                                      | 10.110            | .244342             |
| 180.0                       | .0600                         | 180.0                                      | 11.925            | .288207             |
| 210.0                       | .0580                         | 210.0                                      | 13.695            | .330985             |
| 240.0                       | .0560                         | 240.0                                      | 15.405            | .372313             |
| 270.0                       | .0540                         | 270.0                                      | 17.055            | .412190             |
| 300.0                       | .0520                         | 300.0                                      | 18.645            | .450618             |
| 330.0                       | .0500                         | 330.0                                      | 20.175            | .487596             |
| 360.0                       | .0470                         | 360.0                                      | 21.630            | .522760             |
| 390.0                       | .0440                         | 390.0                                      | 22.995            | .555750             |
| 420.0                       | .0410                         | 420.0                                      | 24.270            | .586565             |
| 450.0                       | .0380                         | 450.0                                      | 25.455            | .615204             |
| 480.0                       | .0350                         | 480.0                                      | 26.550            | .641668             |
| 510.0                       | .0320                         | 510.0                                      | 27.555            | .665958             |
| 540.0                       | .0300                         | 540.0                                      | 28.485            | .688434             |
| 570.0                       | .0270                         | 570.0                                      | 29.340            | .709098             |
| 600.0                       | .0240                         | 600.0                                      | 30.105            | .727587             |
| 630.0                       | .0210                         | 630.0                                      | 30.780            | .743900             |
| 660.0                       | .0180                         | 660.0                                      | 31.365            | .758039             |
| 690.0                       | .0150                         | 690.0                                      | 31.860            | .770002             |
| 720.0                       | .0120                         | 720.0                                      | 32.265            | .779790             |
| 750.0                       | .0100                         | 750.0                                      | 32.595            | .787766             |
| 780.0                       | .0090                         | 780.0                                      | 32.880            | .794654             |
| 810.0                       | .0080                         | 810.0                                      | 33.135            | .800817             |
| 840.0                       | .0070                         | 840.0                                      | 33.360            | .806254             |
| 870.0                       | .0060                         | 870.0                                      | 33.555            | .810967             |
| 900.0                       | .0050                         | 900.0                                      | 33.720            | .814955             |
| 930.0                       | .0030                         | 930.0                                      | 33.840            | .817855             |
| 960.0                       | .0030                         | 960.0                                      | 33.930            | .820030             |
| 990.0                       | .0030                         | 990.0                                      | 34.020            | .822206             |
| 1020.0                      | .0020                         | 1020.0                                     | 34.095            | .824018             |
| 1050.0                      | .0020                         | 1050.0                                     | 34.155            | .825468             |
| 1080.0                      | .0010                         | 1080.0                                     | 34.200            | .826556             |
| 1110.0                      | .0010                         | 1110.0                                     | 34.230            | .827281             |
| 1140.0                      | .0000                         | 1140.0                                     | 34.245            | .827643             |

MIRAN VAPOR ANALYZER .25 ABSORBANCE UNITS PER VOLT

TABLE B-22

EVAPORATION EXPERIMENT NO. BLF6 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 2.9 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

## OUTPUT VOLTAGE DATA FROM MIRAN IA VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES |                   |                     |
|-----------------------------|-------------------------------|--|-------------------|---------------------|
|                             |                               | ELAPSED TIME<br>MINUTES                    | TOTAL<br>VOLT.MIN | TOTAL<br>NORMALIZED |
| .0                          | .0820                         | .0   | .000              | .000000             |
| 40.0                        | .0790                         | 40.0                                       | 3.220             | .072106             |
| 80.0                        | .0770                         | 80.0                                       | 6.340             | .141972             |
| 120.0                       | .0730                         | 120.0                                      | 9.340             | .209151             |
| 160.0                       | .0710                         | 160.0                                      | 12.220            | .273643             |
| 200.0                       | .0680                         | 200.0                                      | 15.000            | .335896             |
| 240.0                       | .0650                         | 240.0                                      | 17.660            | .395462             |
| 280.0                       | .0620                         | 280.0                                      | 20.200            | .452340             |
| 320.0                       | .0590                         | 320.0                                      | 22.620            | .506532             |
| 360.0                       | .0560                         | 360.0                                      | 24.920            | .558036             |
| 400.0                       | .0530                         | 400.0                                      | 27.100            | .606853             |
| 440.0                       | .0490                         | 440.0                                      | 29.140            | .652534             |
| 480.0                       | .0440                         | 480.0                                      | 31.000            | .694186             |
| 520.0                       | .0390                         | 520.0                                      | 32.660            | .731358             |
| 560.0                       | .0350                         | 560.0                                      | 34.140            | .764500             |
| 600.0                       | .0300                         | 600.0                                      | 35.440            | .793611             |
| 640.0                       | .0250                         | 640.0                                      | 36.540            | .818243             |
| 680.0                       | .0200                         | 680.0                                      | 37.440            | .838397             |
| 720.0                       | .0170                         | 720.0                                      | 38.180            | .854968             |
| 760.0                       | .0140                         | 760.0                                      | 38.800            | .868852             |
| 800.0                       | .0120                         | 800.0                                      | 39.320            | .880496             |
| 840.0                       | .0100                         | 840.0                                      | 39.760            | .890349             |
| 880.0                       | .0080                         | 880.0                                      | 40.120            | .898411             |
| 920.0                       | .0070                         | 920.0                                      | 40.420            | .905128             |
| 960.0                       | .0060                         | 960.0                                      | 40.680            | .910951             |
| 1000.0                      | .0050                         | 1000.0                                     | 40.900            | .915877             |
| 1040.0                      | .0040                         | 1040.0                                     | 41.080            | .919908             |
| 1080.0                      | .0030                         | 1080.0                                     | 41.220            | .923043             |
| 1120.0                      | .0020                         | 1120.0                                     | 41.320            | .925282             |
| 1160.0                      | .0020                         | 1160.0                                     | 41.400            | .927074             |
| 1200.0                      | .0010                         | 1200.0                                     | 41.460            | .928417             |
| 1240.0                      | .0000                         | 1240.0                                     | 41.480            | .928865             |

MIRAN VAPOR ANALYZER .25 ABSORBANCE UNITS PER VOLT

TABLE B-23

EVAPORATION EXPERIMENT NO. RLF7 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

## OUTPUT VOLTAGE DATA FROM MIRAN 1A VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES |          |            |
|-----------------------------|-------------------------------|--|----------|------------|
|                             |                               | ELAPSED TIME                               | TOTAL    | TOTAL      |
|                             |                               | MINUTES                                    | VOLT*MIN | NORMALIZED |
| .0                          | .0440                         | .0   | .000     | .000000    |
| 15.0                        | .0430                         | 15.0                                       | .653     | .060451    |
| 30.0                        | .0410                         | 30.0                                       | 1.283    | .118817    |
| 45.0                        | .0400                         | 45.0                                       | 1.890    | .175099    |
| 60.0                        | .0390                         | 60.0                                       | 2.483    | .229992    |
| 75.0                        | .0370                         | 75.0                                       | 3.053    | .282799    |
| 90.0                        | .0350                         | 90.0                                       | 3.592    | .332828    |
| 105.0                       | .0340                         | 105.0                                      | 4.110    | .380772    |
| 120.0                       | .0320                         | 120.0                                      | 4.600    | .426631    |
| 135.0                       | .0310                         | 135.0                                      | 5.077    | .470406    |
| 150.0                       | .0300                         | 150.0                                      | 5.535    | .512791    |
| 165.0                       | .0280                         | 165.0                                      | 5.970    | .553092    |
| 180.0                       | .0270                         | 180.0                                      | 6.382    | .591303    |
| 195.0                       | .0250                         | 195.0                                      | 6.772    | .627439    |
| 210.0                       | .0230                         | 210.0                                      | 7.132    | .660792    |
| 225.0                       | .0210                         | 225.0                                      | 7.462    | .691364    |
| 240.0                       | .0190                         | 240.0                                      | 7.762    | .719158    |
| 255.0                       | .0160                         | 255.0                                      | 8.025    | .743477    |
| 270.0                       | .0140                         | 270.0                                      | 8.250    | .764323    |
| 285.0                       | .0130                         | 285.0                                      | 8.453    | .783083    |
| 300.0                       | .0110                         | 300.0                                      | 8.633    | .797759    |
| 315.0                       | .0090                         | 315.0                                      | 8.783    | .813656    |
| 330.0                       | .0080                         | 330.0                                      | 8.910    | .825468    |
| 345.0                       | .0070                         | 345.0                                      | 9.023    | .835891    |
| 360.0                       | .0060                         | 360.0                                      | 9.120    | .844924    |
| 375.0                       | .0050                         | 375.0                                      | 9.203    | .852567    |
| 390.0                       | .0040                         | 390.0                                      | 9.270    | .858821    |
| 405.0                       | .0030                         | 405.0                                      | 9.323    | .863684    |
| 420.0                       | .0030                         | 420.0                                      | 9.368    | .867854    |
| 435.0                       | .0020                         | 435.0                                      | 9.405    | .871328    |
| 450.0                       | .0020                         | 450.0                                      | 9.435    | .874107    |
| 465.0                       | .0010                         | 465.0                                      | 9.458    | .876192    |
| 480.0                       | .0010                         | 480.0                                      | 9.473    | .877501    |
| 495.0                       | .0010                         | 495.0                                      | 9.488    | .878971    |
| 510.0                       | .0000                         | 510.0                                      | 9.495    | .879666    |

MIRAN VAPOR ANALYZER .025 ABSORBANCE UNITS PER VOLT



TABLE B-24

EVAPORATION EXPERIMENT NO. BLF8 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 50%

## OUTPUT VOLTAGE DATA FROM MIRAN 1A VAPOR ANALYZER

| ANALYZER<br>TIME<br>MINUTES | OUTPUT<br>ABSORBANCE<br>VOLTS | CUMULATIVE DISTRIBUTION FOR TWO SUBSTRATES |          |            |
|-----------------------------|-------------------------------|--|----------|------------|
|                             |                               | ELAPSED TIME                               | TOTAL    | TOTAL      |
|                             |                               | MINUTES                                    | VOLT.MIN | NORMALIZED |
| .0                          | .0500                         | .0   | .000     | .000000    |
| 15.0                        | .0480                         | 15.0                                       | .735     | .059113    |
| 30.0                        | .0460                         | 30.0                                       | 1.440    | .115813    |
| 45.0                        | .0440                         | 45.0                                       | 2.115    | .170100    |
| 60.0                        | .0420                         | 60.0                                       | 2.760    | .221975    |
| 75.0                        | .0410                         | 75.0                                       | 3.382    | .272040    |
| 90.0                        | .0400                         | 90.0                                       | 3.990    | .320898    |
| 105.0                       | .0380                         | 105.0                                      | 4.575    | .367947    |
| 120.0                       | .0370                         | 120.0                                      | 5.137    | .413187    |
| 135.0                       | .0360                         | 135.0                                      | 5.685    | .457220    |
| 150.0                       | .0350                         | 150.0                                      | 6.217    | .500046    |
| 165.0                       | .0340                         | 165.0                                      | 6.735    | .541666    |
| 180.0                       | .0330                         | 180.0                                      | 7.237    | .582080    |
| 195.0                       | .0320                         | 195.0                                      | 7.725    | .621288    |
| 210.0                       | .0300                         | 210.0                                      | 8.190    | .658686    |
| 225.0                       | .0290                         | 225.0                                      | 8.632    | .694274    |
| 240.0                       | .0270                         | 240.0                                      | 9.052    | .728053    |
| 255.0                       | .0260                         | 255.0                                      | 9.450    | .760022    |
| 270.0                       | .0250                         | 270.0                                      | 9.832    | .790785    |
| 285.0                       | .0210                         | 285.0                                      | 10.177   | .818532    |
| 300.0                       | .0190                         | 300.0                                      | 10.477   | .842659    |
| 315.0                       | .0170                         | 315.0                                      | 10.748   | .864374    |
| 330.0                       | .0150                         | 330.0                                      | 10.988   | .883676    |
| 345.0                       | .0130                         | 345.0                                      | 11.198   | .900566    |
| 360.0                       | .0110                         | 360.0                                      | 11.378   | .915042    |
| 375.0                       | .0090                         | 375.0                                      | 11.528   | .927106    |
| 390.0                       | .0070                         | 390.0                                      | 11.648   | .936757    |
| 405.0                       | .0050                         | 405.0                                      | 11.738   | .943996    |
| 420.0                       | .0040                         | 420.0                                      | 11.805   | .949424    |
| 435.0                       | .0020                         | 435.0                                      | 11.850   | .953044    |
| 450.0                       | .0010                         | 450.0                                      | 11.873   | .954853    |
| 465.0                       | .0010                         | 465.0                                      | 11.888   | .956060    |
| 480.0                       | .0000                         | 480.0                                      | 11.895   | .956663    |

MIRAN VAPOR ANALYZER .025 ABSORBANCE UNITS PER VOLT

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APPENDIX C

VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS

TABLE C. 1

EVAPORATION EXPERIMENT NO. GLF1 SERIES 1D 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/TOP SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 45%

VAPOR CONTAMINATION FROM A UNIFORM APRAY OF DEPOSITED DROPLETS  
 (PPM/AB BASED ON MASS BALANCE)

| ELAPSED<br>TIME<br>MINUTES | PPM   | MICROGRAMS<br>PER<br>CUBIC<br>METER | *<br>PER<br>METER<br>SQUARED | *<br>PER<br>GRAM/<br>METER SQD | PPM<br>PER<br>DROP | MICROGRAMS<br>PER<br>CUBIC METER<br>PER DROP |
|----------------------------|-------|-------------------------------------|------------------------------|--------------------------------|--------------------|--|
| .0                         | 2.208 | 13861.830                           | 40926.560                    | 498.570                        | .00150             | 9.417  |
| 30.0                       | 2.001 | 12562.280                           | 37089.690                    | 451.829                        | .00136             | 8.534  |
| 60.0                       | 1.742 | 10937.850                           | 32293.610                    | 393.403                        | .00118             | 7.431  |
| 90.0                       | 1.587 | 9963.187                            | 29415.960                    | 358.347                        | .00108             | 6.768  |
| 120.0                      | 1.449 | 9096.822                            | 26855.050                    | 327.186                        | .00098             | 6.180  |
| 150.0                      | 1.328 | 8338.754                            | 24619.880                    | 299.921                        | .00090             | 5.665  |
| 180.0                      | 1.173 | 7364.095                            | 21742.230                    | 264.865                        | .00080             | 5.003  |
| 210.0                      | 1.087 | 6822.617                            | 20143.540                    | 245.390                        | .00074             | 4.635  |
| 240.0                      | .983  | 6172.844                            | 18225.110                    | 222.019                        | .00067             | 4.194  |
| 270.0                      | .880  | 5523.071                            | 16306.670                    | 198.649                        | .00060             | 3.752  |
| 300.0                      | .794  | 4981.593                            | 14707.980                    | 179.174                        | .00054             | 3.384  |
| 330.0                      | .707  | 4440.116                            | 13109.290                    | 159.698                        | .00048             | 3.016  |
| 360.0                      | .621  | 3898.638                            | 11510.590                    | 140.223                        | .00042             | 2.649  |
| 390.0                      | .552  | 3455.450                            | 10231.640                    | 124.642                        | .00038             | 2.354  |
| 420.0                      | .483  | 3032.274                            | 8952.685                     | 109.062                        | .00033             | 2.060  |
| 450.0                      | .397  | 2490.797                            | 7353.991                     | 89.587                         | .00027             | 1.692  |
| 480.0                      | .328  | 2057.615                            | 6075.036                     | 74.006                         | .00022             | 1.318  |
| 510.0                      | .259  | 1624.432                            | 4796.081                     | 58.426                         | .00018             | 1.104  |
| 540.0                      | .207  | 1292.546                            | 3836.865                     | 46.741                         | .00014             | .883   |
| 570.0                      | .172  | 1082.955                            | 3197.387                     | 38.951                         | .00012             | .736   |
| 600.0                      | .138  | 866.364                             | 2557.910                     | 31.161                         | .00009             | .589   |
| 630.0                      | .104  | 649.773                             | 1918.432                     | 23.370                         | .00007             | .441   |
| 660.0                      | .086  | 541.477                             | 1598.693                     | 19.475                         | .00006             | .368   |
| 690.0                      | .069  | 433.182                             | 1278.955                     | 15.580                         | .00005             | .294   |
| 720.0                      | .052  | 324.887                             | 959.216                      | 11.685                         | .00004             | .221   |
| 750.0                      | .035  | 216.591                             | 639.477                      | 7.790                          | .00002             | .147   |
| 780.0                      | .035  | 216.591                             | 639.477                      | 7.790                          | .00002             | .147   |
| 810.0                      | .017  | 108.296                             | 319.739                      | 3.895                          | .00001             | .074   |
| 840.0                      | .017  | 108.296                             | 319.739                      | 3.895                          | .00001             | .074   |
| 870.0                      | .000  | .000                                | .000                         | .000                           | .00000             | .000   |

\* MICROGRAMS PER CUBIC METER

TABLE C-2

EVAPORATION EXPERIMENT NO. GLF2 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON MICROCRY/TOP SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 39%

| VAPOUR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS<br>(PPM/AB BASED ON MIRAN CALIBRATION DATA) |       |                                     |                              |                                |                    |  |
|---|-------|-------------------------------------|------------------------------|--------------------------------|--------------------|--|
| ELAPSED<br>TIME   | PPM   | MICROGRAMS<br>PER<br>CUBIC<br>METER | *<br>PER<br>METER<br>SQUARED | *<br>PER<br>GRAM/<br>METER SQD | PPM<br>PER<br>DROP | MICROGRAMS<br>PER<br>CUBIC METER<br>PER DROP |
| HOURS   |       |                                     |                              |                                |                    |  |
| .0  | 1.949 | 12237.390                           | 36130.470                    | 413.780                        | .00132             | 8.513  |
| 30.0  | 1.811 | 11371.030                           | 33572.560                    | 384.486                        | .00123             | 7.725  |
| 60.0  | 1.673 | 10504.660                           | 31014.660                    | 355.191                        | .00114             | 7.136  |
| 90.0  | 1.553 | 9746.595                            | 28776.480                    | 329.559                        | .00105             | 6.621  |
| 120.0   | 1.449 | 9096.822                            | 26858.050                    | 307.588                        | .00098             | 6.186  |
| 150.0   | 1.363 | 8555.345                            | 25259.360                    | 289.280                        | .00093             | 5.812  |
| 180.0   | 1.259 | 7905.571                            | 23340.920                    | 267.309                        | .00086             | 5.371  |
| 210.0   | 1.173 | 7364.095                            | 21742.230                    | 249.000                        | .00080             | 5.003  |
| 240.0   | 1.104 | 6930.913                            | 20463.280                    | 234.353                        | .00075             | 4.709  |
| 270.0   | 1.018 | 6389.435                            | 18864.580                    | 216.044                        | .00069             | 4.341  |
| 300.0   | .932  | 5847.957                            | 17265.890                    | 197.735                        | .00063             | 3.973  |
| 330.0   | .863  | 5414.775                            | 15986.940                    | 183.088                        | .00059             | 3.679  |
| 360.0   | .794  | 4981.593                            | 14707.980                    | 168.441                        | .00054             | 3.384  |
| 390.0   | .725  | 4548.411                            | 13429.030                    | 153.794                        | .00049             | 3.090  |
| 420.0   | .655  | 4115.229                            | 12150.070                    | 139.147                        | .00045             | 2.796  |
| 450.0   | .587  | 3682.047                            | 10871.120                    | 124.500                        | .00040             | 2.501  |
| 480.0   | .517  | 3248.865                            | 9592.161                     | 109.853                        | .00035             | 2.207  |
| 510.0   | .449  | 2815.683                            | 8313.207                     | 95.206                         | .00030             | 1.913  |
| 540.0   | .380  | 2382.501                            | 7034.251                     | 80.559                         | .00026             | 1.619  |
| 570.0   | .328  | 2057.615                            | 6075.036                     | 69.574                         | .00022             | 1.398  |
| 600.0   | .276  | 1732.728                            | 5115.820                     | 58.588                         | .00019             | 1.177  |
| 630.0   | .224  | 1407.842                            | 4156.604                     | 47.603                         | .00015             | .956   |
| 660.0   | .190  | 1191.250                            | 3517.126                     | 40.279                         | .00013             | .809   |
| 690.0   | .172  | 1082.955                            | 3197.387                     | 36.618                         | .00012             | .736   |
| 720.0   | .138  | 866.364                             | 2557.910                     | 29.294                         | .00009             | .589   |
| 750.0   | .121  | 758.069                             | 2238.171                     | 25.632                         | .00008             | .515   |
| 780.0   | .121  | 758.069                             | 2238.171                     | 25.632                         | .00008             | .515   |
| 810.0   | .104  | 649.773                             | 1918.432                     | 21.971                         | .00007             | .441   |
| 840.0   | .086  | 541.477                             | 1598.693                     | 18.309                         | .00006             | .368   |
| 870.0   | .069  | 433.182                             | 1278.955                     | 14.647                         | .00005             | .294   |
| 900.0   | .052  | 324.887                             | 959.216                      | 10.985                         | .00004             | .221   |
| 930.0   | .035  | 216.591                             | 639.477                      | 7.324                          | .00002             | .147   |
| 960.0   | .017  | 108.296                             | 319.739                      | 3.662                          | .00001             | .074   |
| 990.0   | .017  | 108.296                             | 319.739                      | 3.662                          | .00001             | .074   |
| 1020.0  | .000  | .000                                | .000                         | .000                           | .00000             | .000   |

\* MICROGRAMS PER CUBIC METER

TABLE C-3

EVAPORATION EXPERIMENT NO. GLF3 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/50 METER ON HICKORY/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 40%

VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS  
 (PPM/AB BASED ON MASS BALANCE)

| ELAPSED<br>TIME<br>MINUTES | PPM   | MICROGRAMS<br>PER<br>CUBIC<br>METER | *<br>PER<br>METER<br>SQUARED | *<br>PER<br>GRAM/<br>METER SQD | PPM    | MICROGRAMS<br>PER<br>CUBIC METER<br>PER DROP |
|----------------------------|-------|-------------------------------------|------------------------------|--------------------------------|--------|--|
| .0                         | 1.484 | 9313.413                            | 27497.530                    | 374.175                        | .00101 | 6.327  |
| 15.0                       | 1.294 | 8122.163                            | 23980.400                    | 326.838                        | .00088 | 5.518  |
| 30.0                       | 1.138 | 7147.503                            | 21102.750                    | 287.618                        | .00077 | 4.856  |
| 45.0                       | 1.018 | 6389.435                            | 18864.580                    | 257.113                        | .00069 | 4.341  |
| 60.0                       | .897  | 5631.366                            | 16626.4                      | 226.608                        | .00061 | 3.826  |
| 75.0                       | .794  | 4981.593                            | 15107.980                    | 200.461                        | .00054 | 3.384  |
| 90.0                       | .707  | 4440.116                            | 13109.290                    | 178.672                        | .00048 | 3.016  |
| 105.0                      | .621  | 3898.638                            | 11510.590                    | 156.882                        | .00042 | 2.649  |
| 120.0                      | .535  | 3357.160                            | 9911.059                     | 135.093                        | .00036 | 2.281  |
| 135.0                      | .449  | 2815.683                            | 8313.207                     | 113.304                        | .00030 | 1.913  |
| 150.0                      | .362  | 2274.206                            | 6714.513                     | 91.515                         | .00025 | 1.545  |
| 165.0                      | .310  | 1949.319                            | 5755.297                     | 78.441                         | .00021 | 1.324  |
| 180.0                      | .259  | 1624.432                            | 4796.081                     | 65.368                         | .00018 | 1.104  |
| 195.0                      | .207  | 1299.546                            | 3836.805                     | 52.294                         | .00014 | .883   |
| 210.0                      | .155  | 974.559                             | 2877.648                     | 39.221                         | .00011 | .662   |
| 225.0                      | .121  | 758.069                             | 2238.171                     | 30.503                         | .00008 | .515   |
| 240.0                      | .086  | 541.477                             | 1598.693                     | 21.789                         | .00006 | .368   |
| 255.0                      | .069  | 435.182                             | 1278.955                     | 17.431                         | .00005 | .294   |
| 270.0                      | .069  | 433.182                             | 1278.955                     | 17.431                         | .00005 | .294   |
| 285.0                      | .052  | 324.887                             | 959.216                      | 13.074                         | .00004 | .221   |
| 300.0                      | .052  | 324.887                             | 959.216                      | 13.074                         | .00004 | .221   |
| 315.0                      | .033  | 216.591                             | 639.477                      | 8.716                          | .00002 | .147   |
| 330.0                      | .017  | 108.295                             | 319.739                      | 4.358                          | .00001 | .074   |
| 345.0                      | .017  | 108.295                             | 319.739                      | 4.358                          | .00001 | .074   |
| 360.0                      | .000  | .000                                | .000                         | .000                           | .00000 | .000   |

\* MICROGRAMS PER CUBIC METER

TABLE C-4

EVAPORATION EXPERIMENT NO. GLF4 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

## VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS

(PPM/AB BASED ON MASS BALANCE)

| ELAPSED<br>TIME<br>MINUTES | PPM   | MICROGRAMS<br>PER<br>CUBIC<br>METER | *<br>PER<br>METER<br>SQUARED | *<br>PER<br>GRAM/<br>METER SQD | PPM<br>PER<br>DROP | MICROGRAMS<br>PER<br>CUBIC METER<br>PER DROP |
|----------------------------|-------|-------------------------------------|------------------------------|--------------------------------|--------------------|--|
| .0                         | 1.259 | 7905.571                            | 23340.920                    | 267.309                        | .00086             | 5.371  |
| 10.0                       | 1.242 | 7797.276                            | 23021.190                    | 263.647                        | .00084             | 5.297  |
| 20.0                       | 1.225 | 7688.981                            | 22701.450                    | 259.986                        | .00083             | 5.223  |
| 30.0                       | 1.173 | 7364.095                            | 21742.230                    | 249.000                        | .00080             | 5.003  |
| 40.0                       | 1.104 | 6930.913                            | 20463.280                    | 234.353                        | .00075             | 4.709  |
| 50.0                       | 1.035 | 6497.730                            | 19184.320                    | 219.706                        | .00070             | 4.414  |
| 60.0                       | 1.000 | 6281.139                            | 18544.840                    | 212.382                        | .00068             | 4.267  |
| 70.0                       | .949  | 5956.252                            | 17585.630                    | 201.397                        | .00064             | 4.046  |
| 80.0                       | .897  | 5631.366                            | 16626.410                    | 190.412                        | .00061             | 3.826  |
| 90.0                       | .845  | 5306.479                            | 15667.200                    | 179.427                        | .00057             | 3.605  |
| 100.0                      | .811  | 5089.838                            | 15027.720                    | 172.103                        | .00055             | 3.458  |
| 110.0                      | .759  | 4765.002                            | 14068.500                    | 161.118                        | .00052             | 3.237  |
| 120.0                      | .707  | 4440.116                            | 13109.290                    | 150.132                        | .00048             | 3.016  |
| 130.0                      | .673  | 4223.524                            | 12469.810                    | 142.809                        | .00046             | 2.869  |
| 140.0                      | .638  | 4006.933                            | 11830.330                    | 135.485                        | .00043             | 2.722  |
| 150.0                      | .587  | 3682.047                            | 10871.120                    | 124.500                        | .00040             | 2.501  |
| 160.0                      | .552  | 3465.456                            | 10231.640                    | 117.177                        | .00038             | 2.354  |
| 170.0                      | .517  | 3248.865                            | 9592.161                     | 109.853                        | .00035             | 2.207  |
| 180.0                      | .483  | 3032.274                            | 8952.685                     | 102.529                        | .00033             | 2.060  |
| 190.0                      | .449  | 2815.683                            | 8313.207                     | 95.206                         | .00030             | 1.913  |
| 200.0                      | .414  | 2599.092                            | 7673.729                     | 87.882                         | .00028             | 1.766  |
| 210.0                      | .380  | 2382.501                            | 7034.251                     | 80.559                         | .00026             | 1.619  |
| 220.0                      | .345  | 2165.910                            | 6394.774                     | 73.235                         | .00023             | 1.471  |
| 230.0                      | .310  | 1949.319                            | 5755.257                     | 65.912                         | .00021             | 1.324  |
| 240.0                      | .276  | 1732.728                            | 5115.820                     | 58.588                         | .00019             | 1.177  |
| 250.0                      | .242  | 1515.137                            | 4476.342                     | 51.265                         | .00016             | 1.030  |
| 260.0                      | .224  | 1407.842                            | 4156.604                     | 47.603                         | .00015             | .956   |
| 270.0                      | .190  | 1191.250                            | 3517.126                     | 40.279                         | .00013             | .809   |
| 280.0                      | .155  | 974.659                             | 2877.648                     | 32.956                         | .00011             | .662   |
| 290.0                      | .138  | 866.364                             | 2557.910                     | 29.294                         | .00009             | .589   |
| 300.0                      | .121  | 758.069                             | 2238.171                     | 25.632                         | .00008             | .515   |
| 310.0                      | .104  | 649.773                             | 1918.432                     | 21.971                         | .00007             | .441   |
| 320.0                      | .086  | 541.477                             | 1598.693                     | 18.309                         | .00005             | .368   |
| 330.0                      | .069  | 433.182                             | 1278.955                     | 14.647                         | .00005             | .290   |
| 340.0                      | .035  | 216.591                             | 639.477                      | 7.324                          | .00002             | .147   |
| 350.0                      | .035  | 216.591                             | 639.477                      | 7.324                          | .00002             | .147   |
| 360.0                      | .017  | 108.296                             | 319.739                      | 3.662                          | .00001             | .074   |
| 370.0                      | .000  | .000                                | .000                         | .000                           | .00000             | .000   |

\* MICROGRAMS PER CUBIC METER

TABLE C-5

EVAPORATION EXPERIMENT NO. GLFS SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 50 GMS/SQ METER ON HICKORY/BOTTOM SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 58%

VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS  
 (PPM/AB BASED ON MASS BALANCE)

| ELAPSED<br>TIME<br><br>MINUTES | PPM   | MICROGRAMS<br>PER<br>CUBIC<br>METER | *<br>PER<br>METER<br>SQUARED | *<br>PER<br>GRAM/<br>METER SQD | PPM    | MICROGRAMS<br>PER<br>CUBIC METER<br>PER DROP |
|--------------------------------|-------|-------------------------------------|------------------------------|--------------------------------|--------|--|
| .0                             | 1.345 | 8447.049                            | 23939.620                    | 339.912                        | .00091 | 5.738  |
| 30.0                           | 1.276 | 8013.867                            | 23660.660                    | 322.480                        | .00087 | 5.444  |
| 60.0                           | 1.225 | 7688.981                            | 22701.450                    | 309.407                        | .00083 | 5.223  |
| 90.0                           | 1.156 | 7255.799                            | 21422.400                    | 291.976                        | .00079 | 4.929  |
| 120.0                          | 1.087 | 6822.617                            | 20143.540                    | 274.544                        | .00074 | 4.635  |
| 150.0                          | 1.035 | 6497.730                            | 19184.320                    | 261.471                        | .00073 | 4.414  |
| 180.0                          | .966  | 6064.548                            | 17905.370                    | 244.039                        | .00066 | 4.120  |
| 210.0                          | .914  | 5739.662                            | 16946.150                    | 230.966                        | .00062 | 3.899  |
| 240.0                          | .863  | 5414.775                            | 15986.940                    | 217.892                        | .00059 | 3.679  |
| 270.0                          | .811  | 5089.888                            | 15027.720                    | 204.819                        | .00055 | 3.458  |
| 300.0                          | .759  | 4765.002                            | 14068.500                    | 191.745                        | .00052 | 3.237  |
| 330.0                          | .690  | 4331.820                            | 12789.550                    | 174.314                        | .00047 | 2.943  |
| 360.0                          | .621  | 3898.638                            | 11510.590                    | 156.882                        | .00042 | 2.649  |
| 390.0                          | .569  | 3573.751                            | 10551.380                    | 143.809                        | .00039 | 2.428  |
| 420.0                          | .517  | 3248.865                            | 9592.161                     | 130.735                        | .00035 | 2.207  |
| 450.0                          | .483  | 3032.274                            | 8952.685                     | 122.020                        | .00033 | 2.060  |
| 480.0                          | .431  | 2707.387                            | 7993.468                     | 108.946                        | .00029 | 1.839  |
| 510.0                          | .397  | 2490.797                            | 7353.991                     | 100.230                        | .00027 | 1.692  |
| 540.0                          | .362  | 2274.206                            | 6714.513                     | 91.515                         | .00025 | 1.545  |
| 570.0                          | .310  | 1949.319                            | 5755.297                     | 78.441                         | .00021 | 1.324  |
| 600.0                          | .276  | 1732.728                            | 5115.820                     | 69.726                         | .00019 | 1.177  |
| 630.0                          | .224  | 1407.842                            | 4156.604                     | 56.652                         | .00015 | .956   |
| 660.0                          | .190  | 1191.250                            | 3517.126                     | 47.936                         | .00013 | .809   |
| 690.0                          | .138  | 866.364                             | 2557.910                     | 34.863                         | .00009 | .589   |
| 720.0                          | .104  | 649.773                             | 1918.432                     | 26.147                         | .00007 | .441   |
| 750.0                          | .069  | 433.182                             | 1278.955                     | 17.431                         | .00005 | .294   |
| 780.0                          | .052  | 324.087                             | 959.216                      | 13.074                         | .00004 | .221   |
| 810.0                          | .035  | 216.591                             | 639.477                      | 8.716                          | .00002 | .147   |
| 840.0                          | .017  | 108.296                             | 319.739                      | 4.358                          | .00001 | .074   |
| 870.0                          | .000  | .000                                | .000                         | .000                           | .00000 | .000   |

\* MICROGRAMS PER CUBIC METER



TABLE C-6

EVAPORATION EXPERIMENT NO. GLF6 SERIES ID 2774 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/BOTTOM SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 55%

VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS  
 (PPM/AB BASED ON MASS BALANCE)

| ELAPSED<br>TIME<br><br>MINUTES | PPM   | MICROGRAMS<br>PER<br>CUBIC<br>METER | *<br>PER<br>METER<br>SQUARED | *<br>PER<br>GRAM/<br>METER SQD | PPM    | MICROGRAMS<br>PER<br>CUBIC METER<br>PER DROP |
|--------------------------------|-------|-------------------------------------|------------------------------|--------------------------------|--------|--|
| 0                              | 1.311 | 8230.457                            | 24300.140                    | 296.026                        | .00089 | 5.591  |
| 30.0                           | 1.276 | 8013.866                            | 23660.660                    | 288.236                        | .00087 | 5.444  |
| 60.0                           | 1.225 | 7688.980                            | 22701.450                    | 276.550                        | .00083 | 5.223  |
| 90.0                           | 1.207 | 7580.684                            | 22381.710                    | 272.655                        | .00082 | 5.150  |
| 120.0                          | 1.138 | 7147.502                            | 21102.750                    | 257.975                        | .00077 | 4.856  |
| 150.0                          | 1.104 | 6930.912                            | 20463.280                    | 249.285                        | .00075 | 4.708  |
| 180.0                          | 1.069 | 6714.320                            | 19823.800                    | 241.495                        | .00073 | 4.561  |
| 210.0                          | 1.018 | 6339.434                            | 18864.580                    | 229.810                        | .00069 | 4.341  |
| 240.0                          | .966  | 6064.547                            | 17905.370                    | 218.124                        | .00066 | 4.120  |
| 270.0                          | .914  | 5739.661                            | 16946.150                    | 206.439                        | .00062 | 3.899  |
| 300.0                          | .862  | 5414.774                            | 15986.930                    | 194.754                        | .00059 | 3.679  |
| 330.0                          | .811  | 5089.883                            | 15027.720                    | 183.069                        | .00055 | 3.458  |
| 360.0                          | .759  | 4765.001                            | 14068.500                    | 171.383                        | .00052 | 3.237  |
| 390.0                          | .707  | 4440.115                            | 13109.290                    | 159.698                        | .00048 | 3.016  |
| 420.0                          | .655  | 4115.229                            | 12150.070                    | 148.013                        | .00045 | 2.796  |
| 450.0                          | .604  | 3790.342                            | 11190.850                    | 136.328                        | .00041 | 2.575  |
| 480.0                          | .552  | 3465.456                            | 10231.640                    | 124.647                        | .00038 | 2.354  |
| 510.0                          | .500  | 3140.569                            | 9272.422                     | 112.957                        | .00034 | 2.134  |
| 540.0                          | .448  | 2815.683                            | 8313.205                     | 101.272                        | .00030 | 1.913  |
| 570.0                          | .397  | 2490.796                            | 7353.989                     | 89.587                         | .00027 | 1.692  |
| 600.0                          | .345  | 2165.910                            | 6394.774                     | 77.902                         | .00023 | .471   |
| 630.0                          | .293  | 1841.023                            | 5435.558                     | 66.216                         | .00020 | 1.251  |
| 660.0                          | .241  | 1516.137                            | 4476.341                     | 54.531                         | .00016 | 1.030  |
| 690.0                          | .190  | 1191.250                            | 3517.125                     | 42.846                         | .00013 | .809   |
| 720.0                          | .138  | 866.364                             | 2557.909                     | 31.161                         | .00009 | .589   |
| 750.0                          | .103  | 649.773                             | 1918.432                     | 23.370                         | .00007 | .441   |
| 780.0                          | .086  | 541.477                             | 1598.693                     | 19.475                         | .00006 | .368   |
| 810.0                          | .052  | 324.886                             | 959.216                      | 11.685                         | .00004 | .221   |
| 840.0                          | .034  | 216.591                             | 639.477                      | 7.790                          | .00002 | .147   |
| 870.0                          | .017  | 108.295                             | 319.739                      | 3.895                          | .00001 | .074   |
| 900.0                          | .000  | .000                                | .000                         | .000                           | .00000 | .000   |

\* MICROGRAMS PER CUBIC METER

TABLE C-7

EVAPORATION EXPERIMENT NO. GLF7 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/BOTTOM SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS  
 (PPM/AD BASED ON MIRAN CALIBRATION DATA)

| ELAPSED<br>TIME<br><br>MINUTES | PPM  | MICROGRAMS<br>PER<br>CUBIC<br>METER | *<br>PER<br>METER<br>SQUARED | *<br>PER<br>GRAM/<br>METER SQD | PPM<br>PER<br>DROP | MICROGRAMS<br>PER<br>CUBIC METER<br>PER DROP |
|--------------------------------|------|-------------------------------------|------------------------------|--------------------------------|--------------------|--|
| .0                             | .816 | 5122.848                            | 15125.030                    | 188.252                        | .00055             | 3.480  |
| 15.0                           | .765 | 4802.670                            | 14179.720                    | 176.486                        | .00052             | 3.263  |
| 30.0                           | .731 | 4589.218                            | 13549.510                    | 168.643                        | .00050             | 3.118  |
| 45.0                           | .714 | 4482.492                            | 13234.400                    | 164.721                        | .00049             | 3.045  |
| 60.0                           | .680 | 4269.040                            | 12604.190                    | 156.877                        | .00046             | 2.900  |
| 75.0                           | .646 | 4055.588                            | 11973.980                    | 149.033                        | .00044             | 2.755  |
| 90.0                           | .629 | 3948.862                            | 11658.880                    | 145.111                        | .00043             | 2.683  |
| 105.0                          | .595 | 3735.410                            | 11028.670                    | 137.267                        | .00040             | 2.538  |
| 120.0                          | .578 | 3628.684                            | 10713.560                    | 133.345                        | .00039             | 2.465  |
| 135.0                          | .544 | 3415.232                            | 10083.350                    | 125.501                        | .00037             | 2.320  |
| 150.0                          | .527 | 3308.506                            | 9768.250                     | 121.580                        | .00036             | 2.248  |
| 165.0                          | .493 | 3095.054                            | 9138.039                     | 113.736                        | .00033             | 2.103  |
| 180.0                          | .459 | 2881.602                            | 8507.830                     | 105.892                        | .00031             | 1.958  |
| 195.0                          | .442 | 2774.876                            | 8192.726                     | 101.970                        | .00030             | 1.885  |
| 210.0                          | .408 | 2561.424                            | 7562.516                     | 94.126                         | .00028             | 1.740  |
| 225.0                          | .374 | 2347.972                            | 6932.307                     | 86.282                         | .00025             | 1.595  |
| 240.0                          | .340 | 2134.520                            | 6302.096                     | 78.438                         | .00023             | 1.450  |
| 255.0                          | .306 | 1921.068                            | 5671.887                     | 70.595                         | .00021             | 1.305  |
| 270.0                          | .272 | 1707.616                            | 5041.677                     | 62.751                         | .00018             | 1.160  |
| 285.0                          | .238 | 1494.164                            | 4411.468                     | 54.907                         | .00016             | 1.015  |
| 300.0                          | .221 | 1387.438                            | 4096.363                     | 50.985                         | .00015             | .943   |
| 315.0                          | .187 | 1173.986                            | 3466.153                     | 43.141                         | .00013             | .798   |
| 330.0                          | .153 | 960.534                             | 2835.943                     | 35.297                         | .00010             | .653   |
| 345.0                          | .119 | 747.082                             | 2205.734                     | 27.453                         | .00008             | .508   |
| 360.0                          | .102 | 640.356                             | 1890.629                     | 23.532                         | .00007             | .435   |
| 375.0                          | .085 | 533.630                             | 1575.524                     | 19.610                         | .00006             | .363   |
| 390.0                          | .068 | 426.904                             | 1260.419                     | 15.688                         | .00005             | .290   |
| 405.0                          | .051 | 320.178                             | 945.314                      | 11.766                         | .00003             | .218   |
| 420.0                          | .034 | 213.452                             | 630.210                      | 7.844                          | .00002             | .145   |
| 435.0                          | .034 | 213.452                             | 630.210                      | 7.844                          | .00002             | .145   |
| 450.0                          | .017 | 106.726                             | 315.105                      | 3.922                          | .00001             | .073   |
| 465.0                          | .017 | 106.726                             | 315.105                      | 3.922                          | .00001             | .073   |
| 480.0                          | .000 | .000                                | .000                         | .000                           | .00000             | .000   |

\* MICROGRAMS PER CUBIC METER

TABLE C-8

EVAPORATION EXPERIMENT NO. GLF8 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/BOTTOM SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 50%

VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS  
 (PPM/AB BASED ON MASS BALANCE)

| ELAPSED<br>TIME<br><br>MINUTES | PPM  | MICROGRAMS<br>PER<br>CUBIC<br>METER | *<br>PER<br>METER<br>SQUARED | *<br>PER<br>GRAM/<br>METER SQD | PPM<br>PER<br>DROP | MICROGRAMS<br>PER<br>CUBIC METER<br>PER DROP |
|--------------------------------|------|-------------------------------------|------------------------------|--------------------------------|--------------------|--|
| .0                             | .799 | 5014.553                            | 14805.290                    | 169.556                        | .00054             | 3.407  |
| 15.0                           | .763 | 4791.684                            | 14147.280                    | 162.020                        | .00052             | 3.255  |
| 30.0                           | .745 | 4680.249                            | 13818.270                    | 158.252                        | .00051             | 3.180  |
| 45.0                           | .728 | 4568.814                            | 13489.270                    | 154.484                        | .00049             | 3.104  |
| 60.0                           | .692 | 4345.946                            | 12831.250                    | 146.948                        | .00047             | 2.952  |
| 75.0                           | .674 | 4234.511                            | 12502.250                    | 143.180                        | .00046             | 2.877  |
| 90.0                           | .639 | 4011.642                            | 11844.230                    | 135.645                        | .00043             | 2.725  |
| 105.0                          | .621 | 3900.207                            | 11515.230                    | 131.877                        | .00042             | 2.650  |
| 120.0                          | .604 | 3788.773                            | 11186.220                    | 128.109                        | .00041             | 2.574  |
| 135.0                          | .568 | 3565.904                            | 10528.210                    | 120.573                        | .00039             | 2.422  |
| 150.0                          | .550 | 3454.469                            | 10199.200                    | 116.805                        | .00037             | 2.347  |
| 165.0                          | .515 | 3231.601                            | 9541.188                     | 109.269                        | .00035             | 2.195  |
| 180.0                          | .497 | 3120.166                            | 9212.182                     | 105.501                        | .00034             | 2.120  |
| 195.0                          | .462 | 2897.297                            | 8554.169                     | 97.966                         | .00031             | 1.968  |
| 210.0                          | .444 | 2785.863                            | 8225.163                     | 94.198                         | .00030             | 1.893  |
| 225.0                          | .408 | 2562.993                            | 7567.149                     | 86.662                         | .00028             | 1.741  |
| 240.0                          | .391 | 2451.559                            | 7238.143                     | 82.894                         | .00027             | 1.665  |
| 255.0                          | .355 | 2228.690                            | 6580.130                     | 75.353                         | .00024             | 1.514  |
| 270.0                          | .337 | 2117.255                            | 6251.123                     | 71.590                         | .00023             | 1.438  |
| 285.0                          | .302 | 1894.386                            | 5593.110                     | 64.054                         | .00020             | 1.287  |
| 300.0                          | .284 | 1782.952                            | 5264.104                     | 60.286                         | .00019             | 1.211  |
| 315.0                          | .249 | 1560.083                            | 4606.091                     | 52.751                         | .00017             | 1.060  |
| 330.0                          | .231 | 1448.649                            | 4277.084                     | 48.983                         | .00016             | .984   |
| 345.0                          | .195 | 1225.780                            | 3619.072                     | 41.447                         | .00013             | .833   |
| 360.0                          | .160 | 1002.911                            | 2961.059                     | 33.911                         | .00011             | .681   |
| 375.0                          | .142 | 891.476                             | 2632.052                     | 30.143                         | .00010             | .606   |
| 390.0                          | .106 | 668.607                             | 1974.039                     | 22.607                         | .00007             | .454   |
| 405.0                          | .089 | 557.172                             | 1645.032                     | 18.840                         | .00006             | .379   |
| 420.0                          | .053 | 334.303                             | 987.019                      | 11.304                         | .00004             | .227   |
| 435.0                          | .036 | 222.869                             | 658.013                      | 7.536                          | .00002             | .151   |
| 450.0                          | .018 | 111.435                             | 329.007                      | 3.768                          | .00001             | .076   |
| 465.0                          | .018 | 111.435                             | 329.007                      | 3.768                          | .00001             | .076   |
| 480.0                          | .000 | .000                                | .000                         | .000                           | .00000             | .000   |

\* MICROGRAMS PER CUBIC METER

TABLE C-9

EVAPORATION EXPERIMENT NO. GLF9 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOF SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 44%

VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS  
 (PPM/AN BASED ON MIRAN CALIBRATION DATA)

| ELAPSED<br>TIME<br><br>MINUTES | PPM   | MICROGRAMS<br>PER<br>CUBIC<br>METER | *<br>PER<br>METER<br>SQUARED | *<br>PER<br>GRAM/<br>METER SQD | PPM<br>PER<br>DROP | MICROGRAMS<br>PER<br>CUBIC METER<br>PER DROP |
|--------------------------------|-------|-------------------------------------|------------------------------|--------------------------------|--------------------|--|
| .0                             | 2.397 | 15048.370                           | 44429.780                    | 652.031                        | .00163             | 10.223                                       |
| 30.0                           | 1.530 | 9605.341                            | 28359.440                    | 416.190                        | .00104             | 6.525  |
| 60.0                           | 1.428 | 8964.983                            | 26468.800                    | 388.444                        | .00097             | 6.090  |
| 90.0                           | 1.394 | 8751.532                            | 25838.600                    | 379.195                        | .00095             | 5.945  |
| 120.0                          | 1.275 | 8004.451                            | 23632.860                    | 346.825                        | .00087             | 5.438  |
| 150.0                          | 1.190 | 7470.820                            | 22057.340                    | 323.703                        | .00081             | 5.075  |
| 180.0                          | 1.122 | 7043.916                            | 20796.920                    | 305.206                        | .00076             | 4.785  |
| 210.0                          | 1.037 | 6510.287                            | 19221.400                    | 282.084                        | .00070             | 4.423  |
| 240.0                          | .969  | 6083.382                            | 17960.970                    | 263.587                        | .00066             | 4.133  |
| 270.0                          | .884  | 5549.752                            | 16385.450                    | 240.465                        | .00060             | 3.770  |
| 300.0                          | .816  | 5122.848                            | 15125.030                    | 221.968                        | .00055             | 3.480  |
| 330.0                          | .731  | 4589.218                            | 13549.510                    | 198.846                        | .00050             | 3.118  |
| 360.0                          | .663  | 4162.314                            | 12289.090                    | 180.349                        | .00045             | 2.828  |
| 390.0                          | .578  | 3628.684                            | 10713.560                    | 157.227                        | .00039             | 2.465  |
| 420.0                          | .510  | 3201.780                            | 9453.145                     | 138.730                        | .00035             | 2.175  |
| 450.0                          | .425  | 2668.150                            | 7877.621                     | 115.608                        | .00029             | 1.813  |
| 480.0                          | .357  | 2241.246                            | 6617.201                     | 97.111                         | .00024             | 1.523  |
| 510.0                          | .289  | 1814.342                            | 5356.782                     | 78.614                         | .00020             | 1.233  |
| 540.0                          | .238  | 1494.164                            | 4411.468                     | 64.741                         | .00016             | 1.015  |
| 570.0                          | .187  | 1173.986                            | 3466.153                     | 50.868                         | .00013             | .798   |
| 600.0                          | .136  | 853.808                             | 2520.839                     | 36.995                         | .00009             | .580   |
| 630.0                          | .102  | 640.356                             | 1890.629                     | 27.746                         | .00007             | .435   |
| 660.0                          | .068  | 426.904                             | 1260.419                     | 18.497                         | .00005             | .290   |
| 690.0                          | .051  | 320.178                             | 945.314                      | 13.873                         | .00003             | .218   |
| 720.0                          | .034  | 213.452                             | 630.210                      | 9.249                          | .00002             | .145   |
| 750.0                          | .017  | 106.726                             | 315.105                      | 4.624                          | .00001             | .073   |
| 780.0                          | .000  | .000                                | .000                         | .000                           | .00000             | .000   |

\* MICROGRAMS PER CUBIC METER

TABLE C-10

EVAPORATION EXPERIMENT NO. GLF10 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 52%

VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS  
 (PPM/AB BASED ON MASS BALANCE)

| ELAPSED<br>TIME<br>MINUTES | PPM   | MICROGRAMS<br>PER<br>CUBIC<br>METER | *<br>PER<br>METER<br>SQUARED | *<br>PER<br>GRAM/<br>METER SQD | PPM<br>PER<br>DROP | MICROGRAMS<br>PER<br>CUBIC METER<br>PER DROP |
|----------------------------|-------|-------------------------------------|------------------------------|--------------------------------|--------------------|--|
| .0                         | 2.329 | 14619.890                           | 43164.730                    | 494.339                        | .00158             | 9.932  |
| 30.0                       | 1.673 | 10504.670                           | 31014.660                    | 355.191                        | .00114             | 7.136  |
| 60.0                       | 1.570 | 9854.892                            | 29096.230                    | 333.221                        | .00107             | 6.695  |
| 90.0                       | 1.484 | 9313.414                            | 27497.530                    | 314.912                        | .00101             | 6.327  |
| 120.0                      | 1.432 | 8988.527                            | 26536.320                    | 303.927                        | .00097             | 6.106  |
| 150.0                      | 1.363 | 8555.346                            | 25259.360                    | 289.280                        | .00093             | 5.812  |
| 180.0                      | 1.294 | 8122.164                            | 23980.410                    | 274.633                        | .00088             | 5.518  |
| 210.0                      | 1.242 | 7797.277                            | 23021.190                    | 263.647                        | .00084             | 5.297  |
| 240.0                      | 1.173 | 7364.095                            | 21742.240                    | 249.900                        | .00080             | 5.003  |
| 270.0                      | 1.121 | 7039.208                            | 20783.020                    | 238.015                        | .00076             | 4.782  |
| 300.0                      | 1.035 | 6497.730                            | 19184.320                    | 219.706                        | .00070             | 4.414  |
| 330.0                      | .983  | 6172.844                            | 18225.110                    | 208.721                        | .00067             | 4.194  |
| 360.0                      | .914  | 5739.662                            | 16946.150                    | 194.074                        | .00062             | 3.899  |
| 390.0                      | .845  | 5306.480                            | 15667.200                    | 179.427                        | .00057             | 3.605  |
| 420.0                      | .776  | 4873.298                            | 14388.240                    | 164.780                        | .00053             | 3.311  |
| 450.0                      | .690  | 4331.820                            | 12789.550                    | 146.471                        | .00047             | 2.943  |
| 480.0                      | .604  | 3790.343                            | 11190.860                    | 128.162                        | .00041             | 2.575  |
| 510.0                      | .535  | 3357.161                            | 9911.901                     | 113.515                        | .00036             | 2.281  |
| 540.0                      | .466  | 2923.979                            | 8632.946                     | 98.868                         | .00032             | 1.986  |
| 570.0                      | .397  | 2490.797                            | 7353.991                     | 84.221                         | .00027             | 1.692  |
| 600.0                      | .345  | 2165.910                            | 6394.775                     | 73.235                         | .00023             | 1.471  |
| 630.0                      | .276  | 1732.728                            | 5115.820                     | 58.588                         | .00019             | 1.177  |
| 660.0                      | .242  | 1516.137                            | 4476.343                     | 51.265                         | .00016             | 1.030  |
| 690.0                      | .207  | 1299.546                            | 3836.865                     | 43.941                         | .00014             | .883   |
| 720.0                      | .173  | 1082.955                            | 3197.387                     | 36.618                         | .00012             | .736   |
| 750.0                      | .138  | 866.364                             | 2557.910                     | 29.294                         | .00009             | .589   |
| 780.0                      | .104  | 649.773                             | 1918.432                     | 21.971                         | .00007             | .441   |
| 810.0                      | .086  | 541.478                             | 1598.694                     | 18.309                         | .00006             | .358   |
| 840.0                      | .069  | 433.182                             | 1278.955                     | 14.647                         | .00005             | .294   |
| 870.0                      | .052  | 324.887                             | 959.216                      | 10.985                         | .00004             | .221   |
| 900.0                      | .017  | 108.296                             | 319.739                      | 3.662                          | .00001             | .074   |
| 930.0                      | .017  | 108.296                             | 319.739                      | 3.662                          | .00001             | .074   |
| 960.0                      | .000  | .000                                | .000                         | .000                           | .00000             | .000   |

\* MICROGRAMS PER CUBIC METER

TABLE C-11

EVAPORATION EXPERIMENT NO. G F11 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 55%

## VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS

(PPM/AB BASED ON MASS BALANCE)

| ELAPSED<br>TIME<br><br>MINUTES | PPM   | MICROGRAMS<br>PER<br>CUBIC<br>MEYER | *<br>PER<br>METER<br>SQUARED | *<br>PER<br>GRAM/<br>METER SQD | PPM<br>PER<br>DROP | MICROGRAMS<br>PER<br>CUBIC METER<br>PER DROP |
|--------------------------------|-------|-------------------------------------|------------------------------|--------------------------------|--------------------|--|
| .0                             | 1.137 | 7141.225                            | 21084.220                    | 280.695                        | .00077             | 4.851  |
| 10.0                           | 1.085 | 6811.630                            | 20111.100                    | 267.740                        | .00074             | 4.627  |
| 20.0                           | .033  | 6482.035                            | 19137.980                    | 254.785                        | .00070             | 4.404  |
| 30.0                           | .998  | 6262.305                            | 18489.240                    | 246.148                        | .00068             | 4.254  |
| 40.0                           | .945  | 5932.710                            | 17516.120                    | 233.193                        | .00064             | 4.030  |
| 50.0                           | .910  | 5712.980                            | 16867.380                    | 224.556                        | .00062             | 3.881  |
| 60.0                           | .857  | 5363.385                            | 15894.260                    | 211.601                        | .00058             | 3.657  |
| 70.0                           | .822  | 5163.655                            | 15245.510                    | 202.964                        | .00056             | 3.508  |
| 80.0                           | .788  | 4943.925                            | 14596.770                    | 194.327                        | .00053             | 3.359  |
| 90.0                           | .752  | 4724.195                            | 13948.020                    | 185.691                        | .00051             | 3.209  |
| 100.0                          | .700  | 4594.600                            | 12974.900                    | 172.736                        | .00048             | 2.985  |
| 110.0                          | .665  | 4174.870                            | 12326.160                    | 164.099                        | .00045             | 2.836  |
| 120.0                          | .613  | 3845.275                            | 11353.040                    | 151.144                        | .00042             | 2.612  |
| 130.0                          | .577  | 3625.545                            | 10704.300                    | 142.507                        | .00039             | 2.463  |
| 140.0                          | .543  | 3405.815                            | 10055.550                    | 133.870                        | .00037             | 2.314  |
| 150.0                          | .490  | 3076.220                            | 9082.433                     | 120.915                        | .00033             | 2.090  |
| 160.0                          | .455  | 2856.690                            | 8433.688                     | 112.278                        | .00031             | 1.941  |
| 170.0                          | .420  | 2636.760                            | 7754.942                     | 103.641                        | .00029             | 1.791  |
| 180.0                          | .385  | 2417.030                            | 7136.197                     | 95.005                         | .00026             | 1.642  |
| 190.0                          | .332  | 2087.435                            | 6163.079                     | 82.049                         | .00023             | 1.418  |
| 200.0                          | .298  | 1867.705                            | 5514.334                     | 73.413                         | .00020             | 1.269  |
| 210.0                          | .262  | 1647.975                            | 4865.589                     | 64.776                         | .00018             | 1.120  |
| 220.0                          | .228  | 1428.245                            | 4216.844                     | 56.139                         | .00015             | .970   |
| 230.0                          | .210  | 1318.380                            | 3892.471                     | 51.821                         | .00014             | .896   |
| 240.0                          | .175  | 1098.650                            | 3243.726                     | 43.184                         | .00012             | .746   |
| 250.0                          | .157  | 988.785                             | 2919.353                     | 38.865                         | .00011             | .672   |
| 260.0                          | .140  | 878.920                             | 2594.981                     | 34.547                         | .00010             | .597   |
| 270.0                          | .123  | 769.055                             | 2270.608                     | 30.229                         | .00008             | .522   |
| 280.0                          | .105  | 659.190                             | 1946.236                     | 25.910                         | .00007             | .448   |
| 290.0                          | .087  | 549.325                             | 1621.863                     | 21.592                         | .00006             | .373   |
| 300.0                          | .070  | 439.460                             | 1297.490                     | 17.274                         | .00005             | .299   |
| 310.0                          | .053  | 329.595                             | 973.118                      | 12.955                         | .00004             | .224   |
| 320.0                          | .053  | 329.595                             | 973.118                      | 12.955                         | .00004             | .224   |
| 330.0                          | .035  | 219.730                             | 648.745                      | 8.637                          | .00002             | .149   |
| 340.0                          | .018  | 109.865                             | 324.373                      | 4.318                          | .00001             | .075   |
| 350.0                          | .018  | 109.865                             | 324.373                      | 4.318                          | .00001             | .075   |
| 360.0                          | .000  | .000                                | .000                         | .000                           | .00000             | .000   |

\* MICROGRAMS PER CUBIC METER

TABLE C-12

EVAPORATION EXPERIMENT NO. GLF12 SERIES 1D 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 40%

VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS  
 (PPM/AB BASED ON MASS BALANCE)

| ELAPSED<br>TIME<br>MINUTES | PPM  | MICROGRAMS<br>PER<br>CUBIC<br>METER | *<br>PER<br>METER<br>SQUARED | *<br>PER<br>GRAM/<br>METER SQD | PPM<br>PER<br>DROP | MICROGRAMS<br>PER<br>CUBIC METER<br>PER DROP |
|----------------------------|------|-------------------------------------|------------------------------|--------------------------------|--------------------|--|
| .0                         | .932 | 5847.957                            | 17265.890                    | 197.735                        | .00063             | 3.973  |
| 10.0                       | .897 | 5631.366                            | 16626.410                    | 190.412                        | .00061             | 3.826  |
| 20.0                       | .880 | 5523.071                            | 16306.670                    | 185.750                        | .00060             | 3.752  |
| 30.0                       | .845 | 5306.479                            | 15667.200                    | 179.427                        | .00057             | 3.605  |
| 40.0                       | .811 | 5089.888                            | 15027.720                    | 172.103                        | .00055             | 3.458  |
| 50.0                       | .794 | 4981.593                            | 14707.980                    | 168.441                        | .00054             | 3.384  |
| 60.0                       | .776 | 4873.297                            | 14388.240                    | 164.780                        | .00053             | 3.311  |
| 70.0                       | .742 | 4656.707                            | 13748.760                    | 157.456                        | .00050             | 3.164  |
| 80.0                       | .725 | 4548.411                            | 13429.030                    | 153.794                        | .00049             | 3.090  |
| 90.0                       | .707 | 4440.116                            | 13109.290                    | 150.132                        | .00048             | 3.016  |
| 100.0                      | .690 | 4331.820                            | 12789.550                    | 146.471                        | .00047             | 2.943  |
| 110.0                      | .673 | 4223.524                            | 12469.810                    | 142.809                        | .00046             | 2.869  |
| 120.0                      | .655 | 4115.229                            | 12150.070                    | 139.147                        | .00045             | 2.796  |
| 130.0                      | .621 | 3898.638                            | 11510.590                    | 131.824                        | .00042             | 2.649  |
| 140.0                      | .604 | 3790.343                            | 11190.850                    | 128.162                        | .00041             | 2.575  |
| 150.0                      | .587 | 3682.047                            | 10871.120                    | 124.500                        | .00040             | 2.501  |
| 160.0                      | .569 | 3573.751                            | 10551.380                    | 120.838                        | .00039             | 2.428  |
| 170.0                      | .552 | 3465.456                            | 10231.640                    | 117.177                        | .00038             | 2.354  |
| 180.0                      | .517 | 3248.865                            | 9592.161                     | 109.853                        | .00035             | 2.207  |
| 190.0                      | .500 | 3140.569                            | 9272.422                     | 106.191                        | .00034             | 2.134  |
| 200.0                      | .483 | 3032.274                            | 8952.685                     | 102.529                        | .00033             | 2.060  |
| 210.0                      | .466 | 2923.979                            | 8632.945                     | 98.868                         | .00032             | 1.986  |
| 220.0                      | .431 | 2707.387                            | 7993.468                     | 91.544                         | .00029             | 1.839  |
| 230.0                      | .414 | 2599.092                            | 7673.729                     | 87.882                         | .00028             | 1.766  |
| 240.0                      | .380 | 2382.501                            | 7034.251                     | 80.559                         | .00026             | 1.619  |
| 250.0                      | .362 | 2274.200                            | 6714.513                     | 76.897                         | .00025             | 1.545  |
| 260.0                      | .328 | 2057.615                            | 6075.036                     | 69.574                         | .00022             | 1.398  |
| 270.0                      | .310 | 1949.319                            | 5755.297                     | 65.912                         | .00021             | 1.324  |
| 280.0                      | .293 | 1841.024                            | 5435.559                     | 62.250                         | .00020             | 1.251  |
| 290.0                      | .259 | 1624.432                            | 4796.081                     | 54.927                         | .00018             | 1.104  |
| 300.0                      | .242 | 1516.137                            | 4476.342                     | 51.265                         | .00016             | 1.030  |
| 310.0                      | .207 | 1299.546                            | 3936.865                     | 43.941                         | .00014             | .883   |
| 320.0                      | .172 | 1082.955                            | 3197.387                     | 36.618                         | .00012             | .736   |
| 330.0                      | .155 | 974.659                             | 2877.648                     | 32.956                         | .00011             | .662   |
| 340.0                      | .135 | 866.364                             | 2557.910                     | 29.294                         | .00009             | .589   |
| 350.0                      | .104 | 649.777                             | 1918.432                     | 21.971                         | .00007             | .441   |
| 360.0                      | .086 | 541.477                             | 1598.693                     | 18.309                         | .00006             | .368   |
| 370.0                      | .052 | 324.887                             | 959.216                      | 10.985                         | .00004             | .221   |
| 380.0                      | .035 | 216.591                             | 639.477                      | 7.324                          | .00002             | .147   |
| 390.0                      | .000 | .000                                | .000                         | .000                           | .00000             | .000   |

\* MICROGRAMS PER CUBIC METER

TABLE C-13

EVAPORATION EXPERIMENT NO. GLE13 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 44%

VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS  
 (PPM/AB BASED ON MASS BALANCE)

| ELAPSED<br>TIME<br><br>MINUTES | PPM   | MICROGRAMS<br>PER<br>CUBIC<br>METER | *<br>PER<br>METER<br>SQUARED | *<br>PER<br>GRAM/<br>METER SQD | PPM<br>PER<br>DROP | MICROGRAMS<br>PER<br>CUBIC METER<br>PER DROP |
|--------------------------------|-------|-------------------------------------|------------------------------|--------------------------------|--------------------|--|
| 0                              | 1.190 | 7470.821                            | 22057.340                    | 307.945                        | .00081             | 5.075  |
| 40.0                           | 1.071 | 6723.739                            | 19851.610                    | 277.151                        | .00073             | 4.568  |
| 80.0                           | 1.020 | 6403.561                            | 18906.290                    | 263.953                        | .00069             | 4.350  |
| 120.0                          | .986  | 6190.108                            | 18276.080                    | 255.155                        | .00067             | 4.205  |
| 160.0                          | .935  | 5869.931                            | 17330.770                    | 241.957                        | .00064             | 3.988  |
| 200.0                          | .901  | 5656.479                            | 16700.560                    | 233.159                        | .00061             | 3.843  |
| 240.0                          | .867  | 5443.027                            | 16070.350                    | 224.360                        | .00059             | 3.698  |
| 280.0                          | .833  | 5229.574                            | 15440.140                    | 215.562                        | .00057             | 3.553  |
| 320.0                          | .799  | 5016.123                            | 14809.100                    | 206.763                        | .00054             | 3.408  |
| 360.0                          | .765  | 4802.671                            | 14179.720                    | 197.965                        | .00052             | 3.263  |
| 400.0                          | .697  | 4375.767                            | 12919.300                    | 180.368                        | .00047             | 2.973  |
| 440.0                          | .663  | 4162.314                            | 12289.090                    | 171.570                        | .00045             | 2.828  |
| 480.0                          | .612  | 3842.136                            | 11343.770                    | 158.372                        | .00042             | 2.610  |
| 520.0                          | .561  | 3521.958                            | 10398.460                    | 145.174                        | .00038             | 2.393  |
| 560.0                          | .493  | 3095.054                            | 9138.040                     | 127.577                        | .00033             | 2.103  |
| 600.0                          | .425  | 2668.150                            | 7877.621                     | 109.980                        | .00029             | 1.813  |
| 640.0                          | .357  | 2241.246                            | 6617.201                     | 92.384                         | .00024             | 1.523  |
| 680.0                          | .306  | 1921.068                            | 5671.887                     | 79.186                         | .00021             | 1.305  |
| 720.0                          | .255  | 1600.890                            | 4726.573                     | 65.988                         | .00017             | 1.088  |
| 760.0                          | .204  | 1280.712                            | 3781.258                     | 52.791                         | .00014             | .870   |
| 800.0                          | .170  | 1067.260                            | 3151.049                     | 43.992                         | .00012             | .725   |
| 840.0                          | .136  | 853.808                             | 2520.839                     | 35.194                         | .00009             | .580   |
| 880.0                          | .119  | 747.082                             | 2205.734                     | 30.795                         | .00008             | .506   |
| 920.0                          | .102  | 640.356                             | 1890.629                     | 26.395                         | .00007             | .435   |
| 960.0                          | .085  | 533.630                             | 1575.524                     | 21.996                         | .00006             | .363   |
| 1000.0                         | .068  | 426.904                             | 1260.420                     | 17.597                         | .00005             | .290   |
| 1040.0                         | .051  | 320.178                             | 945.315                      | 13.198                         | .00003             | .218   |
| 1080.0                         | .034  | 213.452                             | 630.210                      | 8.798                          | .00002             | .165   |
| 1120.0                         | .034  | 213.452                             | 630.210                      | 8.798                          | .00002             | .145   |
| 1160.0                         | .034  | 213.452                             | 630.210                      | 8.798                          | .00002             | .145   |
| 1200.0                         | .017  | 106.726                             | 315.105                      | 4.399                          | .00001             | .073   |
| 1240.0                         | .017  | 106.726                             | 315.105                      | 4.399                          | .00001             | .073   |
| 1280.0                         | .000  | .000                                | .000                         | .000                           | .00000             | .000   |

\* MICROGRAMS PER CUBIC METER



TABLE C-14

EVAPORATION EXPERIMENT NO. GLF14 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON GAK/BOTTOM SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 43%

VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS  
 (PPM/AB BASED ON MIRAN CALIBRATION DATA)

| ELAPSED<br>TIME | PPM   | MICROGRAMS<br>PER<br>CUBIC<br>METER | *<br>PER<br>METER<br>SQUARED | *<br>PER<br>GRAM/<br>METER SQD | PPM<br>PER<br>DRCP | MICROGRAMS<br>PER<br>CUBIC METER<br>PER DROP |
|-----------------|-------|-------------------------------------|------------------------------|--------------------------------|--------------------|--|
| MINUTES         |       |                                     |                              |                                |                    |  |
| 0.0             | 1.225 | 7690.550                            | 22706.080                    | 260.039                        | .00083             | 5.225  |
| 40.0            | 1.173 | 7360.955                            | 21732.960                    | 248.894                        | .00080             | 5.001  |
| 80.0            | 1.120 | 7031.360                            | 20759.850                    | 237.750                        | .00076             | 4.777  |
| 120.0           | 1.085 | 6811.630                            | 20111.100                    | 230.320                        | .00074             | 4.627  |
| 160.0           | 1.050 | 6591.960                            | 19462.360                    | 222.890                        | .00071             | 4.478  |
| 200.0           | 1.015 | 6372.170                            | 18813.610                    | 215.461                        | .00069             | 4.329  |
| 240.0           | .962  | 6042.575                            | 17840.490                    | 204.316                        | .00065             | 4.105  |
| 280.0           | .928  | 5822.845                            | 17191.750                    | 196.886                        | .00063             | 3.956  |
| 320.0           | .892  | 5603.115                            | 16543.000                    | 189.457                        | .00061             | 3.806  |
| 360.0           | .857  | 5383.385                            | 15894.260                    | 182.027                        | .00058             | 3.657  |
| 400.0           | .805  | 5053.790                            | 14921.140                    | 170.882                        | .00055             | 3.433  |
| 440.0           | .770  | 4834.060                            | 14272.350                    | 163.453                        | .00052             | 3.284  |
| 480.0           | .718  | 4504.465                            | 13299.280                    | 152.308                        | .00049             | 3.060  |
| 520.0           | .665  | 4174.870                            | 12326.160                    | 141.164                        | .00045             | 2.836  |
| 560.0           | .612  | 3845.275                            | 11353.040                    | 130.019                        | .00042             | 2.612  |
| 600.0           | .560  | 3515.680                            | 10379.920                    | 118.875                        | .00038             | 2.388  |
| 640.0           | .507  | 3186.085                            | 9406.806                     | 107.730                        | .00034             | 2.164  |
| 680.0           | .438  | 2746.625                            | 8109.315                     | 92.871                         | .00030             | 1.866  |
| 720.0           | .385  | 2417.030                            | 7136.197                     | 81.726                         | .00026             | 1.642  |
| 760.0           | .350  | 2197.300                            | 6487.452                     | 74.297                         | .00024             | 1.493  |
| 800.0           | .298  | 1867.705                            | 5514.334                     | 63.152                         | .00020             | 1.269  |
| 840.0           | .262  | 1647.975                            | 4865.589                     | 55.723                         | .00018             | 1.120  |
| 880.0           | .228  | 1428.245                            | 4216.844                     | 48.293                         | .00015             | .970   |
| 920.0           | .157  | 988.785                             | 2919.353                     | 33.434                         | .00011             | .672   |
| 960.0           | .105  | 659.190                             | 1966.236                     | 22.289                         | .00007             | .448   |
| 1000.0          | .087  | 549.325                             | 1621.863                     | 13.574                         | .00006             | .373   |
| 1040.0          | .087  | 549.325                             | 1621.863                     | 18.574                         | .00006             | .373   |
| 1080.0          | .053  | 329.595                             | 973.118                      | 11.145                         | .00004             | .224   |
| 1120.0          | .035  | 219.730                             | 648.745                      | 7.430                          | .00002             | .149   |
| 1160.0          | .000  | .000                                | .000                         | .000                           | .00000             | .000   |

\* MICROGRAMS PER CUBIC METER

TABLE C-15

EVAPORATION EXPERIMENT NO. GLF15 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 11.3 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS  
 (PPM/AB BASED ON MASS BALANCE)

| ELAPSED<br>TIME<br>MINUTES | PPM  | MICROGRAMS<br>PER<br>CUBIC<br>METER | *<br>PER<br>METER<br>SQUARED | *<br>PER<br>GRAM/<br>METER SQD | PPM<br>PER<br>DROP | MICROGRAMS<br>PER<br>CUBIC METER<br>PER DROP |
|----------------------------|------|-------------------------------------|------------------------------|--------------------------------|--------------------|--|
| .0                         | .720 | 4521.729                            | 13350.250                    | 177.733                        | .00049             | 3.072  |
| 15.0                       | .687 | 4311.417                            | 12729.310                    | 169.466                        | .00047             | 2.929  |
| 30.0                       | .653 | 4101.104                            | 12108.370                    | 161.199                        | .00044             | 2.786  |
| 45.0                       | .637 | 3995.947                            | 11797.900                    | 157.066                        | .00043             | 2.715  |
| 60.0                       | .603 | 3705.634                            | 11176.950                    | 148.799                        | .00041             | 2.572  |
| 75.0                       | .586 | 3680.478                            | 10866.480                    | 144.666                        | .00040             | 2.500  |
| 90.0                       | .570 | 3575.321                            | 10516.010                    | 140.533                        | .00039             | 2.429  |
| 105.0                      | .553 | 3470.165                            | 10245.540                    | 136.399                        | .00038             | 2.357  |
| 120.0                      | .519 | 3259.851                            | 9624.598                     | 128.133                        | .00035             | 2.215  |
| 135.0                      | .502 | 3154.695                            | 9314.128                     | 123.999                        | .00034             | 2.143  |
| 150.0                      | .486 | 3049.538                            | 9003.656                     | 119.866                        | .00033             | 2.072  |
| 165.0                      | .452 | 2839.226                            | 8382.715                     | 111.600                        | .00031             | 1.929  |
| 180.0                      | .435 | 2734.069                            | 8072.244                     | 107.466                        | .00030             | 1.857  |
| 195.0                      | .419 | 2628.913                            | 7761.773                     | 103.333                        | .00028             | 1.786  |
| 210.0                      | .402 | 2523.756                            | 7451.302                     | 99.200                         | .00027             | 1.715  |
| 225.0                      | .368 | 2313.443                            | 6830.360                     | 90.933                         | .00025             | 1.572  |
| 240.0                      | .335 | 2103.129                            | 6209.418                     | 82.666                         | .00023             | 1.429  |
| 255.0                      | .301 | 1892.817                            | 5588.476                     | 74.400                         | .00020             | 1.286  |
| 270.0                      | .268 | 1682.504                            | 4967.535                     | 66.133                         | .00018             | 1.143  |
| 285.0                      | .235 | 1472.191                            | 4346.593                     | 57.866                         | .00016             | 1.000  |
| 300.0                      | .201 | 1261.878                            | 3725.651                     | 49.600                         | .00014             | .857   |
| 315.0                      | .167 | 1051.565                            | 3104.709                     | 41.333                         | .00011             | .714   |
| 330.0                      | .134 | 841.252                             | 2483.767                     | 33.067                         | .00009             | .572   |
| 345.0                      | .101 | 630.939                             | 1862.826                     | 24.800                         | .00007             | .429   |
| 360.0                      | .084 | 525.782                             | 1552.554                     | 20.667                         | .00006             | .357   |
| 375.0                      | .067 | 420.626                             | 1241.884                     | 16.533                         | .00005             | .286   |
| 390.0                      | .050 | 315.470                             | 931.413                      | 12.400                         | .00003             | .214   |
| 405.0                      | .034 | 210.313                             | 620.942                      | 8.267                          | .00002             | .143   |
| 420.0                      | .017 | 105.157                             | 310.471                      | 4.133                          | .00001             | .071   |
| 435.0                      | .017 | 105.157                             | 310.471                      | 4.133                          | .00001             | .071   |
| 450.0                      | .017 | 105.157                             | 310.471                      | 4.133                          | .00001             | .071   |
| 465.0                      | .000 | .000                                | .000                         | .000                           | .00000             | .000   |

\* MICROGRAMS PER CUBIC METER

TABLE C-16

EVAPORATION EXPERIMENT NO. GLF16 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 7 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 11.3 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS  
 (FPM/AB BASED ON MASS BALANCE)

| ELAPSED<br>TIME<br><br>MINUTES | PPM  | MICROGRAMS<br>PER<br>CUBIC<br>METER | *<br>PER<br>METER<br>SQUARED | *<br>PER<br>GRAM/<br>METER SQD | PPM<br>PER<br>DROP | MICROGRAMS<br>PER<br>CUBIC METER<br>PER DROP |
|--------------------------------|------|-------------------------------------|------------------------------|--------------------------------|--------------------|--|
| 0                              | .731 | 4589.218                            | 13549.510                    | 161.628                        | .00050             | 3.118  |
| 15.0                           | .697 | 4375.766                            | 12919.300                    | 154.111                        | .00047             | 2.973  |
| 30.0                           | .663 | 4162.314                            | 12289.090                    | 146.593                        | .00045             | 2.828  |
| 45.0                           | .646 | 4055.583                            | 11873.980                    | 142.834                        | .00044             | 2.755  |
| 60.0                           | .612 | 3842.136                            | 11343.770                    | 135.317                        | .00042             | 2.610  |
| 75.0                           | .595 | 3735.410                            | 11028.570                    | 131.558                        | .00040             | 2.538  |
| 90.0                           | .578 | 3628.684                            | 10713.560                    | 127.799                        | .00039             | 2.465  |
| 105.0                          | .561 | 3521.958                            | 10398.460                    | 124.040                        | .00038             | 2.393  |
| 120.0                          | .544 | 3415.232                            | 10083.350                    | 120.281                        | .00037             | 2.320  |
| 135.0                          | .527 | 3308.506                            | 9768.250                     | 116.523                        | .00036             | 2.248  |
| 150.0                          | .510 | 3201.780                            | 9453.145                     | 112.764                        | .00035             | 2.175  |
| 165.0                          | .476 | 2988.328                            | 8822.936                     | 105.246                        | .00032             | 2.030  |
| 180.0                          | .476 | 2988.328                            | 8822.936                     | 105.246                        | .00032             | 2.030  |
| 195.0                          | .442 | 2774.876                            | 8152.725                     | 97.729                         | .00030             | 1.885  |
| 210.0                          | .425 | 2668.150                            | 7877.621                     | 93.970                         | .00029             | 1.813  |
| 225.0                          | .408 | 2561.424                            | 7562.516                     | 90.211                         | .00028             | 1.740  |
| 240.0                          | .374 | 2347.972                            | 6932.397                     | 84.694                         | .00025             | 1.595  |
| 255.0                          | .357 | 2241.046                            | 6617.201                     | 78.935                         | .00024             | 1.523  |
| 270.0                          | .340 | 2134.520                            | 6302.096                     | 75.176                         | .00022             | 1.450  |
| 285.0                          | .306 | 1921.068                            | 5671.687                     | 67.658                         | .00021             | 1.305  |
| 300.0                          | .272 | 1707.616                            | 5341.677                     | 60.145                         | .00018             | 1.160  |
| 315.0                          | .238 | 1494.164                            | 4411.458                     | 52.625                         | .00016             | 1.015  |
| 330.0                          | .204 | 1280.712                            | 3781.250                     | 45.106                         | .00014             | .870   |
| 345.0                          | .153 | 960.534                             | 2835.943                     | 33.529                         | .00010             | .653   |
| 360.0                          | .119 | 747.082                             | 2205.734                     | 26.312                         | .00008             | .508   |
| 375.0                          | .085 | 533.630                             | 1575.524                     | 18.794                         | .00006             | .363   |
| 390.0                          | .051 | 320.178                             | 945.314                      | 11.276                         | .00003             | .213   |
| 405.0                          | .034 | 213.452                             | 630.230                      | 7.518                          | .00002             | .145   |
| 420.0                          | .017 | 106.726                             | 315.105                      | 3.759                          | .00001             | .073   |
| 435.0                          | .000 | .000                                | .000                         | .000                           | .00000             | .000   |

\* MICROGRAMS PER CUBIC METER

TABLE C-17

EVAPORATION EXPERIMENT NO. RL11 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 39%

VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS  
 (PPM/AB BASED ON MIRAN CALIBRATION DATA)

| ELAPSED<br>TIME<br><br>MINUTES | PPM   | MICROGRAMS<br><br>PER<br>CUBIC<br>METER | *<br><br>PER<br>METER<br>SQUARED | *<br><br>PER<br>GRAM/<br>METER SQD | PPM    | MICROGRAMS<br><br>PER<br>CUBIC METER<br>PER DROP |
|--------------------------------|-------|---|----------------------------------|------------------------------------|--------|--|
| .0                             | 1.345 | 8447.049                                | 24939.620                        | 297.498                            | .00091 | 5.738  |
| 45.0                           | 1.259 | 7905.571                                | 23340.920                        | 278.427                            | .00086 | 5.371  |
| 90.0                           | 1.190 | 7472.389                                | 22061.970                        | 263.171                            | .00081 | 5.076  |
| 135.0                          | 1.138 | 7147.503                                | 21102.750                        | 251.729                            | .00077 | 4.856  |
| 180.0                          | 1.087 | 6822.617                                | 20143.540                        | 240.287                            | .00074 | 4.635  |
| 225.0                          | 1.035 | 6497.730                                | 19184.320                        | 228.844                            | .00070 | 4.414  |
| 270.0                          | .966  | 6064.548                                | 17905.370                        | 213.588                            | .00066 | 4.120  |
| 315.0                          | .914  | 5739.662                                | 16946.150                        | 202.146                            | .00062 | 3.899  |
| 360.0                          | .828  | 5198.184                                | 15347.460                        | 183.075                            | .00056 | 3.531  |
| 405.0                          | .759  | 4765.002                                | 14068.500                        | 167.819                            | .00052 | 3.237  |
| 450.0                          | .675  | 4223.524                                | 12469.810                        | 148.749                            | .00046 | 2.869  |
| 495.0                          | .604  | 3790.343                                | 11190.850                        | 133.493                            | .00041 | 2.575  |
| 540.0                          | .517  | 3248.865                                | 9592.161                         | 114.422                            | .00035 | 2.207  |
| 585.0                          | .431  | 2707.387                                | 7993.468                         | 95.352                             | .00029 | 1.839  |
| 630.0                          | .362  | 2274.206                                | 6714.513                         | 80.096                             | .00025 | 1.545  |
| 675.0                          | .276  | 1732.728                                | 5115.820                         | 61.625                             | .00019 | 1.177  |
| 720.0                          | .224  | 1407.842                                | 4156.604                         | 49.583                             | .00015 | .956   |
| 765.0                          | .155  | 974.659                                 | 2877.648                         | 33.327                             | .00011 | .662   |
| 810.0                          | .121  | 758.069                                 | 2238.171                         | 26.699                             | .00008 | .515   |
| 855.0                          | .069  | 433.182                                 | 1278.955                         | 15.256                             | .00005 | .294   |
| 900.0                          | .052  | 324.887                                 | 959.216                          | 11.442                             | .00004 | .221   |
| 945.0                          | .035  | 216.591                                 | 639.477                          | 7.628                              | .00002 | .147   |
| 990.0                          | .035  | 216.591                                 | 639.477                          | 7.628                              | .00002 | .147   |
| 1035.0                         | .017  | 108.296                                 | 319.739                          | 3.814                              | .00001 | .074   |
| 1080.0                         | .017  | 108.296                                 | 319.739                          | 3.814                              | .00001 | .074   |
| 1125.0                         | .017  | 108.296                                 | 319.739                          | 3.814                              | .00001 | .074   |
| 1170.0                         | .017  | 108.296                                 | 319.739                          | 3.814                              | .00001 | .074   |
| 1215.0                         | .000  | .000                                    | .000                             | .000                               | .00000 | .000   |

\* MICROGRAMS PER CUBIC METER

TABLE C-18

EVAPORATION EXPERIMENT NO. BLE2 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 2.9 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 39%

VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS  
 (PPM/HR BASED ON MIRAN CALIBRATION DATA)

| ELAPSED<br>TIME<br><br>MINUTES | PPM   | MICROGRAMS<br>PER<br>CUBIC<br>METER | *<br>PER<br>METER<br>SQUARED | *<br>PER<br>GRAM/<br>METER SQD | PPM<br>PER<br>DROP | MICROGRAMS<br>PER<br>CUBIC METER<br>PER DROP |
|--------------------------------|-------|-------------------------------------|------------------------------|--------------------------------|--------------------|--|
| 0                              | 1.491 | 9358.929                            | 27631.910                    | 316.451                        | .00101             | 6.358  |
| 40.0                           | 1.407 | 8835.146                            | 26079.560                    | 298.673                        | .00096             | 6.001  |
| 80.0                           | 1.350 | 8412.520                            | 24837.670                    | 284.450                        | .00091             | 5.715  |
| 120.0                          | 1.290 | 8097.050                            | 23906.260                    | 273.783                        | .00088             | 5.501  |
| 160.0                          | 1.240 | 7781.581                            | 22974.850                    | 263.117                        | .00084             | 5.286  |
| 200.0                          | 1.189 | 7466.111                            | 22063.440                    | 252.450                        | .00081             | 5.072  |
| 240.0                          | 1.139 | 7150.643                            | 21112.020                    | 241.783                        | .00077             | 4.858  |
| 280.0                          | 1.089 | 6835.172                            | 20180.610                    | 231.115                        | .00074             | 4.643  |
| 320.0                          | 1.038 | 6519.703                            | 19249.200                    | 220.449                        | .00071             | 4.429  |
| 360.0                          | .988  | 6204.233                            | 18317.780                    | 209.782                        | .00067             | 4.215  |
| 400.0                          | .938  | 5888.764                            | 17386.370                    | 199.115                        | .00064             | 4.001  |
| 440.0                          | .887  | 5568.138                            | 16444.490                    | 188.893                        | .00059             | 3.715  |
| 480.0                          | .821  | 5152.668                            | 15213.080                    | 174.226                        | .00056             | 3.500  |
| 520.0                          | .754  | 4732.062                            | 13971.150                    | 160.003                        | .00051             | 3.215  |
| 560.0                          | .670  | 4208.260                            | 12418.840                    | 142.225                        | .00046             | 2.858  |
| 600.0                          | .603  | 3785.634                            | 11175.950                    | 128.003                        | .00041             | 2.572  |
| 640.0                          | .536  | 3365.069                            | 9935.069                     | 113.780                        | .00036             | 2.286  |
| 680.0                          | .469  | 2945.382                            | 8693.187                     | 99.556                         | .00032             | 2.000  |
| 720.0                          | .402  | 2523.756                            | 7451.362                     | 85.335                         | .00027             | 1.715  |
| 760.0                          | .335  | 2103.130                            | 6209.418                     | 71.113                         | .00023             | 1.429  |
| 800.0                          | .285  | 1787.661                            | 5278.066                     | 60.446                         | .00019             | 1.214  |
| 840.0                          | .235  | 1472.191                            | 4346.593                     | 49.779                         | .00015             | 1.000  |
| 880.0                          | .201  | 1261.870                            | 3725.651                     | 42.668                         | .00014             | .857   |
| 920.0                          | .151  | 946.406                             | 2794.238                     | 32.001                         | .00010             | .643   |
| 960.0                          | .134  | 841.252                             | 2483.767                     | 28.445                         | .00009             | .572   |
| 1000.0                         | .109  | 630.939                             | 1862.826                     | 21.334                         | .00007             | .429   |
| 1040.0                         | .067  | 420.625                             | 1241.884                     | 14.223                         | .00005             | .286   |
| 1080.0                         | .050  | 315.470                             | 931.413                      | 10.607                         | .00003             | .214   |
| 1120.0                         | .034  | 210.313                             | 620.942                      | 7.111                          | .00002             | .143   |
| 1160.0                         | .034  | 210.313                             | 620.942                      | 7.111                          | .00002             | .143   |
| 1200.0                         | .017  | 105.157                             | 310.471                      | 3.556                          | .00001             | .071   |
| 1240.0                         | .017  | 105.157                             | 310.471                      | 3.556                          | .00001             | .071   |
| 1280.0                         | .000  | .000                                | .000                         | .000                           | .00000             | .000   |

\* MICROGRAMS PER CUBIC METER

TABLE C-19

EVAPORATION EXPERIMENT NO. BLF3 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DILUTED DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/YOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 50 DEG F., RELATIVE HUMIDITY 37%

| VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS<br>(PPM/AB BASED ON MIRAN CALIBRATION DATA) |      |                                     |                              |                                |                    |  |
|--|------|-------------------------------------|------------------------------|--------------------------------|--------------------|--|
| ELAPSED<br>TIME<br><br>MINUTES   | PPM  | MICROGRAMS<br>PER<br>CUBIC<br>METER | *<br>PER<br>METER<br>SQUARED | *<br>PER<br>GRAM/<br>METER SQD | PPM<br>PER<br>DROP | MICROGRAMS<br>PER<br>CUBIC METER<br>PER DROP |
| 0.0  | .897 | 5631.366                            | 16626.410                    | 195.332                        | .00061             | 3.820  |
| 15.0   | .845 | 5306.479                            | 15667.200                    | 186.890                        | .00057             | 3.605  |
| 30.0   | .811 | 5089.888                            | 15027.720                    | 179.261                        | .00055             | 3.458  |
| 45.0   | .759 | 4765.002                            | 14068.500                    | 167.819                        | .00052             | 3.237  |
| 60.0   | .725 | 4548.411                            | 13429.030                    | 160.191                        | .00049             | 3.090  |
| 75.0   | .707 | 4440.116                            | 13109.290                    | 154.337                        | .00048             | 3.016  |
| 90.0   | .673 | 4223.524                            | 12469.810                    | 148.749                        | .00046             | 2.869  |
| 105.0  | .638 | 4006.933                            | 11830.330                    | 141.121                        | .00043             | 2.722  |
| 120.0  | .604 | 3790.343                            | 11190.850                    | 133.493                        | .00041             | 2.575  |
| 135.0  | .587 | 3682.047                            | 10871.120                    | 129.678                        | .00040             | 2.501  |
| 150.0  | .552 | 3465.456                            | 10231.640                    | 122.050                        | .00038             | 2.354  |
| 165.0  | .535 | 3357.160                            | 9911.899                     | 118.236                        | .00036             | 2.281  |
| 180.0  | .500 | 3140.569                            | 9272.422                     | 110.608                        | .00034             | 2.134  |
| 195.0  | .466 | 2923.979                            | 8632.945                     | 102.980                        | .00032             | 1.986  |
| 210.0  | .431 | 2707.387                            | 7993.468                     | 95.352                         | .00029             | 1.839  |
| 225.0  | .397 | 2490.797                            | 7353.991                     | 87.724                         | .00027             | 1.692  |
| 240.0  | .365 | 2165.910                            | 6394.774                     | 76.281                         | .00023             | 1.671  |
| 255.0  | .310 | 1949.319                            | 5755.297                     | 68.653                         | .00021             | 1.324  |
| 270.0  | .276 | 1732.738                            | 5115.820                     | 61.025                         | .00019             | 1.127  |
| 285.0  | .262 | 1516.137                            | 4476.342                     | 53.397                         | .00015             | 1.030  |
| 300.0  | .207 | 1299.546                            | 3836.865                     | 45.769                         | .00014             | .983   |
| 315.0  | .172 | 1082.955                            | 3197.387                     | 38.141                         | .00012             | .736   |
| 330.0  | .138 | 866.364                             | 2557.910                     | 30.513                         | .00009             | .588   |
| 345.0  | .104 | 649.773                             | 1918.432                     | 22.884                         | .00007             | .441   |
| 360.0  | .069 | 433.182                             | 1278.955                     | 15.256                         | .00005             | .294   |
| 375.0  | .052 | 324.887                             | 959.216                      | 11.642                         | .00004             | .221   |
| 390.0  | .035 | 216.591                             | 639.477                      | 7.628                          | .00002             | .147   |
| 405.0  | .035 | 216.591                             | 639.477                      | 7.628                          | .00002             | .147   |
| 420.0  | .017 | 108.296                             | 319.739                      | 3.814                          | .00001             | .074   |
| 435.0  | .017 | 108.296                             | 319.739                      | 3.814                          | .00001             | .074   |
| 450.0  | .000 | .000                                | .000                         | .000                           | .00000             | .000   |

\* MICROGRAMS PER CUBIC METER

TABLE C-20

EVAPORATION EXPERIMENT NO. BLF4 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TCP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 20%

VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS  
 (PPM/HR BASED ON MIRAN CALIBRATION DATA)

| ELAPSED<br>TIME<br><br>MINUTES | PPM  | MICROGRAMS<br>PER<br>CUBIC<br>METER | *<br>PER<br>METER<br>SQUARED | *<br>PER<br>GRAM/<br>METER SQD | PPM<br>PER<br>DROP | MICROGRAMS<br>PER<br>CUBIC METER<br>PER DROP |
|--------------------------------|------|-------------------------------------|------------------------------|--------------------------------|--------------------|--|
| 0                              | .880 | 5523.071                            | 16306.670                    | 179.579                        | .00060             | 3.752  |
| 20.0                           | .863 | 5414.775                            | 15986.940                    | 176.058                        | .00059             | 3.679  |
| 40.0                           | .828 | 5198.184                            | 15347.460                    | 169.016                        | .00056             | 3.531  |
| 60.0                           | .794 | 4931.593                            | 14707.980                    | 161.973                        | .00054             | 3.384  |
| 80.0                           | .776 | 4873.297                            | 14388.240                    | 158.452                        | .00053             | 3.311  |
| 100.0                          | .742 | 4656.707                            | 13748.760                    | 151.410                        | .00050             | 3.164  |
| 120.0                          | .690 | 4331.820                            | 12789.550                    | 140.846                        | .00047             | 2.943  |
| 140.0                          | .655 | 4115.229                            | 12150.070                    | 133.804                        | .00045             | 2.796  |
| 160.0                          | .621 | 3898.638                            | 11510.590                    | 126.762                        | .00042             | 2.649  |
| 180.0                          | .587 | 3682.047                            | 10871.120                    | 119.719                        | .00040             | 2.501  |
| 200.0                          | .535 | 3357.160                            | 9911.899                     | 109.156                        | .00036             | 2.281  |
| 220.0                          | .500 | 3140.549                            | 9272.422                     | 102.114                        | .00034             | 2.134  |
| 240.0                          | .449 | 2815.653                            | 8313.207                     | 91.550                         | .00030             | 1.913  |
| 260.0                          | .414 | 2599.092                            | 7673.729                     | 84.508                         | .00028             | 1.766  |
| 280.0                          | .362 | 2274.206                            | 6714.513                     | 73.944                         | .00025             | 1.545  |
| 300.0                          | .310 | 1949.319                            | 5755.297                     | 63.381                         | .00021             | 1.324  |
| 320.0                          | .259 | 1624.432                            | 4796.081                     | 52.817                         | .00018             | 1.104  |
| 340.0                          | .207 | 1299.546                            | 3836.865                     | 42.254                         | .00014             | .883   |
| 360.0                          | .155 | 974.659                             | 2877.648                     | 31.690                         | .00011             | .662   |
| 380.0                          | .104 | 649.773                             | 1918.432                     | 21.127                         | .00007             | .441   |
| 400.0                          | .069 | 433.182                             | 1278.955                     | 14.085                         | .00005             | .294   |
| 420.0                          | .052 | 324.887                             | 959.216                      | 10.563                         | .00004             | .221   |
| 440.0                          | .035 | 216.591                             | 639.477                      | 7.042                          | .00002             | .147   |
| 460.0                          | .035 | 216.591                             | 639.477                      | 7.042                          | .00002             | .147   |
| 480.0                          | .017 | 108.296                             | 319.739                      | 3.521                          | .00001             | .074   |
| 500.0                          | .017 | 108.296                             | 319.739                      | 3.521                          | .00001             | .074   |
| 520.0                          | .017 | 108.296                             | 319.739                      | 3.521                          | .00001             | .074   |
| 540.0                          | .017 | 108.296                             | 319.739                      | 3.521                          | .00001             | .074   |
| 560.0                          | .000 | .000                                | .000                         | .000                           | .00000             | .000   |

\* MICROGRAMS PER CUBIC METER

TABLE C-21

EVAPORATION EXPERIMENT NO. 9LFS SERIES 10 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS  
 (PPM/AB BASED ON MIRAN CALIBRATION DATA)

| ELAPSED<br>TIME<br>MINUTES | PPM   | MICROGRAMS<br>PER<br>CUBIC<br>METER | PER<br>METER<br>SQUARED | *<br>PER<br>GRAM/<br>METER SQD | PPM<br>PER<br>DROP | MICROGRAMS<br>PER<br>CUBIC METER<br>PER DROP |
|----------------------------|-------|-------------------------------------|-------------------------|--------------------------------|--------------------|--|
| .0                         | 1.363 | 8555.345                            | 25259.360               | 314.388                        | .00093             | 5.812  |
| 30.0                       | 1.242 | 7797.276                            | 23021.190               | 286.531                        | .00084             | 5.297  |
| 50.0                       | 1.156 | 7255.799                            | 21422.490               | 266.633                        | .00079             | 4.929  |
| 90.0                       | 1.121 | 7039.207                            | 20783.020               | 256.674                        | .00075             | 4.782  |
| 120.0                      | 1.087 | 6822.617                            | 20143.540               | 250.715                        | .00074             | 4.635  |
| 150.0                      | 1.052 | 6606.026                            | 19504.060               | 242.755                        | .00071             | 4.488  |
| 180.0                      | 1.035 | 6497.730                            | 19184.320               | 238.715                        | .00070             | 4.414  |
| 210.0                      | 1.000 | 6281.139                            | 18544.840               | 230.817                        | .00068             | 4.267  |
| 240.0                      | .966  | 6064.548                            | 17905.370               | 222.857                        | .00066             | 4.120  |
| 270.0                      | .932  | 5847.957                            | 17265.890               | 214.898                        | .00063             | 3.973  |
| 300.0                      | .897  | 5631.366                            | 16626.410               | 206.939                        | .00061             | 3.826  |
| 330.0                      | .863  | 5414.775                            | 15986.940               | 198.980                        | .00059             | 3.679  |
| 360.0                      | .811  | 5089.888                            | 15027.720               | 187.041                        | .00055             | 3.458  |
| 390.0                      | .759  | 4765.002                            | 14068.500               | 175.102                        | .00052             | 3.237  |
| 420.0                      | .707  | 4440.116                            | 13109.290               | 163.163                        | .00048             | 3.016  |
| 450.0                      | .655  | 4115.229                            | 12150.070               | 151.225                        | .00045             | 2.796  |
| 480.0                      | .604  | 3790.343                            | 11190.850               | 139.286                        | .00041             | 2.575  |
| 510.0                      | .552  | 3465.456                            | 10231.640               | 127.347                        | .00038             | 2.354  |
| 540.0                      | .517  | 3248.865                            | 9592.161                | 119.388                        | .00035             | 2.207  |
| 570.0                      | .466  | 2923.979                            | 8632.945                | 107.449                        | .00032             | 1.986  |
| 600.0                      | .414  | 2599.092                            | 7673.729                | 95.510                         | .00028             | 1.766  |
| 630.0                      | .362  | 2274.206                            | 6714.513                | 83.572                         | .00025             | 1.545  |
| 660.0                      | .310  | 1949.319                            | 5755.297                | 71.633                         | .00021             | 1.324  |
| 690.0                      | .259  | 1624.432                            | 4796.081                | 59.694                         | .00018             | 1.104  |
| 720.0                      | .207  | 1299.546                            | 3836.865                | 47.755                         | .00014             | .883   |
| 750.0                      | .172  | 1082.955                            | 3197.387                | 39.796                         | .00012             | .736   |
| 780.0                      | .155  | 974.659                             | 2877.648                | 35.816                         | .00011             | .662   |
| 810.0                      | .138  | 866.364                             | 2557.910                | 31.837                         | .00009             | .589   |
| 840.0                      | .121  | 758.069                             | 2238.171                | 27.857                         | .00008             | .515   |
| 870.0                      | .104  | 649.773                             | 1918.432                | 23.878                         | .00007             | .441   |
| 900.0                      | .086  | 541.477                             | 1598.693                | 19.898                         | .00006             | .368   |
| 930.0                      | .052  | 324.887                             | 959.216                 | 11.939                         | .00004             | .221   |
| 960.0                      | .052  | 324.887                             | 959.216                 | 11.939                         | .00004             | .221   |
| 990.0                      | .052  | 324.887                             | 959.216                 | 11.939                         | .00004             | .221   |
| 1020.0                     | .035  | 216.591                             | 639.477                 | 7.959                          | .00002             | .147   |
| 1050.0                     | .035  | 216.591                             | 639.477                 | 7.959                          | .00002             | .147   |
| 1080.0                     | .017  | 108.296                             | 319.739                 | 3.980                          | .00001             | .074   |
| 1110.0                     | .017  | 108.296                             | 319.739                 | 3.980                          | .00001             | .074   |
| 1140.0                     | .000  | .000                                | .000                    | .000                           | .00000             | .000   |

\* MICROGRAMS PER CUBIC METER



TABLE C-22

EVAPORATION EXPERIMENT NO. BLF6 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100G CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 2.9 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS  
 (PPM/AB BASED ON MIRAN CALIBRATION DATA)

| ELAPSED<br>TIME<br><br>MINUTES | PPM   | MICROGRAMS<br>PER<br>CUBIC<br>METER | *<br>PER<br>METER<br>SQUARED | *<br>PER<br>GRAM/<br>METER SQD | PPM<br>PER<br>DROP | MICROGRAMS<br>PER<br>CUBIC METER<br>PER DROP |
|--------------------------------|-------|-------------------------------------|------------------------------|--------------------------------|--------------------|--|
| .0                             | 1.414 | 8880.231                            | 26218.580                    | 306.382                        | .00096             | 6.033  |
| 40.0                           | 1.363 | 8555.345                            | 25259.360                    | 295.173                        | .00093             | 5.812  |
| 80.0                           | 1.328 | 8338.754                            | 24619.880                    | 287.700                        | .00090             | 5.665  |
| 120.0                          | 1.259 | 7905.571                            | 23340.920                    | 272.755                        | .00086             | 5.371  |
| 160.0                          | 1.225 | 7688.981                            | 22701.450                    | 265.282                        | .00083             | 5.223  |
| 200.0                          | 1.173 | 7364.095                            | 21742.230                    | 254.073                        | .00080             | 5.003  |
| 240.0                          | 1.121 | 7039.207                            | 20783.020                    | 242.864                        | .00076             | 4.782  |
| 280.0                          | 1.069 | 6714.321                            | 19823.800                    | 231.655                        | .00073             | 4.561  |
| 320.0                          | 1.018 | 6389.435                            | 18864.580                    | 220.446                        | .00069             | 4.341  |
| 360.0                          | .966  | 6064.548                            | 17905.370                    | 209.237                        | .00066             | 4.120  |
| 400.0                          | .914  | 5739.662                            | 16946.150                    | 198.028                        | .00062             | 3.899  |
| 440.0                          | .845  | 5306.479                            | 15667.200                    | 183.082                        | .00057             | 3.605  |
| 480.0                          | .759  | 4765.002                            | 14068.500                    | 164.400                        | .00052             | 3.237  |
| 520.0                          | .673  | 4223.524                            | 12469.810                    | 145.718                        | .00046             | 2.869  |
| 560.0                          | .604  | 3790.343                            | 11190.850                    | 130.773                        | .00041             | 2.575  |
| 600.0                          | .517  | 3248.865                            | 9592.161                     | 112.091                        | .00035             | 2.207  |
| 640.0                          | .431  | 2707.387                            | 7993.468                     | 93.409                         | .00029             | 1.839  |
| 680.0                          | .345  | 2165.910                            | 6394.774                     | 74.727                         | .00023             | 1.471  |
| 720.0                          | .293  | 1841.024                            | 5435.559                     | 63.518                         | .00020             | 1.251  |
| 760.0                          | .242  | 1516.137                            | 4476.342                     | 52.309                         | .00016             | 1.030  |
| 800.0                          | .207  | 1299.546                            | 3835.865                     | 44.836                         | .00014             | .883   |
| 840.0                          | .172  | 1082.955                            | 3197.387                     | 37.364                         | .00012             | .736   |
| 880.0                          | .138  | 866.364                             | 2557.910                     | 29.891                         | .00009             | .589   |
| 920.0                          | .121  | 758.069                             | 2238.171                     | 26.155                         | .00008             | .515   |
| 960.0                          | .104  | 649.773                             | 1918.432                     | 22.418                         | .00007             | .441   |
| 1000.0                         | .086  | 541.477                             | 1598.693                     | 18.682                         | .00006             | .368   |
| 1040.0                         | .069  | 433.182                             | 1278.955                     | 14.945                         | .00005             | .294   |
| 1080.0                         | .052  | 324.887                             | 959.216                      | 11.209                         | .00004             | .221   |
| 1120.0                         | .035  | 216.591                             | 639.477                      | 7.473                          | .00002             | .147   |
| 1160.0                         | .035  | 216.591                             | 639.477                      | 7.473                          | .00002             | .147   |
| 1200.0                         | .017  | 108.296                             | 319.739                      | 3.736                          | .00001             | .074   |
| 1240.0                         | .000  | .000                                | .000                         | .000                           | .00000             | .000   |

\* MICROGRAMS PER CUBIC METER

TABLE C-23

EVAPORATION EXPERIMENT NO. BLF7 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS  
 (PPM/AB BASED ON MIRAN CALIBRATION DATA)

| ELAPSED<br>TIME<br>MINUTES | PPM  | MICROGRAMS<br>PER<br>CUBIC<br>METER | *<br>PER<br>METER<br>SQUARED | *<br>PER<br>GRAM/<br>METER SQD | PPM<br>PER<br>DROP | MICROGRAMS<br>PER<br>CUBIC METER<br>PER DROP |
|----------------------------|------|-------------------------------------|------------------------------|--------------------------------|--------------------|--|
| .0                         | .759 | 4765.002                            | 14068.500                    | 183.046                        | .00052             | 3.237  |
| 15.0                       | .742 | 4656.707                            | 13748.760                    | 178.886                        | .00050             | 3.164  |
| 30.0                       | .707 | 4440.116                            | 13109.290                    | 170.566                        | .00048             | 3.016  |
| 45.0                       | .690 | 4331.820                            | 12789.550                    | 166.406                        | .00047             | 2.943  |
| 60.0                       | .673 | 4223.524                            | 12469.810                    | 162.245                        | .00046             | 2.869  |
| 75.0                       | .638 | 4006.933                            | 11830.330                    | 153.925                        | .00043             | 2.722  |
| 90.0                       | .604 | 3790.343                            | 11190.850                    | 145.605                        | .00041             | 2.575  |
| 105.0                      | .587 | 3682.047                            | 10871.120                    | 141.445                        | .00040             | 2.501  |
| 120.0                      | .552 | 3465.456                            | 10231.640                    | 133.124                        | .00033             | 2.354  |
| 135.0                      | .535 | 3357.160                            | 9911.899                     | 128.964                        | .00036             | 2.281  |
| 150.0                      | .517 | 3248.865                            | 9592.161                     | 124.804                        | .00035             | 2.207  |
| 165.0                      | .483 | 3032.274                            | 8952.685                     | 116.484                        | .00033             | 2.060  |
| 180.0                      | .466 | 2923.979                            | 8632.945                     | 112.324                        | .00032             | 1.986  |
| 195.0                      | .431 | 2707.387                            | 7993.468                     | 104.003                        | .00029             | 1.839  |
| 210.0                      | .397 | 2490.797                            | 7353.991                     | 95.683                         | .00027             | 1.692  |
| 225.0                      | .362 | 2274.206                            | 6714.513                     | 87.363                         | .00025             | 1.545  |
| 240.0                      | .328 | 2057.615                            | 6075.036                     | 79.043                         | .00022             | 1.398  |
| 255.0                      | .276 | 1732.728                            | 5115.820                     | 66.562                         | .00019             | 1.177  |
| 270.0                      | .242 | 1516.137                            | 4476.342                     | 58.242                         | .00016             | 1.030  |
| 285.0                      | .224 | 1407.842                            | 4156.604                     | 54.082                         | .00015             | .956   |
| 300.0                      | .190 | 1191.250                            | 3517.126                     | 45.762                         | .00013             | .809   |
| 315.0                      | .155 | 974.659                             | 2877.643                     | 37.441                         | .00011             | .662   |
| 330.0                      | .138 | 865.364                             | 2557.910                     | 33.281                         | .00009             | .589   |
| 345.0                      | .121 | 758.069                             | 2238.171                     | 29.121                         | .00008             | .515   |
| 360.0                      | .104 | 649.773                             | 1918.432                     | 24.961                         | .00007             | .441   |
| 375.0                      | .086 | 541.477                             | 1598.693                     | 20.801                         | .00006             | .369   |
| 390.0                      | .069 | 433.182                             | 1278.955                     | 16.641                         | .00005             | .294   |
| 405.0                      | .052 | 324.887                             | 959.216                      | 12.480                         | .00004             | .221   |
| 420.0                      | .052 | 324.887                             | 959.216                      | 12.480                         | .00004             | .221   |
| 435.0                      | .035 | 216.591                             | 639.477                      | 8.320                          | .00002             | .147   |
| 450.0                      | .035 | 216.591                             | 639.477                      | 8.320                          | .00002             | .147   |
| 465.0                      | .017 | 108.296                             | 319.739                      | 4.160                          | .00001             | .074   |
| 480.0                      | .017 | 108.296                             | 319.739                      | 4.160                          | .00001             | .074   |
| 495.0                      | .017 | 108.296                             | 319.739                      | 4.160                          | .00001             | .074   |
| 510.0                      | .000 | .000                                | .000                         | .000                           | .00000             | .000   |

\* MICROGRAMS PER CUBIC METER

TABLE C-24

EVAPORATION EXPERIMENT NO. BLFB SERIES ID 2\*\*4 FACTORIAL EXPERIMENT:  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 50%

VAPOR CONTAMINATION FROM A UNIFORM ARRAY OF DEPOSITED DROPLETS  
 (PPM/AB BASED ON MIRAN CALIBRATION DATA)

| ELAPSED<br>TIME<br><br>MINUTES | PPM  | MICROGRAMS<br>PER<br>CUBIC<br>METER | *<br>PER<br>METER<br>SQUARED | *<br>PER<br>GRAM/<br>METER SQD | PPM<br>PER<br>DROP | MICROGRAMS<br>PER<br>CUBIC METER<br>PER DROP |
|--------------------------------|------|-------------------------------------|------------------------------|--------------------------------|--------------------|--|
| .0                             | .850 | 5336.300                            | 15755.240                    | 176.903                        | .00058             | 3.625  |
| 15.0                           | .816 | 5122.848                            | 15125.030                    | 169.827                        | .00055             | 3.460  |
| 30.0                           | .782 | 4909.396                            | 14494.820                    | 162.751                        | .00053             | 3.335  |
| 45.0                           | .748 | 4695.944                            | 13864.610                    | 155.675                        | .00051             | 3.190  |
| 60.0                           | .714 | 4482.492                            | 13234.400                    | 148.598                        | .00049             | 3.045  |
| 75.0                           | .697 | 4375.766                            | 12919.300                    | 145.060                        | .00047             | 2.973  |
| 90.0                           | .680 | 4269.040                            | 12604.190                    | 141.522                        | .00046             | 2.900  |
| 105.0                          | .646 | 4055.588                            | 11973.980                    | 134.446                        | .00044             | 2.755  |
| 120.0                          | .629 | 3948.862                            | 11658.880                    | 130.908                        | .00043             | 2.663  |
| 135.0                          | .612 | 3842.136                            | 11343.770                    | 127.370                        | .00042             | 2.610  |
| 150.0                          | .595 | 3735.410                            | 11028.670                    | 123.832                        | .00040             | 2.538  |
| 165.0                          | .578 | 3628.684                            | 10713.560                    | 120.294                        | .00039             | 2.465  |
| 180.0                          | .561 | 3521.958                            | 10398.460                    | 116.756                        | .00038             | 2.393  |
| 195.0                          | .544 | 3415.232                            | 10083.350                    | 113.218                        | .00037             | 2.320  |
| 210.0                          | .510 | 3201.780                            | 9453.145                     | 106.142                        | .00035             | 2.175  |
| 225.0                          | .493 | 3095.054                            | 9138.039                     | 102.604                        | .00033             | 2.103  |
| 240.0                          | .459 | 2881.602                            | 8507.830                     | 95.528                         | .00031             | 1.958  |
| 255.0                          | .442 | 2774.876                            | 8192.726                     | 91.989                         | .00030             | 1.885  |
| 270.0                          | .425 | 2668.150                            | 7877.621                     | 88.451                         | .00029             | 1.813  |
| 285.0                          | .357 | 2241.246                            | 6617.201                     | 74.299                         | .00024             | 1.523  |
| 300.0                          | .323 | 2027.794                            | 5986.991                     | 67.223                         | .00022             | 1.378  |
| 315.0                          | .289 | 1814.342                            | 5356.782                     | 60.147                         | .00020             | 1.233  |
| 330.0                          | .255 | 1600.890                            | 4726.572                     | 53.071                         | .00017             | 1.088  |
| 345.0                          | .221 | 1387.438                            | 4096.363                     | 45.995                         | .00015             | .943   |
| 360.0                          | .187 | 1173.986                            | 3466.153                     | 38.919                         | .00013             | .798   |
| 375.0                          | .153 | 960.534                             | 2835.943                     | 31.843                         | .00010             | .653   |
| 390.0                          | .119 | 747.082                             | 2205.734                     | 24.766                         | .00008             | .508   |
| 405.0                          | .085 | 533.630                             | 1575.524                     | 17.690                         | .00006             | .363   |
| 420.0                          | .068 | 426.904                             | 1260.419                     | 14.152                         | .00005             | .290   |
| 435.0                          | .034 | 213.452                             | 630.210                      | 7.076                          | .00002             | .145   |
| 450.0                          | .017 | 106.726                             | 315.105                      | 3.538                          | .00001             | .073   |
| 465.0                          | .017 | 106.726                             | 315.105                      | 3.538                          | .00001             | .073   |
| 480.0                          | .000 | .000                                | .000                         | .000                           | .00000             | .000   |

\* MICROGRAMS PER CUBIC METER

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APPENDIX D  
EVAPORATION HISTORY OF TEST DROPLET, MEASURED AND THEORETICAL

TABLE D-1

EVAPORATION EXPERIMENT NO. GLF1 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/TOP SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 45%

## EVAPORATION HISTORY OF TEST DROPLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |            |                 |            | THEORETICAL HALF LIFE MODEL DATA |            |            |            |
|-----------------|-------------------------------|------------|-----------------|------------|----------------------------------|------------|------------|------------|
|                 | RESIDUAL MASS                 |            | CUMULATIVE MASS |            | MASS                             | MASS       | TIME       | TIME       |
|                 | MILLIGRAMS                    | FRACTIONAL | MILLIGRAMS      | FRACTIONAL | MILLIGRAMS                       | FRACTIONAL | FRACTIONAL | HALF-LIVES |
| .0              | 6.20707                       | 1.000000   | .000000         | .000000    | 6.20707                          | 1.000000   | .0000      | .00000     |
| 30.0            | 5.66969                       | .913426    | .537370         | .08657     | 5.70427                          | .918997    | .0345      | .12187     |
| 60.0            | 5.19179                       | .836432    | 1.015277        | .16357     | 5.24221                          | .844555    | .0690      | .24374     |
| 90.0            | 4.76674                       | .767953    | 1.440328        | .23205     | 4.81757                          | .776143    | .1034      | .36561     |
| 120.0           | 4.37913                       | .705507    | 1.827939        | .29449     | 4.42733                          | .713273    | .1379      | .48747     |
| 150.0           | 4.02455                       | .648382    | 2.182515        | .35162     | 4.06870                          | .655495    | .1724      | .60934     |
| 180.0           | 3.70521                       | .596934    | 2.501854        | .40307     | 3.73912                          | .602398    | .2069      | .73121     |
| 210.0           | 3.41671                       | .550454    | 2.790360        | .44955     | 3.43624                          | .553601    | .2414      | .85308     |
| 240.0           | 3.15243                       | .507877    | 3.054640        | .49212     | 3.15789                          | .508758    | .2759      | .97495     |
| 270.0           | 2.91457                       | .469557    | 3.292493        | .53044     | 2.90209                          | .467547    | .3103      | 1.09682    |
| 300.0           | 2.70095                       | .435141    | 3.506119        | .56486     | 2.66701                          | .429674    | .3448      | 1.21869    |
| 330.0           | 2.50934                       | .404272    | 3.697723        | .59573     | 2.45098                          | .394869    | .3793      | 1.34055    |
| 360.0           | 2.33976                       | .376951    | 3.867303        | .62305     | 2.25244                          | .362883    | .4138      | 1.46242    |
| 390.0           | 2.19000                       | .352824    | 4.017062        | .64718     | 2.06998                          | .333488    | .4483      | 1.58429    |
| 420.0           | 2.05786                       | .331536    | 4.149202        | .66846     | 1.90231                          | .306475    | .4828      | 1.70616    |
| 450.0           | 1.94554                       | .313440    | 4.261521        | .68656     | 1.74821                          | .281649    | .5172      | 1.82803    |
| 480.0           | 1.85305                       | .298538    | 4.354019        | .70146     | 1.60660                          | .258835    | .5517      | 1.94990    |
| 510.0           | 1.77817                       | .286475    | 4.428898        | .71353     | 1.47646                          | .237868    | .5862      | 2.07177    |
| 540.0           | 1.71870                       | .276895    | 4.488362        | .72311     | 1.35686                          | .219600    | .6207      | 2.19364    |
| 570.0           | 1.67025                       | .269089    | 4.536813        | .73091     | 1.24695                          | .200893    | .6552      | 2.31550    |
| 600.0           | 1.63061                       | .262702    | 4.576455        | .73730     | 1.14595                          | .184620    | .6897      | 2.43737    |
| 630.0           | 1.59978                       | .257735    | 4.607288        | .74227     | 1.05312                          | .169665    | .7241      | 2.55924    |
| 660.0           | 1.57555                       | .253832    | 4.631514        | .74617     | .96781                           | .155921    | .7586      | 2.68111    |
| 690.0           | 1.55573                       | .250639    | 4.651335        | .74936     | .88942                           | .143291    | .7931      | 2.80298    |
| 720.0           | 1.54031                       | .248155    | 4.666751        | .75185     | .81737                           | .131684    | .8276      | 2.92485    |
| 750.0           | 1.52930                       | .246381    | 4.677763        | .75362     | .75116                           | .121017    | .8621      | 3.04672    |
| 780.0           | 1.52049                       | .244962    | 4.686572        | .75504     | .69032                           | .111214    | .8966      | 3.16858    |
| 810.0           | 1.51389                       | .243897    | 4.693179        | .75610     | .63440                           | .102206    | .9310      | 3.29045    |
| 840.0           | 1.50948                       | .243188    | 4.697584        | .75681     | .58301                           | .093927    | .9655      | 3.41232    |
| 870.0           | 1.50728                       | .242833    | 4.699786        | .75717     | .53578                           | .086318    | 1.0000     | 3.53419    |

TABLE D-2

EVAPORATION EXPERIMENT NO. GLF2 SERIES 1D 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/TOP SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 39%

## EVAPORATION HISTORY OF TEST DROPLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |            |                 |            | THEORETICAL HALF LIFE MODEL DATA |            |            |            |
|-----------------|-------------------------------|------------|-----------------|------------|----------------------------------|------------|------------|------------|
|                 | RESIDUAL MASS                 |            | CUMULATIVE MASS |            | MASS                             | MASS       | TIME       | TIME       |
|                 | MILLIGRAMS                    | FRACTIONAL | MILLIGRAMS      | FRACTIONAL | MILLIGRAMS                       | FRACTIONAL | FRACTIONAL | HALF-LIVES |
| .0              | 6.46739                       | 1.000000   | .000000         | .000000    | 6.46739                          | 1.000000   | .0000      | .00000     |
| 30.0            | 5.98728                       | .925765    | .480109         | .07424     | 5.97791                          | .924316    | .0294      | .11354     |
| 60.0            | 5.54241                       | .856978    | .924981         | .14302     | 5.52548                          | .854360    | .0583      | .22708     |
| 90.0            | 5.13057                       | .793299    | 1.336819        | .20670     | 5.10729                          | .789699    | .0882      | .34063     |
| 120.0           | 4.74737                       | .734047    | 1.720025        | .26595     | 4.72075                          | .729932    | .1176      | .45417     |
| 150.0           | 4.38839                       | .678540    | 2.079005        | .32146     | 4.36347                          | .674688    | .1471      | .56771     |
| 180.0           | 4.05363                       | .626780    | 2.413761        | .37322     | 4.03322                          | .623525    | .1765      | .68125     |
| 210.0           | 3.74310                       | .578765    | 2.724290        | .42123     | 3.72797                          | .576426    | .2059      | .77479     |
| 240.0           | 3.45239                       | .533815    | 3.014998        | .46618     | 3.44583                          | .532800    | .2353      | .850833    |
| 270.0           | 3.18151                       | .491930    | 3.285886        | .50807     | 3.18503                          | .492476    | .2647      | 1.02188    |
| 300.0           | 2.93254                       | .453450    | 3.534750        | .54655     | 2.94398                          | .455203    | .2941      | 1.13542    |
| 330.0           | 2.70360                       | .418035    | 3.763793        | .58196     | 2.72117                          | .420752    | .3235      | 1.24896    |
| 360.0           | 2.49217                       | .385345    | 3.975217        | .61466     | 2.51522                          | .388908    | .3529      | 1.36250    |
| 390.0           | 2.29837                       | .355378    | 4.169023        | .64462     | 2.32486                          | .359474    | .3824      | 1.47604    |
| 420.0           | 2.12218                       | .328136    | 4.345210        | .67186     | 2.14890                          | .332267    | .4118      | 1.58958    |
| 450.0           | 1.96361                       | .303618    | 4.503778        | .69638     | 1.98627                          | .307120    | .4412      | 1.70313    |
| 480.0           | 1.82266                       | .281824    | 4.644727        | .71818     | 1.83594                          | .283875    | .4706      | 1.81667    |
| 510.0           | 1.69933                       | .262754    | 4.768058        | .73725     | 1.69699                          | .262391    | .5000      | 1.93021    |
| 540.0           | 1.59362                       | .246409    | 4.873771        | .75359     | 1.56855                          | .242532    | .5294      | 2.04375    |
| 570.0           | 1.50332                       | .232447    | 4.964067        | .76755     | 1.44984                          | .224177    | .5588      | 2.15729    |
| 600.0           | 1.42624                       | .220528    | 5.041148        | .77947     | 1.34011                          | .207210    | .5882      | 2.27083    |
| 630.0           | 1.36237                       | .210653    | 5.105017        | .78935     | 1.23860                          | .191523    | .6176      | 2.38438    |
| 660.0           | 1.30952                       | .202480    | 5.157873        | .79752     | 1.14494                          | .177032    | .6471      | 2.49792    |
| 690.0           | 1.26327                       | .195329    | 5.204121        | .80467     | 1.05828                          | .163634    | .6765      | 2.61146    |
| 720.0           | 1.22363                       | .189200    | 5.243763        | .81080     | .97819                           | .151249    | .7059      | 2.72500    |
| 750.0           | 1.19059                       | .184092    | 5.276799        | .81591     | .90415                           | .139802    | .7353      | 2.83854    |
| 780.0           | 1.15976                       | .179324    | 5.307631        | .82068     | .83572                           | .129221    | .7647      | 2.95208    |
| 810.0           | 1.13113                       | .174897    | 5.336262        | .82510     | .77247                           | .119441    | .7941      | 3.06563    |
| 840.0           | 1.10690                       | .171152    | 5.360487        | .82885     | .71401                           | .110402    | .8235      | 3.17917    |
| 870.0           | 1.08708                       | .168087    | 5.380308        | .83191     | .65797                           | .102046    | .8529      | 3.29271    |
| 900.0           | 1.07167                       | .165703    | 5.395724        | .83430     | .61002                           | .094323    | .8824      | 3.40625    |
| 930.0           | 1.06066                       | .164000    | 5.406736        | .83600     | .56385                           | .087184    | .9116      | 3.51979    |
| 960.0           | 1.05405                       | .162979    | 5.413347        | .83702     | .52118                           | .080586    | .9412      | 3.63333    |
| 990.0           | 1.04964                       | .162298    | 5.417747        | .83770     | .48173                           | .074487    | .9706      | 3.74688    |
| 1020.0          | 1.04744                       | .161957    | 5.419950        | .83804     | .44577                           | .068849    | 1.0000     | 3.86042    |

TABLE D-3

EVAPORATION EXPERIMENT NO. GLF3 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 40%

## EVAPORATION HISTORY OF TEST DROPLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |            |                 |            | THEORETICAL HALF LIFE MODEL DATA |            |            |            |
|-----------------|-------------------------------|------------|-----------------|------------|----------------------------------|------------|------------|------------|
|                 | RESIDUAL MASS                 |            | CUMULATIVE MASS |            | MASS                             | MASS       | TIME       | TIME       |
|                 | MILLIGRAMS                    | FRACTIONAL | MILLIGRAMS      | FRACTIONAL | MILLIGRAMS                       | FRACTIONAL | FRACTIONAL | HALF-LIVES |
| .0              | 5.54674                       | 1.000000   | .000000         | .000000    | 5.54674                          | 1.000000   | .0000      | .00000     |
| 15.0            | 4.89668                       | .882804    | .650056         | .11720     | 4.89933                          | .883291    | .0417      | .17906     |
| 30.0            | 4.32738                       | .780166    | 1.219360        | .21983     | 4.32749                          | .780185    | .0833      | .35811     |
| 45.0            | 3.82268                       | .689175    | 1.724062        | .31082     | 3.82239                          | .639123    | .1250      | .53717     |
| 60.0            | 3.37450                       | .608376    | 2.172238        | .39162     | 3.37624                          | .608689    | .1667      | .71622     |
| 75.0            | 2.97881                       | .537039    | 2.567924        | .46296     | 2.98217                          | .537644    | .2083      | .89528     |
| 90.0            | 2.62754                       | .473709    | 2.919197        | .52629     | 2.63409                          | .474891    | .2507      | 1.07433    |
| 105.0           | 2.31665                       | .417659    | 3.230093        | .58234     | 2.32664                          | .419462    | .2917      | 1.25339    |
| 120.0           | 2.04613                       | .368888    | 3.500614        | .63111     | 2.05508                          | .370503    | .3333      | 1.43244    |
| 135.0           | 1.81598                       | .327393    | 3.730758        | .67260     | 1.81521                          | .327258    | .3750      | 1.61150    |
| 150.0           | 1.62621                       | .293184    | 3.920526        | .70682     | 1.60334                          | .289061    | .4167      | 1.79056    |
| 165.0           | 1.46875                       | .264794    | 4.077993        | .73521     | 1.41620                          | .255322    | .4583      | 1.96961    |
| 180.0           | 1.33550                       | .240773    | 4.211235        | .75923     | 1.25091                          | .225321    | .5000      | 2.14867    |
| 195.0           | 1.22649                       | .221119    | 4.320250        | .77888     | 1.10490                          | .199198    | .5417      | 2.32772    |
| 210.0           | 1.14170                       | .205832    | 4.405040        | .79417     | .97594                           | .175948    | .5833      | 2.50678    |
| 225.0           | 1.07710                       | .194186    | 4.469642        | .80581     | .86203                           | .155412    | .6250      | 2.68583    |
| 240.0           | 1.02865                       | .185450    | 4.518094        | .81455     | .76141                           | .137272    | .6667      | 2.86489    |
| 255.0           | .99231                        | .178899    | 4.554432        | .82110     | .67254                           | .121250    | .7083      | 3.04394    |
| 270.0           | .96001                        | .173076    | 4.586733        | .82692     | .59404                           | .107098    | .7500      | 3.22300    |
| 285.0           | .93174                        | .167980    | 4.614996        | .83202     | .52471                           | .094597    | .7917      | 3.40206    |
| 300.0           | .90752                        | .163613    | 4.639223        | .83639     | .46346                           | .083556    | .8333      | 3.58111    |
| 315.0           | .88733                        | .159973    | 4.659410        | .84003     | .40937                           | .073804    | .8750      | 3.76017    |
| 330.0           | .87522                        | .157789    | 4.671524        | .84221     | .36159                           | .065189    | .9167      | 3.93922    |
| 345.0           | .86714                        | .156333    | 4.679599        | .84367     | .31938                           | .057580    | .9583      | 4.11828    |
| .0              | .86310                        | .155605    | 4.683637        | .84439     | .28211                           | .050866    | 1.0000     | 4.29733    |



TABLE C-4

EVAPORATION EXPERIMENT NO. GLF4 SERIES 10 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICAZORY/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

## EVAPORATION HISTORY OF TEST DROPLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |            |                 |            | THEORETICAL HALF LIFE MODEL DATA |            |            |            |
|-----------------|-------------------------------|------------|-----------------|------------|----------------------------------|------------|------------|------------|
|                 | RESIDUAL MASS                 |            | CUMULATIVE MASS |            | MASS                             | MASS       | TIME       | TIME       |
|                 | MILLIGRAMS                    | FRACTIONAL | MILLIGRAMS      | FRACTIONAL | MILLIGRAMS                       | FRACTIONAL | FRACTIONAL | HALF-LIVES |
| .0              | 6.46739                       | 1.000000   | .000000         | .00000     | 6.46739                          | 1.000000   | .0000      | .00000     |
| 10.0            | 6.07709                       | .939651    | .390303         | .06035     | 6.02601                          | .931891    | .0276      | 10177      |
| 20.0            | 5.69217                       | .880134    | .775222         | .11987     | 5.61642                          | .868422    | .0541      | .20353     |
| 30.0            | 5.31802                       | .822282    | 1.149375        | .17772     | 5.23389                          | .800775    | .0811      | .30530     |
| 40.0            | 4.96271                       | .767343    | 1.561685        | .23266     | 4.87142                          | .734156    | .1081      | .40707     |
| 50.0            | 4.62893                       | .715734    | 1.838462        | .28427     | 4.54523                          | .702792    | .1351      | .50883     |
| 60.0            | 4.31130                       | .66622     | 2.156087        | .33378     | 4.23566                          | .654925    | .1622      | .61060     |
| 70.0            | 4.00714                       | .619591    | 2.460255        | .38041     | 3.94717                          | .610319    | .1892      | .71236     |
| 80.0            | 3.71911                       | .575057    | 2.748271        | .42494     | 3.67834                          | .568751    | .2162      | .81413     |
| 90.0            | 3.44725                       | .533021    | 3.020138        | .46698     | 3.42781                          | .530014    | .2432      | .91590     |
| 100.0           | 3.18885                       | .493065    | 3.278545        | .50693     | 3.19435                          | .493916    | .2703      | 1.01766    |
| 110.0           | 2.94390                       | .455191    | 3.523494        | .54481     | 2.97678                          | .460273    | .2973      | 1.11943    |
| 120.0           | 2.71510                       | .419814    | 3.752292        | .58019     | 2.77104                          | .428927    | .3243      | 1.22120    |
| 130.0           | 2.49976                       | .386517    | 3.967632        | .61348     | 2.58510                          | .399714    | .3514      | 1.32296    |
| 140.0           | 2.29519                       | .354886    | 4.172206        | .64511     | 2.40904                          | .372490    | .3784      | 1.42473    |
| 150.0           | 2.10407                       | .325336    | 4.363318        | .67466     | 2.24496                          | .347120    | .4056      | 1.52649    |
| 160.0           | 1.92642                       | .297866    | 4.540974        | .70213     | 2.09206                          | .323478    | .4324      | 1.62826    |
| 170.0           | 1.75953                       | .272062    | 4.707862        | .72754     | 1.94957                          | .301446    | .4595      | 1.73003    |
| 180.0           | 1.60341                       | .247922    | 4.863983        | .75208     | 1.81679                          | .280915    | .4865      | 1.83179    |
| 190.0           | 1.45805                       | .225447    | 5.009337        | .77455     | 1.69305                          | .261783    | .5135      | 1.93356    |
| 200.0           | 1.32367                       | .204637    | 5.143925        | .79536     | 1.57774                          | .243953    | .5405      | 2.03533    |
| 210.0           | 1.19965                       | .185492    | 5.267745        | .81451     | 1.47028                          | .227338    | .5676      | 2.13709    |
| 220.0           | 1.08659                       | .168011    | 5.380798        | .83199     | 1.37014                          | .211854    | .5946      | 2.23886    |
| 230.0           | .96431                        | .152155    | 5.483084        | .84780     | 1.27682                          | .197425    | .6216      | 2.34062    |
| 240.0           | .89279                        | .138043    | 5.574603        | .86196     | 1.18926                          | .183979    | .6486      | 2.44239    |
| 250.0           | .81204                        | .125558    | 5.655355        | .87444     | 1.10832                          | .171448    | .6757      | 2.54416    |
| 260.0           | .73936                        | .114321    | 5.728033        | .88568     | 1.03330                          | .159771    | .7027      | 2.64592    |
| 270.0           | .67476                        | .104332    | 5.792636        | .89567     | .96222                           | .148889    | .7297      | 2.74769    |
| 280.0           | .62092                        | .096008    | 5.848469        | .90499     | .89734                           | .138749    | .7568      | 2.84946    |
| 290.0           | .57516                        | .088933    | 5.892230        | .91307     | .83622                           | .129299    | .7838      | 2.95122    |
| 300.0           | .53479                        | .082690    | 5.932805        | .91731     | .77927                           | .120492    | .8108      | 3.05299    |
| 310.0           | .49879                        | .077279    | 5.967598        | .92272     | .72620                           | .112285    | .8378      | 3.15475    |
| 320.0           | .47018                        | .072701    | 5.997297        | .92730     | .67674                           | .104638    | .8649      | 3.25652    |
| 330.0           | .44598                        | .068955    | 6.021433        | .93105     | .63064                           | .097511    | .8919      | 3.35829    |
| 340.0           | .42981                        | .066458    | 6.037583        | .93354     | .58769                           | .090870    | .9189      | 3.46005    |
| 350.0           | .41904                        | .064793    | 6.048350        | .93521     | .54766                           | .084681    | .9459      | 3.56182    |
| 360.0           | .41097                        | .063544    | 6.056426        | .93646     | .51036                           | .078911    | .9730      | 3.66359    |
| 370.0           | .40827                        | .063128    | 6.059118        | .93687     | .47560                           | .073539    | 1.0000     | 3.76535    |

TABLE D-5

EVAPORATION EXPERIMENT NO. GLF5 SERIES 10 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON WICKORY/BOTTOM SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 58%

## EVAPORATION HISTORY OF TEST DROPLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |            |                 |            | THEORETICAL HALF LIFE MODEL DATA |            |            |            |
|-----------------|-------------------------------|------------|-----------------|------------|----------------------------------|------------|------------|------------|
|                 | RESIDUAL MASS                 |            | CUMULATIVE MASS |            | MASS                             |            | TIME       | TIME       |
|                 | MILLIGRAMS                    | FRACTIONAL | MILLIGRAMS      | FRACTIONAL | MILLIGRAMS                       | FRACTIONAL | FRACTIONAL | HALF-LIVES |
| 0.0             | 5.54674                       | 1.000000   | .000000         | .000000    | 5.54674                          | 1.000000   | .0000      | .00000     |
| 30.0            | 5.21198                       | .937648    | .334755         | .060355    | 5.19749                          | .937035    | .0345      | .09382     |
| 60.0            | 4.89264                       | .882076    | .654094         | .11792     | 4.87023                          | .878035    | .0690      | .18765     |
| 90.0            | 4.58872                       | .827283    | .958016         | .17272     | 4.56358                          | .822750    | .1034      | .26147     |
| 120.0           | 4.30242                       | .775666    | 1.244320        | .22433     | 4.27623                          | .770945    | .1379      | .37530     |
| 150.0           | 4.03153                       | .726829    | 1.515208        | .27317     | 4.00698                          | .722403    | .1724      | .46912     |
| 180.0           | 3.77606                       | .680771    | 1.770879        | .31923     | 3.75468                          | .674917    | .2069      | .56295     |
| 210.0           | 3.53601                       | .637493    | 2.010753        | .36251     | 3.51827                          | .634275    | .2414      | .65671     |
| 240.0           | 3.30917                       | .596596    | 2.237574        | .40340     | 3.29674                          | .594357    | .2759      | .75060     |
| 270.0           | 3.09554                       | .558083    | 2.451200        | .44192     | 3.08916                          | .556933    | .3103      | .84462     |
| 300.0           | 2.89513                       | .521951    | 2.651613        | .47805     | 2.89465                          | .521846    | .3448      | .93825     |
| 330.0           | 2.71013                       | .488599    | 2.835610        | .51140     | 2.71239                          | .489007    | .3793      | 1.03207    |
| 360.0           | 2.54275                       | .458423    | 3.003987        | .54153     | 2.54161                          | .458217    | .4138      | 1.12590    |
| 390.0           | 2.39079                       | .431026    | 3.155948        | .56897     | 2.38150                          | .429365    | .4483      | 1.21972    |
| 420.0           | 2.25204                       | .406012    | 3.294395        | .59399     | 2.23162                          | .402330    | .4828      | 1.31359    |
| 450.0           | 2.12631                       | .382983    | 3.422431        | .61702     | 2.09111                          | .376998    | .5172      | 1.40737    |
| 480.0           | 2.00758                       | .361546    | 3.539155        | .63806     | 1.95944                          | .353260    | .5517      | 1.50120    |
| 510.0           | 1.90187                       | .342881    | 3.644867        | .65712     | 1.83606                          | .331017    | .5862      | 1.59502    |
| 540.0           | 1.80997                       | .325411    | 3.741770        | .67459     | 1.72046                          | .310175    | .6207      | 1.68885    |
| 570.0           | 1.71902                       | .309926    | 3.827661        | .69007     | 1.61213                          | .290643    | .6552      | 1.78267    |
| 600.0           | 1.64420                       | .296426    | 3.902540        | .70357     | 1.51052                          | .272344    | .6897      | 1.87650    |
| 630.0           | 1.58033                       | .284912    | 3.966408        | .71309     | 1.41550                          | .255196    | .7241      | 1.97032    |
| 660.0           | 1.52747                       | .275383    | 4.019264        | .72462     | 1.32638                          | .239126    | .7585      | 2.06415    |
| 690.0           | 1.48563                       | .267839    | 4.061109        | .73216     | 1.24225                          | .224071    | .7931      | 2.15797    |
| 720.0           | 1.45480                       | .262280    | 4.091941        | .73772     | 1.16461                          | .209962    | .8276      | 2.25180    |
| 750.0           | 1.43277                       | .258309    | 4.113964        | .74169     | 1.09128                          | .196742    | .8621      | 2.34562    |
| 780.0           | 1.41736                       | .255530    | 4.129380        | .74447     | 1.02257                          | .184356    | .8966      | 2.43945    |
| 810.0           | 1.40635                       | .253545    | 4.140392        | .74646     | .95813                           | .172747    | .9310      | 2.53327    |
| 840.0           | 1.39974                       | .252354    | 4.146999        | .74765     | .89785                           | .161870    | .9655      | 2.62710    |
| 870.0           | 1.39754                       | .251957    | 4.149201        | .74804     | .84132                           | .151678    | 1.0000     | 2.72092    |

TABLE D-6

EVAPORATION EXPERIMENT NO. GUF6 SERIES ID 1114 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1200 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 37 GMS/SQ METER ON HICKORY/BOTTOM SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 55%

## EVAPORATION HISTORY OF TEST DROPLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |            |                 |            | THEORETICAL HALF LIFE MODEL DATA |            |            |            |
|-----------------|-------------------------------|------------|-----------------|------------|----------------------------------|------------|------------|------------|
|                 | RESIDUAL MASS                 |            | CUMULATIVE MASS |            | MASS                             | MASS       | TIME       | TIME       |
|                 | MILLIGRAMS                    | FRACTIONAL | MILLIGRAMS      | FRACTIONAL | MILLIGRAMS                       | FRACTIONAL | FRACTIONAL | HALF-LIVES |
| 0               | 6.07935                       | 1.000000   | 0.000000        | 0.00000    | 6.07935                          | 1.000000   | 0.0000     | 0.00000    |
| 30.0            | 5.74900                       | .945660    | .330350         | .05434     | 5.71066                          | .939354    | .0333      | .09026     |
| 60.0            | 5.42966                       | .893132    | .649689         | .10687     | 5.36433                          | .882385    | .0667      | .18052     |
| 90.0            | 5.11913                       | .842052    | .950219         | .15795     | 5.03900                          | .828872    | .1000      | .27078     |
| 120.0           | 4.81961                       | .792784    | 1.259735        | .20722     | 4.73341                          | .778604    | .1333      | .36104     |
| 150.0           | 4.53331                       | .745620    | 1.546040        | .25431     | 4.44634                          | .731385    | .1667      | .45130     |
| 180.0           | 4.25581                       | .700044    | 1.823334        | .29996     | 4.17669                          | .687029    | .2000      | .54156     |
| 210.0           | 3.98933                       | .656210    | 2.090017        | .34379     | 3.92339                          | .645363    | .2333      | .63182     |
| 240.0           | 3.73606                       | .614550    | 2.343286        | .38545     | 3.68545                          | .606224    | .2667      | .72208     |
| 270.0           | 3.49601                       | .575062    | 2.583340        | .42494     | 3.46194                          | .569459    | .3000      | .81234     |
| 300.0           | 3.26917                       | .537750    | 2.810181        | .46225     | 3.25199                          | .534924    | .3333      | .90259     |
| 330.0           | 3.05554                       | .502610    | 3.023808        | .49739     | 3.05477                          | .502483    | .3667      | .99285     |
| 360.0           | 2.85513                       | .469644    | 3.224220        | .53036     | 2.86951                          | .472009    | .4000      | 1.08311    |
| 390.0           | 2.66793                       | .438851    | 3.411419        | .56115     | 2.69548                          | .443385    | .4333      | 1.17337    |
| 420.0           | 2.49394                       | .410232    | 3.585403        | .58977     | 2.53201                          | .416494    | .4667      | 1.26363    |
| 450.0           | 2.33317                       | .383787    | 3.746174        | .61621     | 2.37845                          | .391235    | .5000      | 1.35389    |
| 480.0           | 2.18562                       | .359115    | 3.893730        | .64048     | 2.23421                          | .367508    | .5333      | 1.44415    |
| 510.0           | 2.05127                       | .337417    | 4.028073        | .66258     | 2.09871                          | .345220    | .5667      | 1.53441    |
| 540.0           | 1.93015                       | .317492    | 4.149292        | .68251     | 1.97143                          | .324284    | .6000      | 1.62467    |
| 570.0           | 1.82223                       | .299741    | 4.257116        | .70026     | 1.85187                          | .304617    | .6333      | 1.71493    |
| 600.0           | 1.72753                       | .284164    | 4.351817        | .71584     | 1.73957                          | .286143    | .6667      | 1.80519    |
| 630.0           | 1.64504                       | .270760    | 4.433303        | .72924     | 1.63407                          | .268790    | .7000      | 1.89545    |
| 660.0           | 1.57777                       | .259530    | 4.501576        | .74047     | 1.53497                          | .252489    | .7333      | 1.98571    |
| 690.0           | 1.52271                       | .250473    | 4.556634        | .74953     | 1.44188                          | .237176    | .7667      | 2.07597    |
| 720.0           | 1.43087                       | .243590    | 4.598478        | .75641     | 1.35443                          | .222792    | .8000      | 2.16623    |
| 750.0           | 1.35004                       | .238513    | 4.629311        | .76148     | 1.27229                          | .209281    | .8333      | 2.25649    |
| 780.0           | 1.22581                       | .234534    | 4.653537        | .76547     | 1.19513                          | .196589    | .8667      | 2.34675    |
| 810.0           | 1.40819                       | .231635    | 4.671156        | .76836     | 1.12265                          | .184666    | .9000      | 2.43701    |
| 840.0           | 1.39718                       | .229824    | 4.682168        | .77018     | 1.05457                          | .173467    | .9333      | 2.52727    |
| 870.0           | 1.39057                       | .228737    | 4.688775        | .77126     | .99061                           | .162947    | .9667      | 2.61753    |
| 900.0           | 1.38837                       | .228375    | 4.690977        | .77162     | .93953                           | .153065    | 1.0000     | 2.70778    |

TABLE D-7

EVAPORATION EXPERIMENT NO. GL77 SERIES 10 2MA4 FACTORIAL EXPERIMENT  
 DIBENZYLMALEONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/BOTTOM SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 33%

## EVAPORATION HISTORY OF TEST DROPLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |            |                 |            | THEORETICAL HALF LIFE MODEL DATA |            |            |            |
|-----------------|-------------------------------|------------|-----------------|------------|----------------------------------|------------|------------|------------|
|                 | RESIDUAL MASS                 |            | CUMULATIVE MASS |            | MASS                             | MASS       | TIME       | TIME       |
|                 | MILLIGRAMS                    | FRACTIONAL | MILLIGRAMS      | FRACTIONAL | MILLIGRAMS                       | FRACTIONAL | FRACTIONAL | HALF LIVES |
| 0               | 6.07500                       | 1.000000   | .000000         | .000000    | 6.07500                          | 1.000000   | .0000      | .00000     |
| 15.0            | 5.70494                       | .936085    | .370056         | .360911    | 5.66336                          | .932246    | .0313      | .19123     |
| 30.0            | 5.35478                       | .881446    | .720117         | .71855     | 5.27961                          | .869071    | .0625      | .30265     |
| 45.0            | 5.01656                       | .825771    | 1.053441        | .817127    | 4.92183                          | .810197    | .0938      | .50368     |
| 60.0            | 4.69027                       | .772061    | 1.384727        | .76794     | 4.58835                          | .755286    | .1250      | .66491     |
| 75.0            | 4.37990                       | .720972    | 1.695597        | .727933    | 4.27744                          | .703106    | .1563      | .80614     |
| 90.0            | 4.08147                       | .671847    | 1.993570        | .672015    | 3.98760                          | .656396    | .1875      | .96736     |
| 105.0           | 3.79498                       | .623687    | 2.286025        | .627531    | 3.71740                          | .611919    | .2188      | 1.10859    |
| 120.0           | 3.52041                       | .576993    | 2.554363        | .542051    | 3.46551                          | .570495    | .2500      | 1.20982    |
| 135.0           | 3.25780                       | .536260    | 2.817204        | .46774     | 3.23069                          | .531800    | .2813      | 1.31104    |
| 150.0           | 3.00711                       | .494998    | 3.037806        | .50514     | 3.01179                          | .495754    | .3125      | 1.41227    |
| 165.0           | 2.76837                       | .452593    | 3.306632        | .54430     | 2.80770                          | .462172    | .3438      | 1.51350    |
| 180.0           | 2.54354                       | .419019    | 3.522462        | .58098     | 2.61743                          | .430855    | .3750      | 1.61472    |
| 195.0           | 2.33495                       | .384304    | 3.740354        | .61570     | 2.44009                          | .401661    | .4063      | 1.71595    |
| 210.0           | 2.13559                       | .351554    | 3.939310        | .64845     | 2.27775                          | .374414    | .4375      | 1.81718    |
| 225.0           | 1.95265                       | .321424    | 4.122348        | .67853     | 2.12061                          | .349072    | .4688      | 1.91841    |
| 240.0           | 1.78553                       | .293914    | 4.289470        | .70609     | 1.97692                          | .325418    | .5000      | 1.91963    |
| 255.0           | 1.63432                       | .269025    | 4.440676        | .73098     | 1.84297                          | .303608    | .5313      | 1.72036    |
| 270.0           | 1.49903                       | .246755    | 4.575965        | .75325     | 1.71808                          | .282812    | .5625      | 1.82209    |
| 285.0           | 1.37966                       | .227105    | 4.635738        | .77200     | 1.60166                          | .263648    | .5938      | 1.92331    |
| 300.0           | 1.27223                       | .209420    | 4.802774        | .79058     | 1.49213                          | .245783    | .6250      | 2.02454    |
| 315.0           | 1.17673                       | .192700    | 4.898273        | .80630     | 1.39196                          | .229129    | .6563      | 2.12577    |
| 330.0           | 1.09715                       | .180600    | 4.917855        | .81940     | 1.29764                          | .213603    | .6875      | 2.22699    |
| 345.0           | 1.03348                       | .170120    | 5.041520        | .82998     | 1.20971                          | .199129    | .7188      | 2.32822    |
| 360.0           | .98173                        | .161695    | 5.093248        | .83839     | 1.12774                          | .185736    | .7500      | 2.42945    |
| 375.0           | .93798                        | .154400    | 5.137019        | .84560     | 1.05133                          | .173050    | .7813      | 2.53068    |
| 390.0           | .90217                        | .148505    | 5.172831        | .85149     | .98009                           | .161331    | .8125      | 2.63190    |
| 405.0           | .87432                        | .143920    | 5.200625        | .85608     | .91368                           | .150399    | .8438      | 2.73313    |
| 420.0           | .85442                        | .140645    | 5.220580        | .85935     | .85177                           | .140208    | .8750      | 2.83436    |
| 435.0           | .83850                        | .138925    | 5.236496        | .86197     | .79405                           | .130708    | .9063      | 2.93558    |
| 450.0           | .82657                        | .136060    | 5.248434        | .86394     | .74024                           | .121851    | .9375      | 3.03681    |
| 465.0           | .81851                        | .134750    | 5.256392        | .86525     | .69009                           | .113594    | .9688      | 3.13804    |
| 480.0           | .81463                        | .134095    | 5.260371        | .86590     | .64331                           | .105897    | 1.0000     | 3.23926    |

TABLE D-8

EVAPORATION EXPERIMENT NO. SLES SERIES 10 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPE 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/50 METER ON HICKORY/BOTTOM SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 50%

## EVAPORATION HISTORY OF TEST DROFLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |            |                 |            | THEORETICAL HALF LIVE MODEL DATA |            |            |            |
|-----------------|-------------------------------|------------|-----------------|------------|----------------------------------|------------|------------|------------|
|                 | RESIDUAL MASS                 |            | CUMULATIVE MASS |            | MASS                             | MASS       | TIME       | TIME       |
|                 | MILLIGRAMS                    | FRACTIONAL | MILLIGRAMS      | FRACTIONAL | MILLIGRAMS                       | FRACTIONAL | FRACTIONAL | HALF-LIVES |
| 0.0             | 6.46739                       | 1.000000   | .000000         | .000000    | 6.46739                          | 1.000000   | .0000      | .00000     |
| 15.0            | 6.10178                       | .943469    | .365609         | .05653     | 6.04932                          | .935357    | .0313      | .09641     |
| 30.0            | 5.74864                       | .880865    | .718754         | .11114     | 5.65827                          | .874892    | .0625      | .19282     |
| 45.0            | 5.40380                       | .835546    | 1.063590        | .16445     | 5.29250                          | .818336    | .0938      | .28923     |
| 60.0            | 5.07143                       | .784154    | 1.395942        | .21585     | 4.95037                          | .765435    | .1250      | .38565     |
| 75.0            | 4.75152                       | .734689    | 1.715870        | .26531     | 4.63036                          | .715956    | .1563      | .48206     |
| 90.0            | 4.44408                       | .687151    | 2.023314        | .31285     | 4.33104                          | .669674    | .1875      | .57847     |
| 105.0           | 4.14910                       | .641541    | 2.318294        | .35846     | 4.05107                          | .626384    | .2188      | .67488     |
| 120.0           | 3.86843                       | .597216    | 2.604965        | .40278     | 3.78919                          | .585892    | .2500      | .77129     |
| 135.0           | 3.58822                       | .554817    | 2.879172        | .44518     | 3.54425                          | .548018    | .2813      | .86770     |
| 150.0           | 3.32668                       | .514346    | 3.140914        | .48565     | 3.31514                          | .512592    | .3125      | .96412     |
| 165.0           | 3.07720                       | .475802    | 3.390193        | .52420     | 3.10083                          | .479457    | .3438      | 1.06053    |
| 180.0           | 2.84038                       | .439185    | 3.627008        | .56081     | 2.90039                          | .448463    | .3750      | 1.15694    |
| 195.0           | 2.61603                       | .404496    | 3.851359        | .59550     | 2.71289                          | .419473    | .4063      | 1.25335    |
| 210.0           | 2.40414                       | .371713    | 4.063247        | .62827     | 2.53752                          | .392357    | .4375      | 1.34976    |
| 225.0           | 2.20472                       | .340898    | 4.262670        | .65910     | 2.37349                          | .366993    | .4688      | 1.44617    |
| 240.0           | 2.01778                       | .311990    | 4.449529        | .68801     | 2.22055                          | .343270    | .5000      | 1.54259    |
| 255.0           | 1.84327                       | .285009    | 4.624125        | .71499     | 2.07655                          | .321080    | .5313      | 1.63900    |
| 270.0           | 1.68124                       | .259956    | 4.786156        | .74004     | 1.94231                          | .300324    | .5625      | 1.73541    |
| 285.0           | 1.53167                       | .236829    | 4.935723        | .76317     | 1.81675                          | .280910    | .5938      | 1.83182    |
| 300.0           | 1.39456                       | .215430    | 5.072827        | .78437     | 1.69931                          | .262751    | .6250      | 1.92823    |
| 315.0           | 1.26992                       | .196358    | 5.197466        | .80364     | 1.58946                          | .245766    | .6563      | 2.02464    |
| 330.0           | 1.15715                       | .179013    | 5.309642        | .82099     | 1.48672                          | .229879    | .6875      | 2.12105    |
| 345.0           | 1.05804                       | .163596    | 5.409354        | .83640     | 1.39061                          | .215019    | .7188      | 2.21747    |
| 360.0           | .97494                        | .150748    | 5.492447        | .84925     | 1.30072                          | .201119    | .7500      | 2.31388    |
| 375.0           | .90432                        | .139827    | 5.563076        | .86017     | 1.21663                          | .188118    | .7813      | 2.41029    |
| 390.0           | .84615                        | .130833    | 5.621240        | .86917     | 1.13799                          | .175957    | .8125      | 2.50670    |
| 405.0           | .80045                        | .123767    | 5.666942        | .87623     | 1.06442                          | .164583    | .8438      | 2.60311    |
| 420.0           | .76721                        | .118628    | 5.703179        | .88137     | .99561                           | .153944    | .8750      | 2.69952    |
| 435.0           | .74644                        | .115116    | 5.720953        | .88458     | .93125                           | .143992    | .9063      | 2.79594    |
| 450.0           | .73397                        | .113409    | 5.733417        | .88651     | .87106                           | .134684    | .9375      | 2.89235    |
| 465.0           | .72567                        | .112204    | 5.741726        | .88780     | .81475                           | .125978    | .9688      | 2.98876    |
| 480.0           | .72151                        | .111561    | 5.745881        | .88844     | .76208                           | .117834    | 1.0000     | 3.08517    |

TABLE D-9

EVAPORATION EXPERIMENT NO. GLF9 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 44%

## EVAPORATION HISTORY OF TEST DROPLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |            |                 |            | THEORETICAL HALF LIFE MODEL DATA |            |            |            |
|-----------------|-------------------------------|------------|-----------------|------------|----------------------------------|------------|------------|------------|
|                 | RESIDUAL MASS                 |            | CUMULATIVE MASS |            | MASS                             | MASS       | TIME       | TIME       |
|                 | MILLIGRAMS                    | FRACTIONAL | MILLIGRAMS      | FRACTIONAL | MILLIGRAMS                       | FRACTIONAL | FRACTIONAL | HALF-LIVES |
| .0              | 5.15054                       | 1.000000   | .000000         | .000000    | 5.15054                          | 1.000000   | .0000      | .00000     |
| 30.0            | 4.68260                       | .909147    | .467942         | .09085     | 4.73103                          | .918550    | .0385      | .12257     |
| 60.0            | 4.33013                       | .840712    | .920418         | .15929     | 4.34569                          | .843733    | .0769      | .24514     |
| 90.0            | 3.99385                       | .775424    | 1.156689        | .22458     | 3.99173                          | .775011    | .1154      | .36771     |
| 120.0           | 3.67582                       | .713675    | 1.474727        | .28632     | 3.66660                          | .711886    | .1538      | .49028     |
| 150.0           | 3.38209                       | .656647    | 1.768457        | .34335     | 3.36795                          | .653903    | .1923      | .61285     |
| 180.0           | 3.10659                       | .603157    | 2.043956        | .39684     | 3.09363                          | .600642    | .2308      | .73542     |
| 210.0           | 2.84932                       | .553203    | 2.301222        | .44679     | 2.84166                          | .551720    | .2692      | .85799     |
| 240.0           | 2.61029                       | .506798    | 2.540258        | .49320     | 2.61020                          | .506782    | .3077      | .98056     |
| 270.0           | 2.38948                       | .463928    | 2.761061        | .53607     | 2.39760                          | .465504    | .3462      | 1.10313    |
| 300.0           | 2.18691                       | .424598    | 2.963634        | .57540     | 2.20231                          | .427589    | .3846      | 1.22570    |
| 330.0           | 2.00257                       | .388807    | 3.147975        | .61119     | 2.02293                          | .392761    | .4231      | 1.34827    |
| 360.0           | 1.83646                       | .356556    | 3.314084        | .64344     | 1.85817                          | .360771    | .4615      | 1.47085    |
| 390.0           | 1.68858                       | .327845    | 3.461962        | .67215     | 1.70682                          | .331386    | .5000      | 1.59342    |
| 420.0           | 1.55893                       | .302674    | 3.591609        | .69733     | 1.56780                          | .304394    | .5385      | 1.71599    |
| 450.0           | 1.44752                       | .281042    | 3.703023        | .71896     | 1.44010                          | .279601    | .5769      | 1.83856    |
| 480.0           | 1.35434                       | .262950    | 3.796207        | .73705     | 1.32280                          | .256828    | .6154      | 1.96113    |
| 510.0           | 1.27736                       | .248005    | 3.873184        | .75200     | 1.21506                          | .235909    | .6538      | 2.08370    |
| 540.0           | 1.21456                       | .235812    | 3.935982        | .76419     | 1.11609                          | .216694    | .6923      | 2.20627    |
| 570.0           | 1.16392                       | .225980    | 3.986625        | .77402     | 1.02519                          | .199044    | .7308      | 2.32884    |
| 600.0           | 1.12543                       | .218507    | 4.025114        | .78149     | .94168                           | .182832    | .7692      | 2.45141    |
| 630.0           | 1.09707                       | .213001    | 4.053473        | .78700     | .86498                           | .167940    | .8077      | 2.57398    |
| 660.0           | 1.07681                       | .209068    | 4.073730        | .79093     | .79453                           | .154262    | .8462      | 2.69655    |
| 690.0           | 1.06263                       | .206315    | 4.087911        | .79369     | .72982                           | .141697    | .8846      | 2.81912    |
| 720.0           | 1.05250                       | .204348    | 4.098040        | .79565     | .67037                           | .130156    | .9231      | 2.94169    |
| 750.0           | 1.04643                       | .203168    | 4.104116        | .79683     | .61577                           | .119554    | .9615      | * 06426    |
| 780.0           | 1.04440                       | .202775    | 4.106143        | .79723     | .56562                           | .109817    | 1.0000     | 18683      |

TABLE D-10

EVAPORATION EXPERIMENT NO. GLF10 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 52%

## EVAPORATION HISTORY OF TEST DROPLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |            |                 |            | THEORETICAL HALF LIFE MODEL DATA |            |            |            |
|-----------------|-------------------------------|------------|-----------------|------------|----------------------------------|------------|------------|------------|
|                 | RESIDUAL MASS                 |            | CUMULATIVE MASS |            | MASS                             | MASS       | TIME       | TIME       |
|                 | MILLIGRAMS                    | FRACTIONAL | MILLIGRAMS      | FRACTIONAL | MILLIGRAMS                       | FRACTIONAL | FRACTIONAL | HALF-LIFES |
| .0              | 6.46739                       | 1.000000   | .000000         | .000000    | 6.46739                          | 1.000000   | .0000      | .00000     |
| 30.0            | 5.99051                       | .926264    | .476879         | .07374     | 6.01550                          | .930128    | .0313      | .10450     |
| 60.0            | 5.60408                       | .866512    | .863316         | .13349     | 5.59518                          | .865138    | .0625      | .20900     |
| 90.0            | 5.24025                       | .810257    | 1.227142        | .18974     | 5.20424                          | .804688    | .0938      | .31350     |
| 120.0           | 4.89287                       | .756544    | 1.574524        | .24346     | 4.84060                          | .748463    | .1250      | .41800     |
| 150.0           | 4.55987                       | .705056    | 1.907517        | .29494     | 4.50238                          | .696166    | .1563      | .52250     |
| 180.0           | 4.24332                       | .656111    | 2.224066        | .34389     | 4.18779                          | .647524    | .1875      | .62700     |
| 210.0           | 3.94116                       | .609390    | 2.526227        | .39061     | 3.89518                          | .602280    | .2188      | .73149     |
| 240.0           | 3.65339                       | .564894    | 2.813999        | .43511     | 3.62301                          | .560197    | .2500      | .8399      |
| 270.0           | 3.38001                       | .522623    | 3.087382        | .47738     | 3.36986                          | .521055    | .2813      | .94049     |
| 300.0           | 3.12307                       | .482895    | 3.344321        | .51711     | 3.13440                          | .484647    | .3125      | 1.04199    |
| 330.0           | 2.88258                       | .445709    | 3.584816        | .55429     | 2.91540                          | .450784    | .3438      | 1.14949    |
| 360.0           | 2.65647                       | .410748    | 3.810923        | .58925     | 2.71169                          | .419287    | .3750      | 1.25399    |
| 390.0           | 2.44681                       | .378330    | 4.020586        | .62167     | 2.52222                          | .389990    | .4063      | 1.35849    |
| 420.0           | 2.25359                       | .348454    | 4.213804        | .65155     | 2.34599                          | .362741    | .4375      | 1.46299    |
| 450.0           | 2.07887                       | .321438    | 4.388523        | .67856     | 2.18207                          | .337395    | .4688      | 1.56749    |
| 480.0           | 1.92471                       | .297601    | 4.542686        | .70240     | 2.02960                          | .313821    | .5000      | 1.67199    |
| 510.0           | 1.78904                       | .276625    | 4.678350        | .72338     | 1.88779                          | .291893    | .5313      | 1.77649    |
| 540.0           | 1.66982                       | .258191    | 4.797570        | .74181     | 1.75588                          | .271498    | .5625      | 1.88099    |
| 570.0           | 1.56705                       | .242299    | 4.900346        | .75770     | 1.63320                          | .252528    | .5938      | 1.98549    |
| 600.0           | 1.47866                       | .228633    | 4.988733        | .77137     | 1.51908                          | .234883    | .6250      | 2.08998    |
| 630.0           | 1.40466                       | .217191    | 5.062731        | .78281     | 1.41294                          | .218471    | .6563      | 2.19448    |
| 660.0           | 1.34299                       | .207656    | 5.124397        | .79234     | 1.31421                          | .203206    | .6875      | 2.29898    |
| 690.0           | 1.28955                       | .199393    | 5.177841        | .80061     | 1.22239                          | .189008    | .7188      | 2.40348    |
| 720.0           | 1.24433                       | .192401    | 5.223062        | .80760     | 1.13698                          | .175801    | .7500      | 2.50798    |
| 750.0           | 1.20733                       | .186680    | 5.260061        | .81332     | 1.05753                          | .163518    | .7813      | 2.61248    |
| 780.0           | 1.17855                       | .182230    | 5.288838        | .81777     | .98364                           | .152092    | .8125      | 2.71698    |
| 810.0           | 1.15594                       | .178734    | 5.311449        | .82127     | .91491                           | .141465    | .8438      | 2.82148    |
| 840.0           | 1.13744                       | .175874    | 5.329948        | .82413     | .85098                           | .131581    | .8750      | 2.92598    |
| 870.0           | 1.12305                       | .173649    | 5.344337        | .82635     | .79152                           | .122387    | .9063      | 3.03048    |
| 900.0           | 1.11483                       | .172377    | 5.352559        | .82762     | .73622                           | .113836    | .9375      | 3.13498    |
| 930.0           | 1.11072                       | .171742    | 5.356670        | .82824     | .68478                           | .105882    | .9688      | 3.23948    |
| 960.0           | 1.10867                       | .171424    | 5.358726        | .82856     | .63693                           | .098483    | 1.0000     | 3.34398    |

TABLE D-11

EVAPORATION EXPERIMENT NO. GLF11 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 55%

## EVAPORATION HISTORY OF TEST DROPLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |            |                 |            | THEORETICAL HALF LIFE MODEL DATA |            |            |            |
|-----------------|-------------------------------|------------|-----------------|------------|----------------------------------|------------|------------|------------|
|                 | RESIDUAL MASS                 |            | CUMULATIVE MASS |            | MASS                             | MASS       | TIME       | TIME       |
|                 | MILLIGRAMS                    | FRACTIONAL | MILLIGRAMS      | FRACTIONAL | MILLIGRAMS                       | FRACTIONAL | FRACTIONAL | HALF-LIVES |
| .0              | 5.67880                       | 1.000000   | .000000         | .00000     | 5.67880                          | 1.000000   | .0000      | .00000     |
| 10.0            | 5.33200                       | .938930    | .346806         | .06107     | 5.29797                          | .932938    | .0278      | .10015     |
| 20.0            | 5.00158                       | .886745    | .677227         | .11926     | 4.94268                          | .870374    | .0556      | .20029     |
| 30.0            | 4.68481                       | .824964    | .993995         | .17504     | 4.61122                          | .812005    | .0833      | .30044     |
| 40.0            | 4.38170                       | .771588    | 1.297109        | .22841     | 4.30198                          | .757551    | .1111      | .40059     |
| 50.0            | 4.09224                       | .720616    | 1.586569        | .27938     | 4.01348                          | .706748    | .1389      | .50073     |
| 60.0            | 3.81643                       | .672048    | 1.862375        | .32795     | 3.74433                          | .659352    | .1667      | .60088     |
| 70.0            | 3.55428                       | .625885    | 2.124528        | .37412     | 3.49323                          | .615135    | .1944      | .70102     |
| 80.0            | 3.30305                       | .581645    | 2.375757        | .41836     | 3.25897                          | .573883    | .2222      | .80117     |
| 90.0            | 3.06274                       | .539320    | 2.616064        | .46067     | 3.04042                          | .535397    | .2500      | .90132     |
| 100.0           | 2.83609                       | .499416    | 2.842716        | .50058     | 2.83652                          | .499493    | .2778      | 1.00146    |
| 110.0           | 2.62309                       | .461909    | 3.055715        | .53809     | 2.64630                          | .465996    | .3056      | 1.10161    |
| 120.0           | 2.42374                       | .426805    | 3.255060        | .57319     | 2.46883                          | .434746    | .3333      | 1.20176    |
| 130.0           | 2.23805                       | .394106    | 3.440752        | .60589     | 2.30327                          | .405591    | .3611      | 1.30190    |
| 140.0           | 2.06328                       | .363331    | 3.615520        | .63667     | 2.14881                          | .378391    | .3889      | 1.40205    |
| 150.0           | 1.90217                       | .334960    | 3.776635        | .66504     | 2.00471                          | .353016    | .4167      | 1.50220    |
| 160.0           | 1.75471                       | .308993    | 3.924096        | .69101     | 1.87027                          | .329342    | .4444      | 1.60234    |
| 170.0           | 1.61817                       | .284949    | 4.060633        | .71505     | 1.74484                          | .307256    | .4722      | 1.70249    |
| 180.0           | 1.49256                       | .262829    | 4.186248        | .73717     | 1.62783                          | .286650    | .5000      | 1.80264    |
| 190.0           | 1.38080                       | .243114    | 4.298209        | .75689     | 1.51867                          | .267427    | .5278      | 1.90278    |
| 200.0           | 1.28229                       | .225803    | 4.396516        | .77420     | 1.41682                          | .249492    | .5556      | 2.00293    |
| 210.0           | 1.19490                       | .210415    | 4.483900        | .78959     | 1.32181                          | .232762    | .5833      | 2.10307    |
| 220.0           | 1.11844                       | .196950    | 4.560361        | .80305     | 1.23317                          | .217152    | .6111      | 2.20322    |
| 230.0           | 1.05017                       | .184929    | 4.628631        | .81507     | 1.15047                          | .202590    | .6389      | 2.30337    |
| 240.0           | .99010                        | .174350    | 4.688707        | .82565     | 1.07231                          | .189004    | .6667      | 2.40351    |
| 250.0           | .93821                        | .165213    | 4.740591        | .83479     | 1.00134                          | .176329    | .6944      | 2.50366    |
| 260.0           | .89179                        | .157038    | 4.787014        | .84296     | .93419                           | .164504    | .7222      | 2.60381    |
| 270.0           | .85083                        | .149825    | 4.827975        | .85017     | .87154                           | .153672    | .7500      | 2.70395    |
| 280.0           | .81533                        | .143574    | 4.863475        | .85643     | .81309                           | .143180    | .7778      | 2.80410    |
| 290.0           | .78529                        | .138285    | 4.893514        | .86172     | .75856                           | .133578    | .8056      | 2.90425    |
| 300.0           | .76071                        | .133957    | 4.918090        | .86694     | .70739                           | .124620    | .8333      | 3.00439    |
| 310.0           | .74160                        | .130591    | 4.937206        | .86941     | .66023                           | .116263    | .8611      | 3.10454    |
| 320.0           | .72521                        | .127706    | 4.953590        | .87229     | .61596                           | .108466    | .8889      | 3.20469    |
| 330.0           | .71156                        | .125301    | 4.967243        | .87470     | .57465                           | .101192    | .9167      | 3.30483    |
| 340.0           | .70037                        | .123859    | 4.975436        | .87614     | .53611                           | .094406    | .9444      | 3.40498    |
| 350.0           | .69791                        | .122897    | 4.980898        | .87710     | .50016                           | .088075    | .9722      | 3.50512    |
| 360.0           | .69518                        | .122416    | 4.983628        | .87758     | .46662                           | .082168    | 1.0000     | 3.60527    |



TABLE D-12

EVAPORATION EXPERIMENT NO. GLF12 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F, RELATIVE HUMIDITY 40%

## EVAPORATION HISTORY OF TEST DROPLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |            |                 |            | THEORETICAL HALF LIFE MODEL DATA |            |            |            |
|-----------------|-------------------------------|------------|-----------------|------------|----------------------------------|------------|------------|------------|
|                 | RESIDUAL MASS                 |            | CUMULATIVE MASS |            | MASS                             | MASS       | TIME       | TIME       |
|                 | MILLIGRAMS                    | FRACTIONAL | MILLIGRAMS      | FRACTIONAL | MILLIGRAMS                       | FRACTIONAL | FRACTIONAL | HALF-LIVES |
| .0              | 6.46739                       | 1.000000   | .000000         | .000000    | 6.46739                          | 1.000000   | .0000      | .00000     |
| 10.0            | 6.18207                       | .955883    | .285325         | .04412     | 6.14691                          | .950447    | .0256      | .07332     |
| 20.0            | 5.90482                       | .913014    | .562574         | .08699     | 5.84232                          | .903350    | .0513      | .14664     |
| 30.0            | 5.63564                       | .871395    | .831749         | .12861     | 5.55282                          | .858587    | .0769      | .21996     |
| 40.0            | 5.37723                       | .831458    | 1.090157        | .16856     | 5.27766                          | .816041    | .1026      | .29329     |
| 50.0            | 5.12690                       | .792731    | 1.340488        | .20727     | 5.01614                          | .775604    | .1282      | .36661     |
| 60.0            | 4.88195                       | .754857    | 1.585437        | .24514     | 4.76757                          | .737171    | .1538      | .43993     |
| 70.0            | 4.64506                       | .718231    | 1.822311        | .28177     | 4.53133                          | .700642    | .1795      | .51325     |
| 80.0            | 4.41628                       | .682854    | 2.051110        | .31715     | 4.30679                          | .665923    | .2051      | .58657     |
| 90.0            | 4.19287                       | .648309    | 2.274524        | .35169     | 4.09337                          | .632925    | .2308      | .65989     |
| 100.0           | 3.97484                       | .614596    | 2.492555        | .38540     | 3.89054                          | .601562    | .2564      | .73321     |
| 110.0           | 3.76219                       | .581716    | 2.705204        | .41828     | 3.69775                          | .571753    | .2821      | .80654     |
| 120.0           | 3.55492                       | .549669    | 2.912467        | .45033     | 3.51452                          | .543421    | .3077      | .87986     |
| 130.0           | 3.35573                       | .518870    | 3.111657        | .48113     | 3.34036                          | .516493    | .3333      | .95318     |
| 140.0           | 3.16462                       | .489320    | 3.302771        | .51060     | 3.17484                          | .490899    | .3590      | 1.02650    |
| 150.0           | 2.97889                       | .460602    | 3.488501        | .53940     | 3.01752                          | .466574    | .3846      | 1.09982    |
| 160.0           | 2.79854                       | .432716    | 3.668848        | .56728     | 2.86799                          | .443454    | .4103      | 1.17314    |
| 170.0           | 2.62358                       | .405663    | 3.843811        | .59434     | 2.72587                          | .421480    | .4359      | 1.24647    |
| 180.0           | 2.45669                       | .379858    | 4.010699        | .62014     | 2.59080                          | .400594    | .4615      | 1.31979    |
| 190.0           | 2.29788                       | .355302    | 4.159512        | .64470     | 2.46242                          | .380744    | .4872      | 1.39311    |
| 200.0           | 2.14445                       | .331579    | 4.322942        | .66842     | 2.34040                          | .361877    | .5128      | 1.46643    |
| 210.0           | 1.99640                       | .308688    | 4.470988        | .69131     | 2.22443                          | .343945    | .5385      | 1.53975    |
| 220.0           | 1.85643                       | .287045    | 4.610958        | .71295     | 2.11420                          | .326901    | .5641      | 1.61307    |
| 230.0           | 1.72454                       | .266651    | 4.747854        | .73335     | 2.00943                          | .310703    | .5897      | 1.68639    |
| 240.0           | 1.60072                       | .247506    | 4.866674        | .75249     | 1.90986                          | .295306    | .6154      | 1.75972    |
| 250.0           | 1.48497                       | .229609    | 4.982419        | .77039     | 1.81522                          | .280673    | .6410      | 1.83304    |
| 260.0           | 1.37730                       | .212961    | 5.090089        | .78704     | 1.72527                          | .266765    | .6667      | 1.90636    |
| 270.0           | 1.27771                       | .197562    | 5.189683        | .80244     | 1.63978                          | .253546    | .6923      | 1.97968    |
| 280.0           | 1.18350                       | .182994    | 5.283895        | .81701     | 1.55853                          | .240982    | .7179      | 2.05300    |
| 290.0           | 1.09736                       | .169676    | 5.370030        | .83032     | 1.48130                          | .229041    | .7436      | 2.12632    |
| 300.0           | 1.01930                       | .157606    | 5.448091        | .84239     | 1.40789                          | .217691    | .7692      | 2.19964    |
| 310.0           | .94931                        | .146785    | 5.518076        | .85322     | 1.33813                          | .206904    | .7949      | 2.27297    |
| 320.0           | .89010                        | .137628    | 5.577295        | .86237     | 1.27182                          | .196651    | .8205      | 2.34629    |
| 330.0           | .83895                        | .129721    | 5.628438        | .87028     | 1.20880                          | .186907    | .8462      | 2.41961    |
| 340.0           | .79319                        | .122645    | 5.674198        | .87735     | 1.14890                          | .177645    | .8718      | 2.49293    |
| 350.0           | .75551                        | .116818    | 5.711862        | .88318     | 1.09197                          | .168842    | .8974      | 2.56625    |
| 360.0           | .72590                        | .112240    | 5.741491        | .88776     | 1.03786                          | .160476    | .9231      | 2.63957    |
| 370.0           | .70437                        | .108910    | 5.763025        | .89109     | .98643                           | .152524    | .9487      | 2.71290    |
| 380.0           | .69091                        | .106829    | 5.776484        | .89317     | .93755                           | .144966    | .9744      | 2.78622    |
| 390.0           | .68552                        | .105997    | 5.781868        | .89400     | .89109                           | .137782    | 1.0000     | 2.85954    |

TABLE D-13

EVAPORATION EXPERIMENT NO. GLE13 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 44%

## EVAPORATION HISTORY OF TEST DROPLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |            |                 |            | THEORETICAL HALF LIFE MODEL DATA |            |            |            |
|-----------------|-------------------------------|------------|-----------------|------------|----------------------------------|------------|------------|------------|
|                 | RESIDUAL MASS                 |            | CUMULATIVE MASS |            | MASS                             | MASS       | TIME       | TIME       |
|                 | MILLIGRAMS                    | FRACTIONAL | MILLIGRAMS      | FRACTIONAL | MILLIGRAMS                       | FRACTIONAL | FRACTIONAL | HALF-LIVES |
| .0              | 5.41467                       | 1.000000   | .000000         | .000000    | 5.41467                          | 1.000000   | .0000      | .00000     |
| 40.0            | 5.05545                       | .933657    | .359228         | .06634     | 5.02083                          | .927263    | .0313      | .10895     |
| 80.0            | 4.72323                       | .872301    | .691447         | .12770     | 4.65563                          | .859817    | .0625      | .21790     |
| 120.0           | 4.40451                       | .813440    | 1.010161        | .18656     | 4.31699                          | .797277    | .0938      | .32685     |
| 160.0           | 4.09930                       | .757073    | 1.315370        | .24293     | 4.00299                          | .739265    | .1250      | .43580     |
| 200.0           | 3.80760                       | .703200    | 1.607074        | .29680     | 3.71182                          | .685512    | .1563      | .54175     |
| 240.0           | 3.52670                       | .651323    | 1.887975        | .34868     | 3.44184                          | .635650    | .1875      | .65369     |
| 280.0           | 3.25660                       | .601440    | 2.158071        | .39856     | 3.19149                          | .589415    | .2188      | .76264     |
| 320.0           | 2.99731                       | .553553    | 2.417363        | .44645     | 2.95935                          | .546543    | .2500      | .87159     |
| 360.0           | 2.74832                       | .507661    | 2.665853        | .49234     | 2.74410                          | .506789    | .2813      | .98054     |
| 400.0           | 2.51654                       | .464763    | 2.898136        | .53524     | 2.54450                          | .469927    | .3125      | 1.08949    |
| 440.0           | 2.30046                       | .424857    | 3.114213        | .57514     | 2.35942                          | .435746    | .3438      | 1.19844    |
| 480.0           | 2.09789                       | .387445    | 3.316785        | .61255     | 2.18781                          | .404051    | .3750      | 1.30739    |
| 520.0           | 1.91152                       | .353026    | 3.503152        | .64697     | 2.02867                          | .374662    | .4063      | 1.41634    |
| 560.0           | 1.74406                       | .322099    | 3.670612        | .67790     | 1.88111                          | .347410    | .4375      | 1.52529    |
| 600.0           | 1.59821                       | .295163    | 3.816464        | .70484     | 1.74429                          | .322141    | .4688      | 1.63424    |
| 640.0           | 1.47397                       | .272217    | 3.940708        | .72778     | 1.61741                          | .298709    | .5000      | 1.74319    |
| 680.0           | 1.36863                       | .252763    | 4.046046        | .74724     | 1.49977                          | .276982    | .5313      | 1.85214    |
| 720.0           | 1.27950                       | .236302    | 4.135178        | .76370     | 1.39068                          | .256835    | .5625      | 1.96108    |
| 760.0           | 1.20657                       | .222833    | 4.208104        | .77717     | 1.28953                          | .238154    | .5938      | 2.07003    |
| 800.0           | 1.14715                       | .211859    | 4.267525        | .78814     | 1.19573                          | .220831    | .6250      | 2.17898    |
| 840.0           | 1.09853                       | .202880    | 4.316143        | .79712     | 1.10876                          | .204769    | .6563      | 2.28793    |
| 880.0           | 1.05802                       | .195398    | 4.356657        | .80460     | 1.02811                          | .189875    | .6875      | 2.39688    |
| 920.0           | 1.02290                       | .188913    | 4.391769        | .81109     | .95333                           | .176064    | .7188      | 2.50583    |
| 960.0           | .99319                        | .183426    | 4.421480        | .81657     | .88399                           | .163257    | .7500      | 2.61478    |
| 1000.0          | .96888                        | .178937    | 4.445789        | .82106     | .81969                           | .151383    | .7813      | 2.72373    |
| 1040.0          | .94998                        | .175443    | 4.464696        | .82455     | .76007                           | .140372    | .8125      | 2.83268    |
| 1080.0          | .93647                        | .172951    | 4.478200        | .82795     | .70478                           | .130161    | .8438      | 2.94163    |
| 1120.0          | .92567                        | .170956    | 4.489005        | .82904     | .65352                           | .120694    | .8750      | 3.05058    |
| 1160.0          | .91487                        | .168960    | 4.499808        | .83104     | .60598                           | .111915    | .9063      | 3.15953    |
| 1200.0          | .90676                        | .167464    | 4.507912        | .83254     | .56191                           | .103775    | .9375      | 3.26847    |
| 1240.0          | .90136                        | .166466    | 4.513314        | .83353     | .52103                           | .096226    | .9688      | 3.37742    |
| 1280.0          | .89866                        | .165967    | 4.516015        | .83403     | .48314                           | .089227    | 1.0000     | 3.48637    |

TABLE D-14

EVAPORATION EXPERIMENT NO. GLF14 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINANT DENSITY 30 GMS/CM<sup>3</sup> METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 2.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 43%

## EVAPORATION HISTORY OF TEST DROPLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |            |                 |            | THEORETICAL HALF LIFE MODEL DATA |            |            |            |
|-----------------|-------------------------------|------------|-----------------|------------|----------------------------------|------------|------------|------------|
|                 | RESIDUAL MASS                 |            | CUMULATIVE MASS |            | MASS                             | MASS       | TIME       | TIME       |
|                 | MILLIGRAMS                    | FRACTIONAL | MILLIGRAMS      | FRACTIONAL | MILLIGRAMS                       | FRACTIONAL | FRACTIONAL | HALF-LIVES |
| .0              | 6.46739                       | 1.000000   | .000000         | .000000    | 6.46739                          | 1.000000   | .0000      | .00000     |
| 40.0            | 6.08648                       | .941102    | .380916         | .05890     | 6.03845                          | .933676    | .0345      | .09901     |
| 80.0            | 5.72224                       | .884784    | .745148         | .11522     | 5.63795                          | .871750    | .0690      | .19801     |
| 120.0           | 5.37191                       | .830615    | 1.095479        | .16939     | 5.26402                          | .813932    | .1034      | .29702     |
| 160.0           | 5.03270                       | .778166    | 1.434689        | .22183     | 4.91488                          | .759949    | .1379      | .39603     |
| 200.0           | 4.70461                       | .727436    | 1.762777        | .27256     | 4.58891                          | .709545    | .1724      | .49503     |
| 240.0           | 4.39043                       | .678856    | 2.076962        | .32114     | 4.28455                          | .662485    | .2069      | .59404     |
| 280.0           | 4.09015                       | .632426    | 2.377246        | .36757     | 4.00038                          | .618546    | .2414      | .69305     |
| 320.0           | 3.80098                       | .587715    | 2.666409        | .41229     | 3.73506                          | .577522    | .2759      | .79205     |
| 360.0           | 3.52294                       | .544724    | 2.944449        | .45528     | 3.48733                          | .539218    | .3103      | .89106     |
| 400.0           | 3.25880                       | .503882    | 3.208587        | .49612     | 3.25604                          | .503455    | .3448      | .99007     |
| 440.0           | 3.00857                       | .465190    | 3.458824        | .53481     | 3.04008                          | .470063    | .3793      | 1.08907    |
| 480.0           | 2.77223                       | .428648    | 3.695158        | .57135     | 2.83845                          | .438887    | .4138      | 1.18808    |
| 520.0           | 2.55258                       | .394635    | 3.914811        | .60532     | 2.65019                          | .409778    | .4483      | 1.28709    |
| 560.0           | 2.34961                       | .363301    | 4.117780        | .63670     | 2.47442                          | .382600    | .4828      | 1.38609    |
| 600.0           | 2.16332                       | .334497    | 4.304067        | .66550     | 2.31031                          | .357224    | .5172      | 1.48510    |
| 640.0           | 1.99372                       | .308273    | 4.473672        | .69173     | 2.15708                          | .333531    | .5517      | 1.58411    |
| 680.0           | 1.84358                       | .285357    | 4.623814        | .71494     | 2.01401                          | .311410    | .5862      | 1.68311    |
| 720.0           | 1.71250                       | .264852    | 4.754493        | .73515     | 1.88043                          | .290756    | .6207      | 1.78212    |
| 760.0           | 1.59612                       | .246795    | 4.871270        | .75320     | 1.75571                          | .271472    | .6552      | 1.88113    |
| 800.0           | 1.49325                       | .230888    | 4.974145        | .76911     | 1.63927                          | .253467    | .6897      | 1.98013    |
| 840.0           | 1.40427                       | .217131    | 5.063118        | .78287     | 1.53054                          | .236656    | .7241      | 2.07914    |
| 880.0           | 1.32642                       | .205094    | 5.140970        | .79491     | 1.42903                          | .220960    | .7586      | 2.17815    |
| 920.0           | 1.26525                       | .195636    | 5.202138        | .80436     | 1.33425                          | .206305    | .7931      | 2.27715    |
| 960.0           | 1.22355                       | .189187    | 5.243845        | .81061     | 1.24576                          | .192622    | .8276      | 2.37616    |
| 1000.0          | 1.19296                       | .184458    | 5.274429        | .81554     | 1.16314                          | .179846    | .8621      | 2.47516    |
| 1040.0          | 1.16516                       | .180159    | 5.302233        | .81984     | 1.08599                          | .167918    | .8966      | 2.57417    |
| 1080.0          | 1.14291                       | .176720    | 5.324476        | .82328     | 1.01396                          | .156781    | .9310      | 2.67318    |
| 1120.0          | 1.12901                       | .174570    | 5.338378        | .82543     | .94571                           | .146383    | .9655      | 2.77218    |
| 1160.0          | 1.12345                       | .173710    | 5.343939        | .82629     | .88392                           | .136674    | 1.0000     | 2.87119    |

TABLE D-15

EVAPORATION EXPERIMENT NO. GLF15 SERIES 10 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 11.3 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

## EVAPORATION HISTORY OF TEST DROPLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |            |                 |            | THEORETICAL HALF LIFE MODEL DATA |            |            |            |
|-----------------|-------------------------------|------------|-----------------|------------|----------------------------------|------------|------------|------------|
|                 | RESIDUAL MASS                 |            | CUMULATIVE MASS |            | MASS                             | MASS       | TIME       | TIME       |
|                 | MILLIGRAMS                    | FRACTIONAL | MILLIGRAMS      | FRACTIONAL | MILLIGRAMS                       | FRACTIONAL | FRACTIONAL | HALF-LIVES |
| .0              | 5.67880                       | 1.000000   | .000000         | .000000    | 5.67880                          | 1.000000   | .0000      | .00000     |
| 15.0            | 5.34049                       | .940426    | .338311         | .05957     | 5.34049                          | .932923    | .0323      | .10017     |
| 30.0            | 5.01829                       | .883688    | .660512         | .11631     | 4.94253                          | .870346    | .0645      | .20034     |
| 45.0            | 4.70817                       | .829078    | .970630         | .17092     | 4.61100                          | .811966    | .0968      | .30051     |
| 60.0            | 4.41014                       | .776596    | 1.268666        | .22340     | 4.30171                          | .757502    | .1290      | .40068     |
| 75.0            | 4.12419                       | .726242    | 1.554619        | .27376     | 4.01316                          | .706692    | .1613      | .50085     |
| 90.0            | 3.84629                       | .677306    | 1.832517        | .32269     | 3.74397                          | .659289    | .1935      | .60102     |
| 105.0           | 3.57644                       | .629788    | 2.102360        | .37021     | 3.49284                          | .615066    | .2258      | .70119     |
| 120.0           | 3.31868                       | .584398    | 2.360121        | .41560     | 3.25855                          | .573810    | .2581      | .80136     |
| 135.0           | 3.07301                       | .541136    | 2.605799        | .45886     | 3.03998                          | .535321    | .2903      | .90153     |
| 150.0           | 2.83538                       | .499292    | 2.843422        | .50071     | 2.83607                          | .499413    | .3226      | 1.00169    |
| 165.0           | 2.60984                       | .459576    | 3.068963        | .54042     | 2.64584                          | .465914    | .3548      | 1.10186    |
| 180.0           | 2.39638                       | .421987    | 3.282421        | .57801     | 2.46836                          | .434662    | .3871      | 1.20203    |
| 195.0           | 2.19098                       | .385817    | 3.487823        | .61418     | 2.30279                          | .405507    | .4194      | 1.30220    |
| 210.0           | 1.99363                       | .351066    | 3.685171        | .64893     | 2.14833                          | .378307    | .4516      | 1.40237    |
| 225.0           | 1.80837                       | .318442    | 3.879437        | .68156     | 2.00423                          | .352931    | .4839      | 1.50254    |
| 240.0           | 1.63921                       | .288654    | 4.039592        | .71135     | 1.86979                          | .329258    | .5161      | 1.60271    |
| 255.0           | 1.48617                       | .261704    | 4.192637        | .73830     | 1.74437                          | .307172    | .5484      | 1.70286    |
| 270.0           | 1.34923                       | .237591    | 4.329573        | .76241     | 1.62736                          | .286568    | .5806      | 1.80305    |
| 285.0           | 1.22841                       | .216344    | 4.450398        | .78369     | 1.51021                          | .267346    | .6129      | 1.90322    |
| 300.0           | 1.12369                       | .197875    | 4.555114        | .80213     | 1.41637                          | .249413    | .6452      | 2.00339    |
| 315.0           | 1.03509                       | .182272    | 4.643719        | .81773     | 1.32136                          | .232684    | .6774      | 2.10356    |
| 330.0           | .96254                        | .169506    | 4.716214        | .83049     | 1.23273                          | .217076    | .7097      | 2.20373    |
| 345.0           | .90621                        | .159577    | 4.772594        | .84042     | 1.15004                          | .202515    | .7419      | 2.30390    |
| 360.0           | .85190                        | .151775    | 4.816903        | .84822     | 1.07290                          | .188931    | .7742      | 2.40407    |
| 375.0           | .82566                        | .145392    | 4.853149        | .85461     | 1.00094                          | .176258    | .8065      | 2.50424    |
| 390.0           | .77746                        | .140028    | 4.881342        | .85957     | .93380                           | .164436    | .8387      | 2.60441    |
| 405.0           | .77732                        | .136882    | 4.90171         | .86312     | .87116                           | .153406    | .8710      | 2.70458    |
| 420.0           | .76524                        | .134754    | 4.9135          | .86525     | .81273                           | .143116    | .9032      | 2.80474    |
| 435.0           | .75719                        | .133336    | 4.91618         | .86666     | .75821                           | .133516    | .9355      | 2.90491    |
| 450.0           | .74933                        | .131917    | 4.929673        | .86808     | .70735                           | .124560    | .9677      | 3.00508    |
| 465.0           | .74111                        | .131208    | 4.933760        | .86879     | .65991                           | .116205    | 1.0000     | 3.10525    |

TABLE D-16

EVAPORATION EXPERIMENT NO. GLF16 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 11.3 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

## EVAPORATION HISTORY OF TEST DROPLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |            |                 |            | THEORETICAL HALF LIFE MODEL DATA |            |            |            |
|-----------------|-------------------------------|------------|-----------------|------------|----------------------------------|------------|------------|------------|
|                 | RESIDUAL MASS                 |            | CUMULATIVE MASS |            | MASS                             | MASS       | TIME       | TIME       |
|                 | MILLIGRAMS                    | FRACTIONAL | MILLIGRAMS      | FRACTIONAL | MILLIGRAMS                       | FRACTIONAL | FRACTIONAL | HALF-LIVES |
| .0              | 6.20870                       | 1.000000   | .000000         | .000000    | 6.20870                          | 1.000000   | .0000      | .00000     |
| 15.0            | 5.86534                       | .944697    | .343360         | .05530     | 5.82395                          | .938032    | .0345      | .09229     |
| 30.0            | 5.53833                       | .892027    | .670370         | .10797     | 5.46306                          | .879905    | .0690      | .18458     |
| 45.0            | 5.22358                       | .841333    | .985117         | .15867     | 5.12453                          | .825379    | .1034      | .27687     |
| 60.0            | 4.92109                       | .792613    | 1.287601        | .20739     | 4.80097                          | .774732    | .1379      | .36916     |
| 75.0            | 4.63087                       | .745869    | 1.577822        | .25413     | 4.50910                          | .726255    | .1724      | .46145     |
| 90.0            | 4.34883                       | .700441    | 1.859868        | .29956     | 4.22968                          | .681251    | .2069      | .55374     |
| 105.0           | 4.07496                       | .656331    | 2.133739        | .34367     | 3.96757                          | .639035    | .2414      | .64603     |
| 120.0           | 3.80926                       | .613537    | 2.399434        | .38646     | 3.72171                          | .599436    | .2759      | .73832     |
| 135.0           | 3.55174                       | .572059    | 2.656954        | .42794     | 3.49109                          | .562290    | .3103      | .83061     |
| 150.0           | 3.30240                       | .531899    | 2.906299        | .46810     | 3.27475                          | .527446    | .3448      | .92290     |
| 165.0           | 3.06531                       | .493713    | 3.143381        | .50629     | 3.07182                          | .494762    | .3793      | 1.01519    |
| 180.0           | 2.83641                       | .456844    | 3.372288        | .54316     | 2.88147                          | .464102    | .4138      | 1.10749    |
| 195.0           | 2.61568                       | .421292    | 3.593019        | .57871     | 2.70291                          | .435343    | .4483      | 1.19978    |
| 210.0           | 2.40721                       | .387716    | 3.801488        | .61228     | 2.53542                          | .408366    | .4828      | 1.29207    |
| 225.0           | 2.20691                       | .355455    | 4.001782        | .64454     | 2.37831                          | .383060    | .5172      | 1.38436    |
| 240.0           | 2.01888                       | .325170    | 4.189812        | .67483     | 2.23093                          | .359323    | .5517      | 1.47665    |
| 255.0           | 1.84312                       | .296860    | 4.365580        | .70314     | 2.09268                          | .337057    | .5862      | 1.56894    |
| 270.0           | 1.67552                       | .269867    | 4.533172        | .73013     | 1.96300                          | .316170    | .6207      | 1.66123    |
| 285.0           | 1.52019                       | .244849    | 4.688502        | .75515     | 1.84136                          | .296578    | .6552      | 1.75352    |
| 300.0           | 1.38121                       | .222465    | 4.827481        | .77754     | 1.72723                          | .278199    | .6897      | 1.84581    |
| 315.0           | 1.25859                       | .202713    | 4.950110        | .79729     | 1.62022                          | .260960    | .7241      | 1.93810    |
| 330.0           | 1.15231                       | .185096    | 5.056388        | .81440     | 1.51982                          | .244782    | .7586      | 2.03039    |
| 345.0           | 1.06347                       | .171770    | 5.142228        | .82823     | 1.42564                          | .229620    | .7931      | 2.12268    |
| 360.0           | 1.00107                       | .161236    | 5.207630        | .83876     | 1.33730                          | .215391    | .8276      | 2.21497    |
| 375.0           | .95201                        | .153336    | 5.256681        | .84666     | 1.25443                          | .202044    | .8621      | 2.30726    |
| 390.0           | .91931                        | .148069    | 5.289383        | .85193     | 1.17669                          | .189524    | .8966      | 2.39955    |
| 405.0           | .89887                        | .144777    | 5.309621        | .85522     | 1.10378                          | .177779    | .9310      | 2.49184    |
| 420.0           | .88661                        | .142802    | 5.322084        | .85720     | 1.03538                          | .166763    | .9655      | 2.58413    |
| 435.0           | .88252                        | .142143    | 5.326171        | .85786     | .97122                           | .156429    | 1.0000     | 2.67642    |

TABLE D-17

EVAPORATION EXPERIMENT NO. BLF1 SERIES 10 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 39%

## EVAPORATION HISTORY OF TEST DROPLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |            |                 |            | THEORETICAL HALF LIFE MODEL DATA |            |                    |                    |
|-----------------|-------------------------------|------------|-----------------|------------|----------------------------------|------------|--------------------|--------------------|
|                 | RESIDUAL MASS                 |            | CUMULATIVE MASS |            | MASS                             |            | TIME<br>FRACTIONAL | TIME<br>HALF-LIVES |
|                 | MILLIGRAMS                    | FRACTIONAL | MILLIGRAMS      | FRACTIONAL | MILLIGRAMS                       | FRACTIONAL |                    |                    |
| .0              | 6.33913                       | 1.000000   | .000000         | .000000    | 6.33913                          | 1.000000   | .0000              | .00000             |
| 45.0            | 5.84030                       | .921310    | .498829         | .07869     | 5.78230                          | .912160    | .0370              | .13264             |
| 90.0            | 5.37120                       | .847309    | .967927         | .15269     | 5.27439                          | .832036    | .0741              | .26528             |
| 135.0           | 4.92523                       | .776957    | 1.413900        | .22304     | 4.81109                          | .758951    | .1111              | .39792             |
| 180.0           | 4.49908                       | .709731    | 1.840052        | .29027     | 4.38848                          | .692285    | .1481              | .53056             |
| 225.0           | 4.09275                       | .645632    | 2.246384        | .35437     | 4.00300                          | .631474    | .1852              | .66320             |
| 270.0           | 3.70954                       | .585181    | 2.629590        | .41482     | 3.65138                          | .576006    | .2222              | .79584             |
| 315.0           | 3.34946                       | .528378    | 2.989672        | .47162     | 3.33064                          | .525410    | .2593              | .92849             |
| 360.0           | 3.01581                       | .475744    | 3.323325        | .52426     | 3.03808                          | .479258    | .2963              | 1.06113            |
| 405.0           | 2.71188                       | .427800    | 3.627248        | .57220     | 2.77121                          | .437160    | .3333              | 1.19377            |
| 450.0           | 2.43769                       | .384547    | 3.901439        | .61545     | 2.52779                          | .398760    | .3704              | 1.32641            |
| 495.0           | 2.19323                       | .345983    | 4.145898        | .65402     | 2.30575                          | .363733    | .4074              | 1.45905            |
| 540.0           | 1.97850                       | .312110    | 4.360626        | .68789     | 2.10321                          | .331783    | .4444              | 1.59169            |
| 585.0           | 1.79681                       | .283448    | 4.542319        | .71655     | 1.91847                          | .302639    | .4815              | 1.72433            |
| 630.0           | 1.64485                       | .259476    | 4.694280        | .74052     | 1.74995                          | .276055    | .5185              | 1.85697            |
| 675.0           | 1.52262                       | .240194    | 4.816510        | .75981     | 1.59624                          | .251807    | .5556              | 1.98961            |
| 720.0           | 1.42682                       | .225081    | 4.912312        | .77492     | 1.45602                          | .228688    | .5926              | 2.12225            |
| 765.0           | 1.35414                       | .213616    | 4.984988        | .78638     | 1.32813                          | .209512    | .6296              | 2.25489            |
| 810.0           | 1.30129                       | .205278    | 5.037844        | .79472     | 1.21146                          | .191109    | .6667              | 2.38753            |
| 855.0           | 1.26495                       | .199546    | 5.074183        | .80045     | 1.10505                          | .174322    | .7037              | 2.52017            |
| 900.0           | 1.24182                       | .195898    | 5.097308        | .80410     | 1.00798                          | .159010    | .7407              | 2.65281            |
| 945.0           | 1.22531                       | .193292    | 5.113825        | .80671     | .91944                           | .145042    | .7778              | 2.78546            |
| 990.0           | 1.21009                       | .191208    | 5.127039        | .80879     | .83868                           | .132302    | .8148              | 2.91810            |
| 1035.0          | 1.20218                       | .189644    | 5.136950        | .81036     | .76501                           | .120680    | .8519              | 3.05074            |
| 1080.0          | 1.19557                       | .188602    | 5.143557        | .81140     | .69781                           | .110080    | .8889              | 3.18338            |
| 1125.0          | 1.18897                       | .187560    | 5.150164        | .81244     | .63652                           | .100410    | .9259              | 3.31602            |
| 1170.0          | 1.18236                       | .186518    | 5.156770        | .81348     | .58060                           | .091590    | .9630              | 3.44866            |
| 1215.0          | 1.17908                       | .185997    | 5.160073        | .81400     | .52960                           | .083545    | 1.0000             | 3.58130            |

TABLE D-18

EVAPORATION EXPERIMENT NO. BLF2 SERIES 1D 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 2.9 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 39%

## EVAPORATION HISTORY (TEST) DROPLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |            |                 |            | THEORETICAL HALF LIFE MODEL DATA |            |            |            |
|-----------------|-------------------------------|------------|-----------------|------------|----------------------------------|------------|------------|------------|
|                 | RESIDUAL MASS                 |            | CUMULATIVE MASS |            | MASS                             | MASS       | TIME       | TIME       |
|                 | MILLIGRAMS                    | FRACTIONAL | MILLIGRAMS      | FRACTIONAL | MILLIGRAMS                       | FRACTIONAL | FRACTIONAL | HALF-LIVES |
| .0              | 6.46739                       | 1.000000   | .000000         | .000000    | 6.46739                          | 1.000000   | .0000      | .00000     |
| 40.0            | 5.99055                       | .926270    | .476838         | .07373     | 5.92252                          | .915750    | .0313      | .12697     |
| 80.0            | 5.53852                       | .856376    | .928869         | .14362     | 5.42355                          | .838599    | .0625      | .25395     |
| 120.0           | 5.10578                       | .789466    | 1.361607        | .21053     | 4.96661                          | .767947    | .0938      | .38092     |
| 160.0           | 4.68958                       | .725112    | 1.777807        | .27489     | 4.54818                          | .703248    | .1250      | .50790     |
| 200.0           | 4.28992                       | .663316    | 2.177469        | .33668     | 4.16500                          | .643999    | .1563      | .63487     |
| 240.0           | 3.90680                       | .604076    | 2.560593        | .39592     | 3.81410                          | .589742    | .1875      | .76184     |
| 280.0           | 3.54021                       | .547394    | 2.927179        | .45261     | 3.49276                          | .540057    | .2188      | .88882     |
| 320.0           | 3.19016                       | .493269    | 3.277228        | .50673     | 3.19849                          | .494557    | .2500      | 1.01579    |
| 360.0           | 2.85665                       | .441701    | 3.610739        | .55830     | 2.92902                          | .452891    | .2813      | 1.14276    |
| 400.0           | 2.53968                       | .392690    | 3.927713        | .60731     | 2.68225                          | .414735    | .3125      | 1.26974    |
| 440.0           | 2.24200                       | .346662    | 4.225392        | .65334     | 2.45627                          | .379794    | .3438      | 1.39671    |
| 480.0           | 1.96361                       | .303618    | 4.503777        | .69638     | 2.24933                          | .347796    | .3750      | 1.52369    |
| 520.0           | 1.70452                       | .263557    | 4.762868        | .73644     | 2.05983                          | .318494    | .4063      | 1.65066    |
| 560.0           | 1.47024                       | .227331    | 4.997153        | .77267     | 1.88629                          | .291661    | .4375      | 1.77763    |
| 600.0           | 1.26076                       | .194941    | 5.206631        | .80506     | 1.72737                          | .267089    | .4688      | 1.90461    |
| 640.0           | 1.07333                       | .165961    | 5.394059        | .83404     | 1.58184                          | .244587    | .5000      | 2.03158    |
| 680.0           | .90795                        | .140390    | 5.559436        | .85961     | 1.44857                          | .223980    | .5313      | 2.15856    |
| 720.0           | .76463                        | .118228    | 5.702763        | .88177     | 1.32653                          | .205110    | .5625      | 2.28553    |
| 760.0           | .64335                        | .099476    | 5.824040        | .90052     | 1.21477                          | .187830    | .5938      | 2.41250    |
| 800.0           | .54137                        | .083707    | 5.926023        | .91629     | 1.11242                          | .172005    | .6250      | 2.53948    |
| 840.0           | .45592                        | .070496    | 6.011468        | .92950     | 1.01870                          | .157514    | .6563      | 2.66645    |
| 880.0           | .38426                        | .059415    | 6.083132        | .94059     | .93288                           | .144243    | .6875      | 2.79342    |
| 920.0           | .32638                        | .050465    | 6.141013        | .94953     | .85428                           | .132091    | .7188      | 2.92040    |
| 960.0           | .27952                        | .043220    | 6.187871        | .95678     | .78231                           | .120962    | .7500      | 3.04737    |
| 1000.0          | .24093                        | .037253    | 6.226458        | .96275     | .71640                           | .110771    | .7813      | 3.17435    |
| 1040.0          | .21337                        | .032992    | 6.254021        | .96701     | .65604                           | .101439    | .8125      | 3.30132    |
| 1080.0          | .19408                        | .030008    | 6.273315        | .96999     | .60077                           | .091893    | .8438      | 3.42829    |
| 1120.0          | .18029                        | .027878    | 6.287097        | .97212     | .55016                           | .085006    | .8750      | 3.55527    |
| 1160.0          | .16927                        | .026173    | 6.298122        | .97383     | .50381                           | .077900    | .9063      | 3.68224    |
| 1200.0          | .16100                        | .024894    | 6.306391        | .97511     | .46136                           | .071337    | .9375      | 3.80921    |
| 1240.0          | .15549                        | .024042    | 6.311904        | .97596     | .42249                           | .065326    | .9688      | 3.92619    |
| 1280.0          | .15273                        | .023616    | 6.314660        | .97638     | .38690                           | .059823    | 1.0000     | 4.06316    |

TABLE D-19

EVAPORATION EXPERIMENT NO. 8L51 SERIES TO 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOX SURFACE  
 WINDSPEED 11.3 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

## EVAPORATION HISTORY OF TEST DROPLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |            |                               |            | THEORETICAL HALF LIFE MODEL DATA |                    |                    |                    |
|-----------------|-------------------------------|------------|-------------------------------|------------|----------------------------------|--------------------|--------------------|--------------------|
|                 | RESIDUAL MASS<br>MILLIGRAMS   | FRACTIONAL | CUMULATIVE MASS<br>MILLIGRAMS | FRACTIONAL | MASS<br>MILLIGRAMS               | MASS<br>FRACTIONAL | TIME<br>FRACTIONAL | TIME<br>HALF-LIVES |
| 0               | 6.33913                       | 1.000000   | 0.00000                       | 0.0000     | 6.33913                          | 1.000000           | 0.0000             | 0.00000            |
| 15.0            | 5.93133                       | .935075    | .407799                       | .06433     | 5.95171                          | .929419            | .0333              | .10560             |
| 30.0            | 5.54372                       | .874524    | .795410                       | .12548     | 5.47587                          | .863320            | .0667              | .21120             |
| 45.0            | 5.17630                       | .816563    | 1.162874                      | .18344     | 5.00938                          | .802851            | .1000              | .31680             |
| 60.0            | 4.82906                       | .761786    | 1.510060                      | .23921     | 4.73017                          | .746185            | .1333              | .42240             |
| 75.0            | 4.49354                       | .708921    | 1.845191                      | .29108     | 4.39631                          | .694519            | .1667              | .52799             |
| 90.0            | 4.17093                       | .657966    | 2.168200                      | .34203     | 4.08601                          | .644570            | .2000              | .63359             |
| 105.0           | 3.86407                       | .609559    | 2.475059                      | .39044     | 3.79762                          | .599075            | .2333              | .73919             |
| 120.0           | 3.57336                       | .563399    | 2.769768                      | .43530     | 3.52953                          | .556793            | .2667              | .84479             |
| 135.0           | 3.29477                       | .519751    | 3.044333                      | .48025     | 3.28046                          | .517494            | .3000              | .95039             |
| 150.0           | 3.02025                       | .477713    | 3.310845                      | .52129     | 3.04892                          | .480969            | .3333              | 1.05598            |
| 165.0           | 2.77392                       | .437386    | 3.565216                      | .56241     | 2.83373                          | .447022            | .3667              | 1.16158            |
| 180.0           | 2.55166                       | .399370    | 3.807472                      | .60053     | 2.63372                          | .415471            | .4000              | 1.26718            |
| 195.0           | 2.30555                       | .363702    | 4.033579                      | .63630     | 2.46783                          | .386466            | .4333              | 1.37276            |
| 210.0           | 2.09560                       | .330581    | 4.243535                      | .66942     | 2.27506                          | .358692            | .4667              | 1.47838            |
| 225.0           | 1.90179                       | .300008    | 4.437341                      | .69999     | 2.11449                          | .333561            | .5000              | 1.58398            |
| 240.0           | 1.72007                       | .272620    | 4.610959                      | .72738     | 1.96525                          | .310018            | .5333              | 1.68958            |
| 255.0           | 1.57474                       | .248416    | 4.764388                      | .75118     | 1.82654                          | .288137            | .5667              | 1.79517            |
| 270.0           | 1.43746                       | .226760    | 4.901667                      | .77324     | 1.69762                          | .267300            | .6000              | 1.90077            |
| 285.0           | 1.31634                       | .207652    | 5.022796                      | .79235     | 1.57790                          | .248898            | .6333              | 2.00637            |
| 300.0           | 1.21136                       | .191092    | 5.127773                      | .80891     | 1.46644                          | .231331            | .6667              | 2.11197            |
| 315.0           | 1.12253                       | .177079    | 5.215601                      | .82292     | 1.36294                          | .215003            | .7000              | 2.21757            |
| 330.0           | 1.04985                       | .165615    | 5.289278                      | .83439     | 1.26674                          | .199828            | .7333              | 2.32317            |
| 345.0           | .99333                        | .156698    | 5.345805                      | .84330     | 1.17733                          | .185724            | .7667              | 2.42877            |
| 360.0           | .95295                        | .150328    | 5.386181                      | .84967     | 1.09423                          | .172616            | .8000              | 2.53436            |
| 375.0           | .92469                        | .145870    | 5.414444                      | .85413     | 1.01700                          | .160432            | .8333              | 2.63996            |
| 390.0           | .90450                        | .142685    | 5.434632                      | .85732     | .94522                           | .149109            | .8667              | 2.74555            |
| 405.0           | .88835                        | .140137    | 5.450783                      | .85986     | .87851                           | .138585            | .9000              | 2.85116            |
| 420.0           | .87624                        | .138226    | 5.462895                      | .86177     | .81650                           | .128803            | .9333              | 2.95676            |
| 435.0           | .86816                        | .136953    | 5.470971                      | .86305     | .75887                           | .119712            | .9667              | 3.06236            |
| 450.0           | .86412                        | .136316    | 5.475008                      | .86368     | .70531                           | .111263            | 1.0000             | 3.16795            |



TABLE D-20

EVAPORATION EXPERIMENT NO. BLF4 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 20%

## EVAPORATION HISTORY OF TEST DROPLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |            |                 |            | THEORETICAL HALF LIFE MODEL DATA |            |            |            |
|-----------------|-------------------------------|------------|-----------------|------------|----------------------------------|------------|------------|------------|
|                 | RESIDUAL MASS                 |            | CUMULATIVE MASS |            | MASS                             | MASS       | TIME       | TIME       |
|                 | MILLIGRAMS                    | FRACTIONAL | MILLIGRAMS      | FRACTIONAL | MILLIGRAMS                       | FRACTIONAL | FRACTIONAL | HALF-LIVES |
| .0              | 6.72609                       | 1.000000   | .000000         | .000000    | 6.72609                          | 1.000000   | .0000      | .00000     |
| 20.0            | 6.18235                       | .919161    | .543732         | .08084     | 6.08267                          | .904340    | .0357      | .14596     |
| 40.0            | 5.65477                       | .840723    | 1.071314        | .15928     | 5.50080                          | .817830    | .0714      | .29013     |
| 60.0            | 5.14872                       | .765486    | 1.577362        | .23451     | 4.97459                          | .739596    | .1071      | .43119     |
| 80.0            | 4.65883                       | .692650    | 2.067260        | .30735     | 4.49872                          | .668846    | .1429      | .58025     |
| 100.0           | 4.18508                       | .622216    | 2.541007        | .37778     | 4.06837                          | .604864    | .1786      | .72932     |
| 120.0           | 3.73825                       | .555784    | 2.987836        | .44422     | 3.67919                          | .547003    | .2143      | .87038     |
| 140.0           | 3.31834                       | .493353    | 3.407748        | .50665     | 3.32723                          | .494676    | .2500      | 1.01544    |
| 160.0           | 2.91996                       | .434125    | 3.806127        | .56588     | 3.00895                          | .447355    | .2857      | 1.16051    |
| 180.0           | 2.54312                       | .378097    | 4.182971        | .62190     | 2.72111                          | .404561    | .3214      | 1.30557    |
| 200.0           | 2.19319                       | .326072    | 4.532897        | .67393     | 2.46081                          | .365861    | .3571      | 1.45063    |
| 220.0           | 1.87018                       | .278049    | 4.855906        | .72195     | 2.22541                          | .330862    | .3929      | 1.59570    |
| 240.0           | 1.57409                       | .234027    | 5.151999        | .76597     | 2.01252                          | .299212    | .4286      | 1.74076    |
| 260.0           | 1.30491                       | .194008    | 5.421173        | .80599     | 1.82001                          | .270589    | .4643      | 1.88582    |
| 280.0           | 1.06266                       | .157990    | 5.663430        | .84201     | 1.64590                          | .244704    | .5000      | 2.03089    |
| 300.0           | .85270                        | .126775    | 5.873386        | .87322     | 1.48846                          | .221296    | .5357      | 2.17595    |
| 320.0           | .67505                        | .100362    | 6.051042        | .89964     | 1.34607                          | .200127    | .5714      | 2.32101    |
| 340.0           | .52969                        | .078752    | 6.196396        | .92125     | 1.21730                          | .180982    | .6071      | 2.46608    |
| 360.0           | .41664                        | .061944    | 6.309449        | .93806     | 1.10086                          | .163670    | .6429      | 2.61114    |
| 380.0           | .33589                        | .049938    | 6.390201        | .95006     | .99555                           | .148013    | .6786      | 2.75620    |
| 400.0           | .28205                        | .041934    | 6.444036        | .95807     | .90031                           | .133854    | .7143      | 2.90127    |
| 420.0           | .24437                        | .036331    | 6.481721        | .96367     | .81419                           | .121049    | .7500      | 3.04633    |
| 440.0           | .21745                        | .032324    | 6.508638        | .96767     | .73630                           | .109470    | .7857      | 3.19140    |
| 460.0           | .19591                        | .029128    | 6.530172        | .97087     | .66587                           | .098998    | .8214      | 3.33646    |
| 480.0           | .17976                        | .026726    | 6.546322        | .97327     | .60217                           | .089528    | .8571      | 3.48152    |
| 500.0           | .16900                        | .025126    | 6.557089        | .97487     | .54457                           | .080963    | .8929      | 3.62659    |
| 520.0           | .15823                        | .023525    | 6.567857        | .97648     | .49247                           | .073218    | .9286      | 3.77165    |
| 540.0           | .14746                        | .021924    | 6.578624        | .97808     | .44536                           | .066214    | .9643      | 3.91671    |
| 560.0           | .14208                        | .021124    | 6.584008        | .97888     | .40276                           | .059880    | 1.0000     | 4.06178    |

TABLE D-21

EVAPORATION EXPERIMENT NO. BL59 SERIES ID 2446 FACTORIAL EXPERIMENT  
 DIETHYLHALOATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/50 METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

## EVAPORATION HISTORY OF TEST DROPLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |                        |                               |            | THEORETICAL HALF LIFE MODEL DATA |                    |                    |                    |
|-----------------|-------------------------------|------------------------|-------------------------------|------------|----------------------------------|--------------------|--------------------|--------------------|
|                 | RESIDUAL MASS<br>MILLIGRAMS   | FRACTIONAL<br>ORIGINAL | CUMULATIVE MASS<br>MILLIGRAMS | FRACTIONAL | MASS<br>MILLIGRAMS               | MASS<br>FRACTIONAL | TIME<br>FRACTIONAL | TIME<br>HALF-LIVES |
| .0              | 6.07500                       | 1.000000               | .000000                       | .00000     | 6.07500                          | 1.000000           | .0000              | .00000             |
| 30.0            | 5.74245                       | .945259                | .332553                       | .05474     | 5.71510                          | .940771            | .0263              | .04508             |
| 60.0            | 5.43632                       | .896068                | .638678                       | .10513     | 5.37560                          | .885050            | .0526              | .17517             |
| 90.0            | 5.14561                       | .847015                | .929386                       | .15299     | 5.05823                          | .832630            | .0789              | .26425             |
| 120.0           | 4.86371                       | .800611                | 1.211285                      | .19939     | 4.75863                          | .783314            | .1053              | .35234             |
| 150.0           | 4.59063                       | .755659                | 1.484375                      | .24434     | 4.47673                          | .736919            | .1316              | .44042             |
| 180.0           | 4.32414                       | .711793                | 1.750958                      | .28821     | 4.21163                          | .693272            | .1577              | .52951             |
| 210.0           | 4.06427                       | .669015                | 2.010733                      | .33098     | 3.96218                          | .652210            | .1842              | .61659             |
| 240.0           | 3.81320                       | .627687                | 2.261800                      | .37231     | 3.72750                          | .613581            | .2105              | .70467             |
| 270.0           | 3.57094                       | .587810                | 2.504057                      | .41219     | 3.50673                          | .577239            | .2368              | .79276             |
| 300.0           | 3.33750                       | .549202                | 2.737504                      | .45052     | 3.29903                          | .543050            | .2632              | .88084             |
| 330.0           | 3.11286                       | .512404                | 2.962143                      | .48760     | 3.10363                          | .510886            | .2895              | .96893             |
| 360.0           | 2.89923                       | .477240                | 3.175769                      | .52276     | 2.91980                          | .480626            | .3158              | 1.05701            |
| 390.0           | 2.69882                       | .444250                | 3.376182                      | .55575     | 2.74687                          | .452159            | .3421              | 1.14510            |
| 420.0           | 2.51162                       | .413435                | 3.563380                      | .58656     | 2.58617                          | .425378            | .3684              | 1.23318            |
| 450.0           | 2.33764                       | .384796                | 3.737365                      | .61520     | 2.43112                          | .400184            | .3947              | 1.32127            |
| 480.0           | 2.17686                       | .358332                | 3.898135                      | .64167     | 2.28712                          | .376481            | .4211              | 1.40935            |
| 510.0           | 2.02931                       | .334042                | 4.045692                      | .66596     | 2.15166                          | .354183            | .4474              | 1.49743            |
| 540.0           | 1.89276                       | .311566                | 4.182237                      | .68843     | 2.02422                          | .333205            | .4737              | 1.58552            |
| 570.0           | 1.75723                       | .290902                | 4.307770                      | .70910     | 1.90433                          | .313470            | .5000              | 1.67360            |
| 600.0           | 1.65491                       | .272413                | 4.420089                      | .72759     | 1.79154                          | .294903            | .5263              | 1.76169            |
| 630.0           | 1.55581                       | .256100                | 4.519194                      | .74390     | 1.68543                          | .277636            | .5526              | 1.84977            |
| 660.0           | 1.46991                       | .241561                | 4.605085                      | .75804     | 1.58560                          | .261004            | .5789              | 1.93786            |
| 690.0           | 1.39724                       | .229998                | 4.677762                      | .77000     | 1.49169                          | .245545            | .6053              | 2.02594            |
| 720.0           | 1.33777                       | .220210                | 4.737225                      | .77979     | 1.40333                          | .231002            | .6316              | 2.11402            |
| 750.0           | 1.28932                       | .212234                | 4.785677                      | .78777     | 1.32522                          | .217320            | .6579              | 2.20211            |
| 780.0           | 1.24748                       | .205346                | 4.827521                      | .79465     | 1.24202                          | .204448            | .6842              | 2.29019            |
| 810.0           | 1.21004                       | .199183                | 4.864961                      | .80082     | 1.16846                          | .192339            | .7105              | 2.37828            |
| 840.0           | 1.17700                       | .193746                | 4.897796                      | .80625     | 1.09925                          | .180947            | .7368              | 2.46636            |
| 870.0           | 1.14837                       | .189033                | 4.926626                      | .81097     | 1.03414                          | .170230            | .7632              | 2.55445            |
| 900.0           | 1.12415                       | .185045                | 4.951852                      | .81496     | .97289                           | .160147            | .7895              | 2.64253            |
| 930.0           | 1.10653                       | .182145                | 4.968471                      | .81786     | .91527                           | .150662            | .8158              | 2.73062            |
| 960.0           | 1.09332                       | .179970                | 4.981685                      | .82083     | .86106                           | .141738            | .8421              | 2.81870            |
| 990.0           | 1.08010                       | .177794                | 4.994899                      | .82221     | .81006                           | .133343            | .8684              | 2.90678            |
| 1020.0          | 1.06909                       | .175982                | 5.005910                      | .82402     | .76208                           | .125445            | .8947              | 2.99487            |
| 1050.0          | 1.06028                       | .174532                | 5.016720                      | .82547     | .71694                           | .118115            | .9211              | 3.08295            |
| 1080.0          | 1.05367                       | .173444                | 5.021327                      | .82656     | .67448                           | .111025            | .9474              | 3.17106            |
| 1110.0          | 1.04927                       | .172719                | 5.025731                      | .82728     | .63453                           | .104450            | .9737              | 3.25912            |
| 1140.0          | 1.04797                       | .172357                | 5.027934                      | .82764     | .59695                           | .098263            | 1.0000             | 3.34721            |

TABLE D-22

EVAPORATION EXPERIMENT NO. BLF6 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 2.9 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

## EVAPORATION HISTORY OF TEST DROPLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |            |                 |            | THEORETICAL HALF LIFE MODEL DATA |            |            |            |
|-----------------|-------------------------------|------------|-----------------|------------|----------------------------------|------------|------------|------------|
|                 | RESIDUAL MASS                 |            | CUMULATIVE MASS |            | MASS                             | MASS       | TIME       | TIME       |
|                 | MILLIGRAMS                    | FRACTIONAL | MILLIGRAMS      | FRACTIONAL | MILLIGRAMS                       | FRACTIONAL | FRACTIONAL | HALF-LIVES |
| 0.0             | 6.33804                       | 1.000000   | .000000         | .000000    | 6.33804                          | 1.000000   | .0000      | .00000     |
| 40.0            | 5.80103                       | .927394    | .457009         | .07211     | 5.80431                          | .915789    | .0323      | .12691     |
| 80.0            | 5.43822                       | .858028    | .899826         | .14197     | 5.31553                          | .838670    | .0645      | .25382     |
| 120.0           | 5.01243                       | .790849    | 1.325611        | .20915     | 4.86791                          | .768046    | .0968      | .38074     |
| 160.0           | 4.60368                       | .726327    | 1.734364        | .27364     | 4.45798                          | .703368    | .1290      | .50765     |
| 200.0           | 4.20912                       | .664104    | 2.128925        | .33590     | 4.08257                          | .644137    | .1613      | .63456     |
| 240.0           | 3.83159                       | .604538    | 2.506455        | .39546     | 3.73877                          | .589894    | .1935      | .76147     |
| 280.0           | 3.47109                       | .547660    | 2.863953        | .45234     | 3.42393                          | .540219    | .2258      | .88838     |
| 320.0           | 3.12762                       | .493468    | 3.210419        | .50653     | 3.13560                          | .494727    | .2581      | 1.01530    |
| 360.0           | 2.80119                       | .441964    | 3.536855        | .55804     | 2.87155                          | .453065    | .2903      | 1.14221    |
| 400.0           | 2.49179                       | .393147    | 3.846258        | .60685     | 2.62973                          | .414913    | .3226      | 1.26912    |
| 440.0           | 2.20225                       | .347466    | 4.135792        | .65253     | 2.40828                          | .379973    | .3548      | 1.39603    |
| 480.0           | 1.93826                       | .305814    | 4.399779        | .69419     | 2.20548                          | .347975    | .3871      | 1.52294    |
| 520.0           | 1.70266                       | .268642    | 4.635380        | .73136     | 2.01976                          | .318672    | .4194      | 1.64986    |
| 560.0           | 1.49261                       | .235500    | 4.845434        | .76450     | 1.84967                          | .291836    | .4516      | 1.77677    |
| 600.0           | 1.30810                       | .206389    | 5.029941        | .79361     | 1.69391                          | .267261    | .4839      | 1.90368    |
| 640.0           | 1.15198                       | .181757    | 5.186061        | .81824     | 1.55126                          | .244754    | .5161      | 2.03059    |
| 680.0           | 1.02425                       | .161603    | 5.313797        | .83840     | 1.42063                          | .224144    | .5484      | 2.15751    |
| 720.0           | .91922                        | .145032    | 5.418825        | .85497     | 1.30100                          | .205268    | .5806      | 2.28442    |
| 760.0           | .83122                        | .131148    | 5.506820        | .86885     | 1.19144                          | .187983    | .6129      | 2.41133    |
| 800.0           | .75742                        | .119504    | 5.580623        | .88050     | 1.09111                          | .172152    | .6452      | 2.53824    |
| 840.0           | .69497                        | .109651    | 5.643071        | .89035     | .99923                           | .157655    | .6774      | 2.66515    |
| 880.0           | .64388                        | .101589    | 5.694165        | .89841     | .91508                           | .144379    | .7097      | 2.79207    |
| 920.0           | .60130                        | .094872    | 5.736744        | .90513     | .83002                           | .132221    | .7419      | 2.91898    |
| 960.0           | .56440                        | .089049    | 5.773644        | .91095     | .76745                           | .121087    | .7742      | 3.04589    |
| 1000.0          | .53317                        | .084123    | 5.804869        | .91588     | .70282                           | .110890    | .8065      | 3.17280    |
| 1040.0          | .50763                        | .080092    | 5.830416        | .91991     | .64364                           | .101552    | .8387      | 3.29971    |
| 1080.0          | .48776                        | .076957    | 5.850286        | .92304     | .58944                           | .093000    | .8710      | 3.42663    |
| 1120.0          | .47356                        | .074718    | 5.864479        | .92528     | .53980                           | .085168    | .9032      | 3.55354    |
| 1160.0          | .46221                        | .072926    | 5.875834        | .92707     | .49434                           | .077996    | .9355      | 3.68045    |
| 1200.0          | .45369                        | .071583    | 5.884349        | .92842     | .45272                           | .071428    | .9677      | 3.80736    |
| 1240.0          | .45086                        | .071135    | 5.887188        | .92887     | .41459                           | .065413    | 1.0000     | 3.93427    |

TABLE D-23

EVAPORATION EXPERIMENT NO. BLF7 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

## EVAPORATION HISTORY OF TEST DROPLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |            |                 |            | THEORETICAL HALF LIFE MODEL DATA |            |            |            |
|-----------------|-------------------------------|------------|-----------------|------------|----------------------------------|------------|------------|------------|
|                 | RESIDUAL MASS                 |            | CUMULATIVE MASS |            | MASS                             | MASS       | TIME       | TIME       |
|                 | MILLIGRAMS                    | FRACTIONAL | MILLIGRAMS      | FRACTIONAL | MILLIGRAMS                       | FRACTIONAL | FRACTIONAL | HALF-LIVES |
| .0              | 5.81087                       | 1.000000   | .000000         | .000000    | 5.81087                          | 1.000000   | .0000      | .00000     |
| 15.0            | 5.45960                       | .939549    | .351273         | .06045     | 5.41005                          | .931023    | .0294      | .10311     |
| 30.0            | 5.12044                       | .881183    | .690432         | .11882     | 5.03688                          | .866803    | .0588      | .20622     |
| 45.0            | 4.79339                       | .824901    | 1.017480        | .17510     | 4.68945                          | .807014    | .0882      | .30934     |
| 60.0            | 4.47442                       | .770008    | 1.336451        | .22999     | 4.36599                          | .751348    | .1176      | .41245     |
| 75.0            | 4.16756                       | .717201    | 1.643310        | .28280     | 4.06483                          | .699522    | .1471      | .51556     |
| 90.0            | 3.87685                       | .667172    | 1.934018        | .33283     | 3.78445                          | .651271    | .1765      | .61867     |
| 105.0           | 3.59826                       | .61728     | 2.212614        | .38077     | 3.52341                          | .606348    | .2059      | .72178     |
| 120.0           | 3.33177                       | .573369    | 2.479097        | .42663     | 3.28037                          | .564524    | .2353      | .82489     |
| 135.0           | 3.07740                       | .529594    | 2.733467        | .47041     | 3.05410                          | .525585    | .2647      | .92801     |
| 150.0           | 2.83111                       | .487209    | 2.979761        | .51279     | 2.84344                          | .489331    | .2941      | 1.03112    |
| 165.0           | 2.59693                       | .446908    | 3.213943        | .55309     | 2.64731                          | .455578    | .3235      | 1.13423    |
| 180.0           | 2.37486                       | .408692    | 3.436012        | .59131     | 2.46470                          | .424154    | .3529      | 1.23734    |
| 195.0           | 2.16490                       | .372561    | 3.645968        | .62744     | 2.29469                          | .394897    | .3824      | 1.34045    |
| 210.0           | 1.97110                       | .339208    | 3.839774        | .66079     | 2.13641                          | .367658    | .4118      | 1.44356    |
| 225.0           | 1.79344                       | .308636    | 4.017428        | .69136     | 1.98905                          | .342298    | .4412      | 1.54668    |
| 240.0           | 1.63194                       | .280842    | 4.178934        | .71916     | 1.85185                          | .318687    | .4706      | 1.64979    |
| 255.0           | 1.49062                       | .256523    | 4.320250        | .74348     | 1.72411                          | .296705    | .5000      | 1.75290    |
| 270.0           | 1.36949                       | .235677    | 4.441379        | .76432     | 1.60519                          | .276239    | .5294      | 1.85601    |
| 285.0           | 1.26048                       | .216917    | 4.550395        | .78308     | 1.49447                          | .257185    | .5588      | 1.95912    |
| 300.0           | 1.16357                       | .200241    | 4.647297        | .79976     | 1.39138                          | .239445    | .5882      | 2.06223    |
| 315.0           | 1.08282                       | .186344    | 4.728050        | .81366     | 1.29541                          | .222929    | .6176      | 2.16535    |
| 330.0           | 1.01418                       | .174532    | 4.796689        | .82547     | 1.20606                          | .207552    | .6471      | 2.26846    |
| 345.0           | .95362                        | .164109    | 4.857253        | .83589     | 1.12287                          | .193235    | .6765      | 2.37157    |
| 360.0           | .90113                        | .155076    | 4.909742        | .84492     | 1.04541                          | .179907    | .7059      | 2.47468    |
| 375.0           | .85671                        | .147433    | 4.954156        | .85257     | .97330                           | .167497    | .7353      | 2.57779    |
| 390.0           | .82038                        | .141179    | 4.990495        | .85882     | .90617                           | .155944    | .7647      | 2.68090    |
| 405.0           | .79211                        | .136316    | 5.018758        | .86368     | .84366                           | .145187    | .7941      | 2.78402    |
| 420.0           | .76789                        | .132146    | 5.042984        | .86785     | .78547                           | .135172    | .8235      | 2.88713    |
| 435.0           | .74770                        | .128672    | 5.063172        | .87133     | .73129                           | .125849    | .8529      | 2.99024    |
| 450.0           | .73155                        | .125893    | 5.079322        | .87411     | .68085                           | .117168    | .8824      | 3.09335    |
| 465.0           | .71943                        | .123808    | 5.091435        | .87619     | .63388                           | .109086    | .9118      | 3.19546    |
| 480.0           | .71136                        | .122419    | 5.099511        | .87758     | .59016                           | .101562    | .9412      | 3.29957    |
| 495.0           | .70328                        | .121029    | 5.107586        | .87897     | .54945                           | .094556    | .9706      | 3.40269    |
| 510.0           | .69925                        | .120334    | 5.111623        | .87967     | .51155                           | .088034    | 1.0000     | 3.50580    |

TABLE D-24

EVAPORATION EXPERIMENT NO. BLFB SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ MEYER ON OAK/BOTTOM SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 50%

## EVAPORATION HISTORY OF TEST DROPLET MEASURED AND THEORETICAL

| TIME<br>MINUTES | EXPERIMENTAL EVAPORATION DATA |            |                 |            | THEORETICAL HALF LIFE MODEL DATA |            |            |            |
|-----------------|-------------------------------|------------|-----------------|------------|----------------------------------|------------|------------|------------|
|                 | RESIDUAL MASS                 |            | CUMULATIVE MASS |            | MASS                             | MASS       | TIME       | TIME       |
|                 | MILLIGRAMS                    | FRACTIONAL | MILLIGRAMS      | FRACTIONAL | MILLIGRAMS                       | FRACTIONAL | FRACTIONAL | HALF-LIFES |
| .0              | 6.59674                       | 1.000000   | .000000         | .000000    | 6.59674                          | 1.000000   | .0000      | .00000     |
| 15.0            | 6.20679                       | .940887    | .389952         | .05911     | 6.15493                          | .933026    | .0313      | .10001     |
| 30.0            | 5.83275                       | .884187    | .763988         | .11581     | 5.74271                          | .870538    | .0625      | .20002     |
| 45.0            | 5.47463                       | .829900    | 1.122106        | .17010     | 5.35810                          | .812234    | .0938      | .30003     |
| 60.0            | 5.13243                       | .778025    | 1.464309        | .22197     | 4.99924                          | .757836    | .1250      | .40004     |
| 75.0            | 4.80216                       | .727960    | 1.794575        | .27204     | 4.66442                          | .707080    | .1563      | .50005     |
| 90.0            | 4.47986                       | .679102    | 2.116881        | .32090     | 4.35203                          | .659774    | .1875      | .60006     |
| 105.0           | 4.16969                       | .632053    | 2.427252        | .36795     | 4.06056                          | .615340    | .2188      | .70008     |
| 120.0           | 3.87106                       | .586813    | 2.725684        | .41319     | 3.78861                          | .574315    | .2500      | .80009     |
| 135.0           | 3.58058                       | .542780    | 3.016158        | .45722     | 3.53487                          | .535851    | .2813      | .90010     |
| 150.0           | 3.29806                       | .499954    | 3.298674        | .50005     | 3.29812                          | .499963    | .3125      | 1.00011    |
| 165.0           | 3.02351                       | .458334    | 3.573232        | .54167     | 3.07723                          | .466478    | .3438      | 1.10012    |
| 180.0           | 2.75691                       | .417920    | 3.839832        | .58208     | 2.87114                          | .435236    | .3750      | 1.20013    |
| 195.0           | 2.49827                       | .378712    | 4.098474        | .62129     | 2.67885                          | .406087    | .4063      | 1.30014    |
| 210.0           | 2.25156                       | .341314    | 4.345178        | .65869     | 2.49943                          | .378889    | .4375      | 1.40015    |
| 225.0           | 2.01679                       | .305726    | 4.579945        | .69427     | 2.33204                          | .353514    | .4688      | 1.50016    |
| 240.0           | 1.79396                       | .271947    | 4.802774        | .72805     | 2.17585                          | .329838    | .5000      | 1.60017    |
| 255.0           | 1.58307                       | .239979    | 5.013667        | .76002     | 2.03013                          | .307747    | .5313      | 1.70018    |
| 270.0           | 1.38014                       | .209215    | 5.216601        | .79078     | 1.89416                          | .287136    | .5625      | 1.80019    |
| 285.0           | 1.19710                       | .181468    | 5.399640        | .81853     | 1.76730                          | .267905    | .5938      | 1.90020    |
| 300.0           | 1.03794                       | .157341    | 5.558804        | .84266     | 1.64894                          | .249963    | .6250      | 2.00022    |
| 315.0           | .89469                        | .135626    | 5.702052        | .86437     | 1.53850                          | .233222    | .6563      | 2.10023    |
| 330.0           | .76736                        | .116324    | 5.829382        | .88368     | 1.43546                          | .217602    | .6875      | 2.20024    |
| 345.0           | .65594                        | .099434    | 5.940797        | .90057     | 1.33952                          | .203028    | .7188      | 2.30025    |
| 360.0           | .56044                        | .084958    | 6.036296        | .91504     | 1.24962                          | .189431    | .7500      | 2.40026    |
| 375.0           | .48086                        | .072894    | 6.115878        | .92711     | 1.16593                          | .176744    | .7813      | 2.50027    |
| 390.0           | .41720                        | .063243    | 6.179543        | .93676     | 1.08784                          | .164906    | .8125      | 2.60028    |
| 405.0           | .36945                        | .056004    | 6.227293        | .94400     | 1.01499                          | .153862    | .8438      | 2.70029    |
| 420.0           | .33363                        | .050576    | 6.263104        | .94942     | .94701                           | .143557    | .8750      | 2.80030    |
| 435.0           | .30976                        | .046056    | 6.288979        | .95304     | .88358                           | .133943    | .9063      | 2.90031    |
| 450.0           | .29782                        | .043147    | 6.298917        | .95485     | .82441                           | .124972    | .9375      | 3.00032    |
| 465.0           | .28986                        | .0413940   | 6.306875        | .95606     | .76919                           | .116602    | .9688      | 3.10033    |
| 480.0           | .28589                        | .0413337   | 6.310854        | .95666     | .71768                           | .108793    | 1.0000     | 3.20035    |

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APPENDIX E  
EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

TABLE E-1

EVAPORATION EXPERIMENT NO. GLE1 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 D ETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/TOP SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 45%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |            | ***** EVAPORATION RATE ***** |            |
|------------------|------------|------------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIVES | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .0000      | .00000     | .00000                       | .00000     |
| 30.0             | .0345      | .12187     | -17.91234                    | -19.61007  |
| 60.0             | .0690      | .24374     | -15.93023                    | -19.04545  |
| 90.0             | .1034      | .36561     | -14.16837                    | -18.44951  |
| 120.0            | .1379      | .48747     | -12.92038                    | -18.31362  |
| 150.0            | .1724      | .60934     | -11.81920                    | -18.22875  |
| 180.0            | .2069      | .73121     | -10.64463                    | -17.83216  |
| 210.0            | .2414      | .85308     | -9.61686                     | -17.47077  |
| 240.0            | .2759      | .97495     | -8.80934                     | -17.34543  |
| 270.0            | .3103      | 1.09682    | -7.92842                     | -16.88488  |
| 300.0            | .3448      | 1.21869    | -7.12088                     | -16.36456  |
| 330.0            | .3793      | 1.34055    | -6.38678                     | -15.79822  |
| 360.0            | .4138      | 1.46242    | -5.65268                     | -14.99577  |
| 390.0            | .4483      | 1.58429    | -4.99197                     | -14.14859  |
| 420.0            | .4828      | 1.70616    | -4.40466                     | -13.28563  |
| 450.0            | .5172      | 1.82803    | -3.74397                     | -11.94478  |
| 480.0            | .5517      | 1.94990    | -3.08327                     | -10.32788  |
| 510.0            | .5862      | 2.07177    | -2.45598                     | -8.71274   |
| 540.0            | .6207      | 2.19364    | -1.98211                     | -7.15835   |
| 570.0            | .6552      | 2.31550    | -1.61505                     | -6.00190   |
| 600.0            | .6897      | 2.43737    | -1.32140                     | -5.03001   |
| 630.0            | .7241      | 2.55924    | -1.07276                     | -3.98768   |
| 660.0            | .7586      | 2.68111    | -.80757                      | -3.18131   |
| 690.0            | .7931      | 2.80298    | -.5607                       | -2.63610   |
| 720.0            | .8276      | 2.92485    | -.31387                      | -2.07077   |
| 750.0            | .8621      | 3.04672    | -.06706                      | -1.48001   |
| 780.0            | .8966      | 3.16858    | .19305                       | -.19874    |
| 810.0            | .9310      | 3.29045    | .4023                        | .19096     |
| 840.0            | .9655      | 3.41232    | .6438                        | .60376     |
| 870.0            | 1.0000     | 3.53419    | .87542                       | 1.31333    |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING



TABLE E-2

EVAPORATION EXPERIMENT NO. GLF2 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/TOP SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 39%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |            | ***** EVAPORATION RATE ***** |            |
|------------------|------------|------------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIFES | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .0000      | .00000     | .00000                       | .00000     |
| 30.0             | .0294      | .11354     | -16.00364                    | -17.28695  |
| 60.0             | .0588      | .22708     | -14.82906                    | -17.30391  |
| 90.0             | .0882      | .34063     | -13.72791                    | -17.30485  |
| 120.0            | .1176      | .45417     | -12.77354                    | -17.40154  |
| 150.0            | .1471      | .56771     | -11.98602                    | -17.63494  |
| 180.0            | .1765      | .68125     | -11.15852                    | -17.80293  |
| 210.0            | .2059      | .79479     | -10.35098                    | -17.88458  |
| 240.0            | .2353      | .90833     | -9.69027                     | -18.15285  |
| 270.0            | .2647      | 1.02188    | -9.02958                     | -18.35541  |
| 300.0            | .2941      | 1.13542    | -8.29547                     | -18.29410  |
| 330.0            | .3235      | 1.24896    | -7.63477                     | -18.26344  |
| 360.0            | .3529      | 1.36250    | -7.04748                     | -18.28878  |
| 390.0            | .3824      | 1.47604    | -6.46019                     | -18.17836  |
| 420.0            | .4118      | 1.58958    | -5.87290                     | -17.89777  |
| 450.0            | .4412      | 1.70313    | -5.28560                     | -17.40876  |
| 480.0            | .4706      | 1.81667    | -4.69831                     | -16.67109  |
| 510.0            | .5000      | 1.93021    | -4.11103                     | -15.64594  |
| 540.0            | .5294      | 2.04375    | -3.52374                     | -14.30041  |
| 570.0            | .5588      | 2.15729    | -3.00987                     | -12.94863  |
| 600.0            | .5882      | 2.27083    | -2.56939                     | -11.65109  |
| 630.0            | .6176      | 2.38438    | -2.12894                     | -10.10639  |
| 660.0            | .6471      | 2.49792    | -1.76186                     | -8.70142   |
| 690.0            | .6765      | 2.61146    | -1.54163                     | -7.89245   |
| 720.0            | .7059      | 2.72500    | -1.32141                     | -6.98422   |
| 750.0            | .7353      | 2.83854    | -1.10117                     | -5.98163   |
| 780.0            | .7647      | 2.95208    | -1.02775                     | -5.73121   |
| 810.0            | .7941      | 3.06563    | -.95435                      | -5.45663   |
| 840.0            | .8235      | 3.17917    | -.80751                      | -4.71813   |
| 870.0            | .8529      | 3.29271    | -.66070                      | -3.93070   |
| 900.0            | .8824      | 3.40625    | -.51388                      | -3.10119   |
| 930.0            | .9118      | 3.51979    | -.36706                      | -2.23817   |
| 960.0            | .9412      | 3.63333    | -.22022                      | -1.35119   |
| 990.0            | .9706      | 3.74688    | -.14682                      | -.90463    |
| 1020.0           | 1.0000     | 3.86042    | -.07341                      | -.45328    |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING.

TABLE E-3

EVAPORATION EXPERIMENT NO. GLF3 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 40%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |            | ***** EVAPORATION RATE ***** |            |
|------------------|------------|------------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIVES | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .0000      | .00000     | .00000                       | .00000     |
| 15.0             | .0417      | .17906     | -43.33708                    | -49.09026  |
| 30.0             | .0833      | .35811     | -37.95360                    | -48.64809  |
| 45.0             | .1250      | .53717     | -33.64632                    | -48.82185  |
| 60.0             | .1667      | .71622     | -29.87836                    | -49.11170  |
| 75.0             | .2083      | .89528     | -26.37908                    | -49.11948  |
| 90.0             | .2500      | 1.07433    | -23.41818                    | -49.43577  |
| 105.0            | .2917      | 1.25339    | -20.72644                    | -49.62528  |
| 120.0            | .3333      | 1.43244    | -18.03467                    | -48.88930  |
| 135.0            | .3750      | 1.61150    | -15.34295                    | -46.86356  |
| 150.0            | .4167      | 1.79056    | -12.65120                    | -43.15112  |
| 165.0            | .4583      | 1.96961    | -10.49781                    | -39.64514  |
| 180.0            | .5000      | 2.14867    | -8.86275                     | -36.89266  |
| 195.0            | .5417      | 2.32772    | -7.26772                     | -32.86795  |
| 210.0            | .5833      | 2.50678    | -5.65266                     | -27.46245  |
| 225.0            | .6250      | 2.68583    | -4.30681                     | -22.17883  |
| 240.0            | .6667      | 2.86489    | -3.23010                     | -17.41758  |
| 255.0            | .7083      | 3.04394    | -2.42256                     | -13.54151  |
| 270.0            | .7500      | 3.22300    | -2.15340                     | -12.44198  |
| 285.0            | .7917      | 3.40206    | -1.88422                     | -11.21692  |
| 300.0            | .8333      | 3.58111    | -1.61506                     | -9.87123   |
| 315.0            | .8750      | 3.76017    | -1.34597                     | -8.41313   |
| 330.0            | .9167      | 3.93922    | -1.0753                      | -5.11778   |
| 345.0            | .9583      | 4.11828    | .53837                       | -3.44371   |
| 360.0            | 1.0000     | 4.29733    | -.26916                      | 1.72979    |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING.

TABLE E-4

EVAPORATION EXPERIMENT NO. GLP4 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/TOF SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |            | ***** EVAPORATION RATE ***** |            |
|------------------|------------|------------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIVES | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .0000      | .00000     | .00000                       | .00000     |
| 10.0             | .0270      | .10177     | -39.03028                    | -41.53702  |
| 20.0             | .0541      | .20353     | -38.49193                    | -43.73419  |
| 30.0             | .0811      | .30530     | -37.41528                    | -45.50179  |
| 40.0             | .1081      | .40707     | -35.53102                    | -46.30398  |
| 50.0             | .1351      | .50883     | -33.57762                    | -46.63414  |
| 60.0             | .1622      | .61060     | -31.76257                    | -47.64706  |
| 70.0             | .1892      | .71236     | -30.41676                    | -48.09169  |
| 80.0             | .2162      | .81413     | -28.80164                    | -50.08432  |
| 90.0             | .2432      | .91590     | -27.16663                    | -51.00483  |
| 100.0            | .2703      | 1.01766    | -25.84076                    | -52.40839  |
| 110.0            | .2973      | 1.11943    | -24.49486                    | -53.81227  |
| 120.0            | .3243      | 1.22120    | -22.87985                    | -54.50001  |
| 130.0            | .3514      | 1.32296    | -21.53395                    | -55.71274  |
| 140.0            | .3784      | 1.42473    | -20.45727                    | -57.64461  |
| 150.0            | .4054      | 1.52649    | -19.11139                    | -58.74351  |
| 160.0            | .4324      | 1.62826    | -17.76553                    | -59.11262  |
| 170.0            | .4595      | 1.73003    | -16.68884                    | -61.34209  |
| 180.0            | .4865      | 1.83179    | -15.61212                    | -62.97192  |
| 190.0            | .5135      | 1.93356    | -14.53543                    | -64.47352  |
| 200.0            | .5405      | 2.03533    | -13.45872                    | -65.76878  |
| 210.0            | .5676      | 2.13709    | -12.38203                    | -66.75250  |
| 220.0            | .5946      | 2.23886    | -11.30531                    | -67.28909  |
| 230.0            | .6216      | 2.34062    | -10.22862                    | -67.20718  |
| 240.0            | .6486      | 2.44239    | -9.15191                     | -66.29678  |
| 250.0            | .6757      | 2.54416    | -8.07521                     | -64.31435  |
| 260.0            | .7027      | 2.64592    | -7.26773                     | -63.57304  |
| 270.0            | .7297      | 2.74769    | -6.46018                     | -61.91934  |
| 280.0            | .7568      | 2.84946    | -5.38351                     | -56.07352  |
| 290.0            | .7838      | 2.95122    | -4.57600                     | -51.45465  |
| 300.0            | .8108      | 3.05299    | -4.03759                     | -48.82823  |
| 310.0            | .8378      | 3.15475    | -3.49926                     | -45.28086  |
| 320.0            | .8649      | 3.25652    | -2.96092                     | -40.72754  |
| 330.0            | .8919      | 3.35829    | -2.42259                     | -35.13295  |
| 340.0            | .9189      | 3.46005    | -1.61504                     | -24.30171  |
| 350.0            | .9459      | 3.56182    | -1.07670                     | -16.61760  |
| 360.0            | .9730      | 3.66359    | -.80756                      | -12.70856  |
| 370.0            | 1.0000     | 3.76535    | -.26918                      | -6.26410   |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING.

TABLE E-5

EVAPORATION EXPERIMENT NO. GLF5 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/BOTTOM SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 58%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |            | ***** EVAPORATION RATE ***** |            |
|------------------|------------|------------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIFES | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .0000      | .00000     | .00000                       | .00000     |
| 30.0             | .0345      | .09382     | -11.15850                    | -11.87519  |
| 60.0             | .0690      | .18735     | -10.64463                    | -12.06770  |
| 90.0             | .1034      | .28147     | -10.13074                    | -12.24580  |
| 120.0            | .1379      | .37530     | -9.54346                     | -12.30357  |
| 150.0            | .1724      | .46912     | -9.02959                     | -12.42327  |
| 180.0            | .2069      | .56295     | -8.51570                     | -12.50889  |
| 210.0            | .2414      | .65677     | -8.00182                     | -12.55201  |
| 240.0            | .2759      | .75060     | -7.56136                     | -12.67116  |
| 270.0            | .3103      | .84442     | -7.12088                     | -12.75955  |
| 300.0            | .3448      | .93825     | -6.68042                     | -12.79895  |
| 330.0            | .3793      | 1.03207    | -6.16654                     | -12.62087  |
| 360.0            | .4138      | 1.12590    | -5.57925                     | -12.17053  |
| 390.0            | .4483      | 1.21972    | -5.06538                     | -11.75190  |
| 420.0            | .4828      | 1.31355    | -4.62490                     | -11.39104  |
| 450.0            | .5172      | 1.40737    | -4.25785                     | -11.11759  |
| 480.0            | .5517      | 1.50120    | -3.89079                     | -10.74985  |
| 510.0            | .5862      | 1.59502    | -3.52374                     | -10.27686  |
| 540.0            | .6207      | 1.68835    | -3.23009                     | -9.92618   |
| 570.0            | .6552      | 1.78267    | -2.86304                     | -9.23781   |
| 600.0            | .6897      | 1.87650    | -2.49599                     | -8.42027   |
| 630.0            | .7241      | 1.97032    | -2.12891                     | -7.47219   |
| 660.0            | .7586      | 2.06415    | -1.76187                     | -6.39791   |
| 690.0            | .7931      | 2.15797    | -1.39482                     | -5.20760   |
| 720.0            | .8276      | 2.25180    | -1.02775                     | -3.1852    |
| 750.0            | .8621      | 2.34562    | -.75411                      | -2.84198   |
| 780.0            | .8966      | 2.43945    | -.51437                      | -2.01099   |
| 810.0            | .9310      | 2.53327    | -.36707                      | -1.44775   |
| 840.0            | .9655      | 2.62710    | -.22015                      | -.87271    |
| 870.0            | 1.0000     | 2.72092    | -.07340                      | -.29133    |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING

TABLE E-6

EVAPORATION EXPERIMENT NO. GLF6 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/BOTTOM SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 55%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |            | ***** EVAPORATION RATE ***** |            |
|------------------|------------|------------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIFES | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .0000      | .00000     | .00000                       | .00000     |
| 30.0             | .0333      | .09026     | -11.01168                    | -11.64443  |
| 60.0             | .0667      | .18052     | -10.64463                    | -11.91832  |
| 90.0             | .1000      | .27078     | -10.35098                    | -12.29256  |
| 120.0            | .1333      | .36104     | -9.98392                     | -12.59349  |
| 150.0            | .1667      | .45130     | -9.54346                     | -12.79817  |
| 180.0            | .2000      | .54156     | -9.24930                     | -13.21317  |
| 210.0            | .2333      | .63182     | -8.88277                     | -13.53647  |
| 240.0            | .2667      | .72208     | -8.44229                     | -13.73736  |
| 270.0            | .3000      | .81234     | -8.00182                     | -13.91468  |
| 300.0            | .3333      | .90259     | -7.56136                     | -14.06112  |
| 330.0            | .3667      | .99285     | -7.12088                     | -14.16780  |
| 360.0            | .4000      | 1.08311    | -6.68042                     | -14.22445  |
| 390.0            | .4333      | 1.17337    | -6.23995                     | -14.21882  |
| 420.0            | .4667      | 1.26363    | -5.79949                     | -14.13710  |
| 450.0            | .5000      | 1.35389    | -5.35902                     | -13.96352  |
| 480.0            | .5333      | 1.44415    | -4.91854                     | -13.68104  |
| 510.0            | .5667      | 1.53441    | -4.47810                     | -13.27172  |
| 540.0            | .6000      | 1.62467    | -4.03761                     | -12.71720  |
| 570.0            | .6333      | 1.71493    | -3.59716                     | -12.00087  |
| 600.0            | .6667      | 1.80519    | -3.15668                     | -11.10866  |
| 630.0            | .7000      | 1.89545    | -2.71622                     | -10.03183  |
| 660.0            | .7333      | 1.98571    | -2.27575                     | -8.76874   |
| 690.0            | .7667      | 2.07597    | -1.83528                     | -7.32725   |
| 720.0            | .8000      | 2.16623    | -1.39481                     | -5.72606   |
| 750.0            | .8333      | 2.25649    | -1.02775                     | -4.30890   |
| 780.0            | .8667      | 2.34675    | -.80753                      | -3.44312   |
| 810.0            | .9000      | 2.43701    | -.58730                      | -2.53543   |
| 840.0            | .9333      | 2.52727    | -.36705                      | -1.59711   |
| 870.0            | .9667      | 2.61753    | -.22024                      | -.96286    |
| 900.0            | 1.0000     | 2.70778    | -.07340                      | -.32142    |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING.

TABLE E-7

EVAPORATION EXPERIMENT NO. GLF7 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/BOTTOM SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |            | ***** EVAPORATION RATE ***** |            |
|------------------|------------|------------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIFES | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .0000      | .00000     | .00000                       | .00000     |
| 15.0             | .0313      | .10123     | -24.67042                    | -26.27069  |
| 30.0             | .0625      | .20245     | -23.34407                    | -26.48384  |
| 45.0             | .0938      | .30368     | -22.54822                    | -27.30565  |
| 60.0             | .1250      | .40491     | -21.75241                    | -28.17445  |
| 75.0             | .1563      | .50614     | -20.69135                    | -28.69925  |
| 90.0             | .1875      | .60736     | -19.89550                    | -29.61314  |
| 105.0            | .2188      | .70859     | -19.09967                    | -30.57477  |
| 120.0            | .2500      | .80982     | -18.30387                    | -31.58603  |
| 135.0            | .2813      | .91104     | -17.50803                    | -32.64822  |
| 150.0            | .3125      | 1.01227    | -16.71223                    | -33.76220  |
| 165.0            | .3438      | 1.11350    | -15.91640                    | -34.92748  |
| 180.0            | .3750      | 1.21472    | -14.85532                    | -35.45266  |
| 195.0            | .4063      | 1.31595    | -14.05946                    | -36.58424  |
| 210.0            | .4375      | 1.41718    | -13.26369                    | -37.72876  |
| 225.0            | .4688      | 1.51841    | -12.20256                    | -37.96404  |
| 240.0            | .5000      | 1.61963    | -11.14147                    | -37.90721  |
| 255.0            | .5313      | 1.72086    | -10.08038                    | -37.47011  |
| 270.0            | .5625      | 1.82209    | -9.01929                     | -36.55162  |
| 285.0            | .5938      | 1.92331    | -7.95822                     | -35.04207  |
| 300.0            | .6250      | 2.02454    | -7.16240                     | -34.20115  |
| 315.0            | .6563      | 2.12577    | -6.36655                     | -32.86811  |
| 330.0            | .6875      | 2.22699    | -5.30547                     | -29.37688  |
| 345.0            | .7188      | 2.32822    | -4.24437                     | -24.94926  |
| 360.0            | .7500      | 2.42945    | -3.44855                     | -21.33934  |
| 375.0            | .7813      | 2.53068    | -2.91803                     | -18.89515  |
| 390.0            | .8125      | 2.63190    | -2.38746                     | -16.07659  |
| 405.0            | .8438      | 2.73313    | -1.85691                     | -12.90238  |
| 420.0            | .8750      | 2.83436    | -1.32637                     | -9.43058   |
| 435.0            | .9063      | 2.93558    | -1.06109                     | -7.68765   |
| 450.0            | .9375      | 3.03681    | -.79582                      | -5.84902   |
| 465.0            | .9688      | 3.13804    | -.53055                      | -3.93726   |
| 480.0            | 1.0000     | 3.23926    | -.26527                      | -1.97823   |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING.

TABLE E-8

EVAPORATION EXPERIMENT NO. GL-55 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/BOTTOM SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 50%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |            | ***** EVAPORATION RATE ***** |            |
|------------------|------------|------------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIFES | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .0000      | .00000     | .00000                       | .00000     |
| 15.0             | .0313      | .09641     | -24.37395                    | -25.83440  |
| 30.0             | .0625      | .19282     | -23.54300                    | -26.48659  |
| 45.0             | .0938      | .28923     | -22.98908                    | -27.51385  |
| 60.0             | .1250      | .38565     | -22.15812                    | -28.25737  |
| 75.0             | .1563      | .48206     | -21.32719                    | -29.02887  |
| 90.0             | .1875      | .57847     | -20.49627                    | -29.82788  |
| 105.0            | .2188      | .67488     | -19.66534                    | -30.65329  |
| 120.0            | .2500      | .77129     | -19.11136                    | -32.00077  |
| 135.0            | .2813      | .86770     | -18.28047                    | -32.94863  |
| 150.0            | .3125      | .96412     | -17.44952                    | -33.92565  |
| 165.0            | .3438      | 1.06053    | -16.61860                    | -34.92755  |
| 180.0            | .3750      | 1.15694    | -15.78766                    | -35.94760  |
| 195.0            | .4063      | 1.25335    | -14.95675                    | -36.97628  |
| 210.0            | .4375      | 1.34976    | -14.12584                    | -37.99992  |
| 225.0            | .4688      | 1.44617    | -13.29488                    | -38.99957  |
| 240.0            | .5000      | 1.54259    | -12.46394                    | -39.94978  |
| 255.0            | .5313      | 1.63900    | -11.63302                    | -40.81627  |
| 270.0            | .5625      | 1.73541    | -10.80208                    | -41.55352  |
| 285.0            | .5938      | 1.83182    | -9.97117                     | -42.10278  |
| 300.0            | .6250      | 1.92823    | -9.14025                     | -42.38855  |
| 315.0            | .6563      | 2.02464    | -8.30929                     | -42.31702  |
| 330.0            | .6875      | 2.12105    | -7.47839                     | -41.77560  |
| 345.0            | .7188      | 2.21747    | -6.64745                     | -40.63344  |
| 360.0            | .7500      | 2.31388    | -5.53952                     | -36.74697  |
| 375.0            | .7813      | 2.41029    | -4.70859                     | -33.67440  |
| 390.0            | .8125      | 2.50670    | -3.87764                     | -29.63795  |
| 405.0            | .8438      | 2.60311    | -3.04676                     | -24.61686  |
| 420.0            | .8750      | 2.69952    | -2.21583                     | -18.57884  |
| 435.0            | .9063      | 2.79594    | -1.38490                     | -11.99925  |
| 450.0            | .9375      | 2.89235    | -.83093                      | -7.32167   |
| 465.0            | .9688      | 2.98876    | -.55397                      | -4.93718   |
| 480.0            | 1.0000     | 3.08517    | -.27699                      | -2.48282   |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING.

TABLE E-9

EVAPORATION EXPERIMENT NO. GLF9 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 44%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |            | ***** EVAPORATION RATE ***** |            |
|------------------|------------|------------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIVES | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .0000      | .00000     | .00000                       | .00000     |
| 30.0             | .0385      | .12257     | -15.59807                    | -17.15682  |
| 60.0             | .0769      | .24514     | -11.74921                    | -13.97530  |
| 90.0             | .1154      | .36771     | -11.20901                    | -14.45533  |
| 120.0            | .1538      | .49028     | -10.60127                    | -14.85447  |
| 150.0            | .1923      | .61285     | -9.79101                     | -14.91062  |
| 180.0            | .2308      | .73542     | -9.18328                     | -15.22535  |
| 210.0            | .2692      | .85799     | -8.57556                     | -15.50151  |
| 240.0            | .3077      | .98056     | -7.96786                     | -15.72196  |
| 270.0            | .3462      | 1.10313    | -7.36012                     | -15.86478  |
| 300.0            | .3846      | 1.22570    | -6.75241                     | -15.90308  |
| 330.0            | .4231      | 1.34827    | -6.14470                     | -15.80396  |
| 360.0            | .4615      | 1.47085    | -5.53698                     | -15.52903  |
| 390.0            | .5000      | 1.59342    | -4.92927                     | -15.03535  |
| 420.0            | .5385      | 1.71599    | -4.32155                     | -14.27790  |
| 450.0            | .5769      | 1.83856    | -3.71382                     | -13.21447  |
| 480.0            | .6154      | 1.96113    | -3.10612                     | -11.81258  |
| 510.0            | .6538      | 2.08370    | -2.56591                     | -10.34623  |
| 540.0            | .6923      | 2.20627    | -2.09324                     | -8.87674   |
| 570.0            | .7308      | 2.32884    | -1.68810                     | -7.47014   |
| 600.0            | .7692      | 2.45141    | -1.28296                     | -5.87148   |
| 630.0            | .8077      | 2.57398    | -.94534                      | -4.43818   |
| 660.0            | .8462      | 2.69655    | -.67524                      | -3.22975   |
| 690.0            | .8846      | 2.81912    | -.47267                      | -2.29103   |
| 720.0            | .9231      | 2.94169    | -.33762                      | -1.65220   |
| 750.0            | .9615      | 3.06426    | -.20257                      | -.99704    |
| 780.0            | 1.0000     | 3.18683    | -.06753                      | -.33302    |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING.



TABLE E-10

EVAPORATION EXPERIMENT NO. GLF10 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 52%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |            | ***** EVAPORATION RATE ***** |            |
|------------------|------------|------------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIVES | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .0000      | .00000     | .00000                       | .00000     |
| 30.0             | .0313      | .10450     | -15.89597                    | -17.16138  |
| 60.0             | .0625      | .20900     | -12.88123                    | -14.86560  |
| 90.0             | .0938      | .31350     | -12.12753                    | -14.96751  |
| 120.0            | .1250      | .41800     | -11.57940                    | -15.30564  |
| 150.0            | .1563      | .52250     | -11.09978                    | -15.74312  |
| 180.0            | .1875      | .62700     | -10.55164                    | -16.08210  |
| 210.0            | .2188      | .73149     | -10.07202                    | -16.52803  |
| 240.0            | .2500      | .83599     | -9.59239                     | -16.98086  |
| 270.0            | .2813      | .94049     | -9.11277                     | -17.43660  |
| 300.0            | .3125      | 1.04499    | -8.56465                     | -17.73606  |
| 330.0            | .3438      | 1.14949    | -8.01650                     | -17.98594  |
| 360.0            | .3750      | 1.25399    | -7.53688                     | -18.34916  |
| 390.0            | .4063      | 1.35849    | -6.98875                     | -18.47266  |
| 420.0            | .4375      | 1.46299    | -6.44061                     | -18.48339  |
| 450.0            | .4688      | 1.56749    | -5.82397                     | -18.11846  |
| 480.0            | .5000      | 1.67199    | -5.13878                     | -17.26731  |
| 510.0            | .5313      | 1.77649    | -4.52214                     | -16.34756  |
| 540.0            | .5625      | 1.88099    | -3.97398                     | -15.39165  |
| 570.0            | .5938      | 1.98549    | -3.42585                     | -14.13893  |
| 600.0            | .6250      | 2.08998    | -2.94624                     | -12.88631  |
| 630.0            | .6563      | 2.19448    | -2.46663                     | -11.35694  |
| 660.0            | .6875      | 2.29898    | -2.05552                     | -9.89866   |
| 690.0            | .7188      | 2.40348    | -1.78145                     | -8.93437   |
| 720.0            | .7500      | 2.50798    | -1.50738                     | -7.83460   |
| 750.0            | .7813      | 2.61248    | -1.23331                     | -6.60657   |
| 780.0            | .8125      | 2.71698    | -.95923                      | -5.26385   |
| 810.0            | .8438      | 2.82148    | -.75369                      | -4.21684   |
| 840.0            | .8750      | 2.92598    | -.61665                      | -3.50620   |
| 870.0            | .9063      | 3.03048    | -.47962                      | -2.76203   |
| 900.0            | .9375      | 3.13498    | -.27407                      | -1.58993   |
| 930.0            | .9688      | 3.23948    | -.13793                      | -.79788    |
| 960.0            | 1.0000     | 3.34398    | -.06811                      | -.39965    |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING.

TABLE E-11

EVAPORATION EXPERIMENT NO. GLF11 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 55%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |            | ***** EVAPORATION RATE ***** |            |
|------------------|------------|------------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIFES | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .0000      | .00000     | .00000                       | .00000     |
| 10.0             | .0278      | .10015     | -34.68059                    | -36.93630  |
| 20.0             | .0556      | .20029     | -33.04211                    | -37.51610  |
| 30.0             | .0833      | .30044     | -31.67679                    | -38.39779  |
| 40.0             | .1111      | .40059     | -30.31138                    | -39.28443  |
| 50.0             | .1389      | .50073     | -28.94597                    | -40.16839  |
| 60.0             | .1667      | .60088     | -27.58063                    | -41.03967  |
| 70.0             | .1944      | .70102     | -26.21529                    | -41.88517  |
| 80.0             | .2222      | .80117     | -25.12292                    | -43.19287  |
| 90.0             | .2500      | .90132     | -24.03068                    | -44.55667  |
| 100.0            | .2778      | 1.00146    | -22.66522                    | -45.38341  |
| 110.0            | .3056      | 1.10161    | -21.29991                    | -46.11280  |
| 120.0            | .3333      | 1.20176    | -19.93452                    | -46.70634  |
| 130.0            | .361       | 1.30190    | -18.56915                    | -47.11711  |
| 140.0            | .388       | 1.40205    | -17.47685                    | -48.10176  |
| 150.0            | .4167      | 1.50220    | -16.11145                    | -48.09969  |
| 160.0            | .44        | 1.60234    | -14.74608                    | -47.72309  |
| 170.0            | .4722      | 1.70249    | -13.65376                    | -47.91645  |
| 180.0            | .5000      | 1.80264    | -12.56148                    | -47.79329  |
| 190.0            | .5278      | 1.90278    | -11.19612                    | -46.05299  |
| 200.0            | .5556      | 2.00293    | -9.83070                     | -43.53673  |
| 210.0            | .5833      | 2.10307    | -8.73841                     | -41.52947  |
| 220.0            | .6111      | 2.20322    | -7.64612                     | -38.82258  |
| 230.0            | .6389      | 2.30337    | -6.82691                     | -36.91644  |
| 240.0            | .6667      | 2.40351    | -6.00764                     | -34.45740  |
| 250.0            | .6944      | 2.50366    | -5.18843                     | -31.40448  |
| 260.0            | .7222      | 2.60381    | -4.64230                     | -29.56156  |
| 270.0            | .7500      | 2.70395    | -4.09612                     | -27.33929  |
| 280.0            | .7778      | 2.80410    | -3.54994                     | -24.72547  |
| 290.0            | .8056      | 2.90425    | -3.00387                     | -21.72238  |
| 300.0            | .8333      | 3.00439    | -2.45766                     | -18.34667  |
| 310.0            | .8611      | 3.10454    | -1.91155                     | -14.63769  |
| 320.0            | .8889      | 3.20469    | -1.63843                     | -12.82975  |
| 330.0            | .9167      | 3.30483    | -1.36534                     | -10.89648  |
| 340.0            | .9444      | 3.40498    | -.81926                      | -6.61449   |
| 350.0            | .9722      | 3.50512    | -.54617                      | -4.44417   |
| 360.0            | 1.0000     | 3.60527    | -.27306                      | -2.23057   |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING.

TABLE E-12

EVAPORATION EXPERIMENT NO. GUF12 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 40%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |            | ***** EVAPORATION RATE ***** |            |
|------------------|------------|------------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIFES | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .0000      | .00000     | .00000                       | .00000     |
| 10.0             | .0256      | .07332     | -28.53246                    | -29.84934  |
| 20.0             | .0513      | .14664     | -27.72496                    | -30.36642  |
| 30.0             | .0769      | .21996     | -26.91746                    | -30.89013  |
| 40.0             | .1026      | .29329     | -25.84080                    | -31.07965  |
| 50.0             | .1282      | .36661     | -25.03316                    | -31.57837  |
| 60.0             | .1538      | .43993     | -24.49490                    | -32.44973  |
| 70.0             | .1795      | .51325     | -23.68740                    | -32.98020  |
| 80.0             | .2051      | .58657     | -22.87980                    | -33.50616  |
| 90.0             | .2308      | .65989     | -22.34145                    | -34.46112  |
| 100.0            | .2564      | .73321     | -21.80315                    | -35.47555  |
| 110.0            | .2821      | .80654     | -21.26482                    | -36.55530  |
| 120.0            | .3077      | .87986     | -20.72638                    | -37.70702  |
| 130.0            | .3333      | .95318     | -19.91894                    | -38.38909  |
| 140.0            | .3590      | 1.02650    | -19.11139                    | -39.05708  |
| 150.0            | .3846      | 1.09982    | -18.57299                    | -40.32334  |
| 160.0            | .4103      | 1.17314    | -18.03469                    | -41.67789  |
| 170.0            | .4359      | 1.24647    | -17.49636                    | -43.13031  |
| 180.0            | .4615      | 1.31979    | -16.68881                    | -43.93431  |
| 190.0            | .4872      | 1.39311    | -15.88129                    | -44.69795  |
| 200.0            | .5128      | 1.46643    | -15.34298                    | -46.27251  |
| 210.0            | .5385      | 1.53975    | -14.80458                    | -47.95976  |
| 220.0            | .5641      | 1.61307    | -13.99705                    | -48.76253  |
| 230.0            | .5897      | 1.68639    | -13.18958                    | -49.46379  |
| 240.0            | .6154      | 1.75972    | -12.38198                    | -50.02701  |
| 250.0            | .6410      | 1.83304    | -11.57451                    | -50.40962  |
| 260.0            | .6667      | 1.90636    | -10.76699                    | -50.55847  |
| 270.0            | .6923      | 1.97968    | -9.95947                     | -50.41199  |
| 280.0            | .7179      | 2.05300    | -9.42110                     | -51.48296  |
| 290.0            | .7436      | 2.12632    | -8.61358                     | -50.76488  |
| 300.0            | .7692      | 2.19964    | -7.80610                     | -49.52919  |
| 310.0            | .7949      | 2.27297    | -6.99855                     | -47.67896  |
| 320.0            | .8205      | 2.34629    | -5.92181                     | -43.02753  |
| 330.0            | .8462      | 2.41961    | -5.11432                     | -39.42571  |
| 340.0            | .8718      | 2.49293    | -4.57596                     | -37.31059  |
| 350.0            | .8974      | 2.56625    | -3.76844                     | -32.25900  |
| 360.0            | .9231      | 2.63957    | -2.96092                     | -26.38024  |
| 370.0            | .9487      | 2.71290    | -2.15340                     | -19.77226  |
| 380.0            | .9744      | 2.78622    | -1.34585                     | -12.59811  |
| 390.0            | 1.0000     | 2.85954    | -.53837                      | -5.07915   |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING.

TABLE E-13

EVAPORATION EXPERIMENT NO. GLF13 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 44%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |            | ***** EVAPORATION RATE ***** |            |
|------------------|------------|------------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIVES | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .0000      | .00000     | .00000                       | .00000     |
| 40.0             | .0313      | .10895     | -8.98071                     | -9.61886   |
| 80.0             | .0625      | .21790     | -8.30548                     | -9.52134   |
| 120.0            | .0938      | .32685     | -7.96784                     | -9.79524   |
| 160.0            | .1250      | .43580     | -7.63023                     | -10.07860  |
| 200.0            | .1563      | .54475     | -7.29260                     | -10.37059  |
| 240.0            | .1875      | .65369     | -7.02251                     | -10.78192  |
| 280.0            | .2188      | .76264     | -6.75242                     | -11.22709  |
| 320.0            | .2500      | .87159     | -6.48230                     | -11.71035  |
| 360.0            | .2813      | .98054     | -6.21222                     | -12.23694  |
| 400.0            | .3125      | 1.08949    | -5.89708                     | -12.49473  |
| 440.0            | .3438      | 1.19844    | -5.40193                     | -12.71470  |
| 480.0            | .3750      | 1.30739    | -5.06431                     | -13.07104  |
| 520.0            | .4063      | 1.41634    | -4.65916                     | -13.19777  |
| 560.0            | .4375      | 1.52529    | -4.18650                     | -12.99754  |
| 600.0            | .4688      | 1.63424    | -3.64631                     | -12.35354  |
| 640.0            | .5000      | 1.74319    | -3.10610                     | -11.41040  |
| 680.0            | .5313      | 1.85214    | -2.63345                     | -10.41867  |
| 720.0            | .5625      | 1.96108    | -2.22829                     | -9.42986   |
| 760.0            | .5938      | 2.07003    | -1.82316                     | -8.18171   |
| 800.0            | .6250      | 2.17898    | -1.48553                     | -7.01187   |
| 840.0            | .6563      | 2.28793    | -1.21544                     | -5.99091   |
| 880.0            | .6875      | 2.39688    | -1.01286                     | -5.18359   |
| 920.0            | .7188      | 2.50583    | -.87781                      | -4.64664   |
| 960.0            | .7500      | 2.61478    | -.74277                      | -4.04941   |
| 1000.0           | .7813      | 2.72373    | -.60772                      | -3.39628   |
| 1040.0           | .8125      | 2.83268    | -.47267                      | -2.69411   |
| 1080.0           | .8438      | 2.94163    | -.33761                      | -1.95206   |
| 1120.0           | .8750      | 3.05058    | -.27011                      | -1.57999   |
| 1160.0           | .9063      | 3.15953    | -.27010                      | -1.59861   |
| 1200.0           | .9375      | 3.26847    | -.20258                      | -1.20967   |
| 1240.0           | .9688      | 3.37742    | -.13505                      | -.81128    |
| 1280.0           | 1.0000     | 3.48637    | -.06753                      | -.40686    |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING.

TABLE E-14

EVAPORATION EXPERIMENT NO. GLF14 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 43%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |            | ***** EVAPORATION RATE ***** |            |
|------------------|------------|------------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIFES | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .0000      | .00000     | .00000                       | .00000     |
| 40.0             | .0345      | .09901     | -9.52289                     | -10.11887  |
| 80.0             | .0690      | .19801     | -9.10582                     | -10.29158  |
| 120.0            | .1034      | .29702     | -8.75827                     | -10.54432  |
| 160.0            | .1379      | .39603     | -8.48025                     | -10.89774  |
| 200.0            | .1724      | .49503     | -8.20218                     | -11.27547  |
| 240.0            | .2069      | .59404     | -7.85465                     | -11.57041  |
| 280.0            | .2414      | .69305     | -7.50704                     | -11.87031  |
| 320.0            | .2759      | .79205     | -7.22907                     | -12.30029  |
| 360.0            | .3103      | .89106     | -6.95101                     | -12.76062  |
| 400.0            | .3448      | .99007     | -6.60346                     | -13.10515  |
| 440.0            | .3793      | 1.08907    | -6.25591                     | -13.44808  |
| 480.0            | .4138      | 1.18808    | -5.90836                     | -13.78372  |
| 520.0            | .4483      | 1.28709    | -5.49130                     | -13.91314  |
| 560.0            | .4828      | 1.38609    | -5.07424                     | -13.96702  |
| 600.0            | .5172      | 1.48510    | -4.65718                     | -13.92292  |
| 640.0            | .5517      | 1.58411    | -4.24013                     | -13.75447  |
| 680.0            | .5862      | 1.68311    | -3.75355                     | -13.16769  |
| 720.0            | .6207      | 1.78212    | -3.26697                     | -12.33510  |
| 760.0            | .6552      | 1.88113    | -2.91943                     | -11.82934  |
| 800.0            | .6897      | 1.98013    | -2.57189                     | -11.13909  |
| 840.0            | .7241      | 2.07914    | -2.22432                     | -10.24410  |
| 880.0            | .7586      | 2.17815    | -1.94629                     | -9.48977   |
| 920.0            | .7931      | 2.27715    | -1.52922                     | -7.81666   |
| 960.0            | .8276      | 2.37616    | -1.04265                     | -5.51123   |
| 1000.0           | .8621      | 2.47516    | -.76461                      | -4.14519   |
| 1040.0           | .8966      | 2.57417    | -.69510                      | -3.85825   |
| 1080.0           | .9310      | 2.67318    | -.55608                      | -3.14670   |
| 1120.0           | .9655      | 2.77218    | -.34755                      | -1.99087   |
| 1160.0           | 1.0000     | 2.87119    | -.17903                      | -.80033    |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING.

TABLE E-15

EVAPORATION EXPERIMENT NO. GLF15 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 11.3 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |            | ***** EVAPORATION RATE ***** |            |
|------------------|------------|------------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIVES | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .0000      | .00000     | .00000                       | .00000     |
| 15.0             | .0323      | .10017     | -22.55406                    | -23.98281  |
| 30.0             | .0645      | .20034     | -21.48005                    | -24.30728  |
| 45.0             | .0968      | .30051     | -20.67455                    | -24.93679  |
| 60.0             | .1290      | .40068     | -19.86905                    | -25.58479  |
| 75.0             | .1613      | .50085     | -19.06355                    | -26.24959  |
| 90.0             | .1935      | .60102     | -18.52652                    | -27.35325  |
| 105.0            | .2258      | .70119     | -17.98955                    | -28.56444  |
| 120.0            | .2581      | .80136     | -17.18403                    | -29.40466  |
| 135.0            | .2903      | .90153     | -16.37855                    | -30.26697  |
| 150.0            | .3226      | 1.00169    | -15.84155                    | -31.72801  |
| 165.0            | .3548      | 1.10186    | -15.03603                    | -32.71719  |
| 180.0            | .3871      | 1.20203    | -14.23053                    | -33.72264  |
| 195.0            | .4194      | 1.30220    | -13.69353                    | -35.49227  |
| 210.0            | .4516      | 1.40237    | -13.15653                    | -37.47598  |
| 225.0            | .4839      | 1.50254    | -12.35102                    | -38.78583  |
| 240.0            | .5161      | 1.60271    | -11.27704                    | -39.06760  |
| 255.0            | .5484      | 1.70288    | -10.20301                    | -38.98681  |
| 270.0            | .5806      | 1.80305    | -9.12903                     | -38.42331  |
| 285.0            | .6129      | 1.90322    | -8.05504                     | -37.23769  |
| 300.0            | .6452      | 2.00339    | -6.98102                     | -35.28001  |
| 315.0            | .6774      | 2.10356    | -5.90701                     | -32.40769  |
| 330.0            | .7097      | 2.20373    | -4.83302                     | -28.51239  |
| 345.0            | .7419      | 2.30390    | -3.75899                     | -23.55598  |
| 360.0            | .7742      | 2.40407    | -2.95354                     | -19.45993  |
| 375.0            | .8065      | 2.50424    | -2.41650                     | -16.62053  |
| 390.0            | .8387      | 2.60441    | -1.87951                     | -13.36414  |
| 405.0            | .8710      | 2.70458    | -1.34251                     | -9.80783   |
| 420.0            | .9032      | 2.80474    | -.80550                      | -5.97756   |
| 435.0            | .9355      | 2.90491    | -.53702                      | -4.02755   |
| 450.0            | .9677      | 3.00508    | -.53701                      | -4.07083   |
| 465.0            | 1.0000     | 3.10525    | -.26848                      | -2.04625   |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING.

TABLE E-16

EVAPORATION EXPERIMENT NO. GLF16 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 11.3 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |            | ***** EVAPORATION RATE ***** |            |
|------------------|------------|------------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIVES | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .0000      | .00000     | .00000                       | .00000     |
| 15.0             | .0345      | .09229     | -22.89067                    | -24.23070  |
| 30.0             | .0690      | .18458     | -21.80065                    | -24.43944  |
| 45.0             | .1034      | .27687     | -20.98313                    | -24.94035  |
| 60.0             | .1379      | .36916     | -20.16562                    | -25.44194  |
| 75.0             | .1724      | .46145     | -19.34807                    | -25.94031  |
| 90.0             | .2069      | .55374     | -18.80306                    | -26.84459  |
| 105.0            | .2414      | .64603     | -18.25805                    | -27.81838  |
| 120.0            | .2759      | .73832     | -17.71301                    | -28.87034  |
| 135.0            | .3103      | .83061     | -17.16800                    | -30.01088  |
| 150.0            | .3448      | .92290     | -16.62302                    | -31.25224  |
| 165.0            | .3793      | 1.01519    | -15.80546                    | -32.01345  |
| 180.0            | .4138      | 1.10749    | -15.26044                    | -33.40401  |
| 195.0            | .4483      | 1.19978    | -14.71546                    | -34.92931  |
| 210.0            | .4828      | 1.29207    | -13.89791                    | -35.84563  |
| 225.0            | .5172      | 1.38436    | -13.35291                    | -37.56566  |
| 240.0            | .5517      | 1.47665    | -12.53535                    | -38.55011  |
| 255.0            | .5862      | 1.56894    | -11.71786                    | -39.47263  |
| 270.0            | .6207      | 1.66123    | -11.17281                    | -41.40115  |
| 285.0            | .6552      | 1.75352    | -10.35532                    | -42.29266  |
| 300.0            | .6897      | 1.84581    | -9.26527                     | -41.64830  |
| 315.0            | .7241      | 1.93810    | -8.17525                     | -40.32910  |
| 330.0            | .7586      | 2.03039    | -7.08521                     | -38.17547  |
| 345.0            | .7931      | 2.12268    | -5.72269                     | -33.31601  |
| 360.0            | .8276      | 2.21497    | -4.36011                     | -27.04178  |
| 375.0            | .8621      | 2.30726    | -3.27011                     | -21.32649  |
| 390.0            | .8966      | 2.39955    | -2.18009                     | -14.72352  |
| 405.0            | .9310      | 2.49184    | -1.36254                     | -9.41129   |
| 420.0            | .9655      | 2.58413    | -.81753                      | -5.72491   |
| 435.0            | 1.0000     | 2.67642    | -.27249                      | -1.91703   |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING.

TABLE E-17

EVAPORATION EXPERIMENT NO. BLF1 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 39%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |            | ***** EVAPORATION RATE ***** |            |
|------------------|------------|------------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIVES | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .0000      | .00000     | .00000                       | .00000     |
| 45.0             | .0370      | .13264     | -11.08510                    | -12.03189  |
| 90.0             | .0741      | .26528     | -10.42439                    | -12.30293  |
| 135.0            | .1111      | .39792     | -9.91051                     | -12.75555  |
| 180.0            | .1481      | .53056     | -9.47005                     | -13.34315  |
| 225.0            | .1852      | .66320     | -9.02959                     | -13.98565  |
| 270.0            | .2222      | .79584     | -8.51569                     | -14.55223  |
| 315.0            | .2593      | .92849     | -8.00183                     | -15.14413  |
| 360.0            | .2963      | 1.06113    | -7.41452                     | -15.58509  |
| 405.0            | .3333      | 1.19377    | -6.75384                     | -15.78736  |
| 450.0            | .3704      | 1.32641    | -6.09313                     | -15.84497  |
| 495.0            | .4074      | 1.45995    | -5.43243                     | -15.70143  |
| 540.0            | .4444      | 1.59169    | -4.77173                     | -15.28863  |
| 585.0            | .4815      | 1.72433    | -4.03762                     | -14.24467  |
| 630.0            | .5185      | 1.85697    | -3.37691                     | -13.01437  |
| 675.0            | .5556      | 1.98961    | -2.71621                     | -11.30840  |
| 720.0            | .5926      | 2.12225    | -2.12893                     | -9.45849   |
| 765.0            | .6296      | 2.25489    | -1.61504                     | -7.56045   |
| 810.0            | .6667      | 2.38753    | -1.17458                     | -5.72191   |
| 855.0            | .7037      | 2.52017    | -.80753                      | -4.04685   |
| 900.0            | .7407      | 2.65281    | -.51388                      | -2.62320   |
| 945.0            | .7778      | 2.78546    | -.36705                      | -1.89895   |
| 990.0            | .8148      | 2.91810    | -.29364                      | -1.53573   |
| 1035.0           | .8519      | 3.05074    | -.22024                      | -1.16133   |
| 1080.0           | .8889      | 3.18338    | -.14682                      | -.77847    |
| 1125.0           | .9259      | 3.31602    | -.14681                      | -.78275    |
| 1170.0           | .9630      | 3.44866    | -.14682                      | -.78717    |
| 1215.0           | 1.0000     | 3.58130    | -.07340                      | -.39484    |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING.



TABLE E-18

EVAPORATION EXPERIMENT NO. BLF2 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 2.9 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 39%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |            | ***** EVAPORATION RATE ***** |            |
|------------------|------------|------------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIVES | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .0000      | .00000     | .00000                       | .00000     |
| 40.0             | .0313      | .12697     | -11.92095                    | -12.86984  |
| 80.0             | .0625      | .25395     | -11.30078                    | -13.19605  |
| 120.0            | .0938      | .38092     | -10.81844                    | -13.70350  |
| 160.0            | .1250      | .50790     | -10.40499                    | -14.34949  |
| 200.0            | .1563      | .63487     | -9.99154                     | -15.06303  |
| 240.0            | .1875      | .76184     | -9.57810                     | -15.85578  |
| 280.0            | .2188      | .88882     | -9.16467                     | -16.74236  |
| 320.0            | .2500      | 1.01579    | -8.75122                     | -17.74128  |
| 360.0            | .2813      | 1.14276    | -8.33778                     | -18.87652  |
| 400.0            | .3125      | 1.26974    | -7.92433                     | -20.17962  |
| 440.0            | .3438      | 1.39671    | -7.44198                     | -21.46754  |
| 480.0            | .3750      | 1.52369    | -6.95962                     | -22.92232  |
| 520.0            | .4063      | 1.65066    | -6.47728                     | -24.57644  |
| 560.0            | .4375      | 1.77763    | -5.85712                     | -25.76472  |
| 600.0            | .4688      | 1.90461    | -5.23695                     | -26.86428  |
| 640.0            | .5000      | 2.03158    | -4.68569                     | -28.23376  |
| 680.0            | .5313      | 2.15856    | -4.13444                     | -29.44975  |
| 720.0            | .5625      | 2.28553    | -3.58317                     | -30.30728  |
| 760.0            | .5938      | 2.41250    | -3.03193                     | -30.47896  |
| 800.0            | .6250      | 2.53948    | -2.54957                     | -30.45814  |
| 840.0            | .6563      | 2.66645    | -2.13613                     | -30.30152  |
| 880.0            | .6875      | 2.79342    | -1.79159                     | -30.15383  |
| 920.0            | .7188      | 2.92040    | -1.44704                     | -28.67402  |
| 960.0            | .7500      | 3.04737    | -1.17143                     | -27.10377  |
| 1000.0           | .7813      | 3.17435    | -.96470                      | -25.89553  |
| 1040.0           | .8125      | 3.30132    | -.68908                      | -20.88639  |
| 1080.0           | .8438      | 3.42829    | -.48235                      | -16.07384  |
| 1120.0           | .8750      | 3.55527    | -.34453                      | -12.35866  |
| 1160.0           | .9063      | 3.68224    | -.27563                      | -10.53128  |
| 1200.0           | .9375      | 3.80921    | -.20573                      | -8.30423   |
| 1240.0           | .9688      | 3.93619    | -.13782                      | -5.73256   |
| 1280.0           | 1.0000     | 4.06316    | -.05891                      | -2.91781   |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING.

TABLE E-19

EVAPORATION EXPERIMENT NO. BLE3 SERIES 10 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |            | ***** EVAPORATION RATE ***** |            |
|------------------|------------|------------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIFES | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .9000      | .00000     | .00000                       | .00000     |
| 15.0             | .6333      | .10560     | -27.18661                    | -29.05578  |
| 30.0             | .0667      | .21120     | -25.84076                    | -29.54838  |
| 45.0             | .1000      | .31680     | -24.49487                    | -29.99754  |
| 60.0             | .1333      | .42239     | -23.14902                    | -30.38781  |
| 75.0             | .1667      | .52799     | -22.34147                    | -31.51477  |
| 90.0             | .2000      | .63359     | -21.53395                    | -32.72807  |
| 105.0            | .2333      | .73919     | -20.45729                    | -33.56083  |
| 120.0            | .2667      | .84479     | -19.38054                    | -34.38100  |
| 135.0            | .3000      | .95039     | -18.57304                    | -35.73452  |
| 150.0            | .3333      | 1.05598    | -17.76550                    | -37.18866  |
| 165.0            | .3667      | 1.16158    | -16.95799                    | -38.75349  |
| 180.0            | .4000      | 1.26718    | -16.15047                    | -40.43987  |
| 195.0            | .4333      | 1.37278    | -15.07377                    | -41.44542  |
| 210.0            | .4667      | 1.47838    | -13.99706                    | -42.34081  |
| 225.0            | .5000      | 1.58398    | -12.92039                    | -43.06683  |
| 240.0            | .5333      | 1.68958    | -11.57450                    | -42.45657  |
| 255.0            | .5667      | 1.79517    | -10.22863                    | -41.17537  |
| 270.0            | .6000      | 1.90077    | -9.15193                     | -40.35946  |
| 285.0            | .6333      | 2.00637    | -8.07526                     | -38.88835  |
| 300.0            | .6667      | 2.11197    | -6.99851                     | -36.62376  |
| 315.0            | .7000      | 2.21757    | -5.92184                     | -33.44169  |
| 330.0            | .7333      | 2.32317    | -4.84516                     | -29.25563  |
| 345.0            | .7667      | 2.42877    | -3.76842                     | -24.04899  |
| 360.0            | .8000      | 2.53436    | -2.69174                     | -17.90578  |
| 375.0            | .8333      | 2.63996    | -1.88422                     | -12.91715  |
| 390.0            | .8667      | 2.74556    | -1.34587                     | -9.43248   |
| 405.0            | .9000      | 2.85116    | -1.07670                     | -7.68317   |
| 420.0            | .9333      | 2.95676    | -.80752                      | -5.84203   |
| 435.0            | .9667      | 3.06236    | -.53835                      | -3.93090   |
| 450.0            | 1.0000     | 3.16795    | -.26918                      | -1.97465   |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING.

TABLE E-20

EVAPORATION EXPERIMENT NO. BUF4 SERIES 10 2\*\*6 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON G/LK/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 20%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |            | ***** EVAPORATION RATE ***** |            |
|------------------|------------|------------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIFES | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .0000      | .00000     | .00000                       | .00000     |
| 20.0             | .0357      | .14506     | -27.18661                    | -29.57765  |
| 40.0             | .0714      | .29013     | -26.37911                    | -31.37671  |
| 60.0             | .1071      | .43519     | -25.30240                    | -33.05405  |
| 80.0             | .1429      | .58025     | -24.49488                    | -35.36398  |
| 100.0            | .1786      | .72532     | -23.68735                    | -38.06933  |
| 120.0            | .2143      | .87038     | -22.74146                    | -40.19811  |
| 140.0            | .2500      | 1.01544    | -20.99561                    | -42.55692  |
| 160.0            | .2857      | 1.16051    | -19.91891                    | -45.88292  |
| 180.0            | .3214      | 1.30557    | -18.84220                    | -49.83426  |
| 200.0            | .3571      | 1.45063    | -17.49633                    | -53.65784  |
| 220.0            | .3929      | 1.59570    | -16.15047                    | -58.08504  |
| 240.0            | .4286      | 1.74076    | -14.80459                    | -63.26011  |
| 260.0            | .4643      | 1.88582    | -13.45874                    | -69.37216  |
| 280.0            | .5000      | 2.03089    | -12.11283                    | -76.66820  |
| 300.0            | .5357      | 2.17595    | -10.49782                    | -82.80666  |
| 320.0            | .5714      | 2.32101    | -8.88275                     | -88.50693  |
| 340.0            | .6071      | 2.46608    | -7.26772                     | -92.28659  |
| 360.0            | .6429      | 2.61114    | -5.65266                     | -91.25497  |
| 380.0            | .6786      | 2.75620    | -4.03760                     | -80.85277  |
| 400.0            | .7143      | 2.90127    | -2.69176                     | -64.19083  |
| 420.0            | .7500      | 3.04633    | -1.88422                     | -51.86247  |
| 440.0            | .7857      | 3.19140    | -1.34586                     | -41.62996  |
| 460.0            | .8214      | 3.33646    | -1.07671                     | -36.96545  |
| 480.0            | .8571      | 3.48152    | -.80750                      | -30.21372  |
| 500.0            | .8929      | 3.62659    | -.53836                      | -21.42661  |
| 520.0            | .9286      | 3.77165    | -.53838                      | -22.88552  |
| 540.0            | .9643      | 3.91671    | -.53836                      | -24.55564  |
| 560.0            | 1.0000     | 4.06178    | -.26917                      | -12.74254  |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING.

TABLE E-21

EVAPORATION EXPERIMENT NO. BLE5 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |            | ***** EVAPORATION RATE ***** |            |
|------------------|------------|------------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIFES | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .0000      | .00000     | .00000                       | .00000     |
| 30.0             | .0263      | .08808     | -11.08510                    | -11.72705  |
| 60.0             | .0526      | .17617     | -10.20416                    | -11.40298  |
| 90.0             | .0789      | .26425     | -9.69027                     | -11.44050  |
| 120.0            | .1053      | .35234     | -9.39664                     | -11.73683  |
| 150.0            | .1316      | .44042     | -9.10298                     | -12.04642  |
| 180.0            | .1579      | .52851     | -8.88277                     | -12.47943  |
| 210.0            | .1842      | .61659     | -8.66253                     | -12.94818  |
| 240.0            | .2105      | .70467     | -8.36887                     | -13.33287  |
| 270.0            | .2368      | .79276     | -8.07524                     | -13.73785  |
| 300.0            | .2632      | .88084     | -7.78159                     | -14.16426  |
| 330.0            | .2895      | .96893     | -7.48795                     | -14.61336  |
| 360.0            | .3158      | 1.05701    | -7.12088                     | -14.92097  |
| 390.0            | .3421      | 1.14510    | -6.68042                     | -15.03754  |
| 420.0            | .3684      | 1.23318    | -6.23995                     | -15.09294  |
| 450.0            | .3947      | 1.32127    | -5.79948                     | -15.07157  |
| 480.0            | .4211      | 1.40935    | -5.35902                     | -14.95547  |
| 510.0            | .4474      | 1.49743    | -4.91855                     | -14.72432  |
| 540.0            | .4737      | 1.58552    | -4.55150                     | -14.60847  |
| 570.0            | .5000      | 1.67360    | -4.18443                     | -14.38433  |
| 600.0            | .5263      | 1.76169    | -3.74397                     | -13.74373  |
| 630.0            | .5526      | 1.84977    | -3.30349                     | -12.89925  |
| 660.0            | .5789      | 1.93786    | -2.86304                     | -11.77262  |
| 690.0            | .6053      | 2.02594    | -2.42257                     | -10.53301  |
| 720.0            | .6316      | 2.11402    | -1.98210                     | -9.00095   |
| 750.0            | .6579      | 2.20211    | -1.61506                     | -7.60978   |
| 780.0            | .6842      | 2.29019    | -1.39481                     | -6.79250   |
| 810.0            | .7105      | 2.37828    | -1.24800                     | -6.26556   |
| 840.0            | .7368      | 2.46636    | -1.10115                     | -5.68350   |
| 870.0            | .7632      | 2.55445    | -.95435                      | -5.04857   |
| 900.0            | .7895      | 2.64253    | -.80753                      | -4.36395   |
| 930.0            | .8158      | 2.73062    | -.65729                      | -3.22429   |
| 960.0            | .8421      | 2.81870    | -.44047                      | -2.44746   |
| 990.0            | .8684      | 2.90678    | -.44047                      | -2.47738   |
| 1020.0           | .8947      | 2.99487    | -.36706                      | -2.08579   |
| 1050.0           | .9211      | 3.08295    | -.29365                      | -1.68250   |
| 1080.0           | .9474      | 3.17104    | -.22023                      | -1.26973   |
| 1110.0           | .9737      | 3.25912    | -.14682                      | -.85005    |
| 1140.0           | 1.0000     | 3.34721    | -.07341                      | -.42591    |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING.

TABLE E-22

EVAPORATION EXPERIMENT NO. BLF6 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 2.9 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |            | ***** EVAPORATION RATE ***** |            |
|------------------|------------|------------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIFES | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .0000      | .00000     | .00000                       | .00000     |
| 40.0             | .0323      | .12671     | -11.42523                    | -12.31308  |
| 80.0             | .0645      | .25382     | -11.07041                    | -12.90216  |
| 120.0            | .0968      | .38074     | -10.64462                    | -13.45975  |
| 160.0            | .1290      | .50765     | -10.21884                    | -14.06863  |
| 200.0            | .1613      | .63456     | -9.86402                     | -14.85313  |
| 240.0            | .1935      | .76147     | -9.43824                     | -15.61232  |
| 280.0            | .2258      | .88838     | -9.01245                     | -16.45630  |
| 320.0            | .2581      | 1.01530    | -8.58666                     | -17.40063  |
| 360.0            | .2903      | 1.14221    | -8.16088                     | -18.46501  |
| 400.0            | .3226      | 1.26912    | -7.73509                     | -19.67479  |
| 440.0            | .3548      | 1.39603    | -7.23834                     | -20.83183  |
| 480.0            | .3871      | 1.52294    | -6.59967                     | -21.58064  |
| 520.0            | .4194      | 1.64986    | -5.89003                     | -21.92523  |
| 560.0            | .4516      | 1.77677    | -5.25134                     | -22.29869  |
| 600.0            | .4839      | 1.90368    | -4.61267                     | -22.34940  |
| 640.0            | .5161      | 2.03059    | -3.90302                     | -21.47388  |
| 680.0            | .5484      | 2.15751    | -3.19339                     | -19.76075  |
| 720.0            | .5806      | 2.28442    | -2.62568                     | -18.10416  |
| 760.0            | .6129      | 2.41133    | -2.19988                     | -16.77397  |
| 800.0            | .6452      | 2.53824    | -1.84507                     | -15.43943  |
| 840.0            | .6774      | 2.66515    | -1.53121                     | -14.23799  |
| 880.0            | .7097      | 2.79207    | -1.27736                     | -12.57373  |
| 920.0            | .7419      | 2.91898    | -1.06446                     | -11.22003  |
| 960.0            | .7742      | 3.04589    | -.92252                      | -10.35966  |
| 1000.0           | .8065      | 3.17280    | -.78061                      | -9.27940   |
| 1040.0           | .8387      | 3.29971    | -.63868                      | -7.97431   |
| 1080.0           | .8710      | 3.42663    | -.49675                      | -6.45488   |
| 1120.0           | .9032      | 3.55354    | -.35482                      | -6.74876   |
| 1160.0           | .9355      | 3.68045    | -.28386                      | -3.89245   |
| 1200.0           | .9677      | 3.80736    | -.21290                      | -2.97412   |
| 1240.0           | 1.0000     | 3.93427    | -.07097                      | -.99762    |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING.

TABLE E-23

EVAPORATION EXPERIMENT NO. BLF7 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |           | ***** EVAPORATION RATE ***** |            |
|------------------|------------|-----------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIFE | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .0000      | .00000    | .00000                       | .00000     |
| 15.0             | .0294      | .10311    | -23.41817                    | -24.92490  |
| 30.0             | .0588      | .20622    | -22.61065                    | -25.65944  |
| 45.0             | .0882      | .30934    | -21.80316                    | -26.43126  |
| 60.0             | .1176      | .41245    | -21.26476                    | -27.61628  |
| 75.0             | .1471      | .51556    | -20.45728                    | -28.52379  |
| 90.0             | .1765      | .61867    | -19.38054                    | -29.04878  |
| 105.0            | .2059      | .72178    | 18.57304                     | -29.99384  |
| 120.0            | .2353      | .82489    | -17.76554                    | -30.98447  |
| 135.0            | .2647      | .92801    | -16.95797                    | -32.02069  |
| 150.0            | .2941      | 1.03112   | -16.41964                    | -33.70141  |
| 165.0            | .3235      | 1.13423   | -15.61212                    | -34.93359  |
| 180.0            | .3529      | 1.23734   | -14.80458                    | -36.22427  |
| 195.0            | .3824      | 1.34045   | -13.99708                    | -37.56993  |
| 210.0            | .4118      | 1.44356   | -12.92038                    | -38.08979  |
| 225.0            | .4412      | 1.54668   | -11.84367                    | -38.37428  |
| 240.0            | .4706      | 1.64979   | -10.76700                    | -38.33827  |
| 255.0            | .5000      | 1.75290   | -9.42110                     | -36.72621  |
| 270.0            | .5294      | 1.85601   | -8.07523                     | -34.26392  |
| 285.0            | .5588      | 1.95912   | -7.26773                     | -33.50469  |
| 300.0            | .5882      | 2.06223   | -6.46018                     | -32.26208  |
| 315.0            | .6176      | 2.16535   | -5.38349                     | -28.89006  |
| 330.0            | .6471      | 2.26846   | -4.57595                     | -26.21846  |
| 345.0            | .6765      | 2.37157   | -4.03762                     | -24.60325  |
| 360.0            | .7059      | 2.47468   | -3.49927                     | -22.56484  |
| 375.0            | .7353      | 2.57779   | -2.96094                     | -20.08332  |
| 390.0            | .7647      | 2.68090   | -2.42256                     | -17.15947  |
| 405.0            | .7941      | 2.78402   | -1.88422                     | -13.82247  |
| 420.0            | .8235      | 2.88713   | -1.61505                     | -12.22169  |
| 435.0            | .8529      | 2.99024   | -1.34587                     | -10.45964  |
| 450.0            | .8824      | 3.09335   | -1.07670                     | -8.55252   |
| 465.0            | .9118      | 3.19646   | -.80751                      | -6.52229   |
| 480.0            | .9412      | 3.29957   | -.53837                      | -.39781    |
| 495.0            | .9706      | 3.40269   | -.53835                      | -4.44811   |
| 510.0            | 1.0000     | 3.50580   | -.26916                      | -2.23680   |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING.

TABLE E-24

EVAPORATION EXPERIMENT NO. BLF8 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 50%

## EVAPORATION RATE FOR A DROPLET IN A UNIFORM ARRAY

| ***** TIME ***** |            |            | ***** EVAPORATION RATE ***** |            |
|------------------|------------|------------|------------------------------|------------|
| MINUTES          | FRACTIONAL | HALF-LIVES | MICROGRAMS PER MINUTE        | NORMALIZED |
| .0               | .0000      | .00000     | .00000                       | .00000     |
| 15.0             | .0313      | .10001     | -25.99681                    | -27.63011  |
| 30.0             | .0625      | .20002     | -24.93570                    | -28.20183  |
| 45.0             | .0938      | .30003     | -23.87458                    | -28.76802  |
| 60.0             | .1250      | .40004     | -22.81352                    | -29.32234  |
| 75.0             | .1563      | .50005     | -22.01771                    | -30.24575  |
| 90.0             | .1875      | .60006     | -21.48710                    | -31.64047  |
| 105.0            | .2188      | .70008     | -20.69135                    | -32.73674  |
| 120.0            | .2500      | .80009     | -19.89549                    | -33.90428  |
| 135.0            | .2813      | .90010     | -19.36496                    | -35.67734  |
| 150.0            | .3125      | 1.00011    | -18.83440                    | -37.67228  |
| 165.0            | .3438      | 1.10012    | -18.30386                    | -39.93567  |
| 180.0            | .3750      | 1.20013    | -17.77331                    | -42.52806  |
| 195.0            | .4063      | 1.30014    | -17.24279                    | -45.53006  |
| 210.0            | .4375      | 1.40015    | -16.44695                    | -48.18713  |
| 225.0            | .4688      | 1.50016    | -15.65112                    | -51.19332  |
| 240.0            | .5000      | 1.60017    | -14.85529                    | -54.62565  |
| 255.0            | .5313      | 1.70018    | -14.05949                    | -58.58659  |
| 270.0            | .5625      | 1.80019    | -13.52894                    | -64.66519  |
| 285.0            | .5938      | 1.90020    | -12.20258                    | -67.24358  |
| 300.0            | .6250      | 2.00022    | -10.61095                    | -67.43937  |
| 315.0            | .6563      | 2.10023    | -9.54984                     | -70.41322  |
| 330.0            | .6875      | 2.20024    | -8.48874                     | -72.97523  |
| 345.0            | .7188      | 2.30025    | -7.42766                     | -74.69927  |
| 360.0            | .7500      | 2.40026    | -6.36656                     | -74.93804  |
| 375.0            | .7813      | 2.50027    | -5.30548                     | -72.78369  |
| 390.0            | .8125      | 2.60028    | -4.24437                     | -67.11245  |
| 405.0            | .8438      | 2.70029    | -3.18326                     | -56.83954  |
| 420.0            | .8750      | 2.80030    | -2.38746                     | -47.20572  |
| 435.0            | .9063      | 2.90031    | -1.59166                     | -33.89648  |
| 450.0            | .9375      | 3.00032    | -.79583                      | -17.62754  |
| 465.0            | .9688      | 3.10033    | -.53055                      | -12.07436  |
| 480.0            | 1.0000     | 3.20035    | -.26525                      | -6.12060   |

NORMALIZED: MICROGRAMS PER MINUTE PER FRACTION OF LIQUID CONTAMINATION REMAINING.

Blank



APPENDIX F  
SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

TABLE F-1

EVAPORATION EXPERIMENT NO. GLF1 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/TOP SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 45%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 4.700       | 4.700       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER SQ METER   | .000        | 27.861      | 27.861      |
| GRAMS PER DROPLET    | .00000      | .00639      | .00639      |

|   |              |
|---|--------------|
| ESTIMATED MEAN DROPLET MASS             | .00639 GRAMS |
| STANDARD DEVIATION OF TEST DROPLET MASS | .00000 GRAMS |
| STANDARD ERROR OF MEAN MASS ESTIMANT    | .00000 GRAMS |

|                             |                  |
|-----------------------------|------------------|
| EQUIVALENT DROPLET DIAMETER | 2.26 MILLIMETERS |
|-----------------------------|------------------|

DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES .0155945 GRAMS

FOR CONVERSION FACTOR PPM/AB \* CALCULATION \* 69.000

FOR CONVERSION FACTOR PPM/AB \* CALIBRATION \* 69.000

RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT 75 LITERS PER MINUTE TO TOTAL MASS

BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) 3.01621 PERCENT

BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) 2.84553 PERCENT

TABLE --2

EVAPORATION EXPERIMENT NO. GLF2 SERIES 10 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/TOP SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 39%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 5.000       | 5.000       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER SQ METER   | .000        | 29.636      | 29.636      |
| GRAMS PER DROPLET    | .00000      | .00679      | .00679      |

|   |              |
|---|--------------|
| ESTIMATED MEAN DROPLET MASS             | .00679 GRAMS |
| STANDARD DEVIATION OF TEST DROPLET MASS | .00000 GRAMS |
| STANDARD ERROR OF MEAN MASS ESTIMANT    | .00000 GRAMS |

|                             |                  |
|-----------------------------|------------------|
| EQUIVALENT DROPLET DIAMETER | 2.31 MILLIMETERS |
|-----------------------------|------------------|

DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES .0137671 GRAMS

FOR CONVERSION FACTOR PPM/AB \* CALCULATION \* 69.000

FOR CONVERSION FACTOR PPM/AB \* CALIBRATION \* 69.000

RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT 75 LITERS PER MINUTE TO TOTAL MASS

BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) 3.29408 PERCENT

BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) 3.14947 PERCENT

TABLE F-3

EVAPORATION EXPERIMENT NO. GLF3 SERIES 1D 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 40%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 4.200       | 4.200       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER SQ METER   | .000        | 24.902      | 24.902      |
| GRAMS PER DROPLET    | .00000      | .00571      | .00571      |

|   |                  |
|---|------------------|
| ESTIMATED MEAN DROPLET MASS             | .00571 GRAMS     |
| STANDARD DEVIATION OF TEST DROPLET MASS | .00000 GRAMS     |
| STANDARD ERROR OF MEAN MASS ESTIMANT    | .00000 GRAMS     |
| EQUIVALENT DROPLET DIAMETER             | 2.18 MILLIMETERS |

DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES .0052388 GRAMS

FOR CONVERSION FACTOR PPM/AB \* CALCULATION \* 69.000

FOR CONVEPSION FAUTOR PPM/AB \* CALIBRATION \* 69.000

RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT 75 LITERS PER MINUTE TO TOTAL MASS

BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) .92962 PERCENT

BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) .85546 PERCENT

# TABLE F-4

EVAPORATION EXPERIMENT NO. GLF4 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 5.000       | 5.000       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER SQ METER   | .000        | 29.636      | 29.636      |
| GRAMS PER DROPLET    | .00000      | .00679      | .00679      |

|   |              |
|---|--------------|
| ESTIMATED MEAN DROPLET MASS             | .00679 GRAMS |
| STANDARD DEVIATION OF TEST DROPLET MASS | .00000 GRAMS |
| STANDARD ERROR OF MEAN MASS ESTIMANT    | .00000 GRAMS |

|                             |                  |
|-----------------------------|------------------|
| EQUIVALENT DROPLET DIAMETER | 2.31 MILLIMETERS |
|-----------------------------|------------------|

DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES .0029546 GRAMS

FOR CONVERSION FACTOR PPM/AB \* CALCULATION \* 69.000

FOR CONVERSION FACTOR PPM/AB \* CALIBRATION \* 69.000

RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT 75 LITERS PER MINUTE TO TOTAL MASS

BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) .99138 PERCENT

BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) .96024 PERCENT

TABLE F-5

EVAPORATION EXPERIMENT NO. GLF5 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/BOTTOM SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 58%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 4.200       | 4.200       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER SQ METER   | .000        | 24.902      | 24.902      |
| GRAMS PER DROPLET    | .00000      | .00571      | .00571      |

|   |                  |
|---|------------------|
| ESTIMATED MEAN DROPLET MASS             | .00571 GRAMS     |
| STANDARD DEVIATION OF TEST DROPLET MASS | .00000 GRAMS     |
| STANDARD ERROR OF MEAN MASS ESTIMANT    | .00000 GRAMS     |
| EQUIVALENT DROPLET DIAMETER             | 2.18 MILLIMETERS |

DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES .0095029 GRAMS

FOR CONVERSION FACTOR PPM/AB \* CALCULATION \* 65.000

FOR CONVERSION FACTOR PPM/AB \* CALIBRATION \* 69.000

RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT 75 LITERS PER MINUTE TO TOTAL MASS

BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) 2.92763 PERCENT

BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) 2.81124 PERCENT

TABLE F-6

EVAPORATION EXPERIMENT NO. GLF6 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/BOTTOM SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 55%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 4.700       | 4.700       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER SQ METER   | .000        | 27.861      | 27.861      |
| GRAMS PER DROPLET    | .00000      | .00639      | .00639      |

|   |              |
|---|--------------|
| ESTIMATED MEAN DROPLET MASS             | .00639 GRAMS |
| STANDARD DEVIATION OF TEST DROPLET MASS | .00000 GRAMS |
| STANDARD ERROR OF MEAN MASS ESTIMANT    | .00000 GRAMS |

|                             |                  |
|-----------------------------|------------------|
| EQUIVALENT DROPLET DIAMETER | 2.26 MILLIMETERS |
|-----------------------------|------------------|

|  |                |
|--|----------------|
| DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES | .0092592 GRAMS |
|--|----------------|

|  |        |
|--|--------|
| FOR CONVERSION FACTOR PPM/AB * CALCULATION * | 69.000 |
|--|--------|

|  |        |
|--|--------|
| FOR CONVERSION FACTOR PPM/AB * CALIBRATION * | 69.000 |
|--|--------|

|  |                                    |
|--|------------------------------------|
| RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT | 75 LITERS PER MINUTE TO TOTAL MASS |
|--|------------------------------------|

|  |                 |
|--|-----------------|
| BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) | 3.00333 PERCENT |
|--|-----------------|

|  |                 |
|--|-----------------|
| BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) | 2.89986 PERCENT |
|--|-----------------|

# TABLE F-7

EVAPORATION EXPERIMENT NO. GLF7 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/BOTTOM SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 30%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 4.600       | 4.600       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER SQ METER   | .000        | 27.269      | 27.269      |
| GRAMS PER DROPLET    | .00000      | .00625      | .00625      |

|   |              |
|---|--------------|
| ESTIMATED MEAN DROPLET MASS             | .00625 GRAMS |
| STANDARD DEVIATION OF TEST DROPLET MASS | .00000 GRAMS |
| STANDARD ERROR OF MEAN MASS ESTIMANT    | .00000 GRAMS |

|                             |                  |
|-----------------------------|------------------|
| EQUIVALENT DROPLET DIAMETER | 2.25 MILLIMETERS |
|-----------------------------|------------------|

DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES .0028816 GRAMS

FOR CONVERSION FACTOR PPM/AB \* CALCULATION \* 68.000

FOR CONVERSION FACTOR PPM/AB \* CALIBRATION \* 68.000

RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT 75 LITERS PER MINUTE TO TOTAL MASS

BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) .91973 PERCENT

BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) .88750 PERCENT



TABLE F-8

EVAPORATION EXPERIMENT NO. GLF8 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON HICKORY/BOTTOM SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 50%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 5.000       | 5.000       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER SQ METER   | .000        | 29.636      | 29.636      |
| GRAMS PER DROPLET    | .00000      | .00679      | .00679      |

|   |              |
|---|--------------|
| ESTIMATED MEAN DROPLET MASS             | .00679 GRAMS |
| STANDARD DEVIATION OF TEST DROPLET MASS | .00000 GRAMS |
| STANDARD ERROR OF MEAN MASS ESTIMATE    | .00000 GRAMS |

|                             |                  |
|-----------------------------|------------------|
| EQUIVALENT DROPLET DIAMETER | 2.31 MILLIMETERS |
|-----------------------------|------------------|

DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES .0028207 GRAMS

FOR CONVERSION FACTOR PPM/AB \* CALCULATION \* 71.000

FOR CONVERSION FACTOR PPM/AB \* CALIBRATION \* 71.000

RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT 75 LITERS PER MINUTE TO TOTAL MASS

BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) .94023 PERCENT

BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) .91060 PERCENT

TABLE F-9

EVAPORATION EXPERIMENT NO. GLF9 SERIES 1D 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 66%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 3.900       | 3.900       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER SQ METER   | .000        | 23.127      | 23.127      |
| GRAMS PER DROPLET    | .00000      | .00530      | .00530      |

|   |              |
|---|--------------|
| ESTIMATED MEAN DROPLET MASS             | .00530 GRAMS |
| STANDARD DEVIATION OF TEST DROPLET MASS | .00000 GRAMS |
| STANDARD ERROR OF MEAN MASS ESTIMANT    | .00000 GRAMS |

|                             |                  |
|-----------------------------|------------------|
| EQUIVALENT DROPLET DIAMETER | 2.13 MILLIMETERS |
|-----------------------------|------------------|

DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES .0169294 GRAMS

FOR CONVERSION FACTOR PPM/AB \* CALCULATION \* 68.000

FOR CONVERSION FACTOR PPM/AB \* CALIBRATION \* 68.000

RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT 75 LITERS PER MINUTE TO TOTAL MASS

BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) 3.43337 PERCENT

BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) 3.21008 PERCENT

TABLE F-10

EVAPORATION EXPERIMENT NO. GLF10 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/50 METER ON QAC/TOP SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 52%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 5.000       | 5.000       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER 50 METER   | .000        | 29.636      | 29.636      |
| GRAMS PER DROPLET    | .00000      | .00679      | .00679      |

|   |              |
|---|--------------|
| ESTIMATED MEAN DROPLET MASS             | .00679 GRAMS |
| STANDARD DEVIATION OF TEST DROPLET MASS | .00000 GRAMS |
| STANDARD ERROR OF MEAN MASS ESTIMANT    | .00000 GRAMS |

|                             |                  |
|-----------------------------|------------------|
| EQUIVALENT DROPLET DIAMETER | 2.31 MILLIMETERS |
|-----------------------------|------------------|

DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES .0164475 GRAMS

FOR CONVERSION FACTOR PPM/AB \* CALCULATION \* 69.000

FOR CONVERSION FACTOR PPM/AB \* CALIBRATION \* 69.000

RATIO OF TEST MASS ANALYZED BY MIMAN SAMPLING AT 75 LITERS PER MINUTE TO TOTAL MASS

BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) 3.50908 PERCENT

BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) 3.33631 PERCENT

# TABLE F-11

EVAPORATION EXPERIMENT NO. GLF11 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 55%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 4.300       | 4.300       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER SQ METER   | .000        | 25.494      | 25.494      |
| GRAMS PER DROPLET    | .00000      | .00584      | .00584      |

|   |              |
|---|--------------|
| ESTIMATED MEAN DROPLET MASS             | .00584 GRAMS |
| STANDARD DEVIATION OF TEST DROPLET MASS | .00000 GRAMS |
| STANDARD ERROR OF MEAN MASS ESTIMANT    | .00000 GRAMS |

|                             |                  |
|-----------------------------|------------------|
| EQUIVALENT DROPLET DIAMETER | 2.20 MILLIMETERS |
|-----------------------------|------------------|

DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES .0026779 GRAMS

FOR CONVERSION FACTOR PPM/AB \* CALCULATION \* 70.000

FOR CONVERSION FACTOR PPM/AB \* CALIBRATION \* 70.000

RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT 75 LITERS PER MINUTE TO TOTAL MASS

BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) .93151 PERCENT

BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) .89947 PERCENT

TABLE F-12

EVAPORATION EXPERIMENT NO. GLF12 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 40%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 5.000       | 5.000       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER SQ METER   | .000        | 29.636      | 29.636      |
| GRAMS PER DROPLET    | .00000      | .00679      | .00679      |

ESTIMATED MEAN DROPLET MASS .00679 GRAMS

STANDARD DEVIATION OF TEST DROPLET MASS .00000 GRAMS

STANDARD ERROR OF MEAN MASS ESTIMANT .00000 GRAMS

EQUIVALENT DROPLET DIAMETER 2.31 MILLIMETERS

DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES .0023392 GRAMS

FOR CONVERSION FACTOR PPM/AB \* CALCULATION \* 69.000

FOR CONVERSION FACTOR PPM/AB \* CALIBRATION \* 69.000

RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT 75 LITERS PER MINUTE TO TOTAL MASS

BASED ON CALCULATED CONVERSION FACTOR (PPM/AD) .94087 PERCENT

BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) .91630 PERCENT

TABLE F-13

EVAPORATION EXPERIMENT NO. GLF13 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 44%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 4.100       | 4.100       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER SQ METER   | .000        | 24.310      | 24.310      |
| GRAMS PER DROPLET    | .00000      | .00557      | .00557      |

ESTIMATED MEAN DROPLET MASS .00557 GRAMS

STANDARD DEVIATION OF TEST DROPLET MASS .00000 GRAMS

STANDARD ERROR OF MEAN MASS ESTIMANT .00000 GRAMS

EQUIVALENT DROPLET DIAMETER 2.16 MILLIMETERS

DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES .0112063 GRAMS

FOR CONVERSION FACTOR PPM/AB \* CALCULATION \* 68.000

FOR CONVERSION FACTOR PPM/AB \* CALIBRATION \* 68.000

RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT 75 LITERS PER MINUTE TO TOTAL MASS

BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) 3.49889 PERCENT

BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) 3.35829 PERCENT

TABLE F-14

EVAPORATION EXPERIMENT NO. GLF14 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 43%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 5.000       | 5.000       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER SQ METER   | .000        | 29.636      | 29.636      |
| GRAMS PER DROPLET    | .00000      | .00679      | .00679      |

|   |              |
|---|--------------|
| ESTIMATED MEAN DROPLET MASS             | .00679 GRAMS |
| STANDARD DEVIATION OF TEST DROPLET MASS | .00000 GRAMS |
| STANDARD ERROR OF MEAN MASS ESTIMANT    | .00000 GRAMS |

|                             |                  |
|-----------------------------|------------------|
| EQUIVALENT DROPLET DIAMETER | 2.31 MILLIMETERS |
|-----------------------------|------------------|

DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES .0115358 GRAMS

FOR CONVERSION FACTOR PPM/AB \* CALCULATION \* 70.000

FOR CONVERSION FACTOR PPM/AB \* CALIBRATION \* 70.000

RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT 75 LITERS PER MINUTE TO TOTAL MASS

BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) 3.44828 PERCENT

BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) 3.32711 PERCENT

TABLE F-15

EVAPORATION EXPERIMENT NO. GLF15 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 11.3 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 4.300       | 4.300       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER SQ METER   | .000        | 25.494      | 25.494      |
| GRAMS PER DROPLET    | .00000      | .00584      | .00584      |

|   |                  |
|---|------------------|
| ESTIMATED MEAN DROPLET MASS             | .00584 GRAMS     |
| STANDARD DEVIATION OF TEST DROPLET MASS | .00000 GRAMS     |
| STANDARD ERROR OF MEAN MASS ESTIMATE    | .00000 GRAMS     |
| EQUIVALENT DROPLET DIAMETER             | 2.20 MILLIMETERS |

DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES .0025435 GRAMS

FOR CONVERSION FACTOR PPM/AB \* CALCULATION \* 67.000

FOR CONVERSION FACTOR PPM/AB \* CALIBRATION \* 67.000

RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT 75 LITERS PER MINUTE TO TOTAL MASS

BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) .09725 PERCENT

BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) .06682 PERCENT



# TABLE F-16

EVAPORATION EXPERIMENT NO. GLF16 SERIES 1D 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
WINDSPEED 11.3 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 4.800       | 4.800       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER SQ METER   | .000        | 28.452      | 28.452      |
| GRAMS PER DROPLET    | .00000      | .00652      | .00652      |

|   |              |
|---|--------------|
| ESTIMATED MEAN DROPLET MASS             | .00652 GRAMS |
| STANDARD DEVIATION OF TEST DROPLET MASS | .00000 GRAMS |
| STANDARD ERROR OF MEAN MASS ESTIMANT    | .00000 GRAMS |

|                             |                  |
|-----------------------------|------------------|
| EQUIVALENT DROPLET DIAMETER | 2.28 MILLIMETERS |
|-----------------------------|------------------|

DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES .0025814 GRAMS

FOR CONVERSION FACTOR PPM/AB \* CALCULATION \* 68.000

FOR CONVERSION FACTOR PPM/AB \* CALIBRATION \* 68.000

RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT 75 LITERS PER MINUTE TO TOTAL MASS

BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) .88416 PERCENT

BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) .85591 PERCENT

TABLE F-17

EVAPORATION EXPERIMENT NO. 9LFI SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 39%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 4.800       | 4.800       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER SQ METER   | .000        | 28.452      | 28.452      |
| GRAMS PER DROPLET    | .00000      | .00652      | .00652      |

|   |              |
|---|--------------|
| ESTIMATED MEAN DROPLET MASS             | .00652 GRAMS |
| STANDARD DEVIATION OF TEST DROPLET MASS | .00000 GRAMS |
| STANDARD ERROR OF MEAN MASS ESTIMATE    | .00000 GRAMS |

|                             |                  |
|-----------------------------|------------------|
| EQUIVALENT DROPLET DIAMETER | 2.28 MILLIMETERS |
|-----------------------------|------------------|

DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES .0142544 GRAMS

FOR CONVERSION FACTOR PPM/AB \* CALCULATION \* 69.000

FOR CONVERSION FACTOR PPM/AB \* CALIBRATION \* 69.000

RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT 75 LITERS PER MINUTE TO TOTAL MASS

BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) 3.21189 PERCENT

BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) 3.05913 PERCENT

TABLE F-18

EVAPORATION EXPERIMENT NO. BLF2 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 2.9 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 39%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 5.000       | 5.000       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER SQ METER   | .000        | 29.636      | 29.636      |
| GRAMS PER DROPLET    | .00000      | .00679      | .00679      |

|   |              |
|---|--------------|
| ESTIMATED MEAN DROPLET MASS             | .00679 GRAMS |
| STANDARD DEVIATION OF TEST DROPLET MASS | .00000 GRAMS |
| STANDARD ERROR OF MEAN MASS ESTIMANT    | .00000 GRAMS |

|                             |                  |
|-----------------------------|------------------|
| EQUIVALENT DROPLET DIAMETER | 2.31 MILLIMETERS |
|-----------------------------|------------------|

DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES .0140384 GRAMS

FOR CONVERSION FACTOR PPM/AB \* CALCULATION \* 67.000

FOR CONVERSION FACTOR PPM/AB \* CALIBRATION \* 67.000

RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT 75 LITERS PER MINUTE TO TOTAL MASS

BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) 3.94337 PERCENT

BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) 3.79591 PERCENT

# TABLE F-19

EVAPORATION EXPERIMENT NO. BLF3 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 4.800       | 4.800       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER SQ METER   | .000        | 28.452      | 28.452      |
| GRAMS PER DROPLET    | .00000      | .00652      | .00652      |

|   |              |
|---|--------------|
| ESTIMATED MEAN DROPLET MASS             | .00652 GRAMS |
| STANDARD DEVIATION OF TEST DROPLET MASS | .00000 GRAMS |
| STANDARD ERROR OF MEAN MASS ESTIMANT    | .00000 GRAMS |

|                             |                  |
|-----------------------------|------------------|
| EQUIVALENT DROPLET DIAMETER | 2.28 MILLIMETERS |
|-----------------------------|------------------|

DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES .0031677 GRAMS

FOR CONVERSION FACTOR PPM/AB \* CALCULATION \* 69.000

FOR CONVERSION FACTOR PPM/AB \* CALIBRATION \* 69.000

RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT 75 LITERS PER MINUTE TO TOTAL MASS

BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) .91917 PERCENT

BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) .88523 PERCENT

TABLE F-20

EVAPORATION EXPERIMENT NO. BLF4 SERIES TO 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/TOP SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 20%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 5.200       | 5.200       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER SQ METER   | .000        | 30.819      | 30.819      |
| GRAMS PER DROPLET    | .00000      | .00707      | .00707      |

ESTIMATED MEAN DROPLET MASS .00707 GRAMS  
 STANDARD DEVIATION OF TEST DROPLET MASS .00000 GRAMS  
 STANDARD ERROR OF MEAN MASS ESTIMANT .00000 GRAMS

EQUIVALENT DROPLET DIAMETER 2.34 MILLIMETERS

DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES .0041423 GRAMS

FOR CONVERSION FACTOR PPM/AB \* CALCULATION \* 69.000

FOR CONVERSION FACTOR PPM/AB \* CALIBRATION \* 69.000

RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT 75 LITERS PER MINUTE TO TOTAL MASS

BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) 1.04513 PERCENT

BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) 1.00329 PERCENT

# TABLE F-21

EVAPORATION EXPERIMENT NO. BLE5 SERIES 1D 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 4.600       | 4.600       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER SQ METER   | .000        | 27.269      | 27.269      |
| GRAMS PER DROPLET    | .00000      | .00625      | .00625      |

|   |              |
|---|--------------|
| ESTIMATED MEAN DROPLET MASS             | .00625 GRAMS |
| STANDARD DEVIATION OF TEST DROPLET MASS | .00000 GRAMS |
| STANDARD ERROR OF MEAN MASS ESTIMANT    | .00000 GRAMS |

|                             |                  |
|-----------------------------|------------------|
| EQUIVALENT DROPLET DIAMETER | 2.25 MILLIMETERS |
|-----------------------------|------------------|

DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES .0096249 GRAMS

FOR CONVERSION FACTOR PPM/AB \* CALCULATION \* 69.000

FOR CONVERSION FACTOR PPM/AB \* CALIBRATION \* 9.000

RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT 75 LITERS PER MINUTE TO TOTAL MASS

BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) 3.21802 PERCENT

BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) 3.11039 PERCENT

TABLE F-22

EVAPORATION EXPERIMENT NO. BLF6 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 2.9 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 4.900       | 4.900       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER SQ METER   | .000        | 29.044      | 29.044      |
| GRAMS PER DROPLET    | .00000      | .00666      | .00666      |

|   |              |
|---|--------------|
| ESTIMATED MEAN DROPLET MASS             | .00666 GRAMS |
| STANDARD DEVIATION OF TEST DROPLET MASS | .00000 GRAMS |
| STANDARD ERROR OF MEAN MASS ESTIMANT    | .00000 GRAMS |

|                             |                  |
|-----------------------------|------------------|
| EQUIVALENT DROPLET DIAMETER | 2.30 MILLIMETERS |
|-----------------------------|------------------|

DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES .0133203 GRAMS

FOR CONVERSION FACTOR PPM/AB \* CALCULATION \* 69.000

FOR CONVERSION FACTOR PPM/AB \* CALIBRATION \* 69.000

RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT 75 LITERS PER MINUTE TO TOTAL MASS

BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) 3.75394 PERCENT

BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) 3.61117 PERCENT

TABLE F-23

EVAPORATION EXPERIMENT NO. BLF7 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 10G CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 4.400       | 4.400       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER SQ METER   | .000        | 26.086      | 26.086      |
| GRAMS PER DROPLET    | .00000      | .00598      | .00598      |

|   |              |
|---|--------------|
| ESTIMATED MEAN DROPLET MASS             | .00598 GRAMS |
| STANDARD DEVIATION OF TEST DROPLET MASS | .00000 GRAMS |
| STANDARD ERROR OF MEAN MASS ESTIMANT    | .00000 GRAMS |

|                             |                  |
|-----------------------------|------------------|
| EQUIVALENT DROPLET DIAMETER | 2.22 MILLIMETERS |
|-----------------------------|------------------|

DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES .002403 GRAMS

FOR CONVERSION FACTOR PPM/AB \* CALC BY \* 69.000

FOR CONVERSION FACTOR PPM/AB \* CALIBRATION \* 69.000

RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT 75 LITERS PER MINUTE TO TOTAL MASS

BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) .93294 PERCENT

BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) .90161 PERCENT



TABLE F-24

EVAPORATION EXPERIMENT NO. 8LF3 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 GMS/SQ METER ON OAK/BOTTOM SURFACE  
 WINDSPEED 11.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 50%

## SUMMARY OF LIQUID CONTAMINATION BY SUBSTRATE POSITION

|                      | SUBSTRATE 1 | SUBSTRATE 2 | SUBSTRATE 3 |
|----------------------|-------------|-------------|-------------|
| CONTAMINATION, GRAMS | .000        | 5.100       | 5.100       |
| NUMBER OF DROPLETS   | .000        | 736.000     | 736.000     |
| GRAMS PER SQ METER   | .000        | 30.228      | 30.228      |
| GRAMS PER DROPLET    | .00000      | .00693      | .00693      |

|   |              |
|---|--------------|
| ESTIMATED MEAN DROPLET MASS             | .00693 GRAMS |
| STANDARD DEVIATION OF TEST DROPLET MASS | .00000 GRAMS |
| STANDARD ERROR OF MEAN MASS ESTIMANT    | .00000 GRAMS |

|                             |                  |
|-----------------------------|------------------|
| EQUIVALENT DROPLET DIAMETER | 2.33 MILLIMETERS |
|-----------------------------|------------------|

|  |                |
|--|----------------|
| DIFFERENCE BETWEEN SAMPLE MASS ESTIMATES | .0030017 GRAMS |
|--|----------------|

|  |        |
|--|--------|
| FOR CONVERSION FACTOR PPM/AB * CALCULATION * | 68.000 |
|--|--------|

|  |        |
|--|--------|
| FOR CONVERSION FACTOR PPM/AB * CALIBRATION * | 68.000 |
|--|--------|

|   |  |
|---|--|
| RATIO OF TEST MASS ANALYZED BY MIRAN SAMPLING AT 75 LITERS PER MINUTE TO TOTAL MASS |  |
|---|--|

|  |                 |
|--|-----------------|
| BASED ON CALCULATED CONVERSION FACTOR (PPM/AB) | 1.01144 PERCENT |
|--|-----------------|

|  |                |
|--|----------------|
| BASE ON CALIBRATION CONVERSION FACTOR (PPM/AB) | .98053 PERCENT |
|--|----------------|

Blank

APPENDIX G  
PLOTS OF DROPLET RESIDUAL MASS VERSUS TIME

EVAPORATION EXPERIMENT NO. GLF1    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA.,    100 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/TOP SURFACE  
WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F.,    RELATIVE HUMIDITY 45%

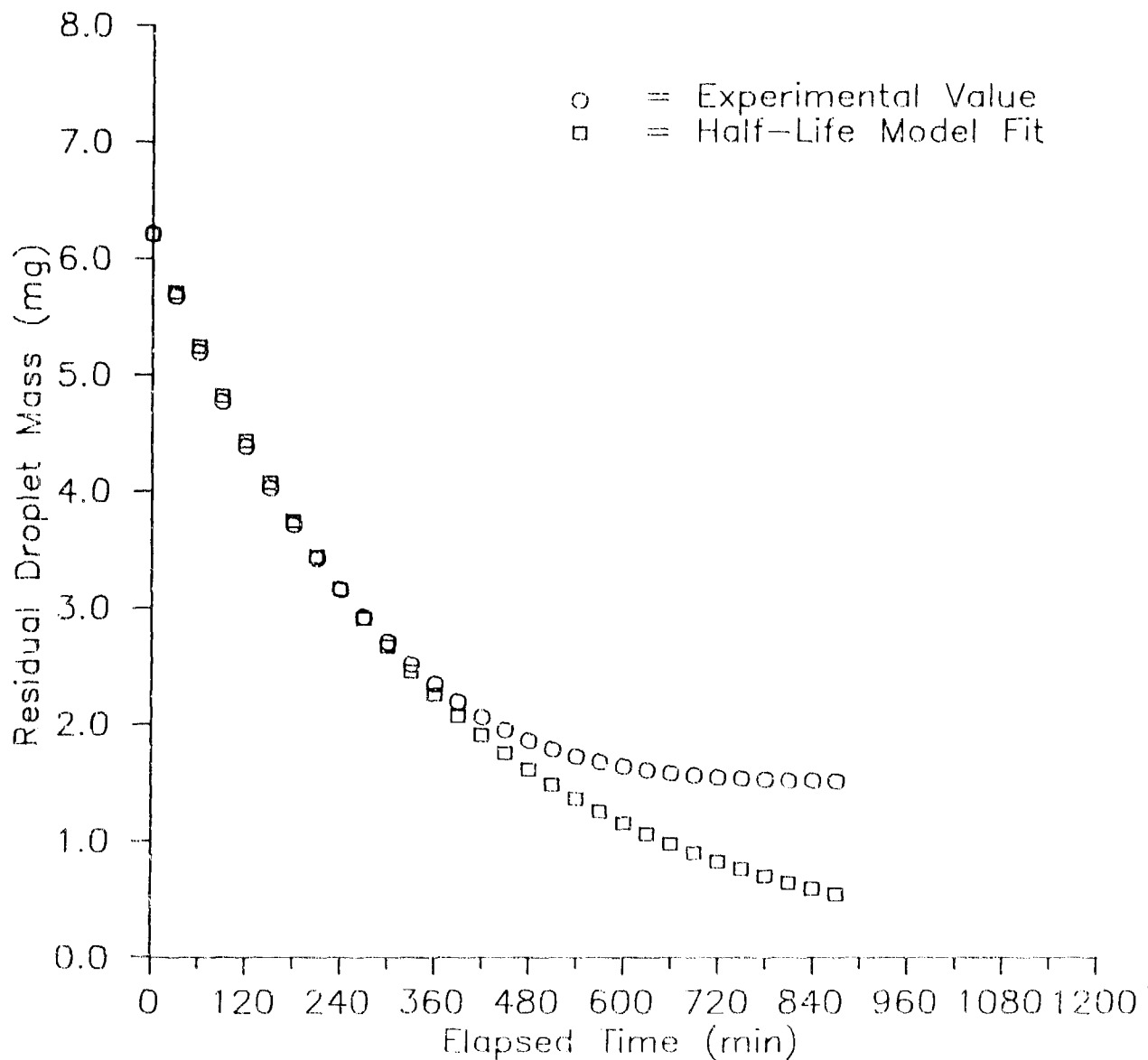


Figure G-1. Droplet Residual Mass Versus Time.

EVAPORATION EXPERIMENT NO. GLF2    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/TOP SURFACE  
WINDSPEED 3 MPH,    AIR TEMPERATURE 60 DEG F.,    RELATIVE HUMIDITY 39%

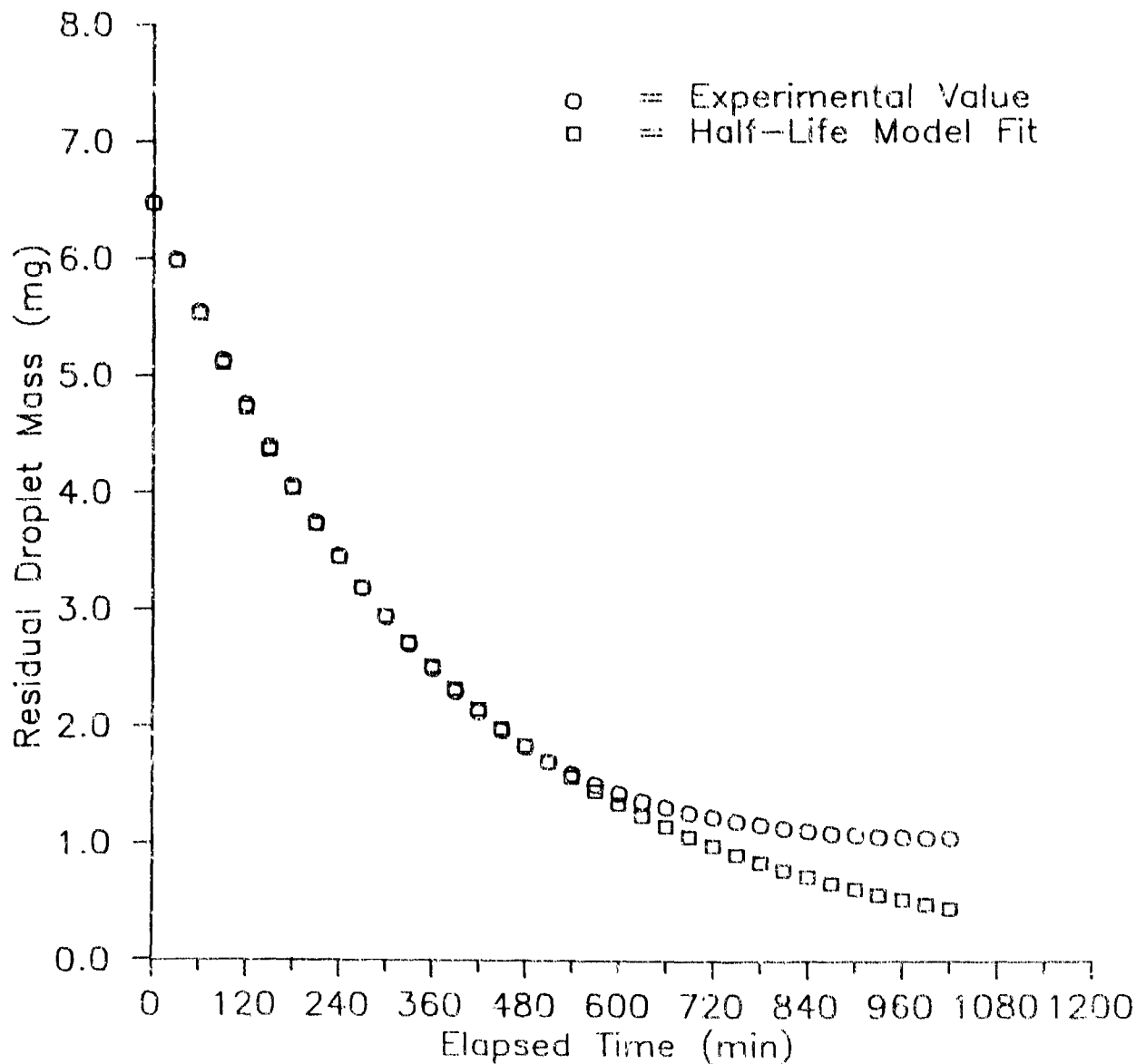


Figure G-2. Droplet Residual Mass Versus Time.

EVAPORATION EXPERIMENT NO. GLF3    SERIES ID 2004 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/TOP SURFACE  
WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 40%

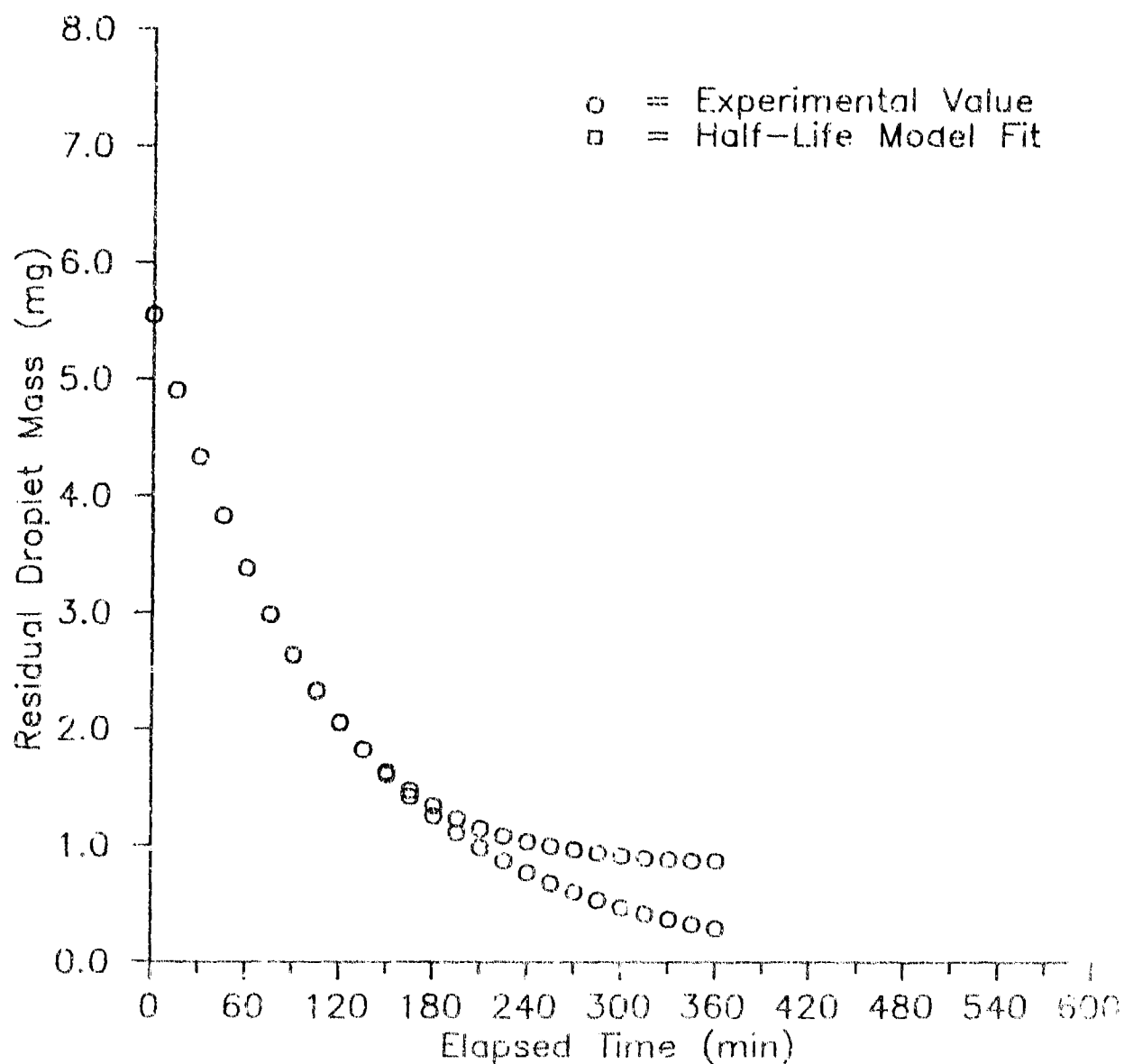


Figure G-3. Droplet Residual Mass Versus Time.

EVAPORATION EXPERIMENT NO. GLF4    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/TOP SURFACE  
WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

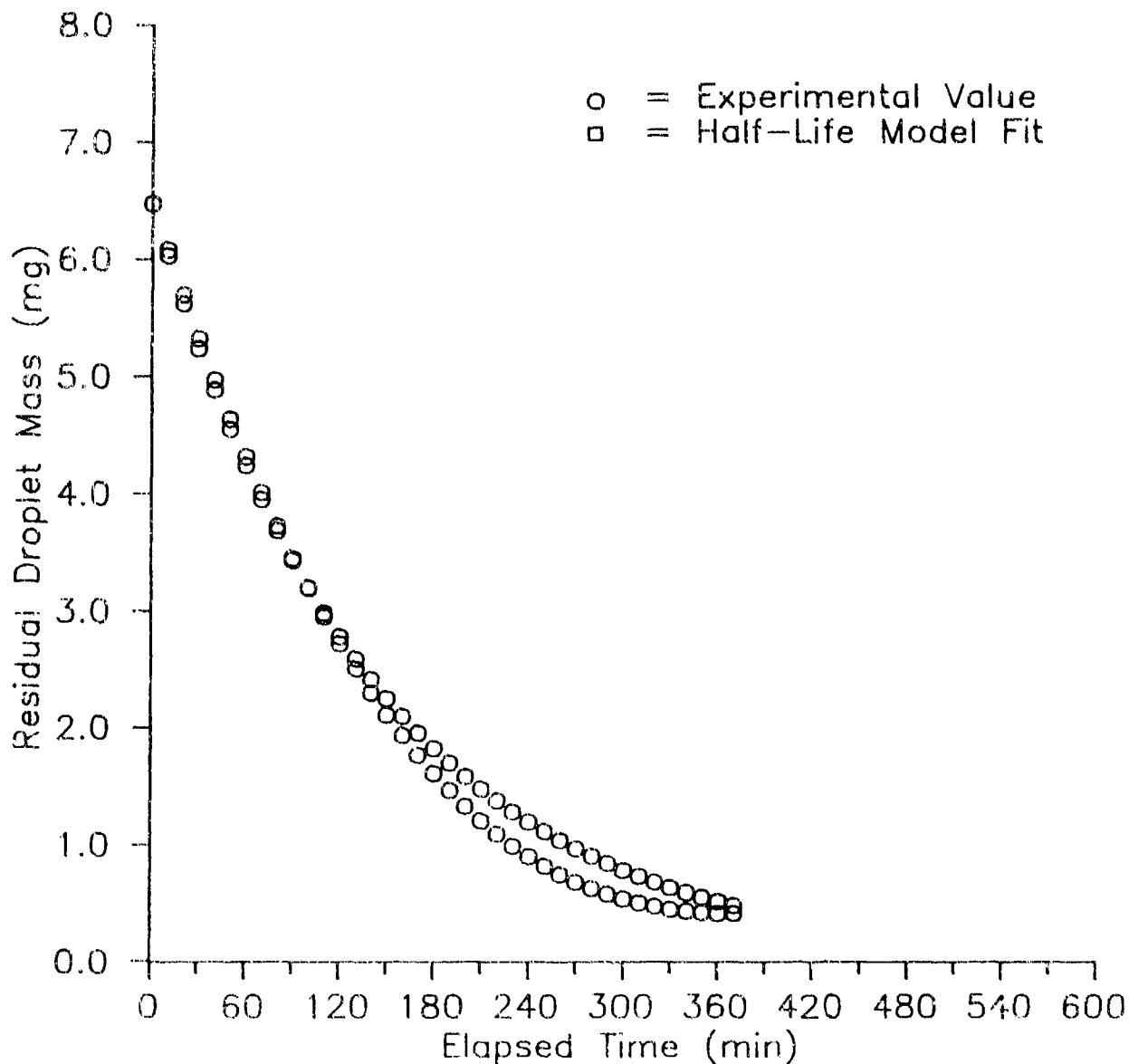


Figure G-4. Droplet Residual Mass Versus Time.

EVAPORATION EXPERIMENT NO. CLF5    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/BOTTOM  
WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 58%

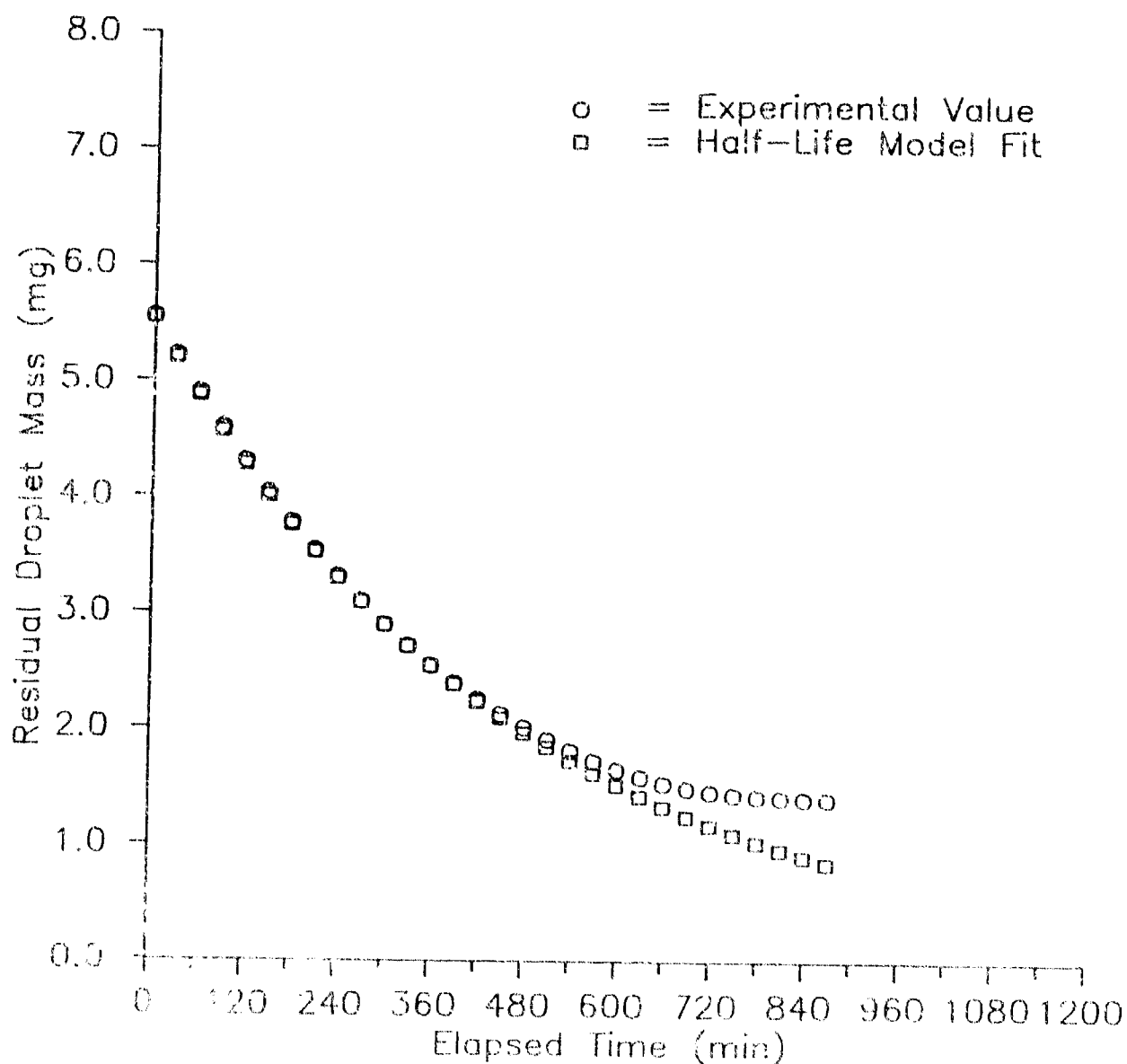


Figure G-5. Droplet Residual Mass Versus Time.



EVAPORATION EXPERIMENT NO. GLF6    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/BOTTOM  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 55%

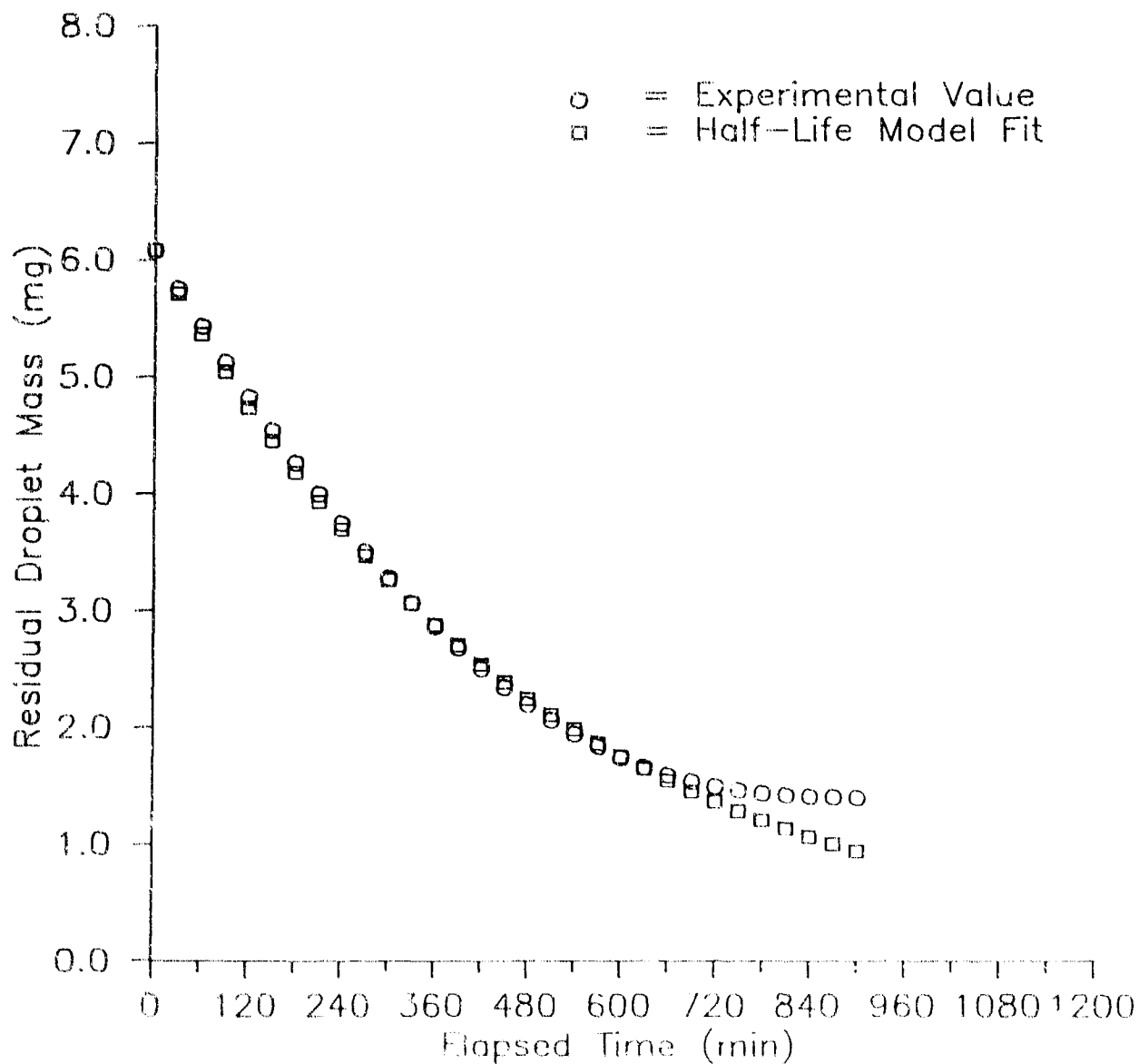


Figure G-6. Droplet Residual Mass Versus Time.

EVAPORATION EXPERIMENT NO. GLF7    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA.    100 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/BOTTOM  
WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

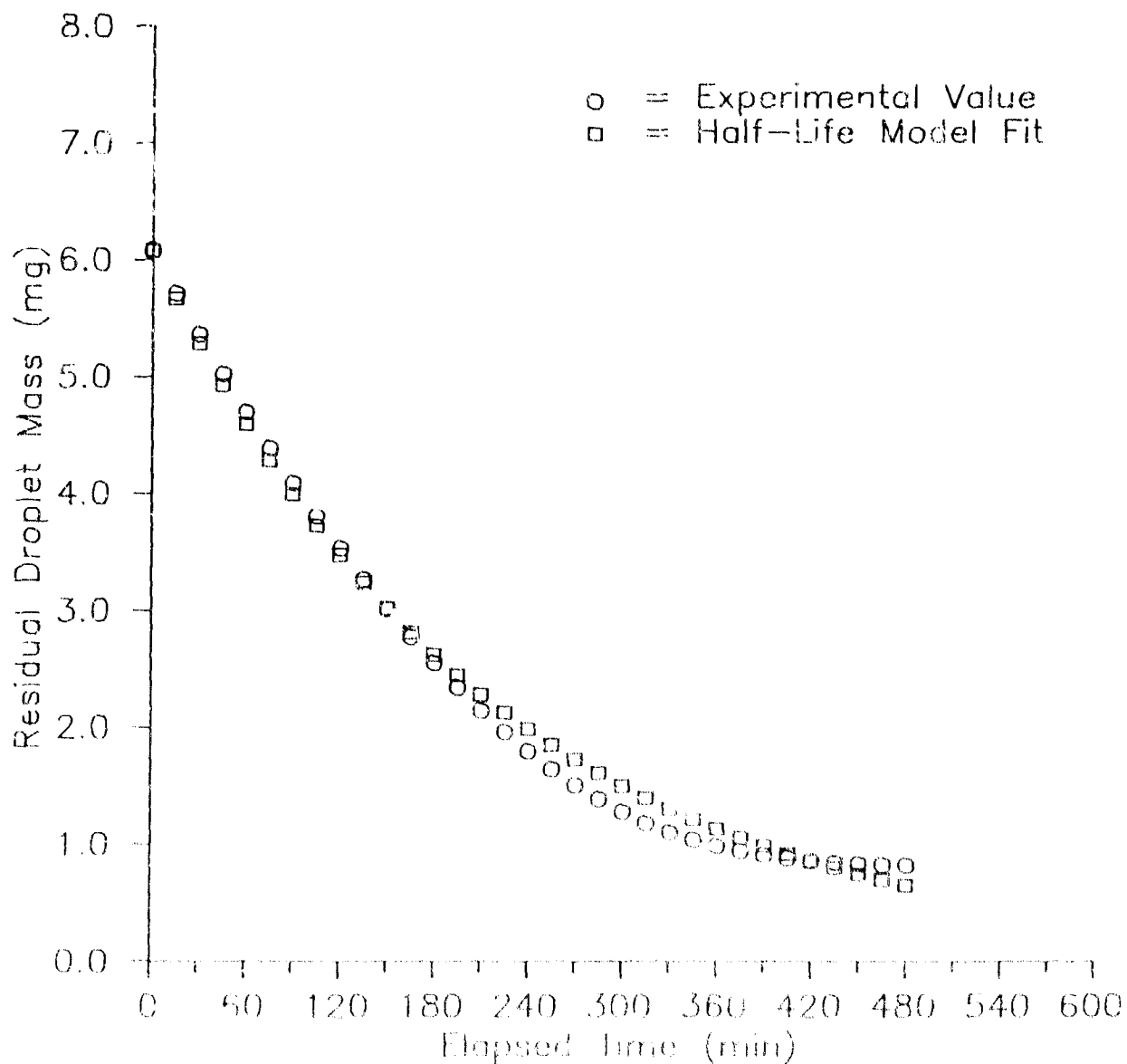


Figure G-7. Droplet Residual Mass Versus Time.

EVAPORATION EXPERIMENT NO. GLF8    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/BOTTOM  
 WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 50%

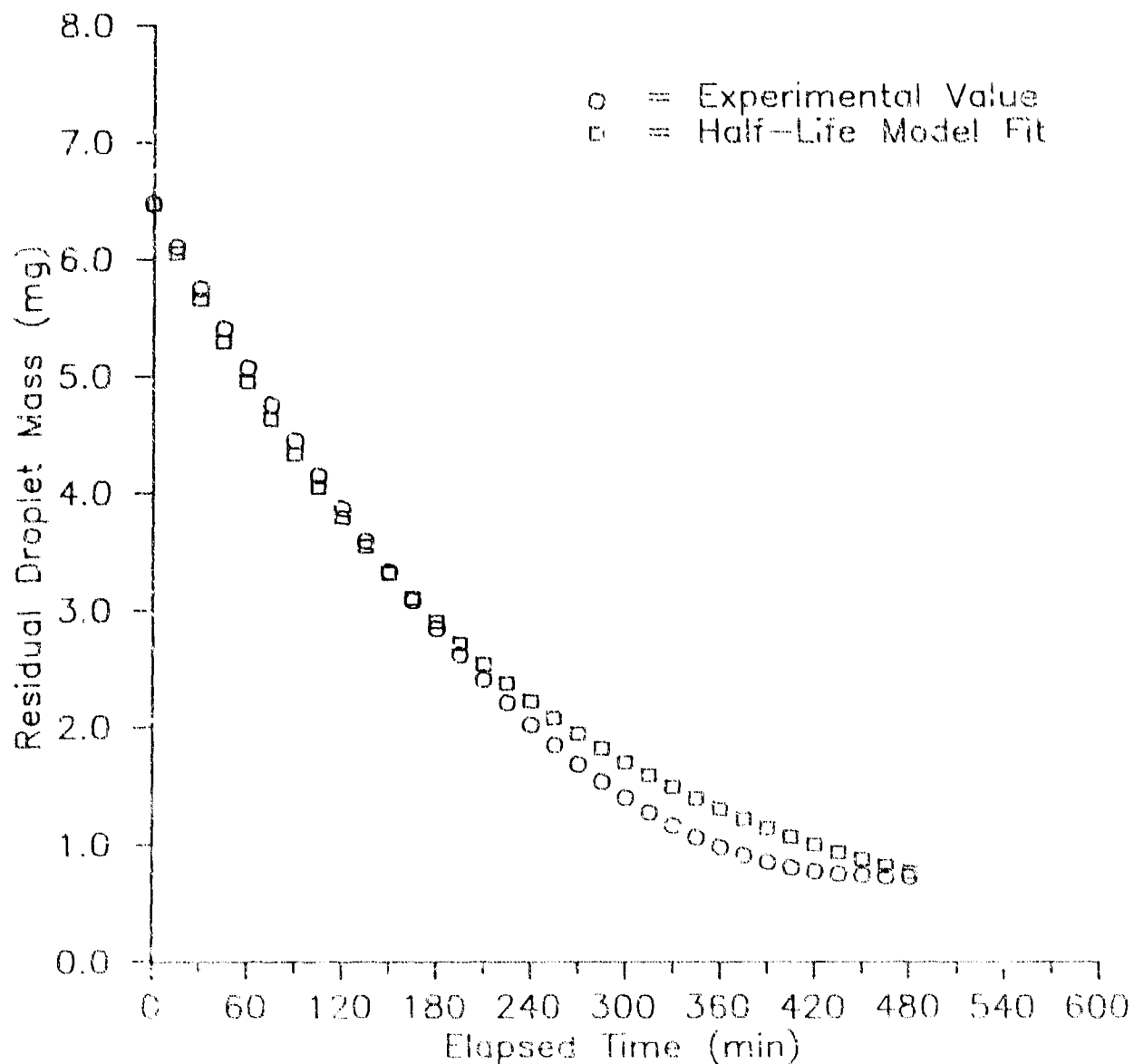


Figure C-8 Droplet Residual Mass Versus Time.

EVAPORATION EXPERIMENT NO. GLF9    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA.    100 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/TOP SURFACE  
WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F.    RELATIVE HUMIDITY 44%

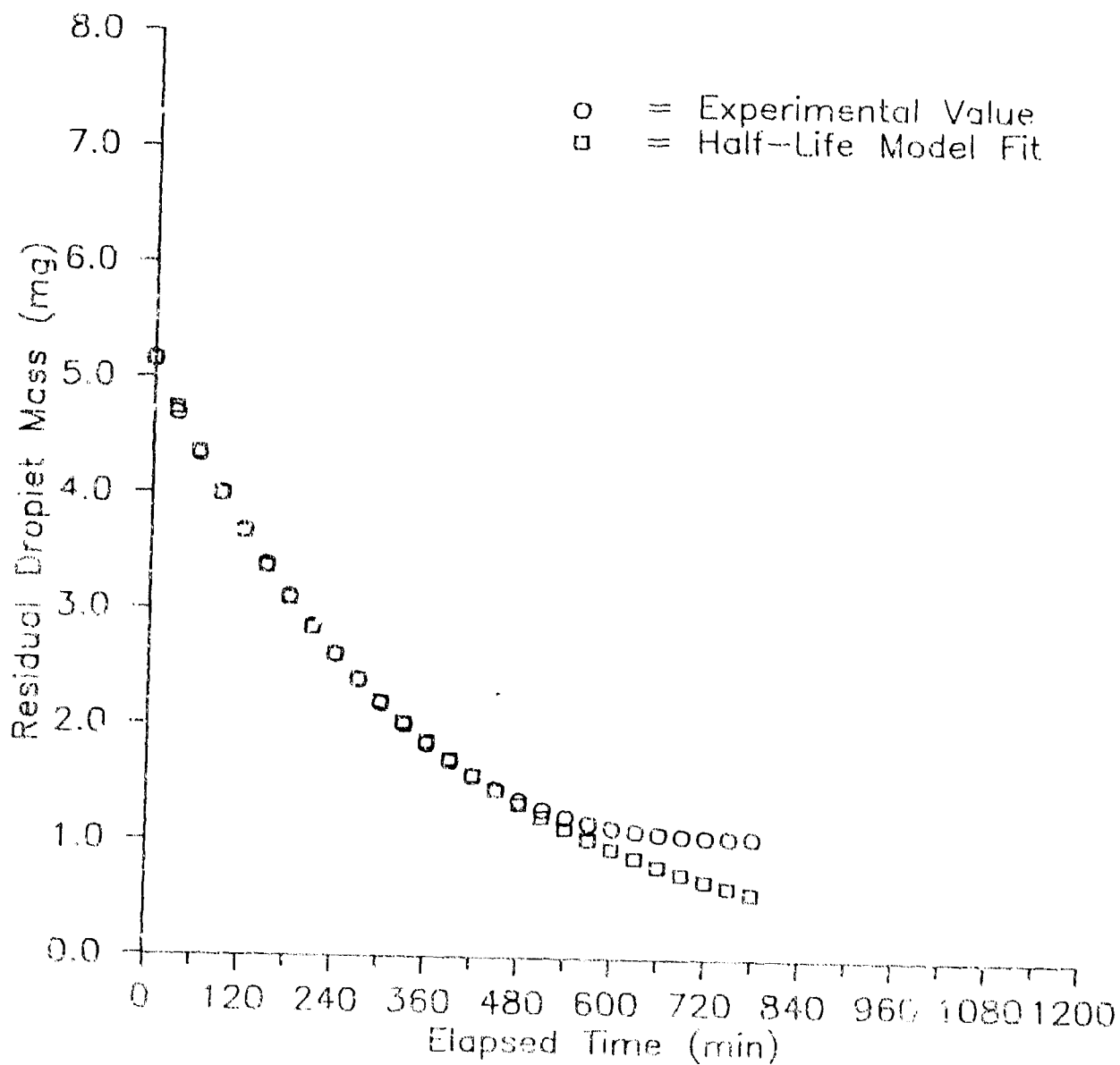


Figure G-9. Droplet Residual Mass Versus Time.

EVAPORATION EXPERIMENT NO. GLF10 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA, 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 50 G/SQ METER ON OAK LEAF/TOP SURFACE  
 WINDSPEED 2.3 MPH, AIR TEMPERATURE 60 DEG F, RELATIVE HUMIDITY 52%

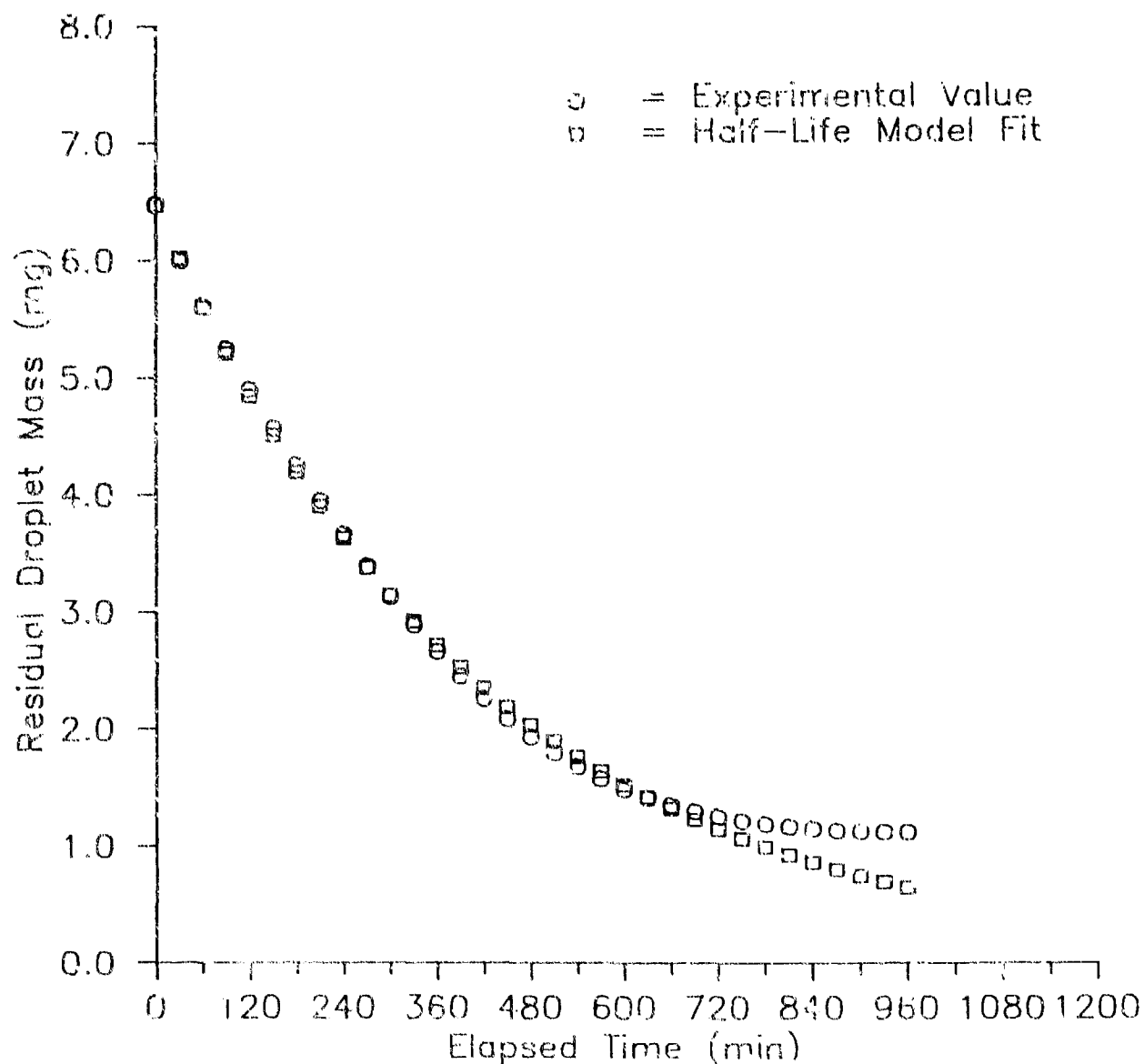


Figure G-10. Droplet Residual Mass Versus Time.

EVAPORATION EXPERIMENT NO. GLF11 SERIES ID 2-4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/TOP SURFACE  
WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 55%

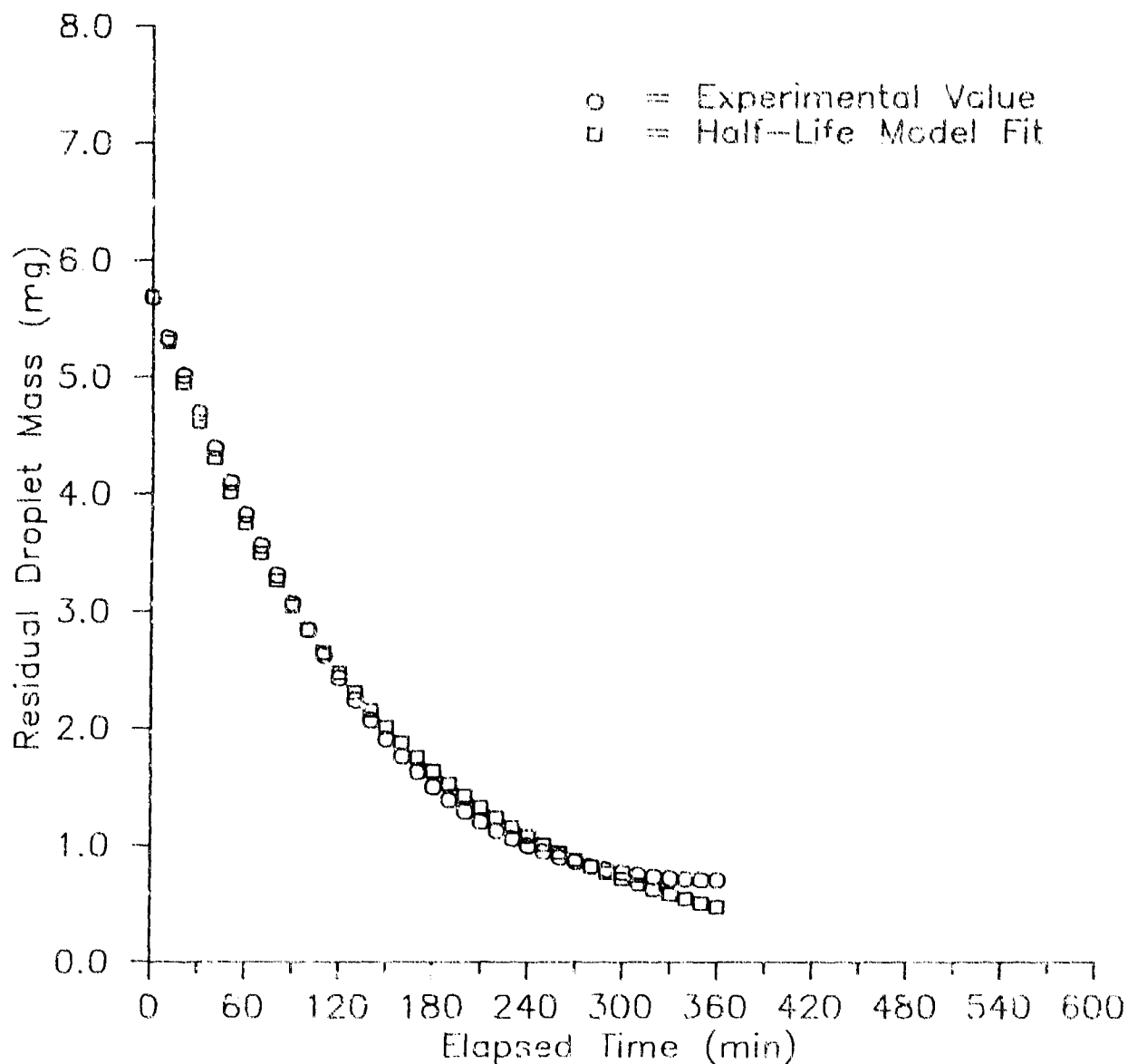


Figure G-11. Droplet Residual Mass Versus Time.

EVAPORATION EXPERIMENT NO. GLF12 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/TOP SURFACE  
WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 40%

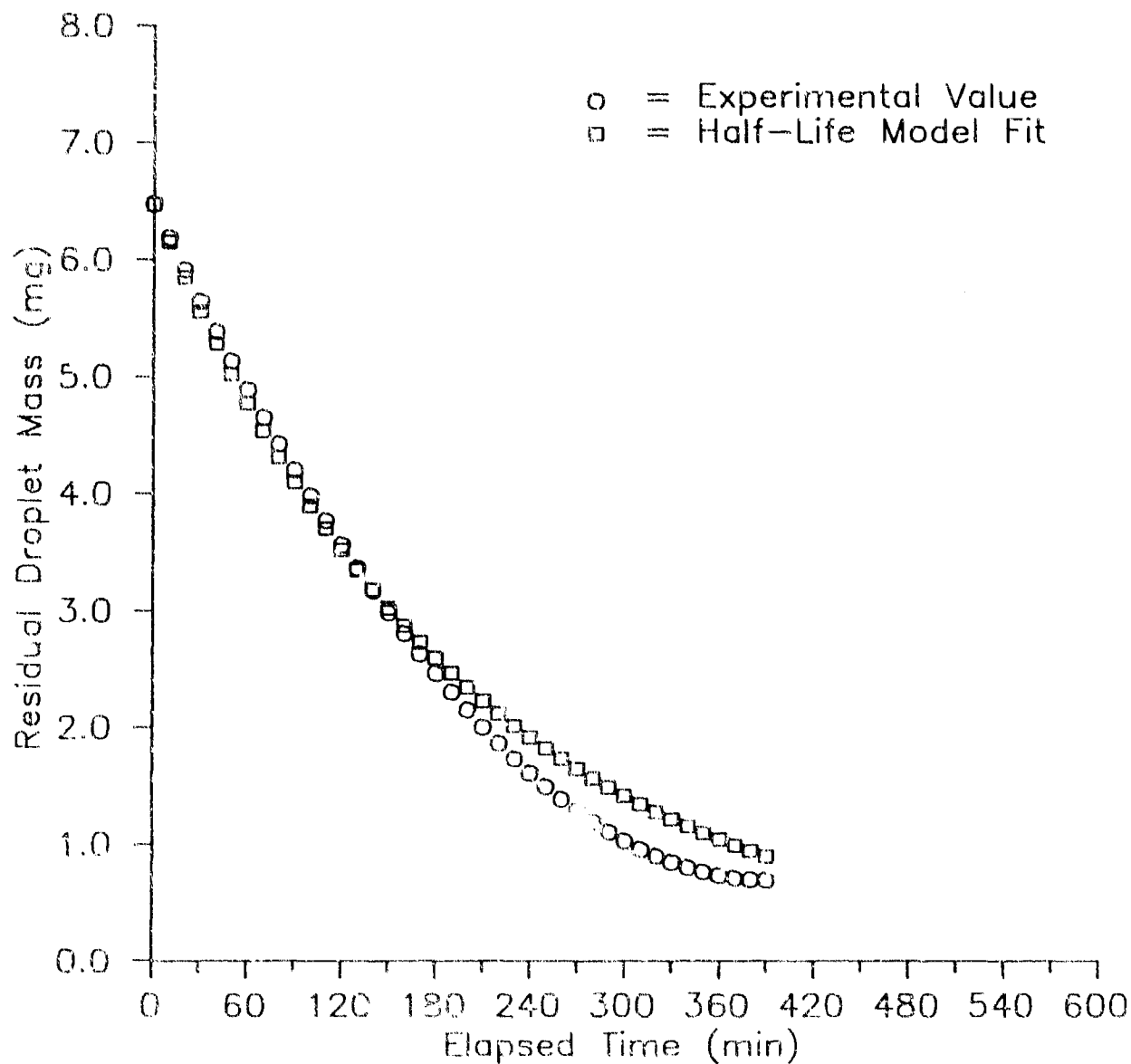


Figure G-12. Droplet Residual Mass Versus Time.

EVAPORATION EXPERIMENT NO. GLF13 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/BOTTOM SURFACE  
WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 44%

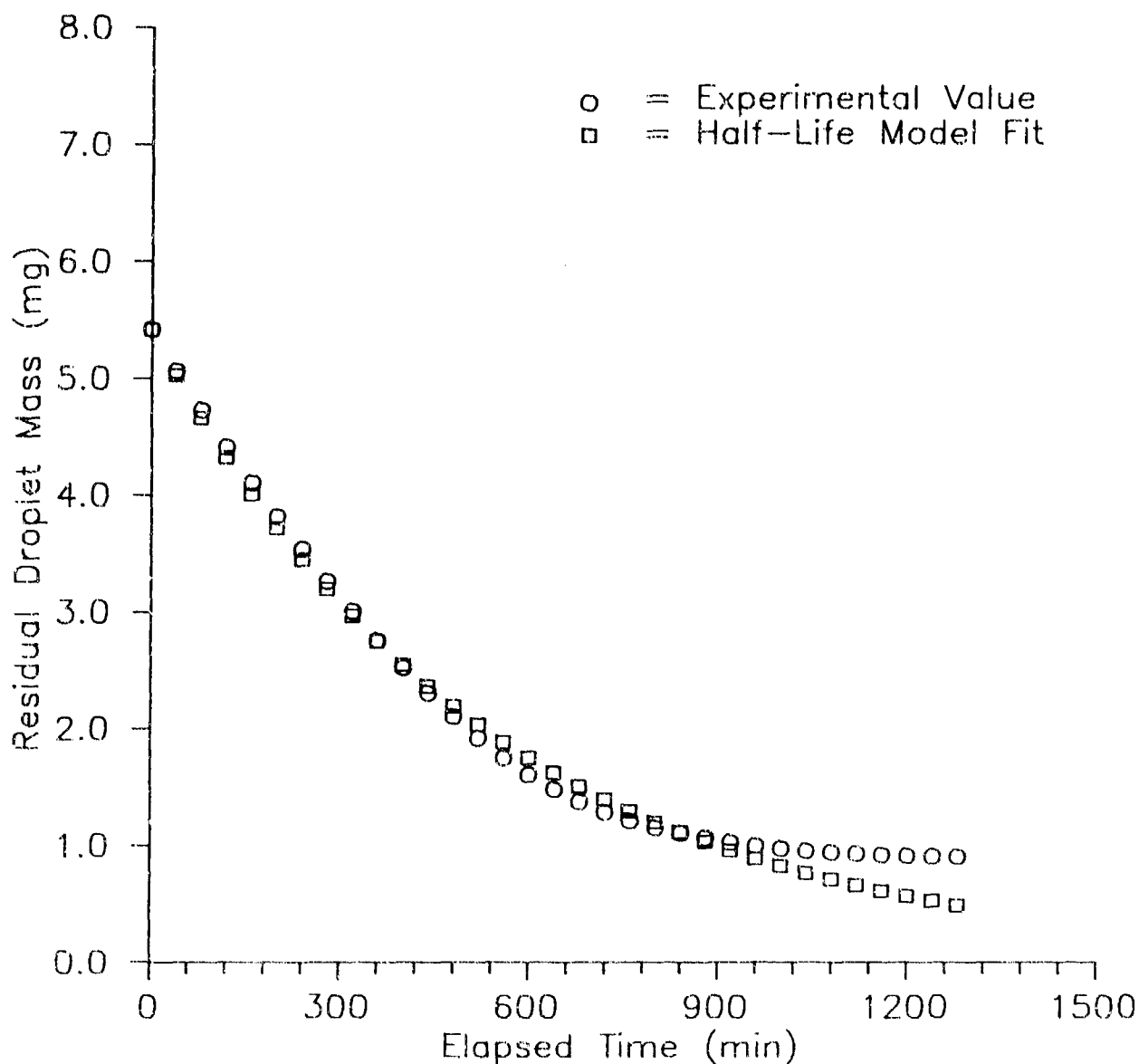


Figure G-13. Droplet Residual Mass Versus Time.



EVAPORATION EXPERIMENT NO. GLF14 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/BOTTOM SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 43%

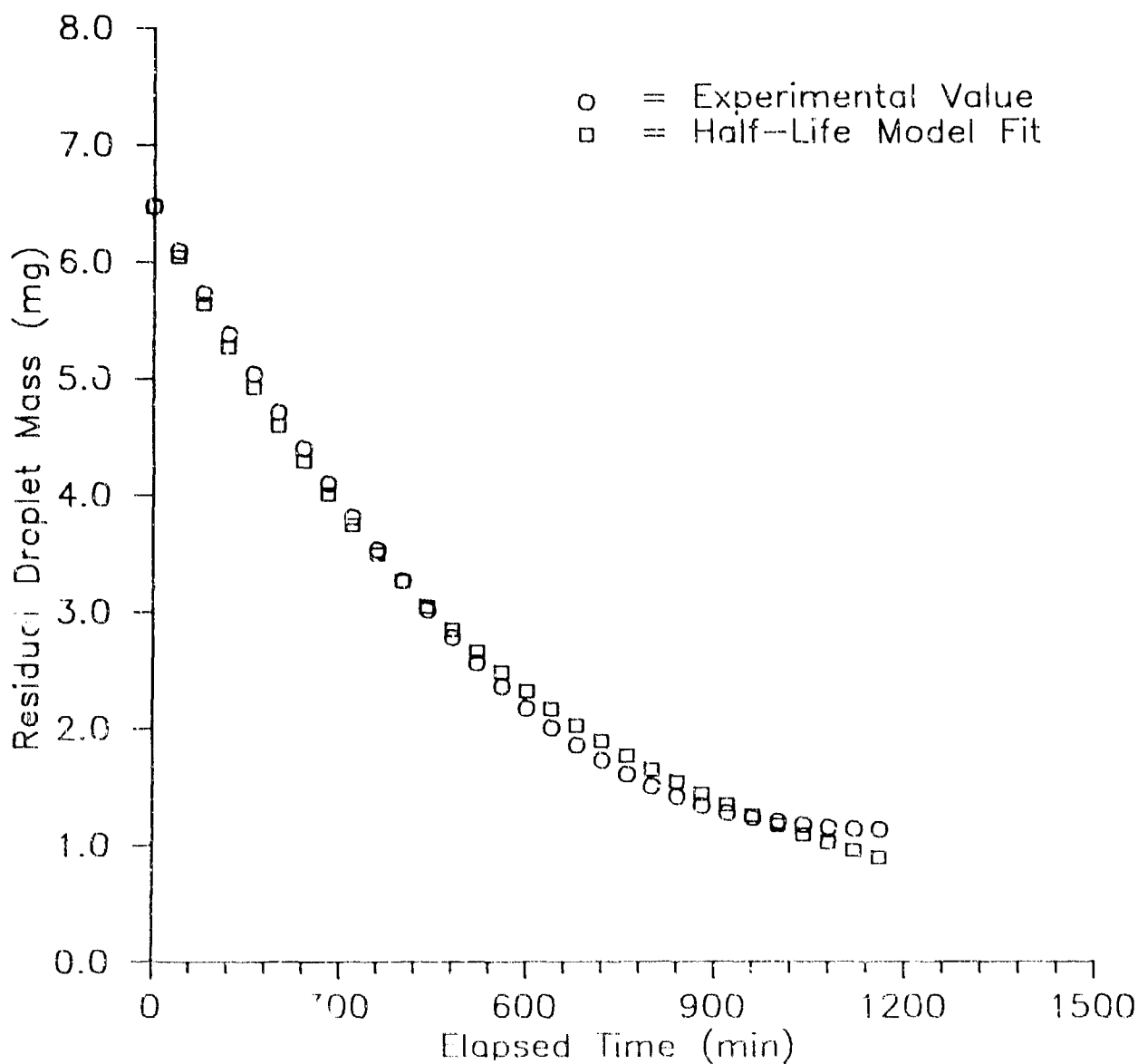


Figure G-14. Droplet Residual Mass Versus Time.

EVAPORATION EXPERIMENT NO. GLF15 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/BOTTOM SURFACE  
WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

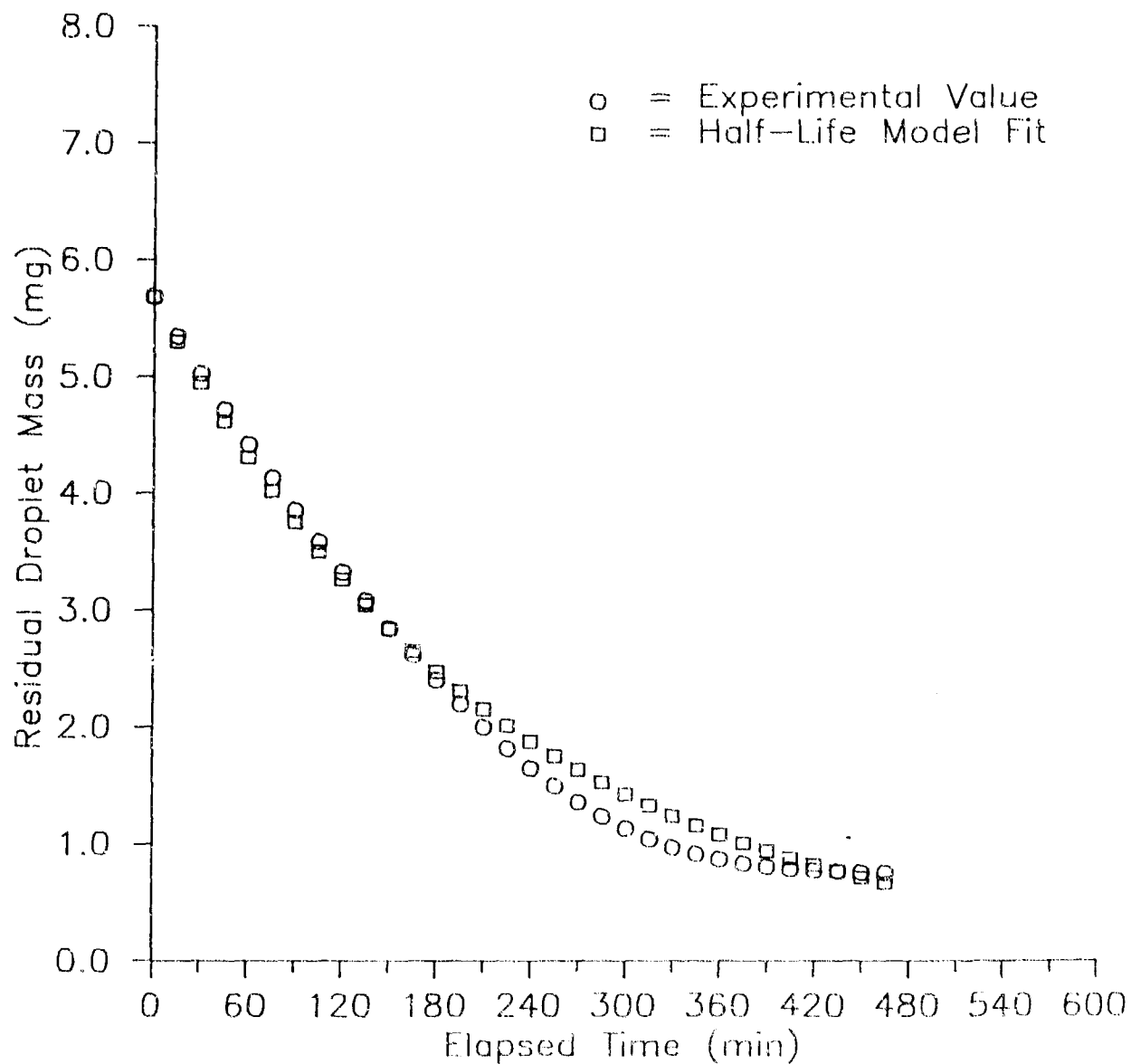


Figure G-15. Droplet Residual Mass Versus Time.

EVAPORATION EXPERIMENT NO. SLF16 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/BOTTOM SURFACE  
WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

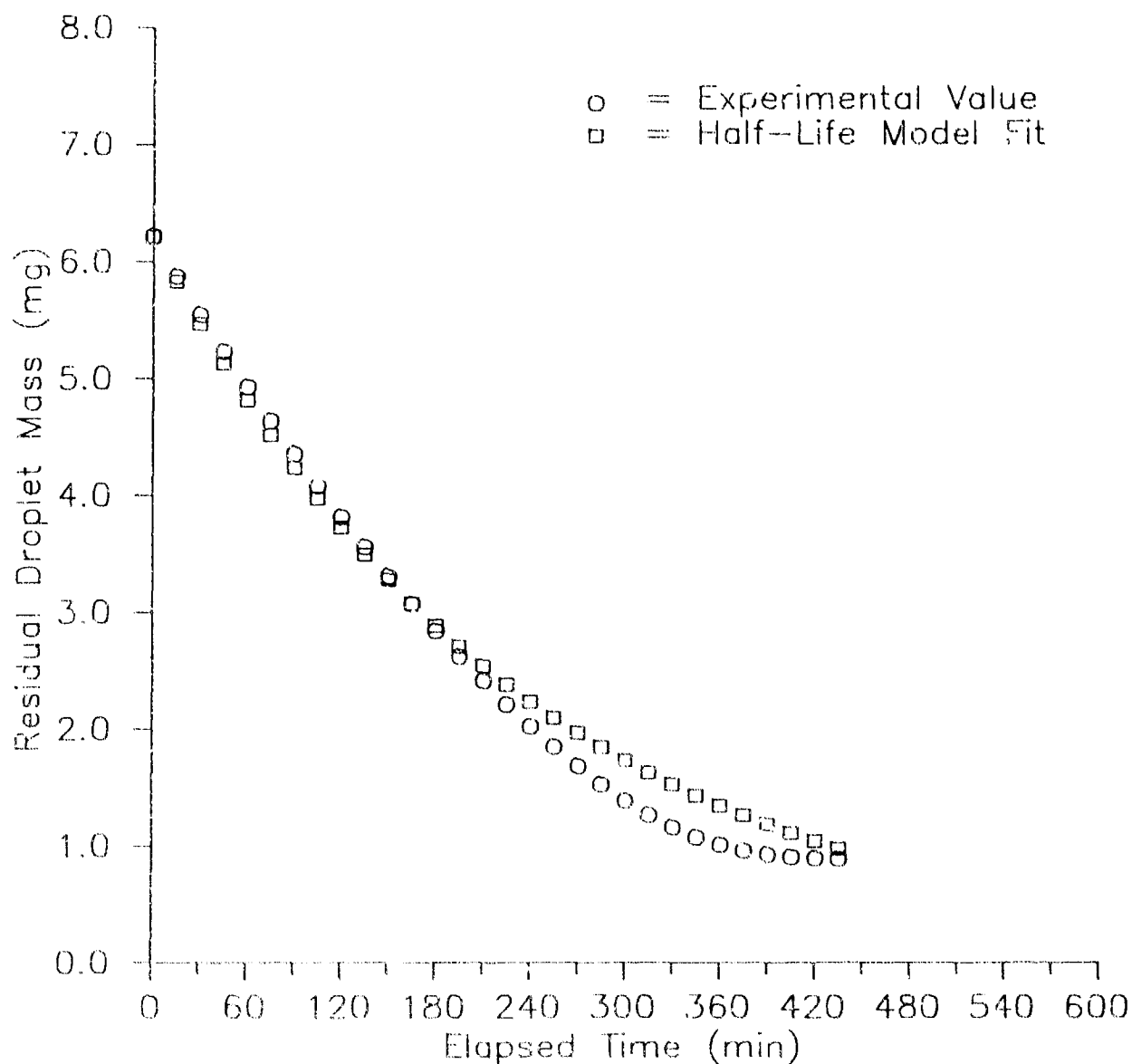


Figure G-16. Droplet Residual Mass Versus Time.

EVAPORATION EXPERIMENT NO. BLF1    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/TOP SURFACE  
WINDSPEED 3 MPH,    AIR TEMPERATURE 60 DEG F.,    RELATIVE HUMIDITY 39%

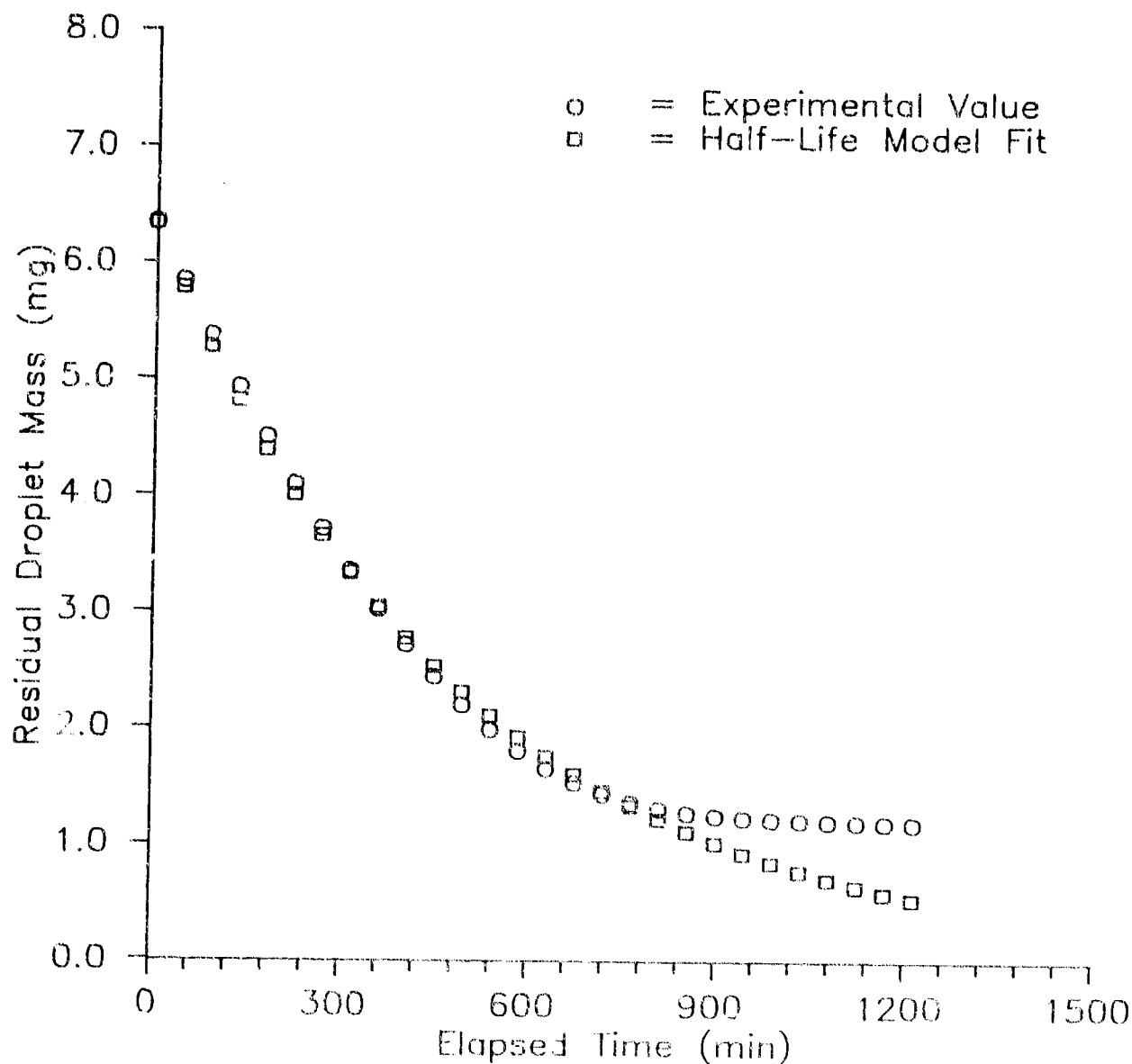


Figure G-17. Droplet Residual Mass Versus Time.

EVAPORATION EXPERIMENT NO. BLF2    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/TOP SURFACE  
 WINDSPEED 2.9 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 39%

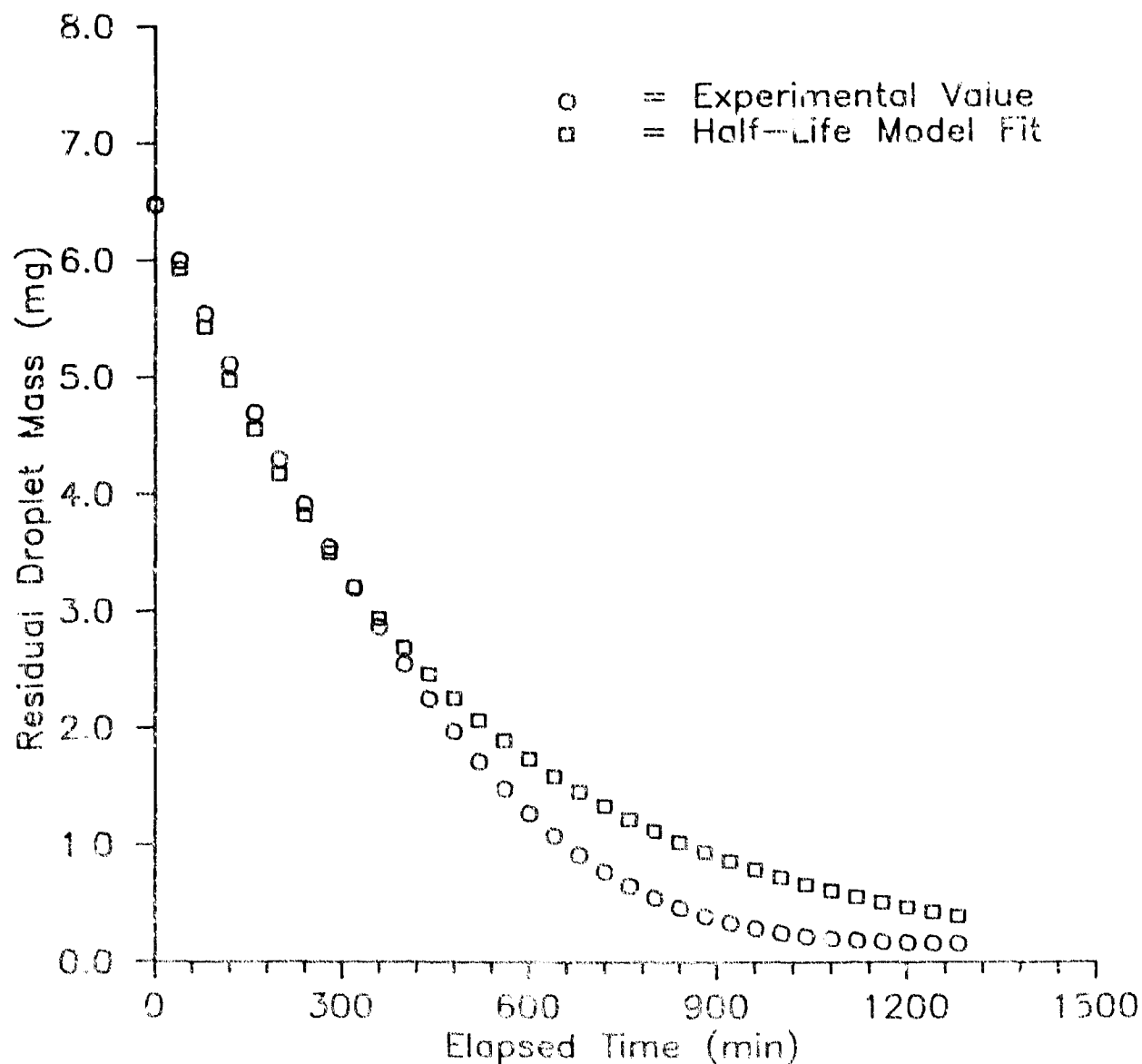


Figure G-18. Droplet Residual Mass Versus Time.

EVAPORATION EXPERIMENT NO. BLF3    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/TOP SURFACE  
 WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

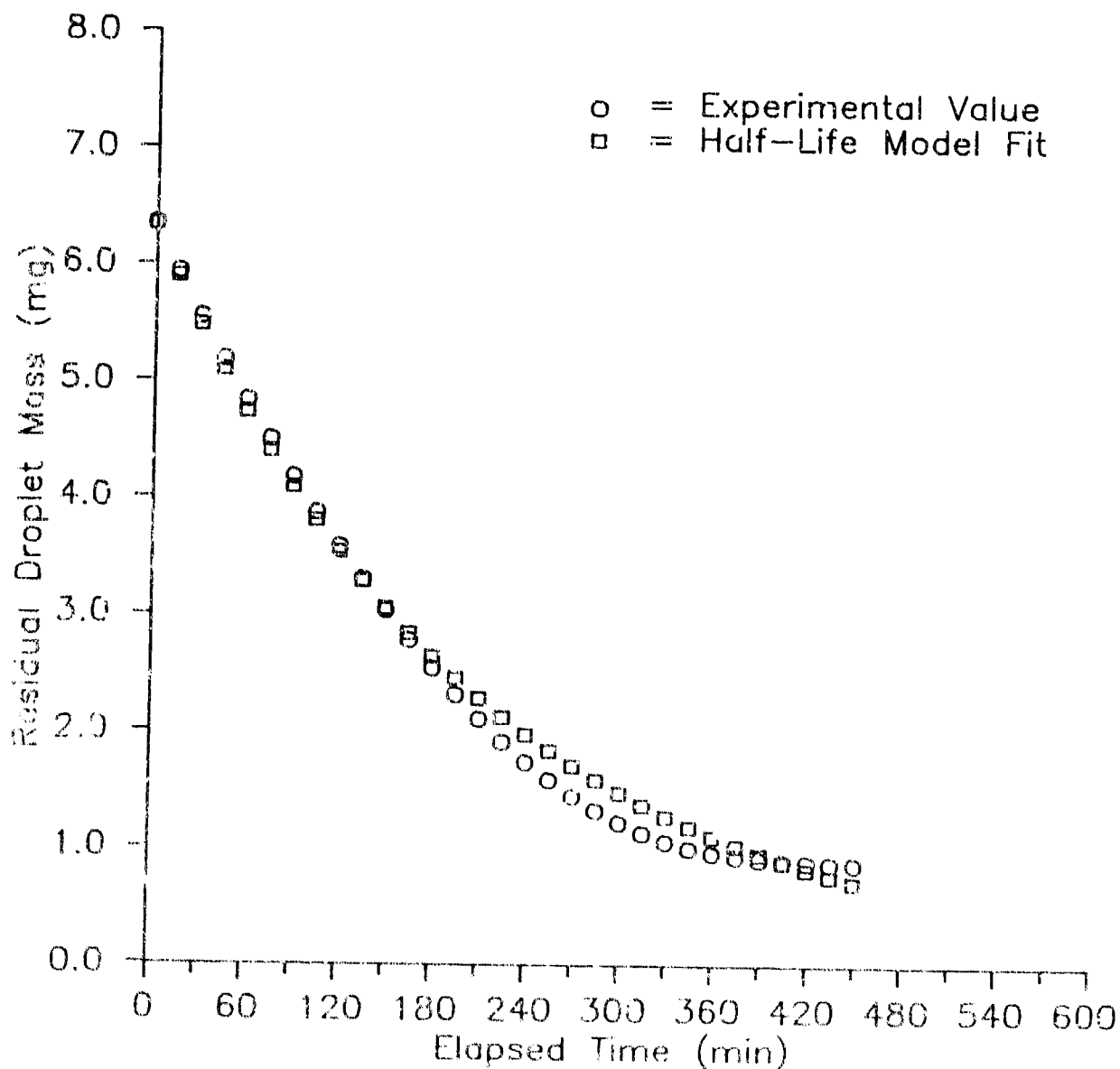


Figure G-19 Droplet Residual Mass Versus Time.

EVAPORATION EXPERIMENT NO. BLF4    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/TOP SURFACE  
WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 20%

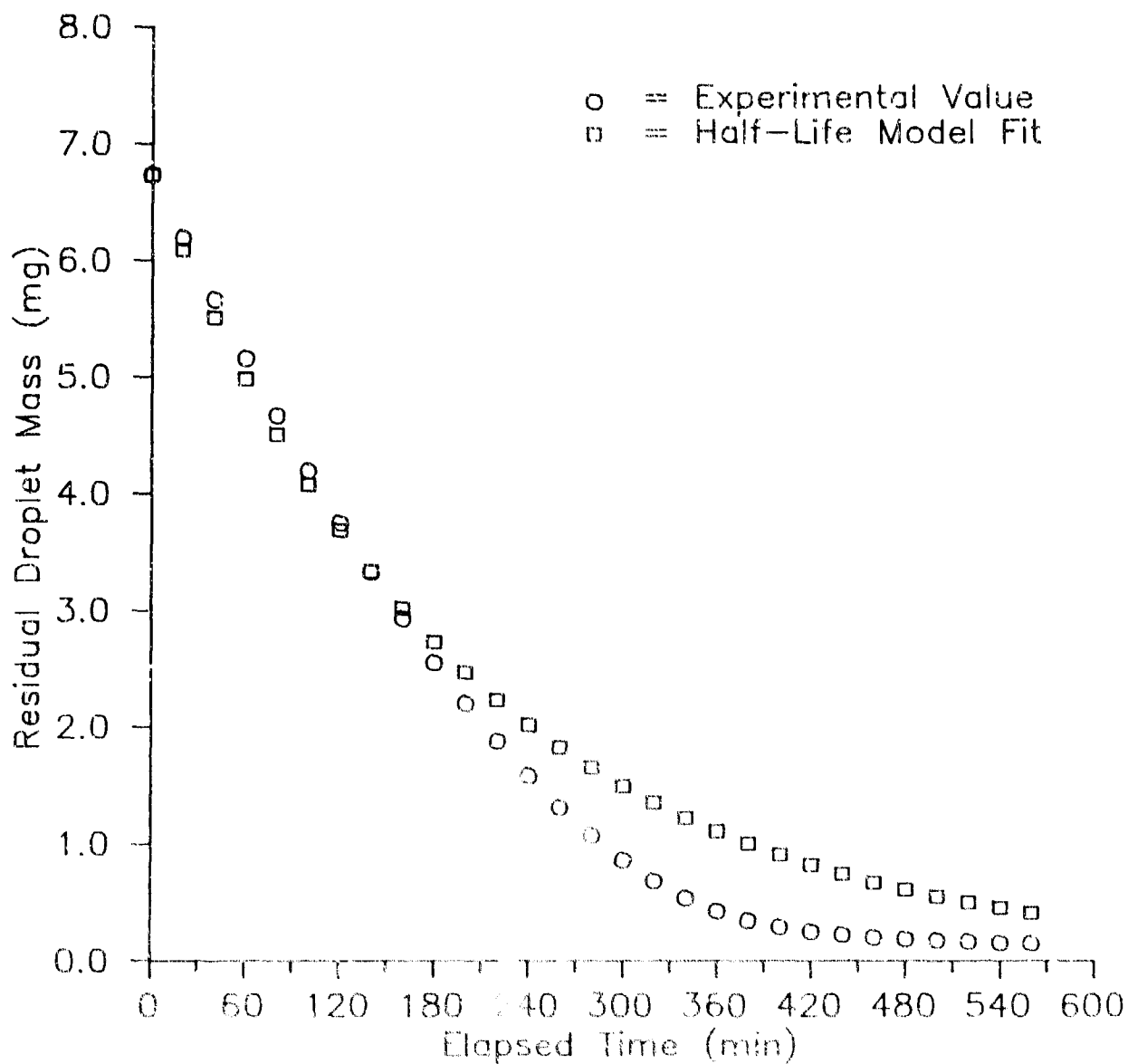


Figure G-20. Droplet Residual Mass Versus Time.

EVAPORATION EXPERIMENT NO. BLF5    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/BOTTOM SURFACE  
WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

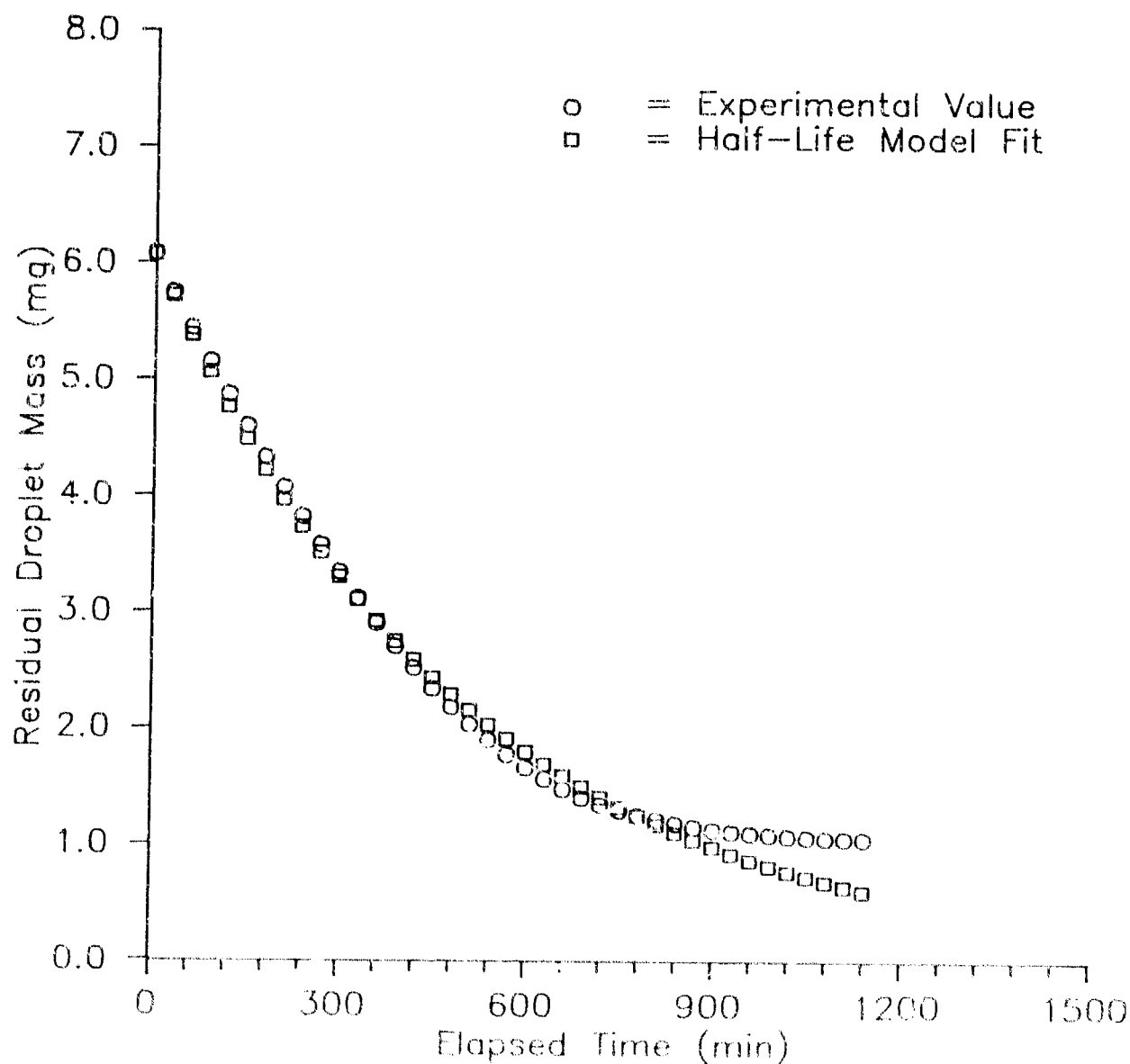


Figure G-21. Droplet Residual Mass Versus Time.



EVAPORATION EXPERIMENT NO. BLF6 SERIES ID 2004 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/BOTTOM SURFACE  
 WINDSPEED 2.9 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

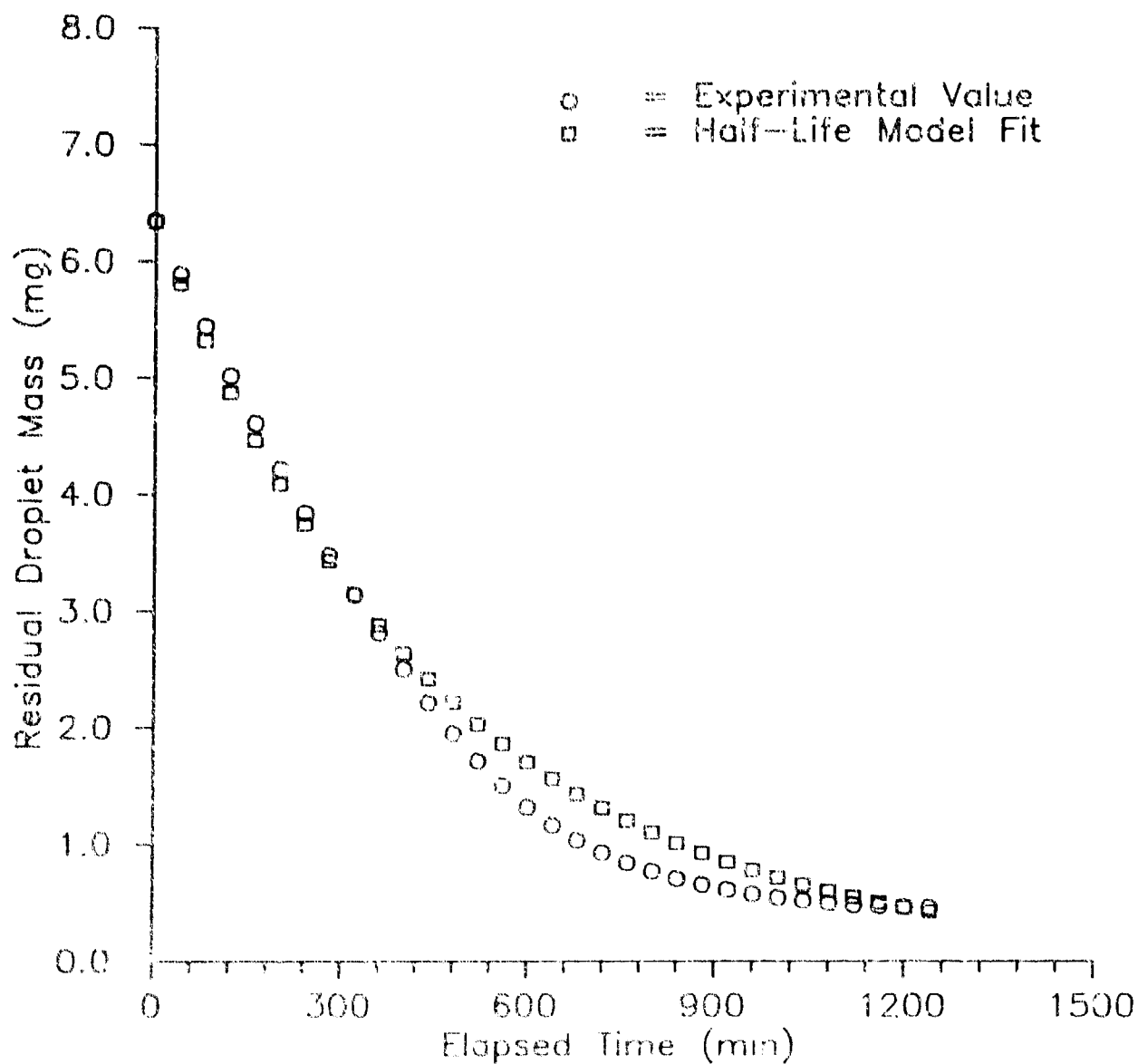


Figure G-22 Droplet Residual Mass Versus Time.

EVAPORATION EXPERIMENT NO. BLF7    SERIES ID 2++4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/BOTTOM SURFACE  
WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

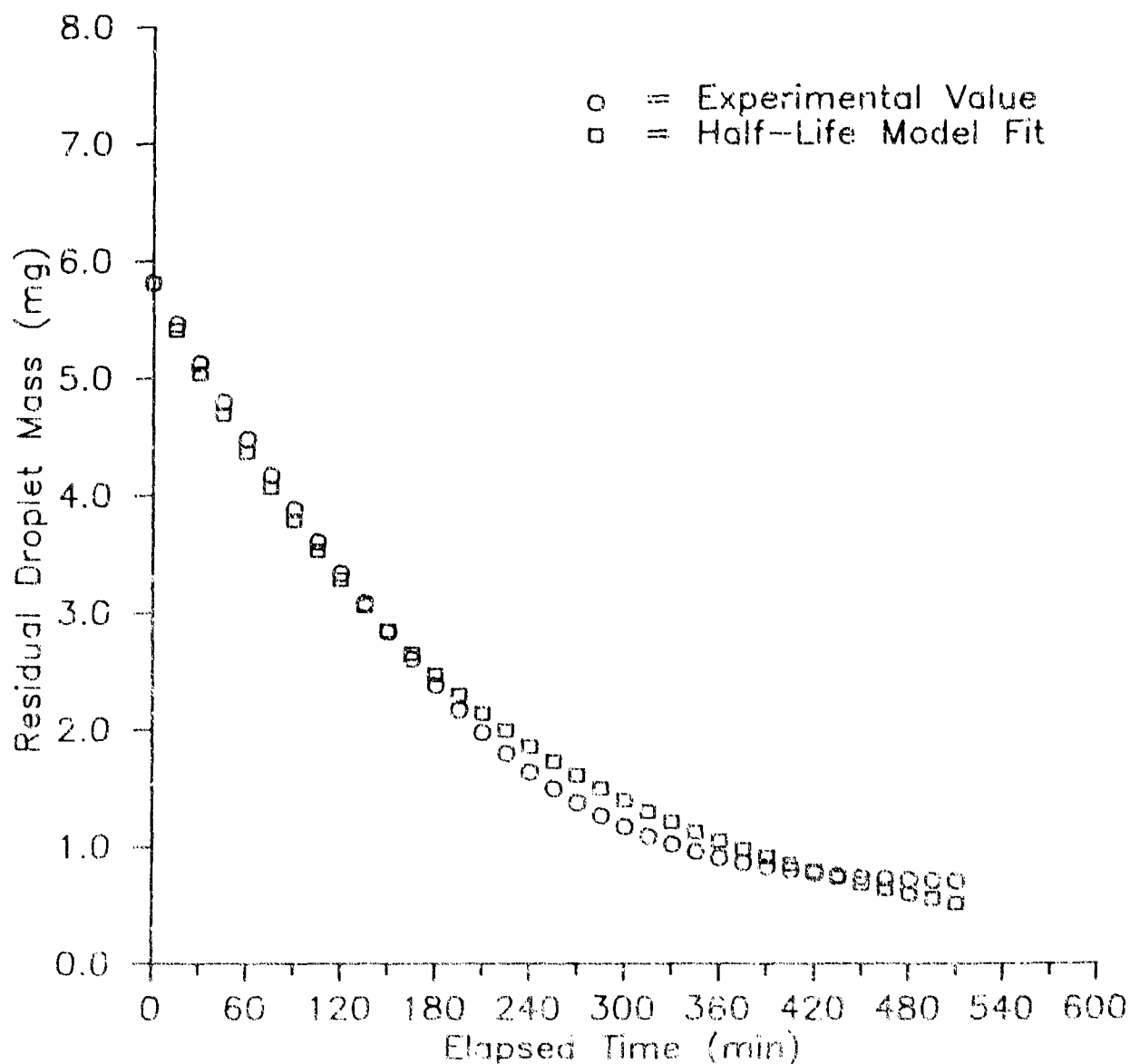


Figure G-23. Droplet Residual Mass Versus Time.

EVAPORATION EXPERIMENT NO. BLE8    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/BOTTOM SURFACE  
 WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 50%

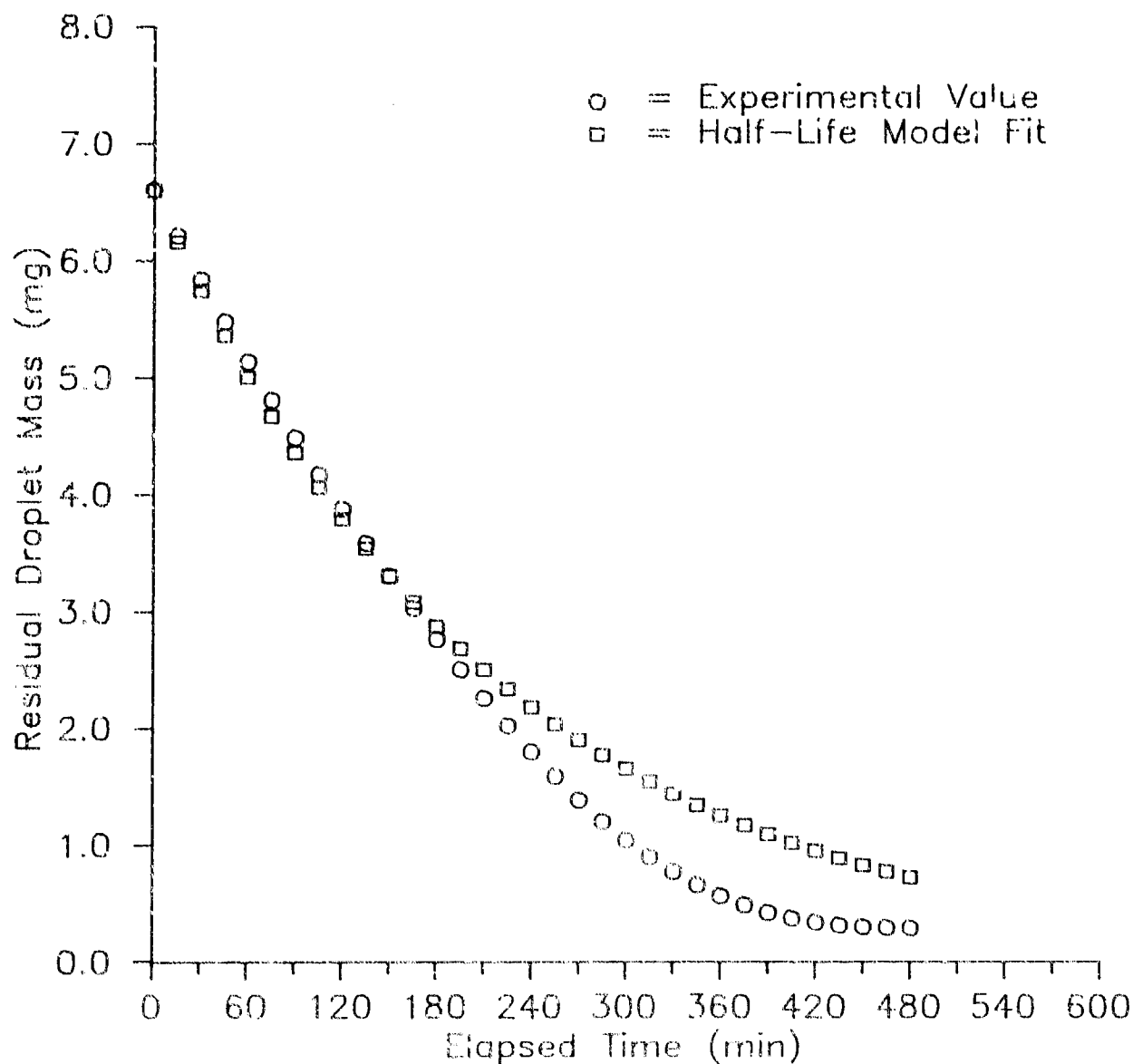


Figure C-24. Droplet Residual Mass Versus Time.

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APPENDIX H  
PLOTS OF DROPLET EVAPORATION RATE VERSUS TIME

EVAPORATION EXPERIMENT NO. GLF1    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA.,    100 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/TOP SURFACE  
WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F.,    RELATIVE HUMIDITY 45%

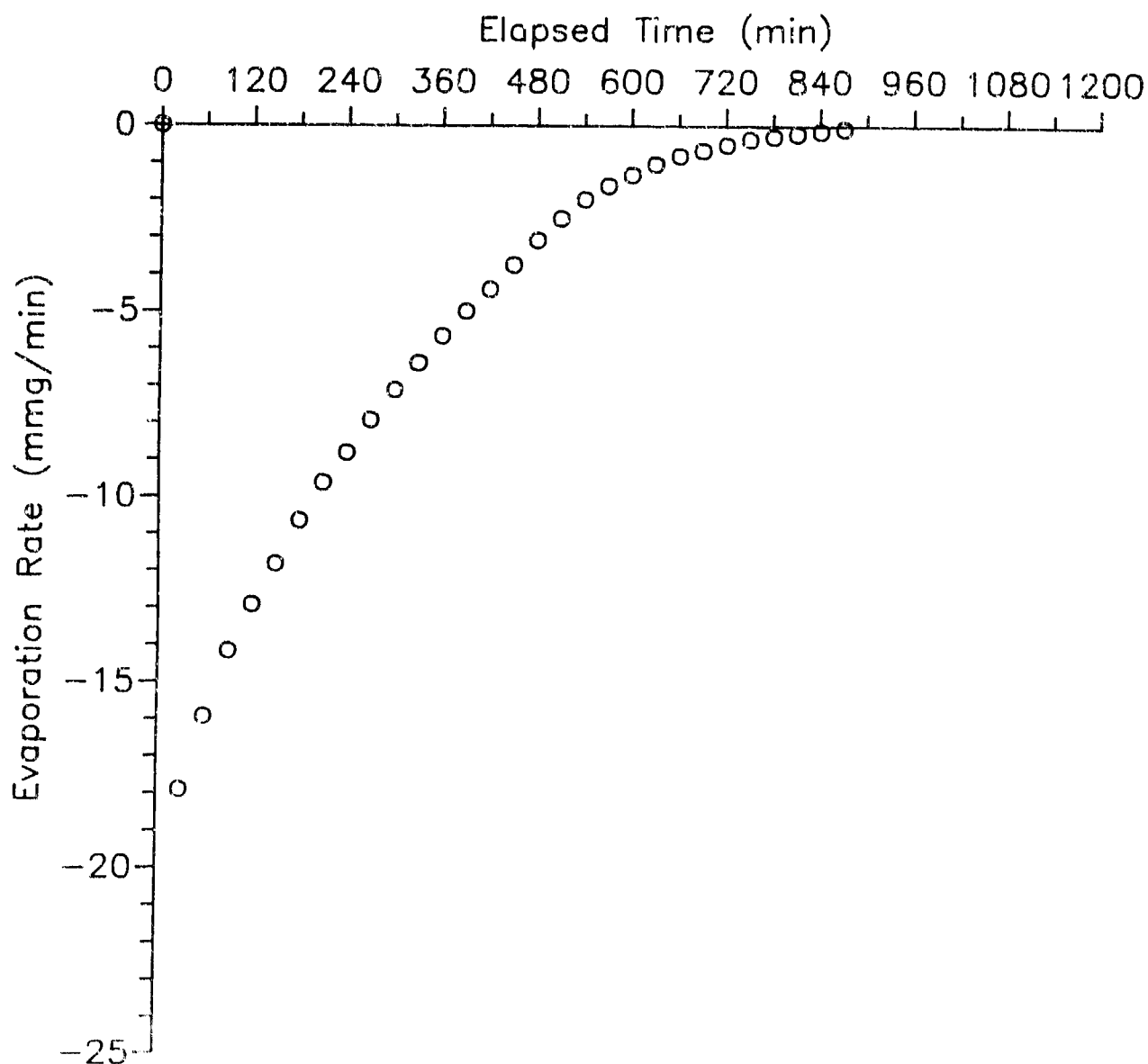


Figure H-1. Droplet Evaporation Rate Versus Time.

EVAPORATION EXPERIMENT NO. GLF2    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/TOP SURFACE  
WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

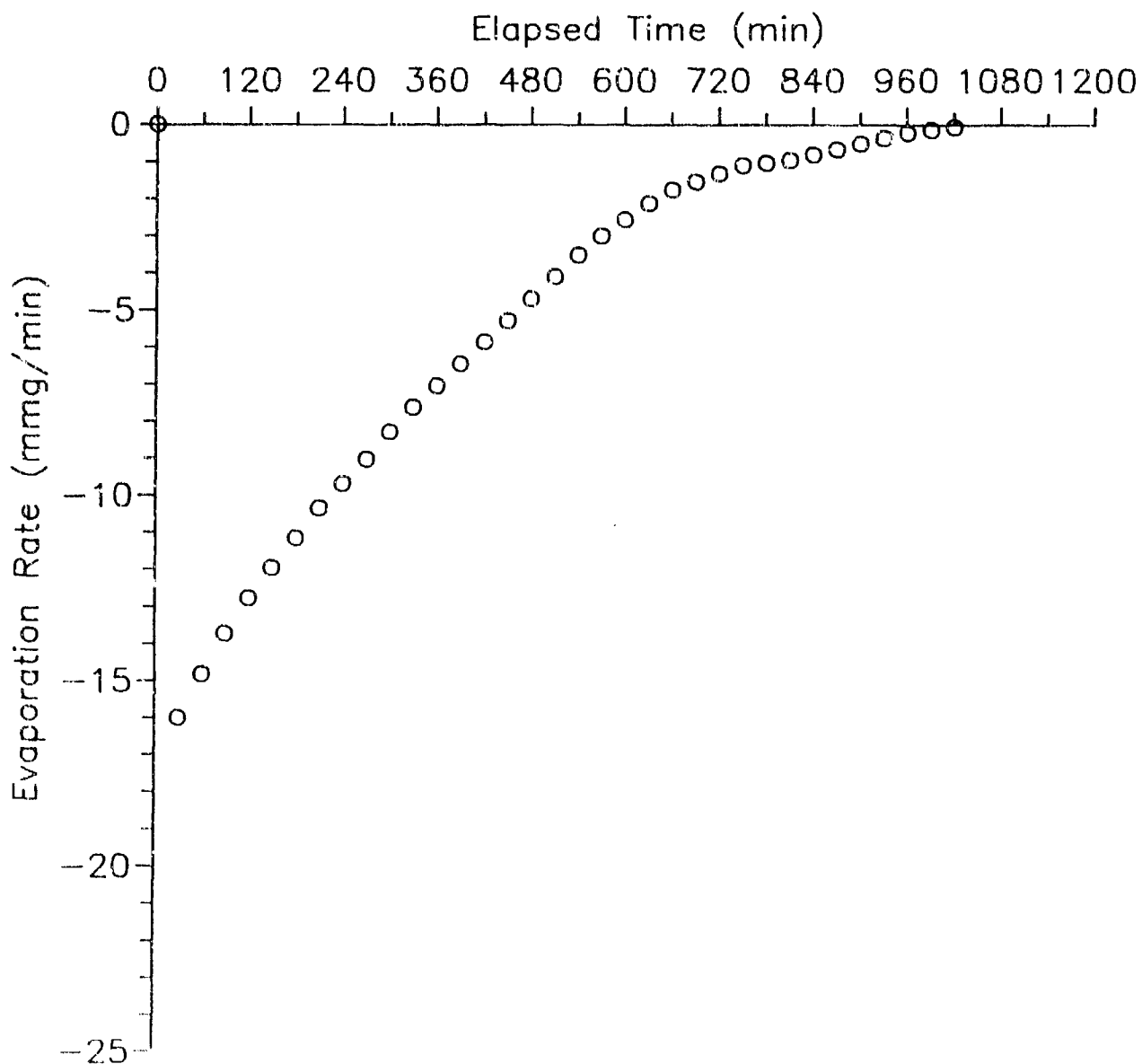


Figure H-2. Droplet Evaporation Rate Versus Time.

EVAPORATION EXPERIMENT NO. GLF3    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/TOP SURFACE  
WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 40%

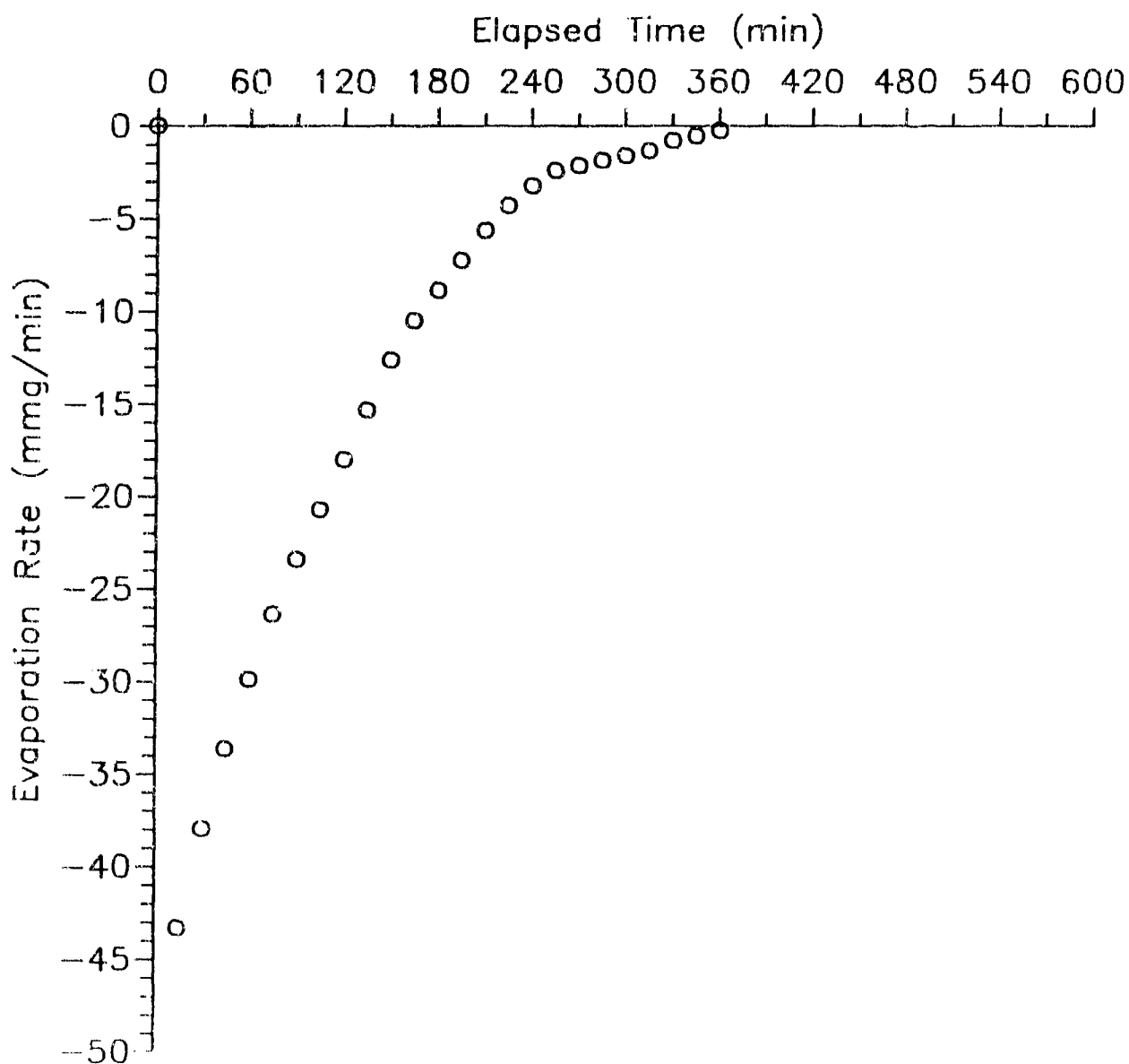


Figure H-3. Droplet Evaporation Rate Versus Time.



EVAPORATION EXPERIMENT NO. GLF4    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/TOP SURFACE  
WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

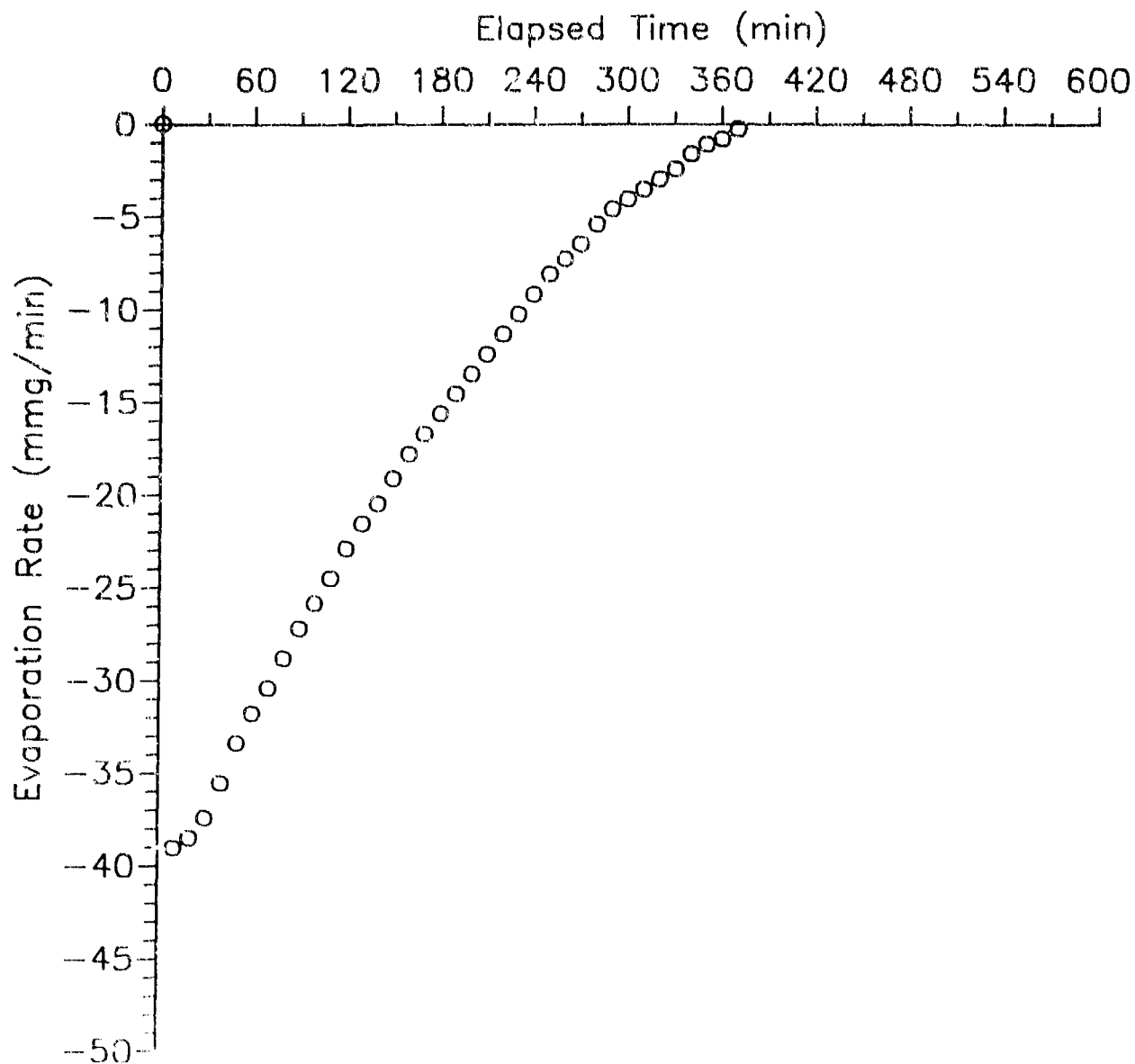


Figure H-4. Droplet Evaporation Rate Versus Time.

EVAPORATION EXPERIMENT NO. GLF5    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/BOTTOM  
WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 58%

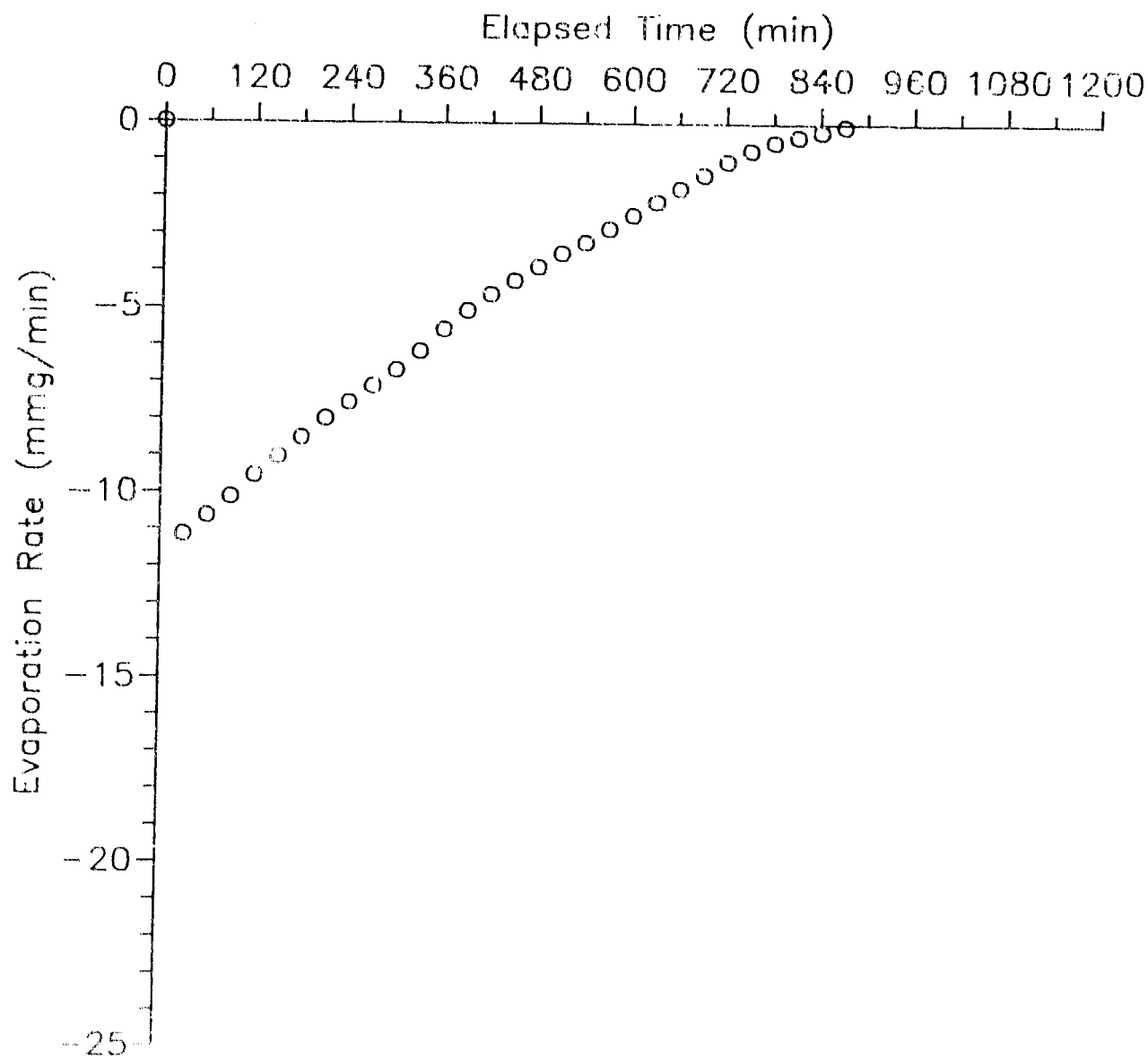


Figure H-5. Droplet Evaporation Rate Versus Time

EVAPORATION EXPERIMENT NO. GLF6    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/BOTTOM  
WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 55%

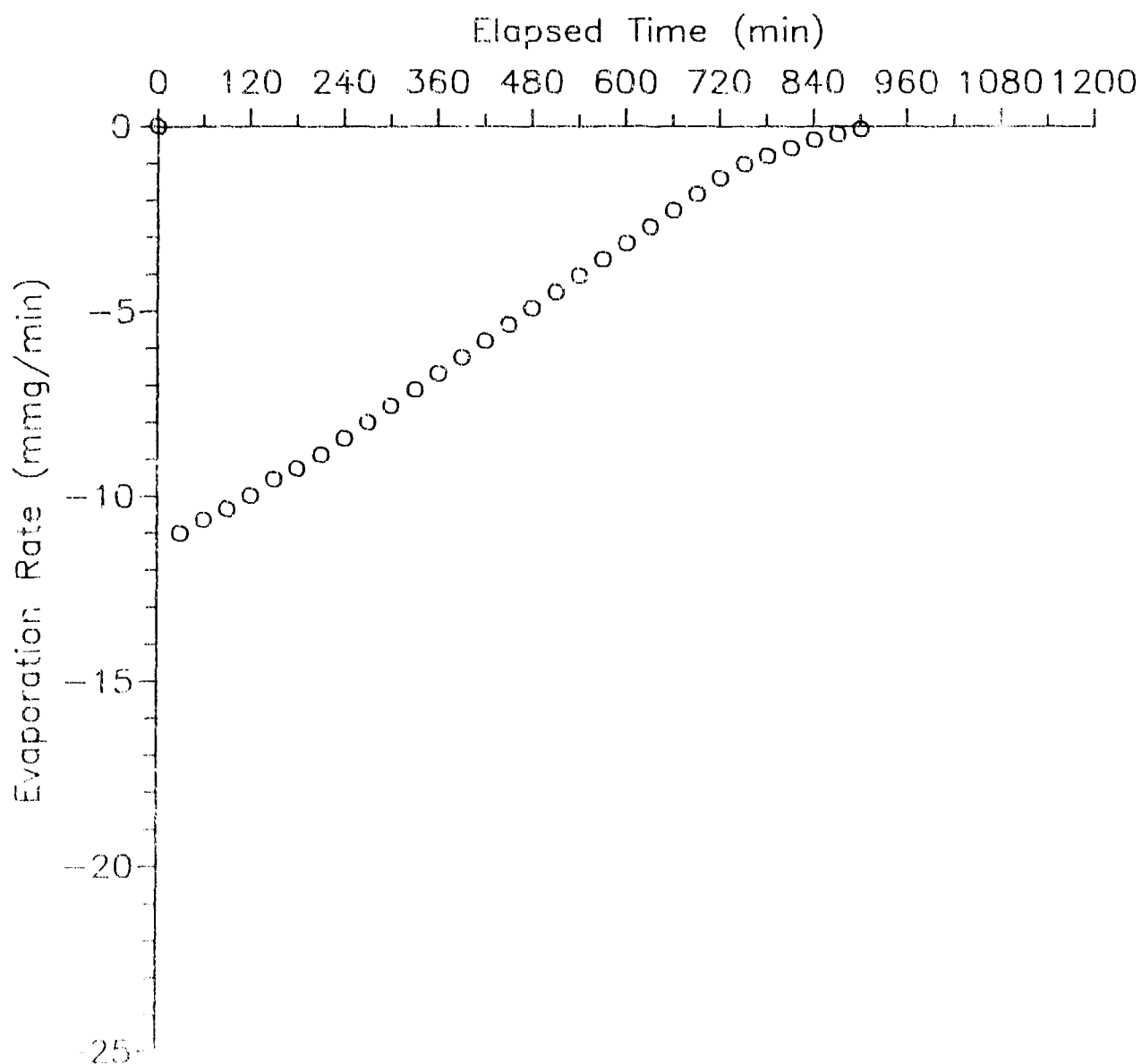


Figure H-6. Droplet Evaporation Rate Versus Time.

EVAPORATION EXPERIMENT NO. GLF7    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/BOTTOM  
WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

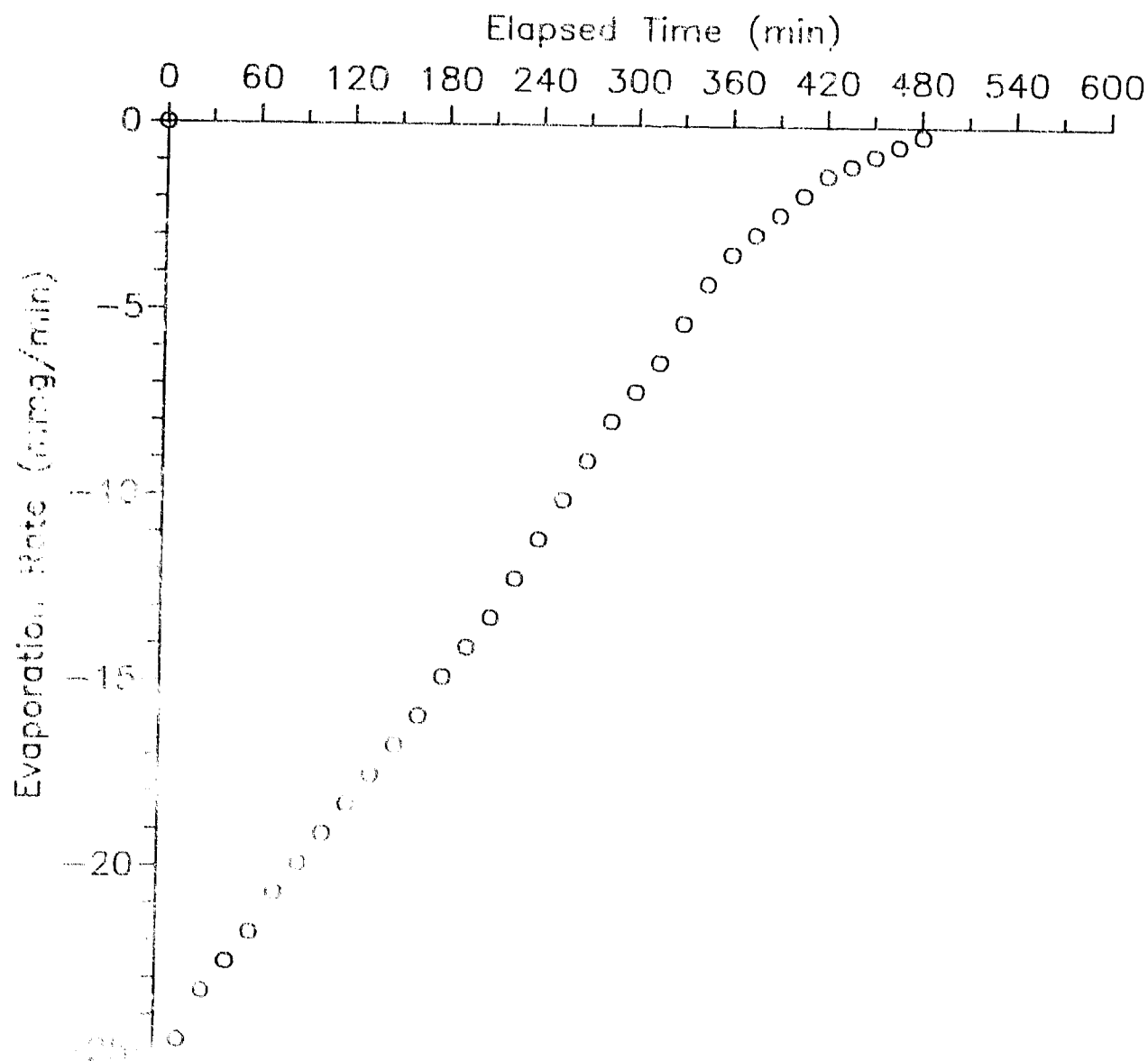


Figure H-7. Droplet Evaporation Rate Versus Time.

EVAPORATION EXPERIMENT NO. GLF8    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/BOTTOM  
WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 50%

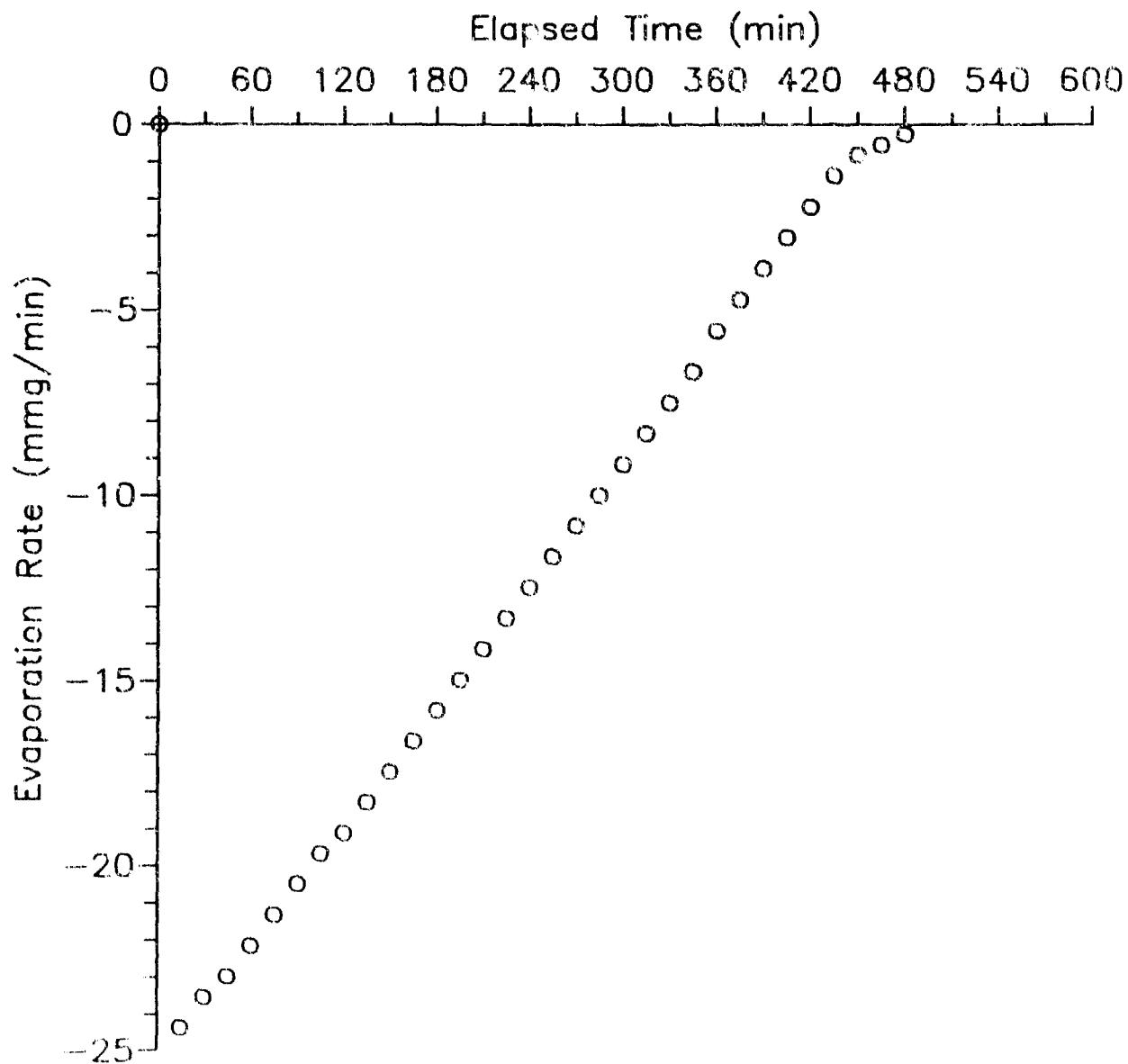


Figure H-8. Droplet Evaporation Rate Versus Time.

EVAPORATION EXPERIMENT NO. GLF9    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/TOP SURFACE  
WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 44%

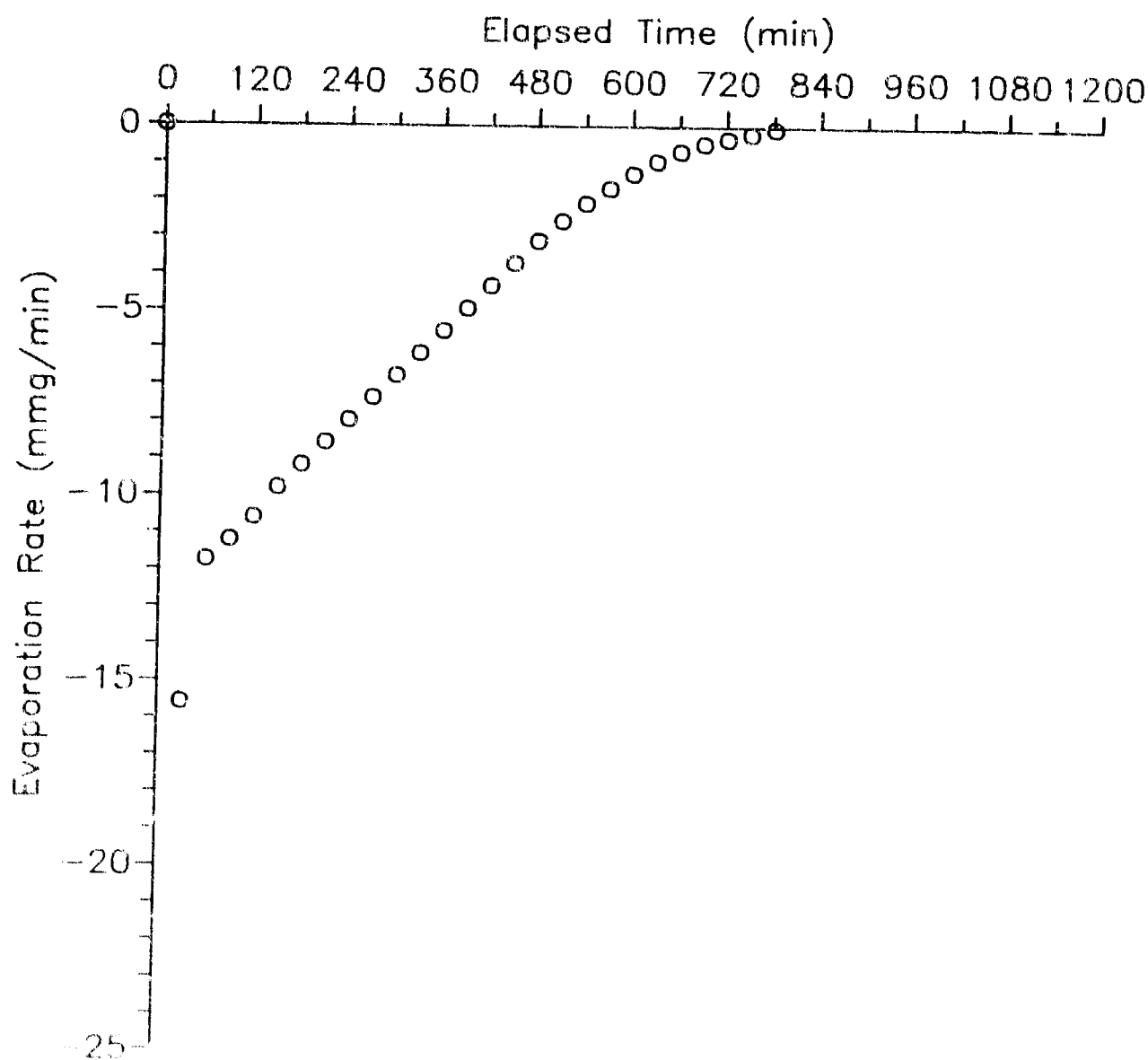


Figure H-9. Droplet Evaporation: Rate Versus Time

EVAPORATION EXPERIMENT NO. GLF10 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/TOP SURFACE  
WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 52%

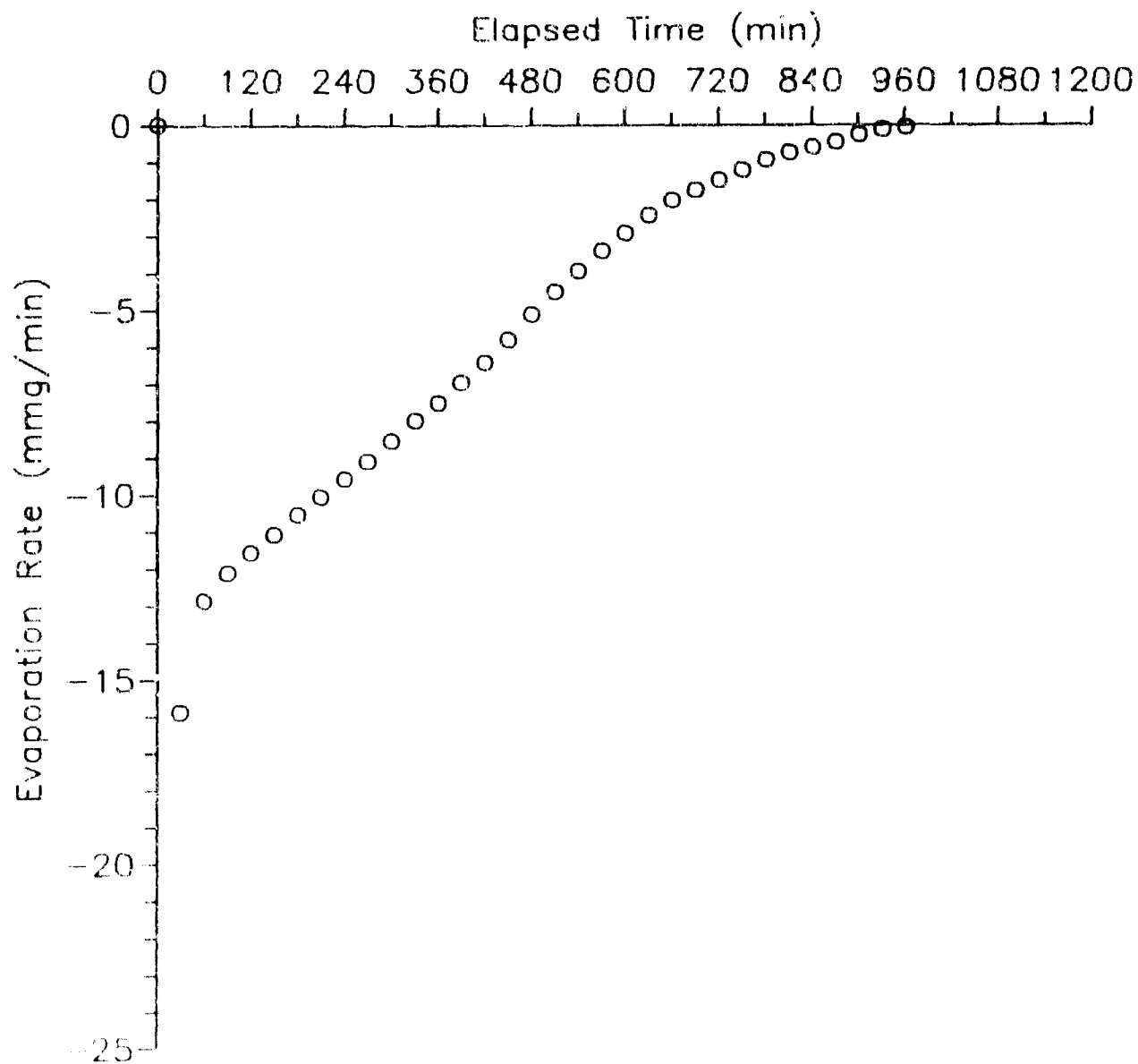


Figure H-10. Displet Evaporation Rate Versus Time.

EVAPORATION EXPERIMENT NO. GLF11 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALGNATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/TOP SURFACE  
WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 55%

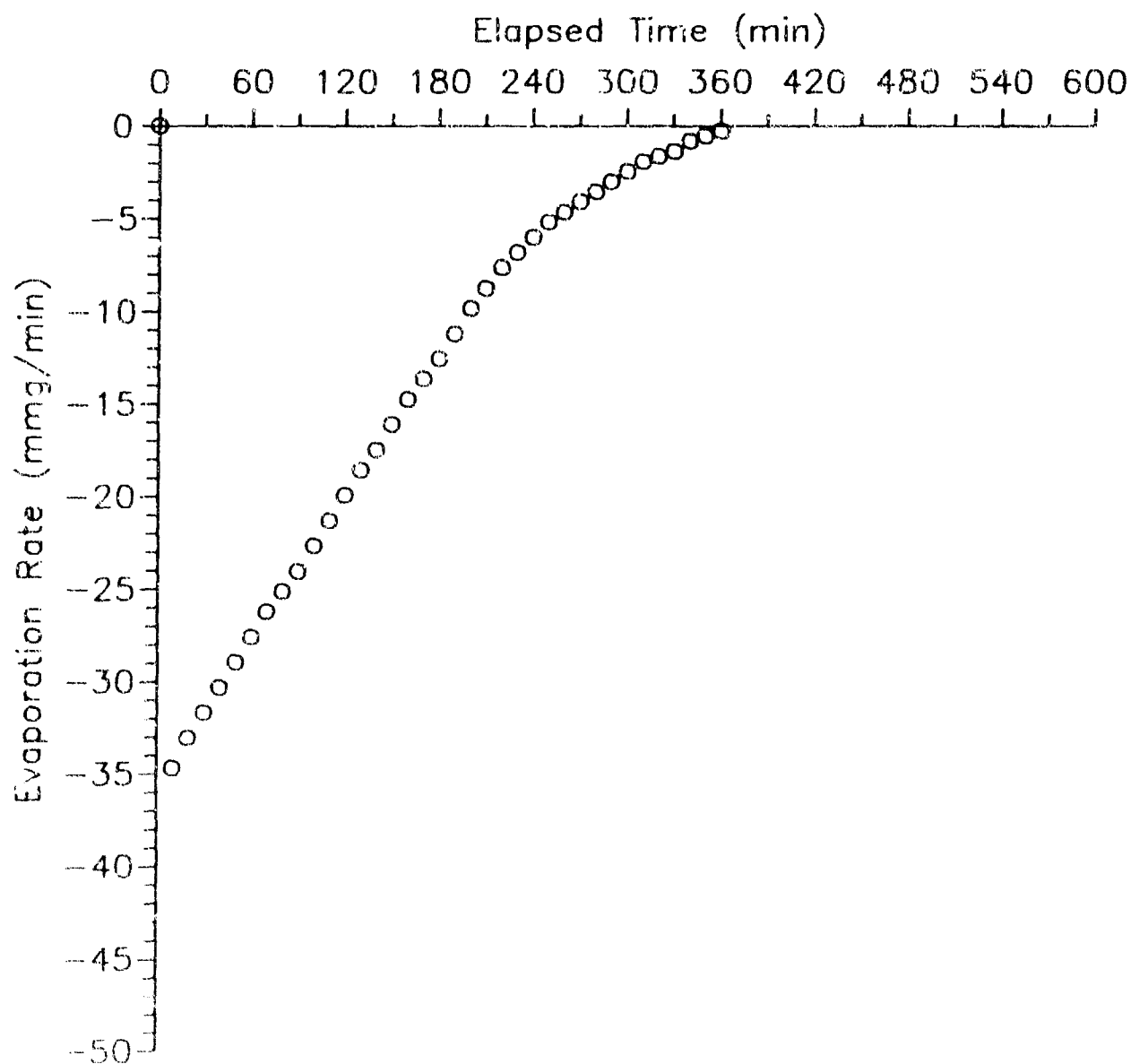


Figure H-11. Droplet Evaporation Rate Versus Time.



EVAPORATION EXPERIMENT NO. GLF12 SERIES ID 2-4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/TOP SURFACE  
WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 40%

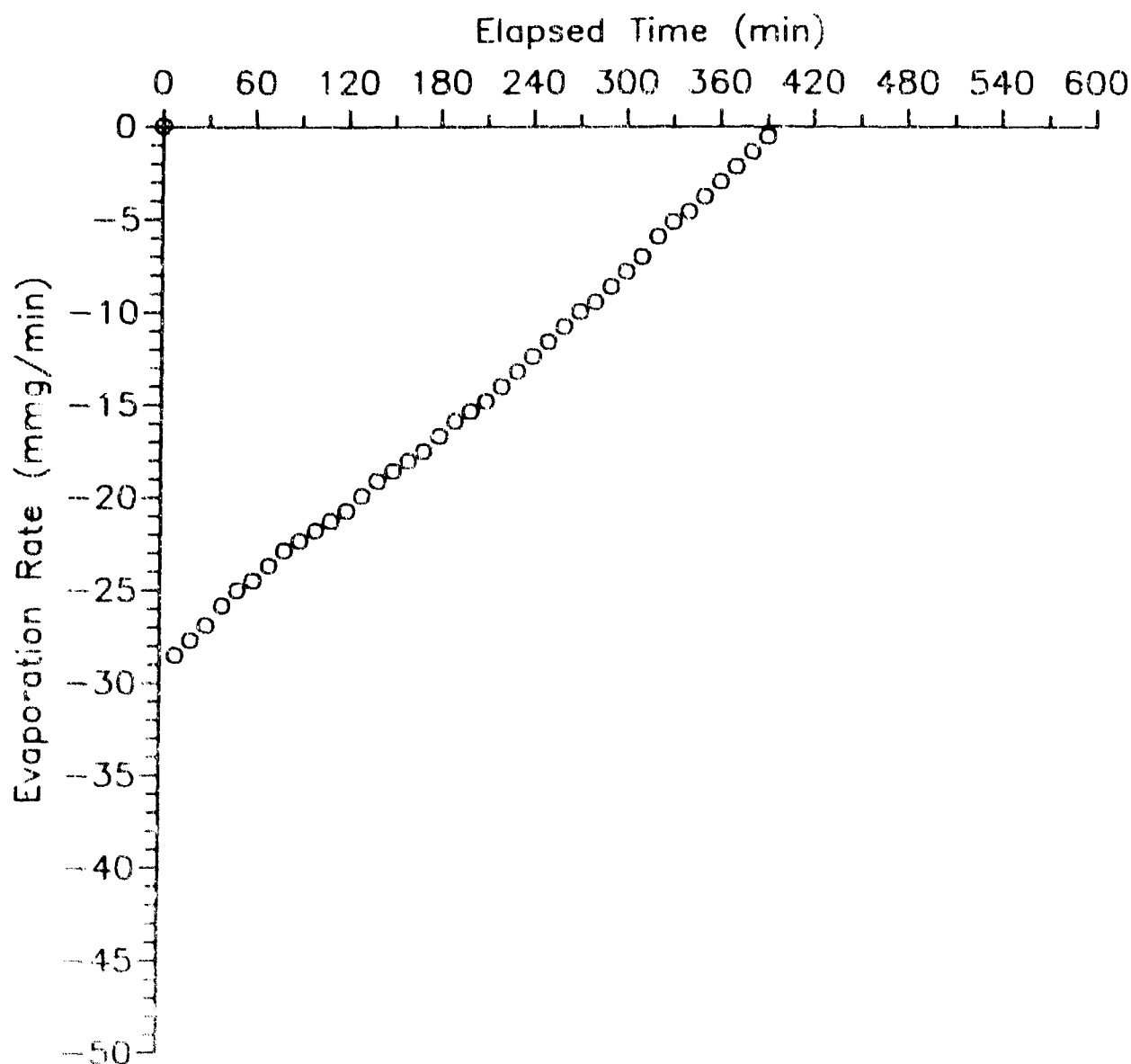


Figure H-12 Droplet Evaporation Rate Versus Time.

EVAPORATION EXPERIMENT NO. GLF13 SERIES 10 2x4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF BOTTOM SURFACE  
WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F, RELATIVE HUMIDITY 44%

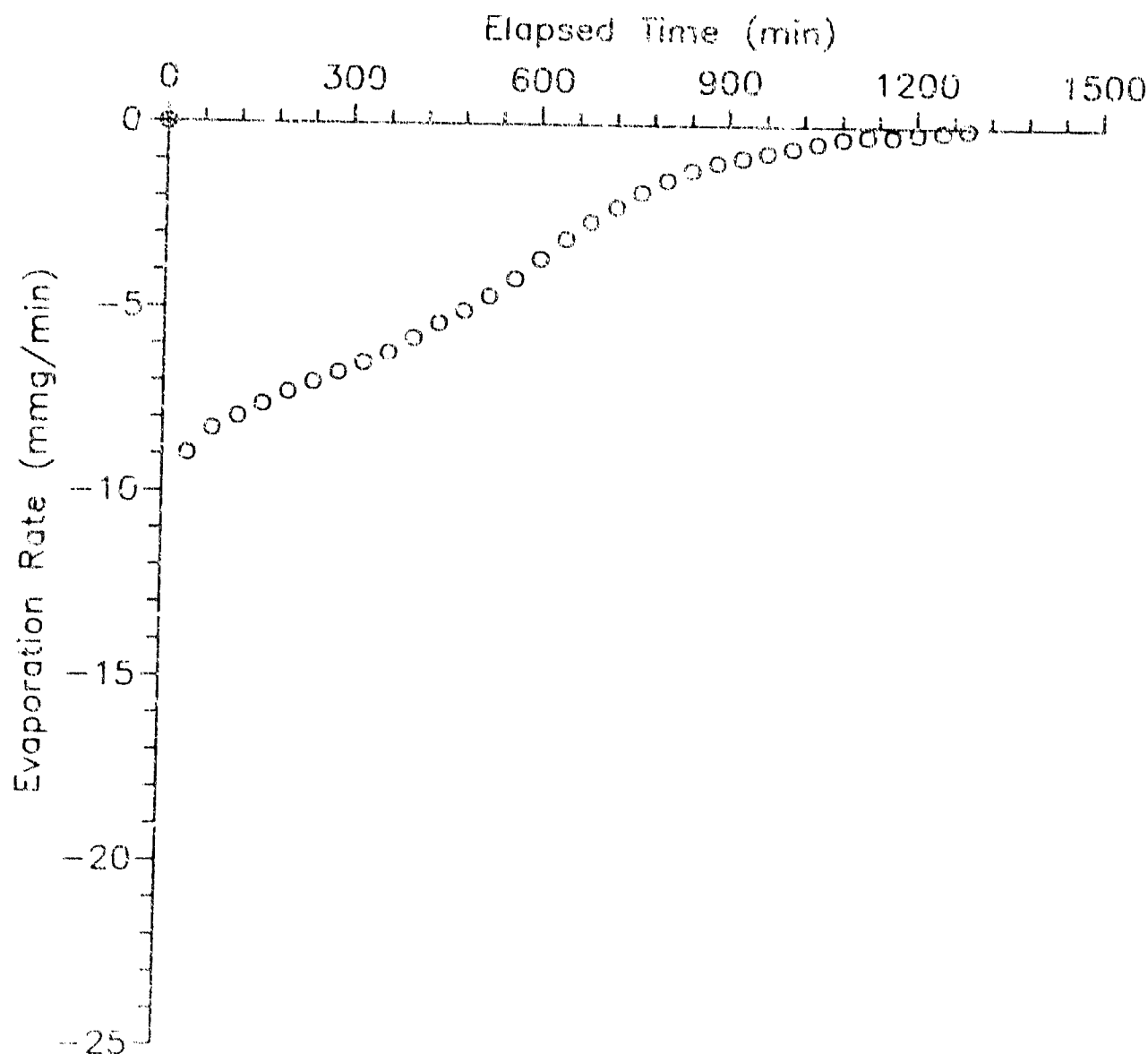


Figure H-13. Droplet Evaporation Rate Versus Time

EVAPORATION EXPERIMENT NO. GLF14 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/BOTTOM SURFACE  
WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 43%

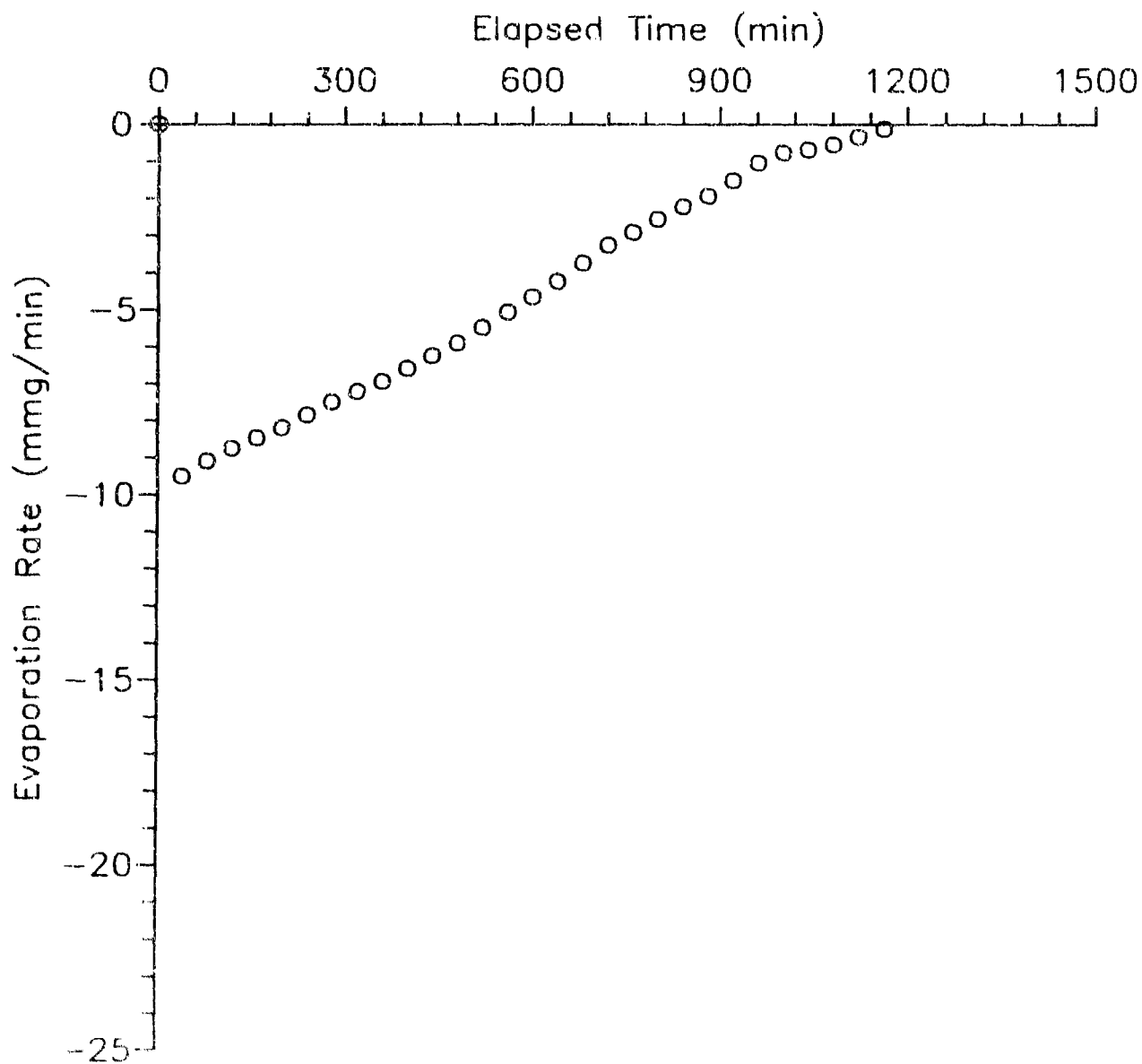


Figure H-14. Droplet Evaporation Rate Versus Time.

EVAPORATION EXPERIMENT NO. GLF15 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/BOTTOM SURFACE  
WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

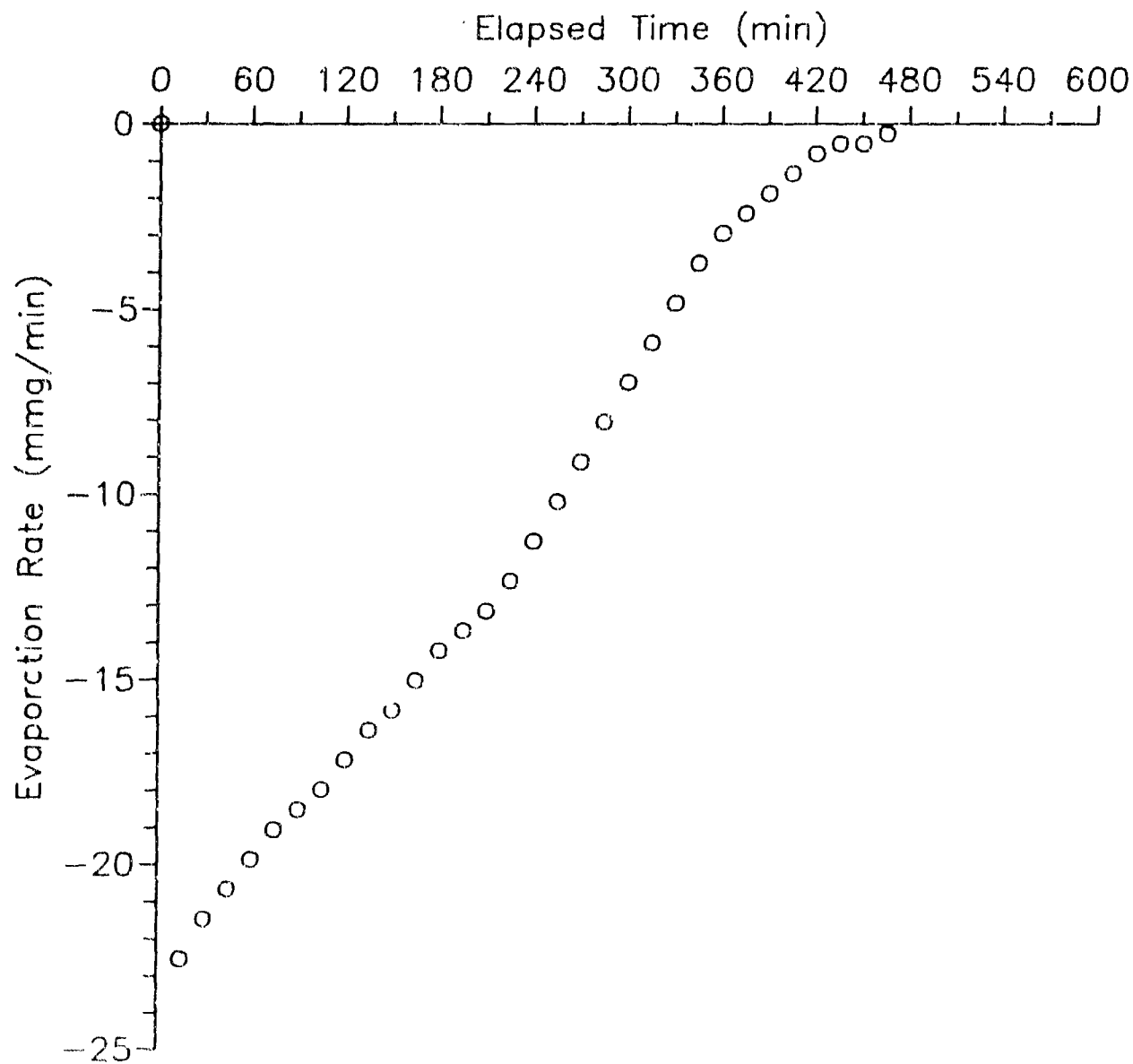


Figure H-15. Droplet Evaporation Rate Versus Time.

EVAPORATION EXPERIMENT NO. GLF16 SERIES ID 2-4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 g/SQ METER ON OAK LEAF/BOTTOM SURFACE  
WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

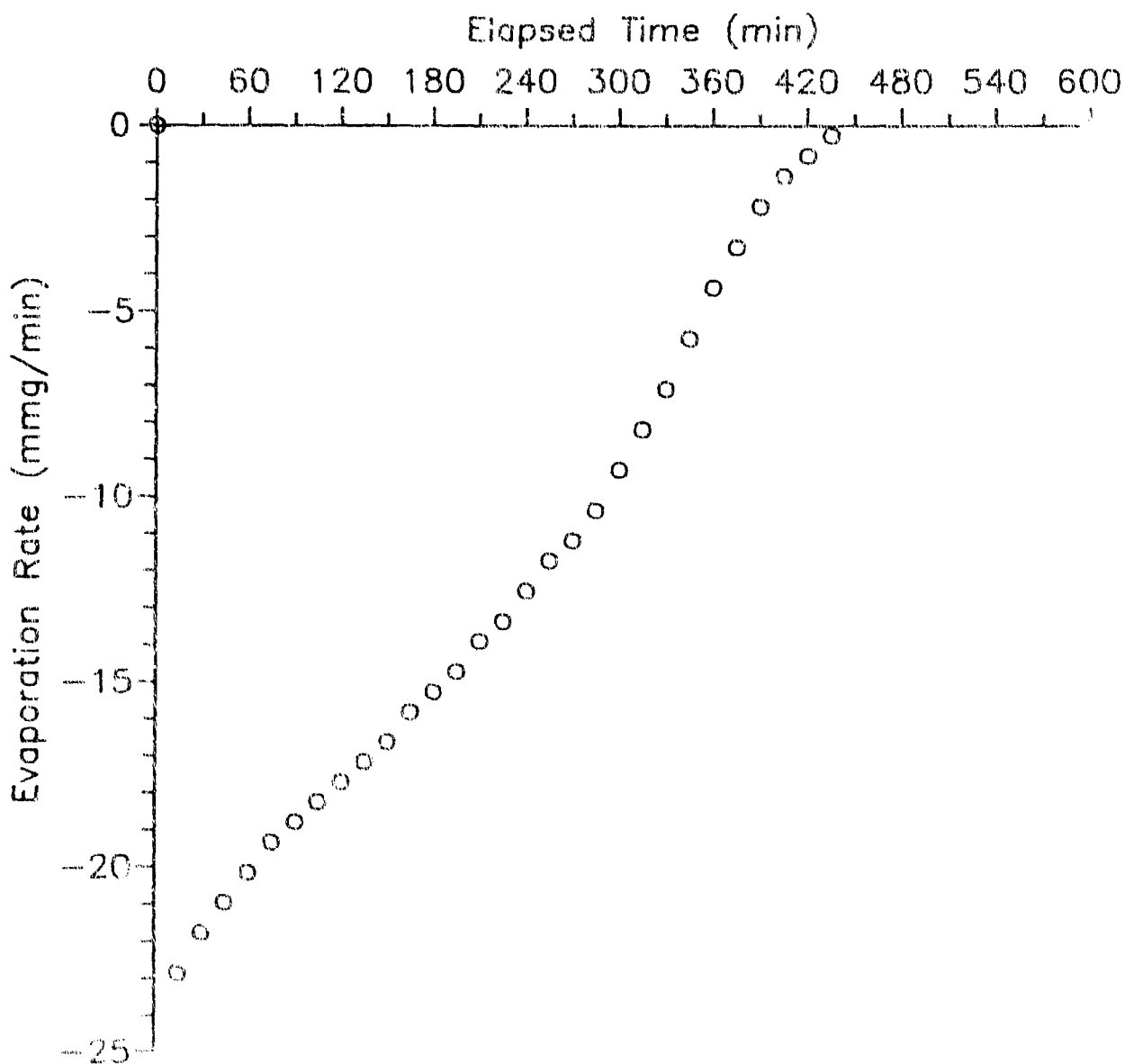


Figure H-16. Droplet Evaporation Rate Versus Time.

EVAPORATION EXPERIMENT NO. BLF1    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/TOP SURFACE  
WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 39%

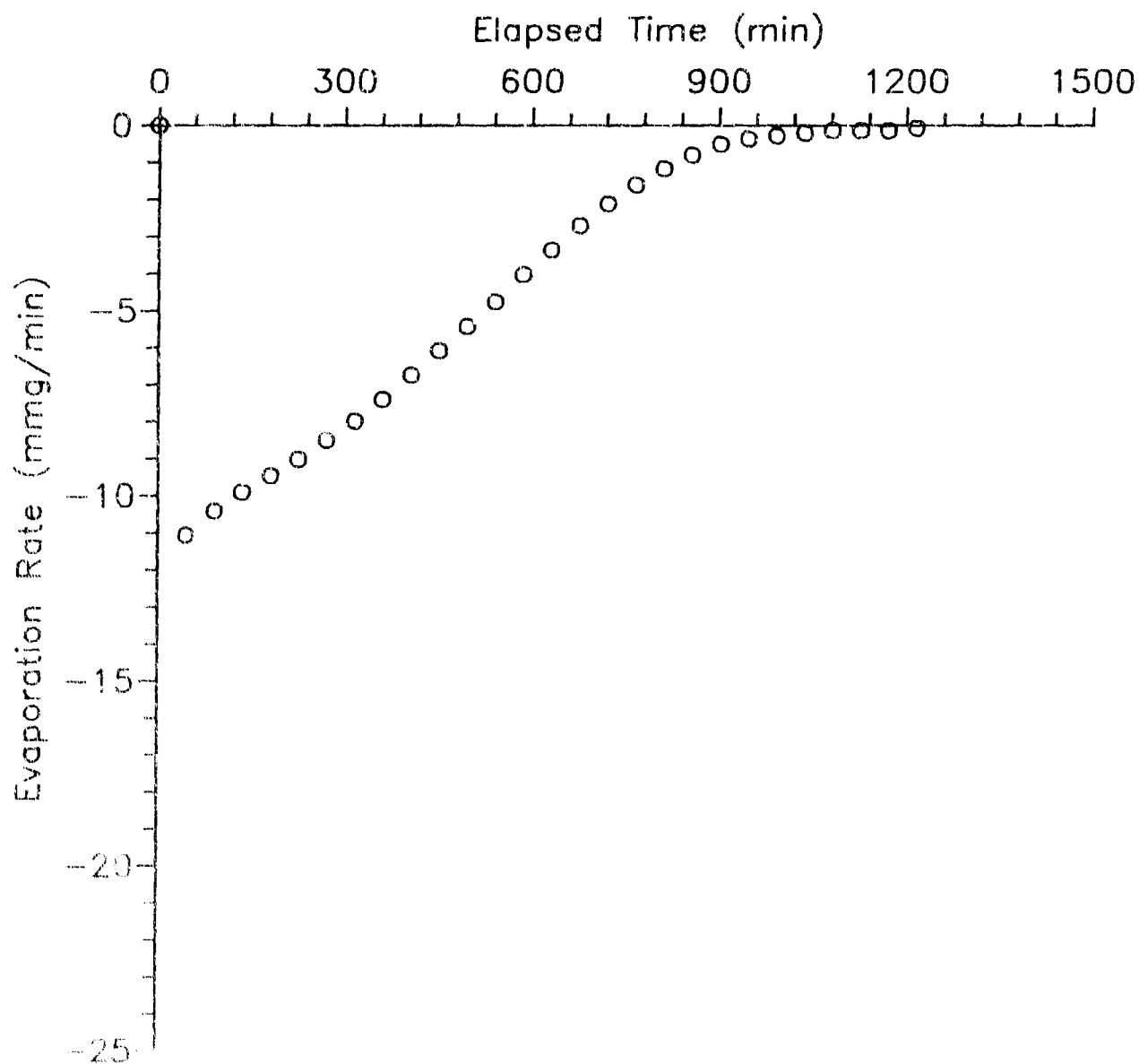


Figure H-17. Droplet Evaporation Rate Versus Time

EVAPORATION EXPERIMENT NO. BLF2    SERIES ID 2-4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/TOP SURFACE  
WINDSPEED 2.9 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 39%

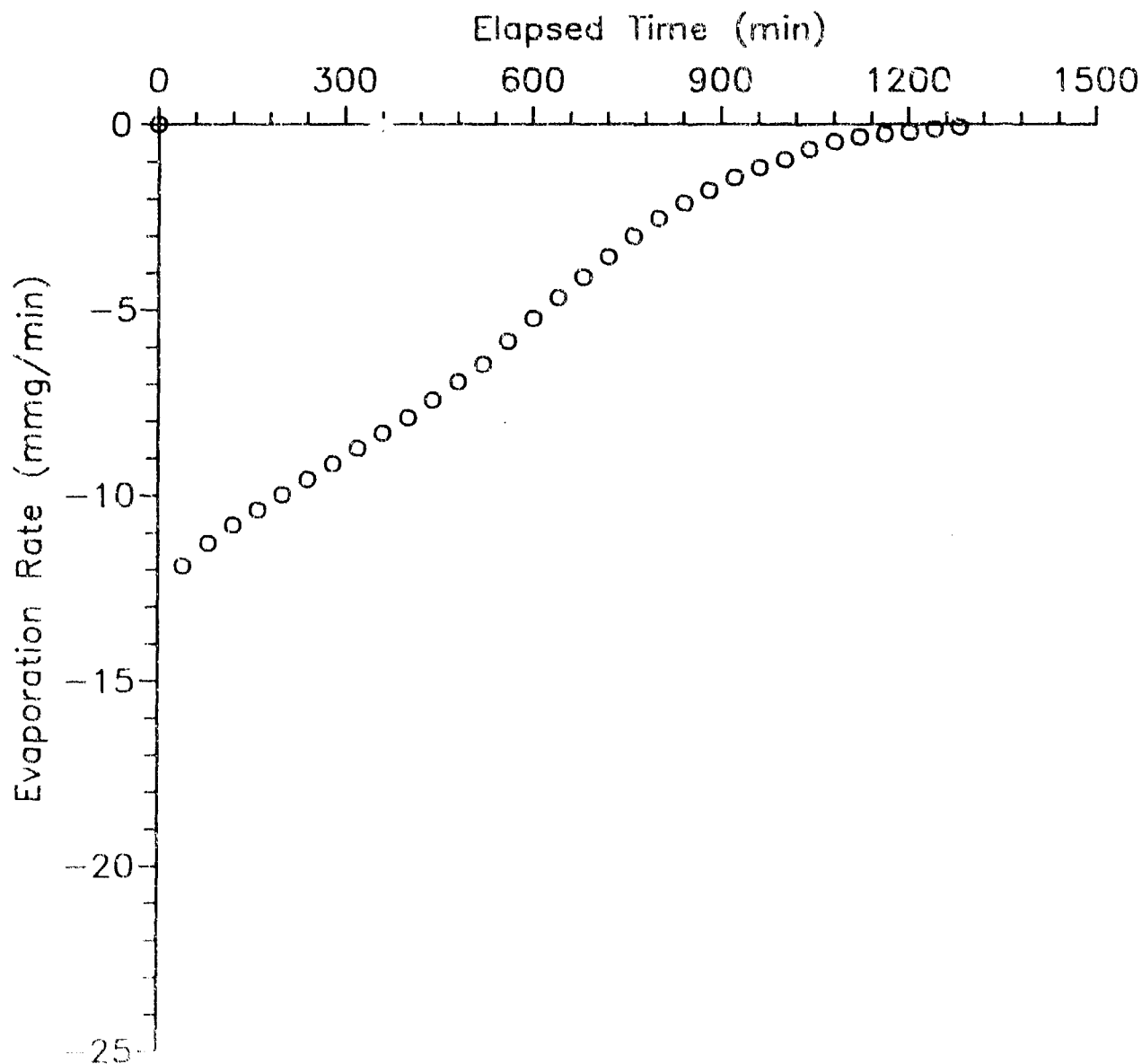


Figure H-18. Droplet Evaporation Rate Versus Time.

EVAPORATION EXPERIMENT NO. BLF3    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/TOP SURFACE  
 WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

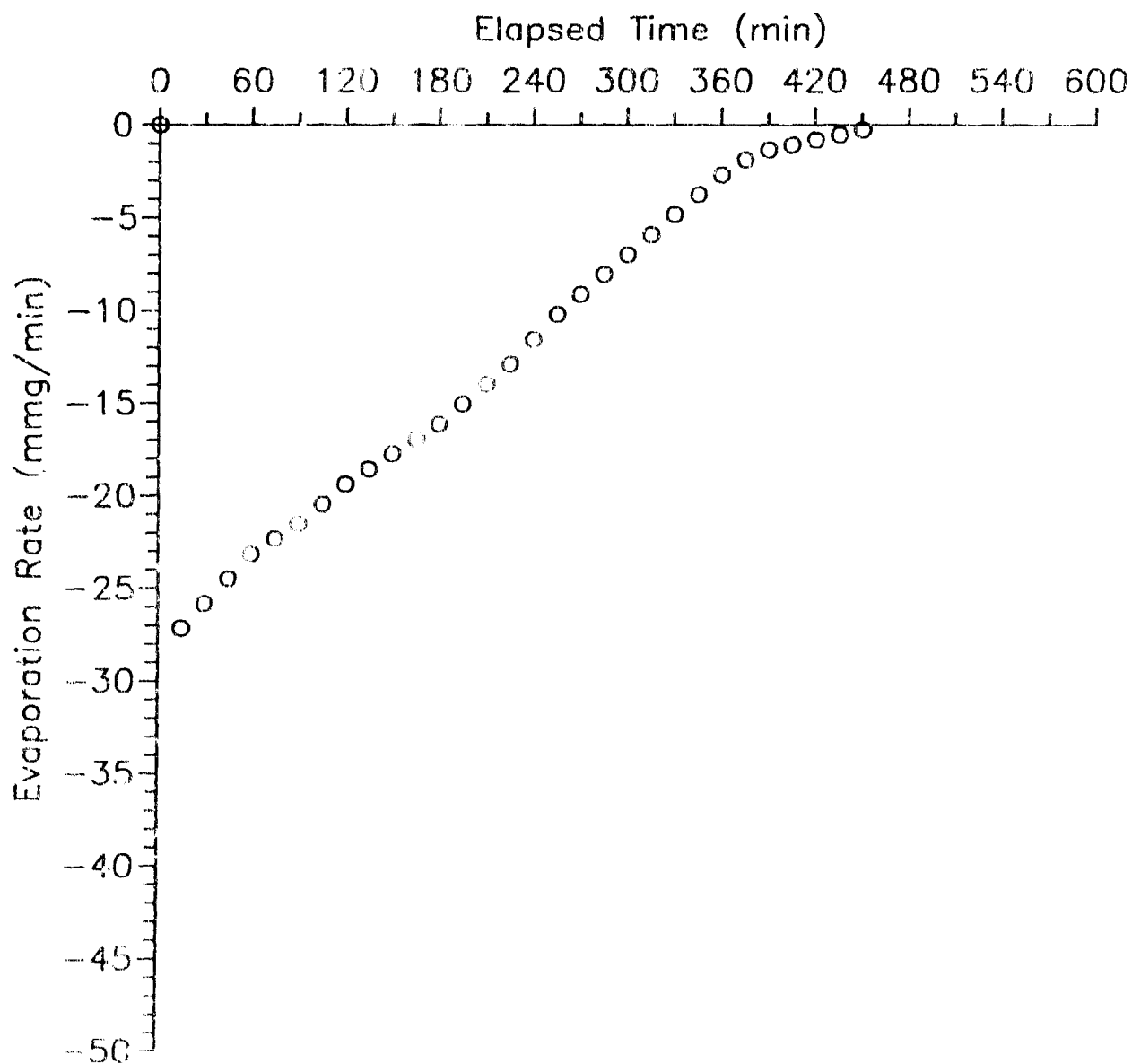


Figure 19. Impact Evaporation Rate vs. Time



EVAPORATION EXPERIMENT NO. BLF4    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/TOP SURFACE  
WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 20%

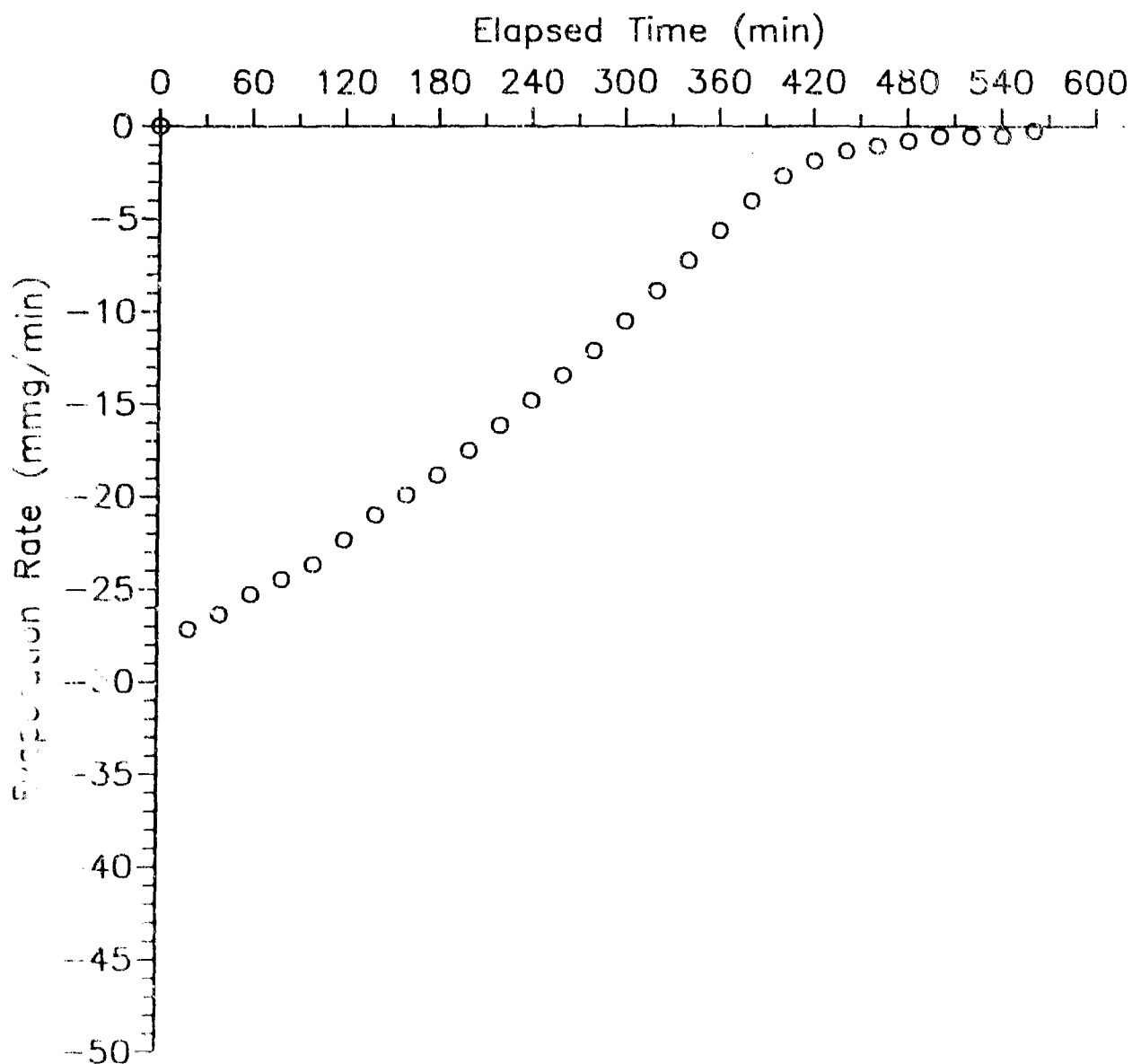


Figure H-20. Droplet Evaporation Rate Versus Time.

EVAPORATION EXPERIMENT NO. BLF5    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/BOTTOM SURFACE  
WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

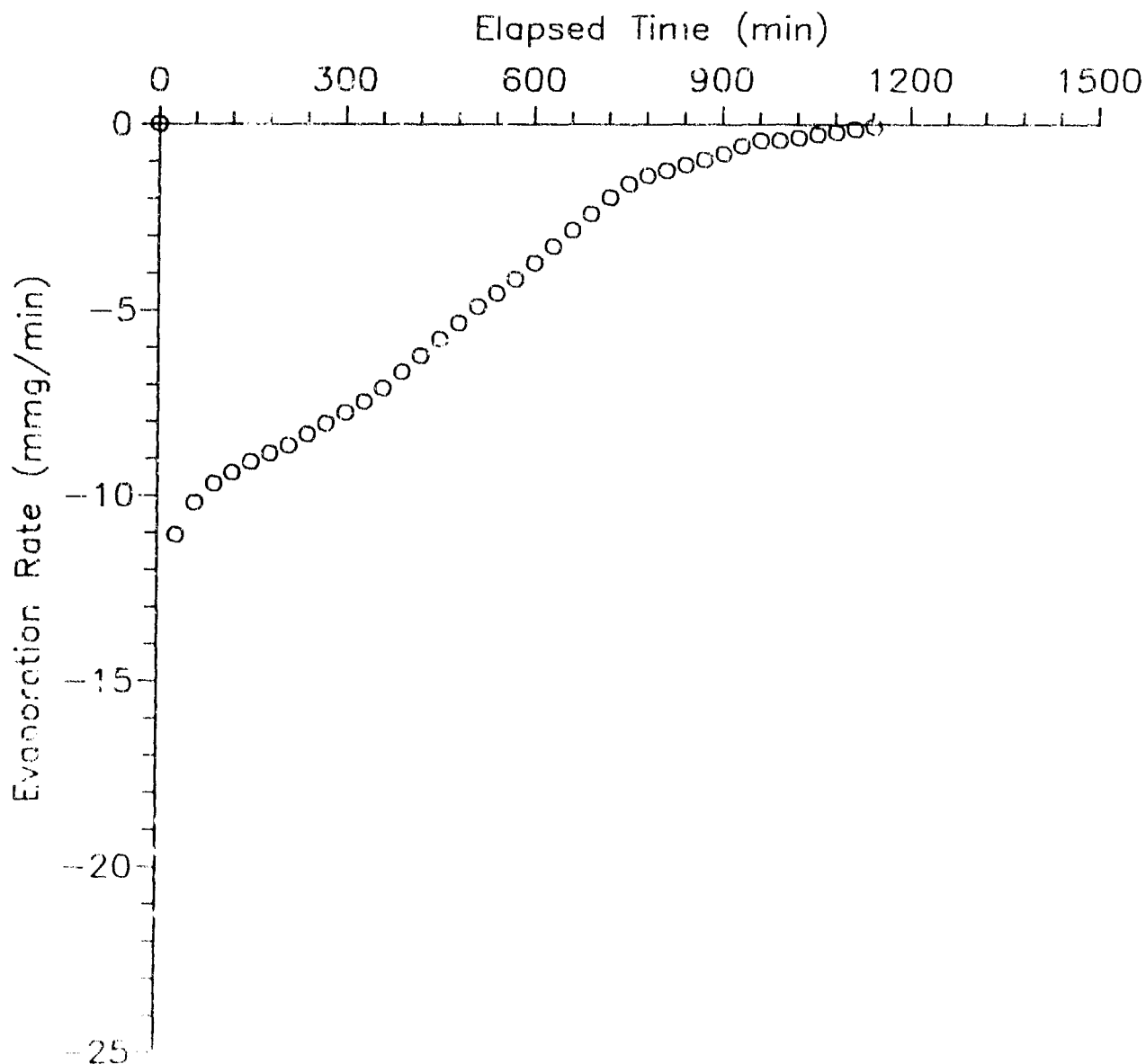


Figure H-21 Droplet Evaporation Rate Versus Time

EVAPORATION EXPERIMENT NO. BLF6    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/BOTTOM SURFACE  
WINDSPEED 2.9 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

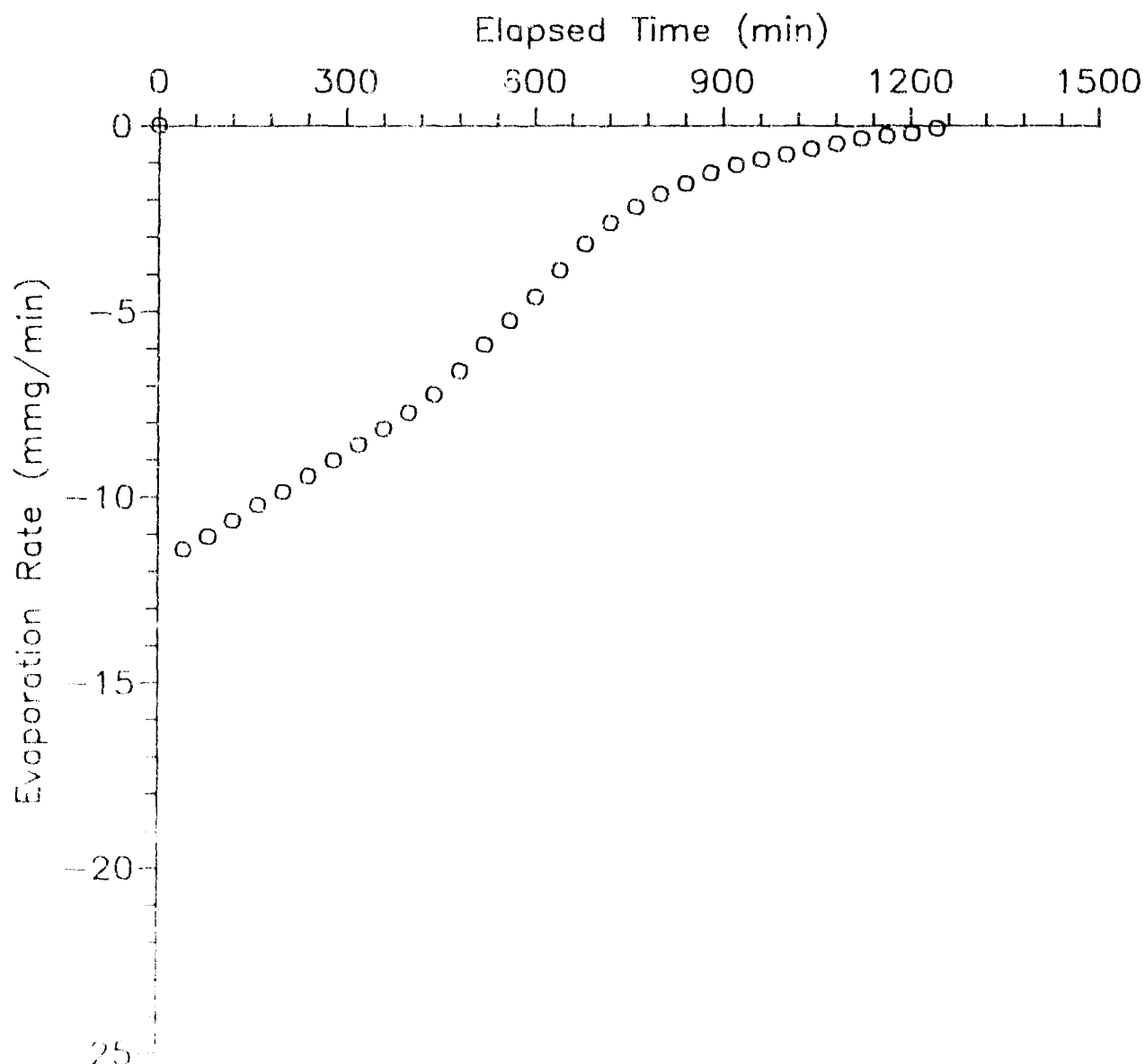


Figure H-22    Droplet Evaporation Rate Versus Time.

EVAPORATION EXPERIMENT NO. BLF7    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/BOTTOM SURFACE  
WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

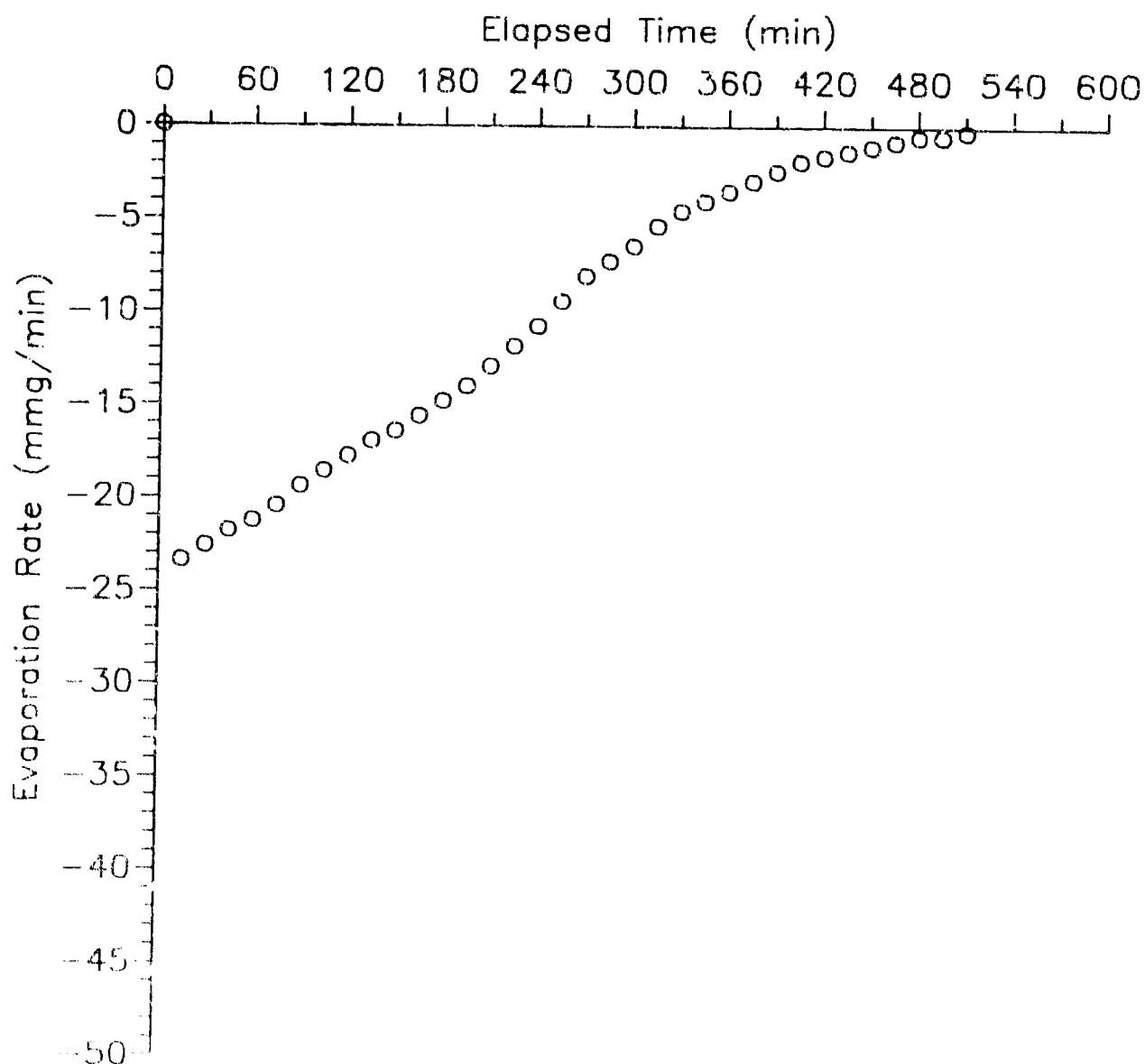


Figure H-25 Droplet Evaporation Rate Versus Time

EVAPORATION EXPERIMENT NO. BLF8    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/BOTTOM SURFACE  
WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 50%

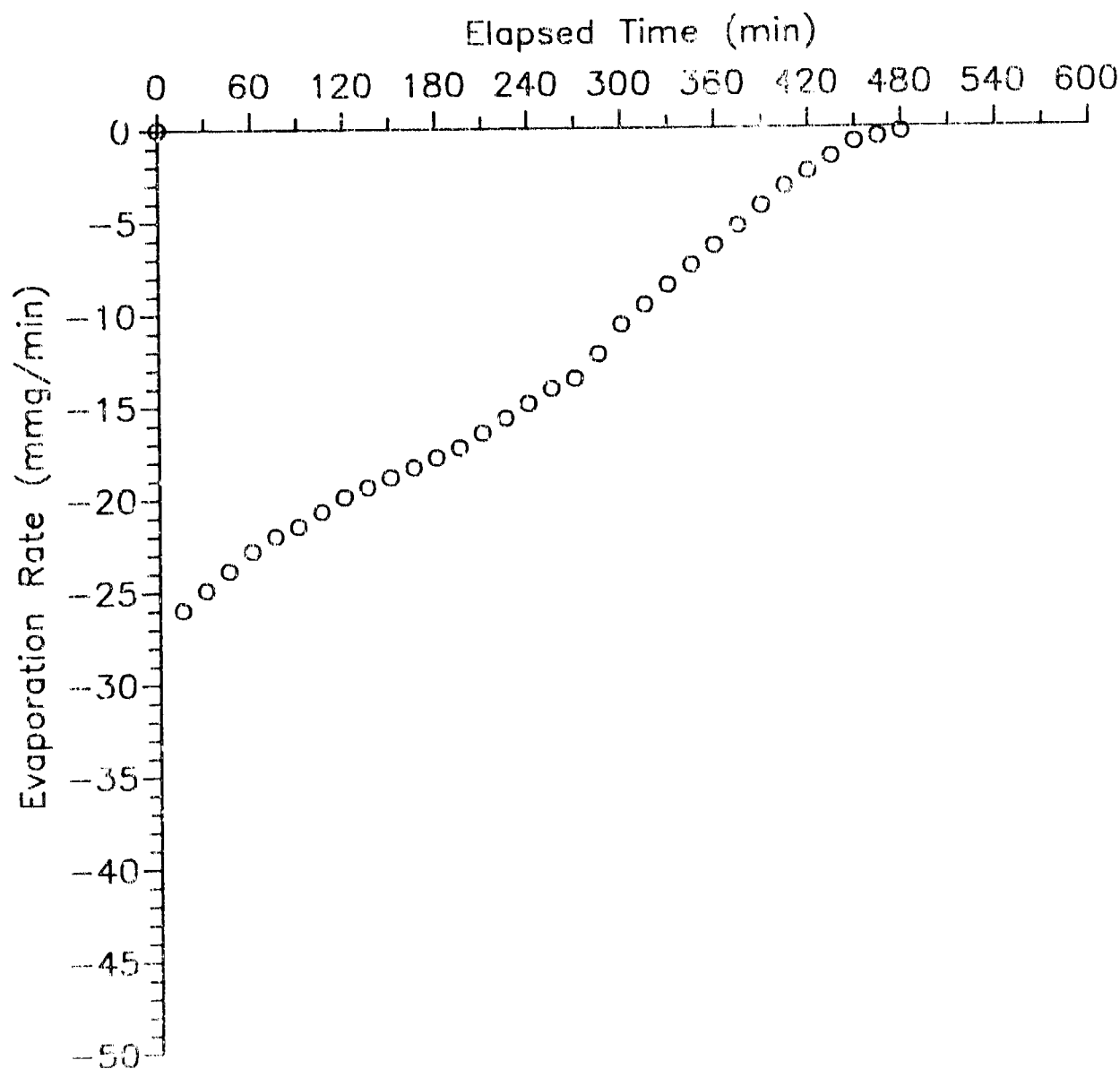


Figure H-24. Droplet Evaporation Rate Versus Time.

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APPENDIX I  
PLOTS OF FRACTIONAL DROPLET MASS VERSUS DROPLET HALF-LIFE

EVAPORATION EXPERIMENT NO. GLF1    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA.,    100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/TOP SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F.,    RELATIVE HUMIDITY 45%

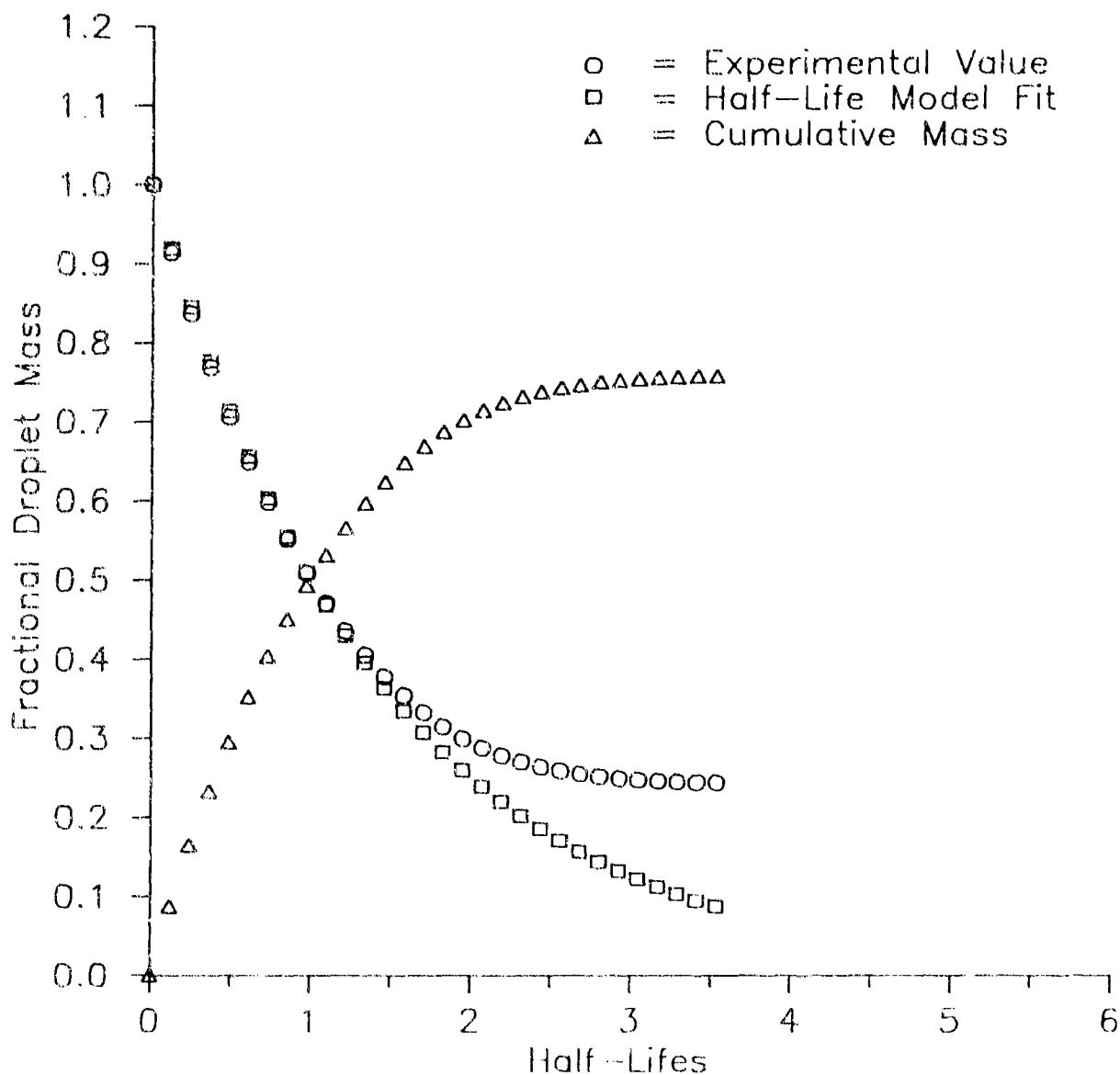


Figure I-1. Fractional Droplet Mass Versus Droplet Half-Life.



EVAPORATION EXPERIMENT NO. GLF2    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/TOP SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 39%

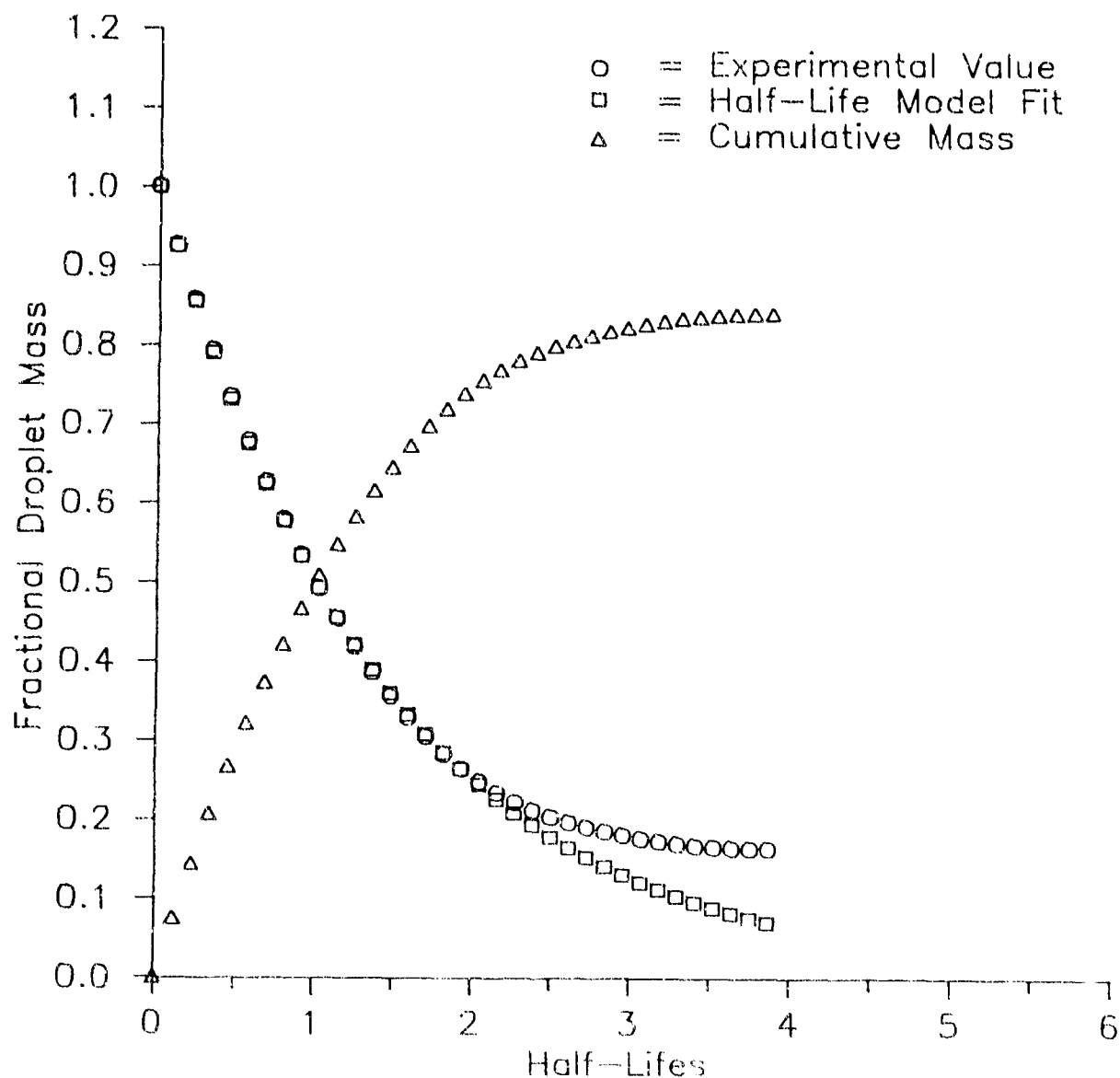


Figure 1-2. Fractional Droplet Mass Versus Droplet Half-Life.

EVAPORATION EXPERIMENT NO. GLF3    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/TOP SURFACE  
 WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 40%

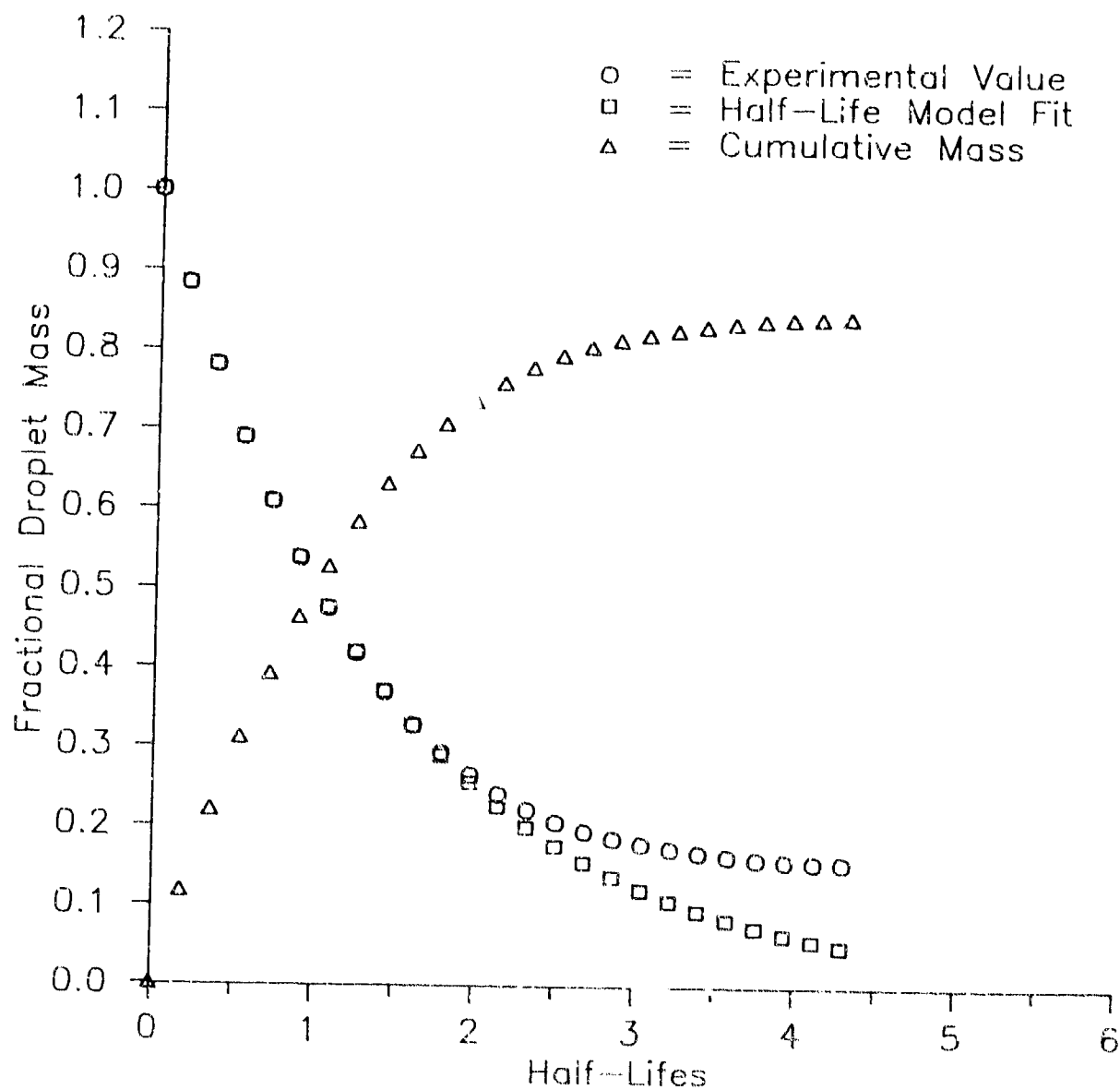


Figure 1-3. Fractional Droplet Mass Versus Droplet Half-Life.

EVAPORATION EXPERIMENT NO. GLF4    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/TOP SURFACE  
 WINDSPEED 11 MPH. AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

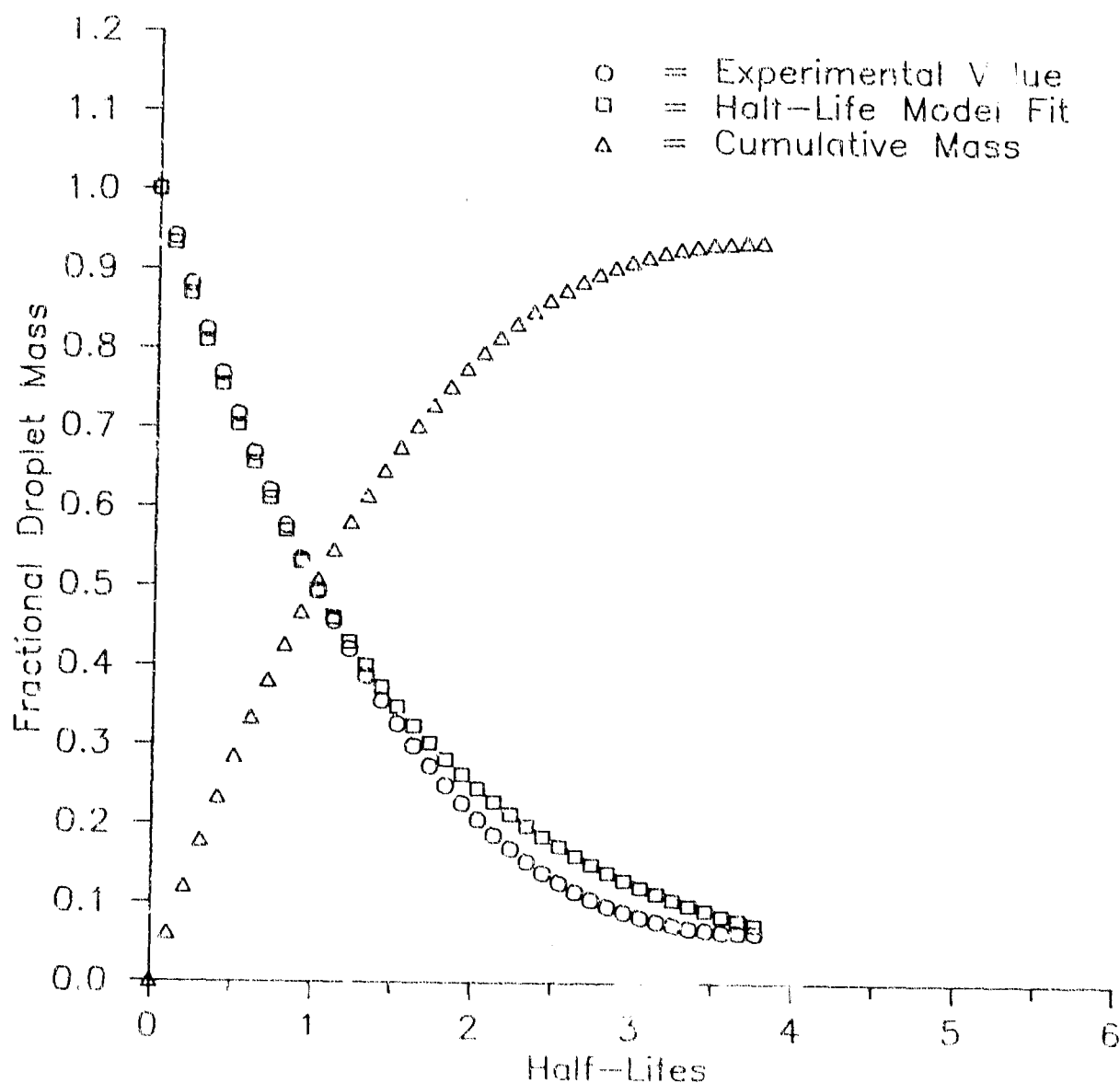


Figure 1-4. Fractional Droplet Mass Versus Droplet Half-Life.

EVAPORATION EXPERIMENT NO. GLF5    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/BOTTOM  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 58%

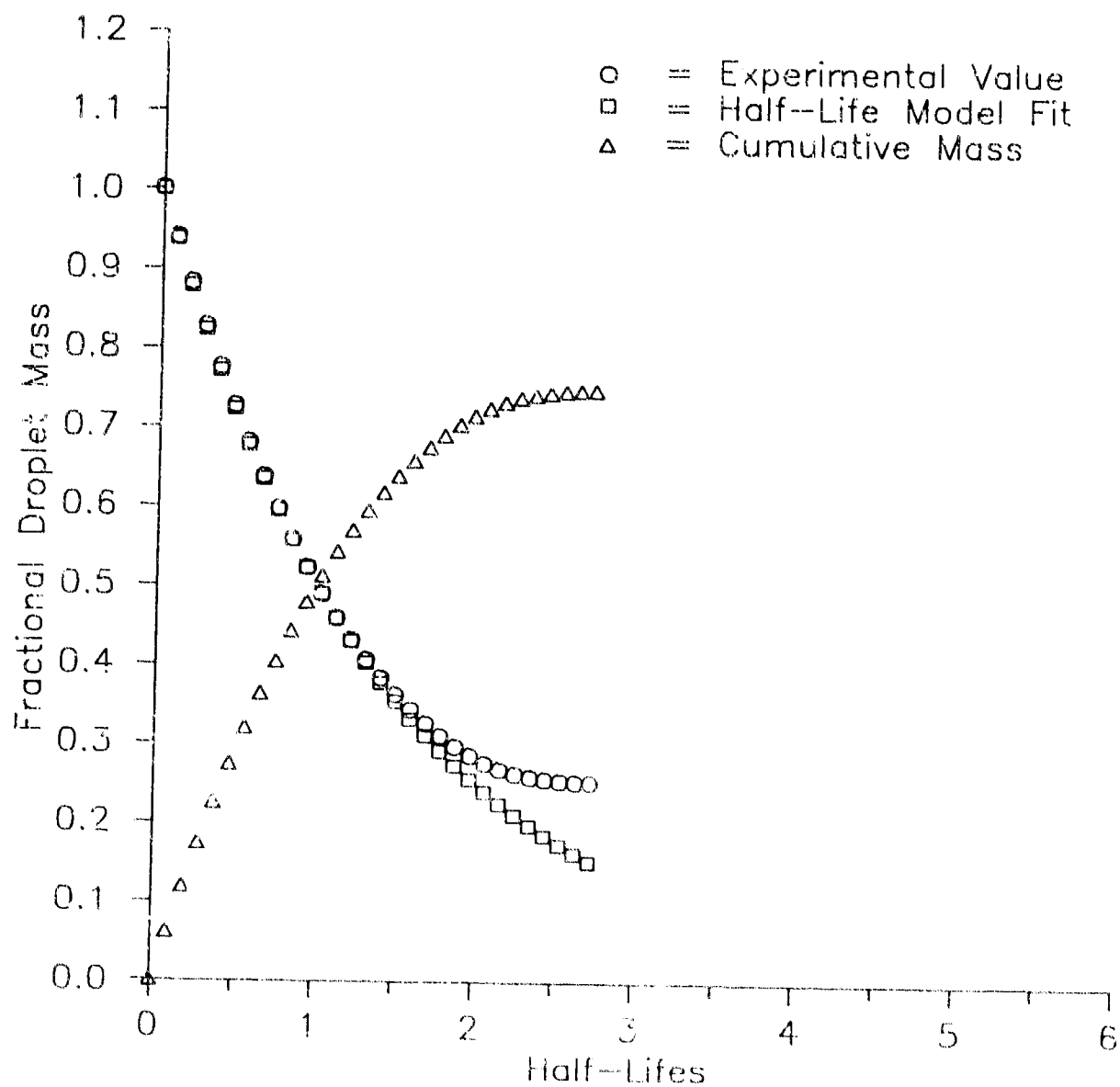


Figure 1-5. Fractional Droplet Mass Versus Droplet Half-Life.

EVAPORATION EXPERIMENT NO. GLFS    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/BOTTOM  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 55%

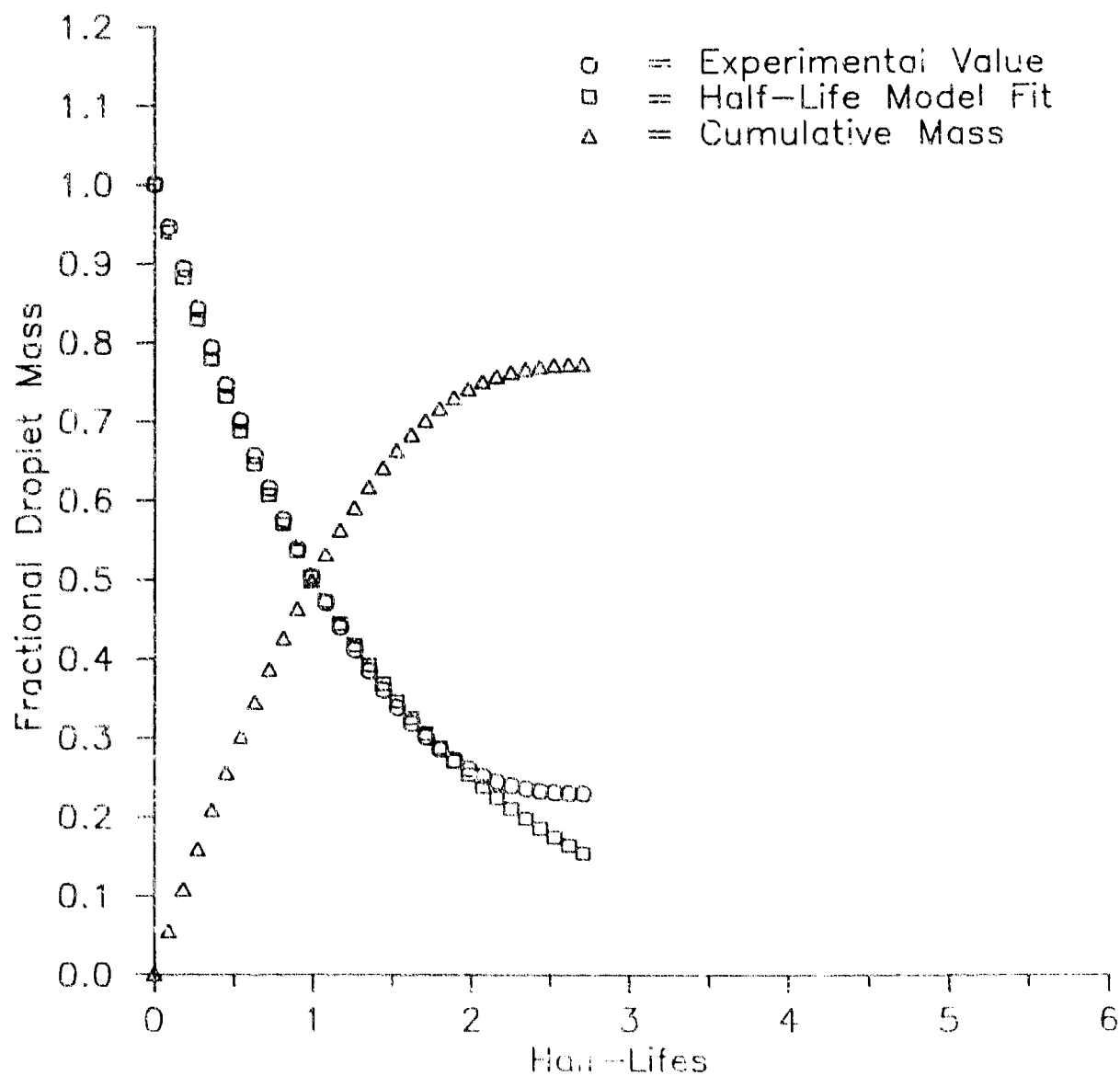


Figure I-6. Fractional Droplet Mass Versus Droplet Half-Life

EVAPORATION EXPERIMENT NO. GLF7    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/BOTTOM  
 WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

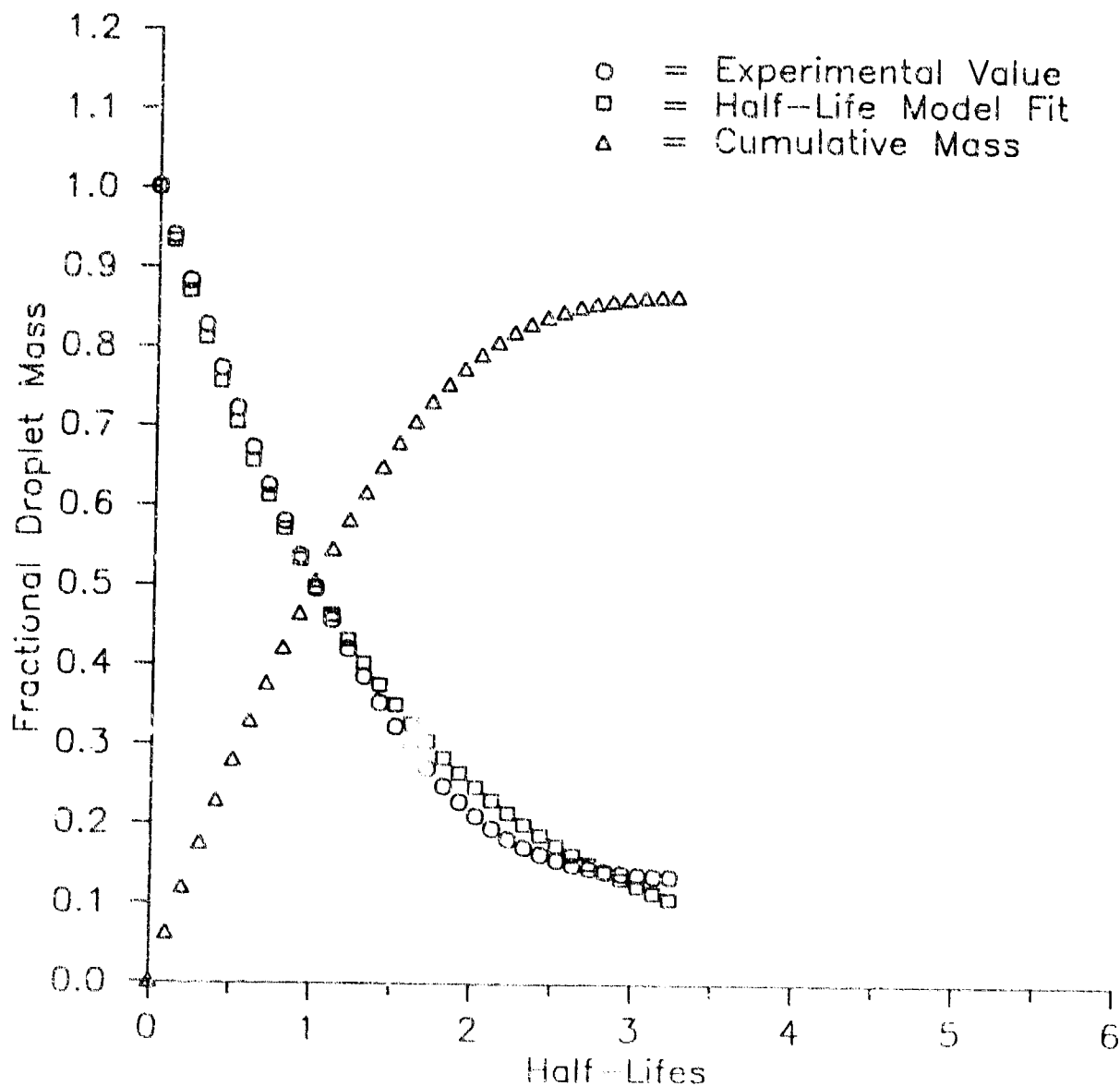


Figure 1-7. Fractional Droplet Mass Versus Droplet Half-Life.

EVAPORATION EXPERIMENT NO. GLF8    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON HICKORY LEAF/BOTTOM  
 WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 50%

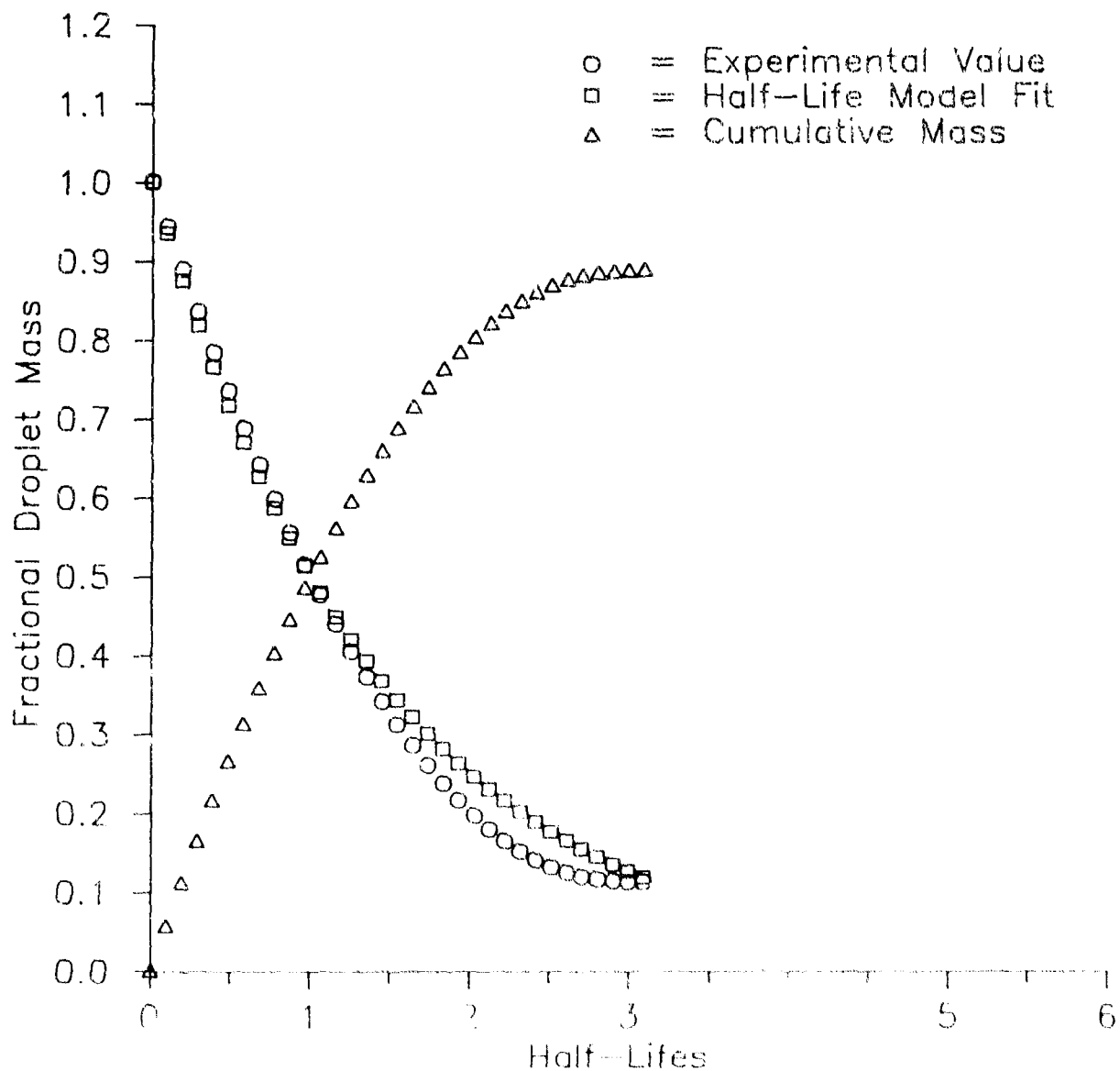


Figure 1-8. Fractional Droplet Mass Versus Droplet Half-Life.

EVAPORATION EXPERIMENT NO. GLF9    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/TOP SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 44%

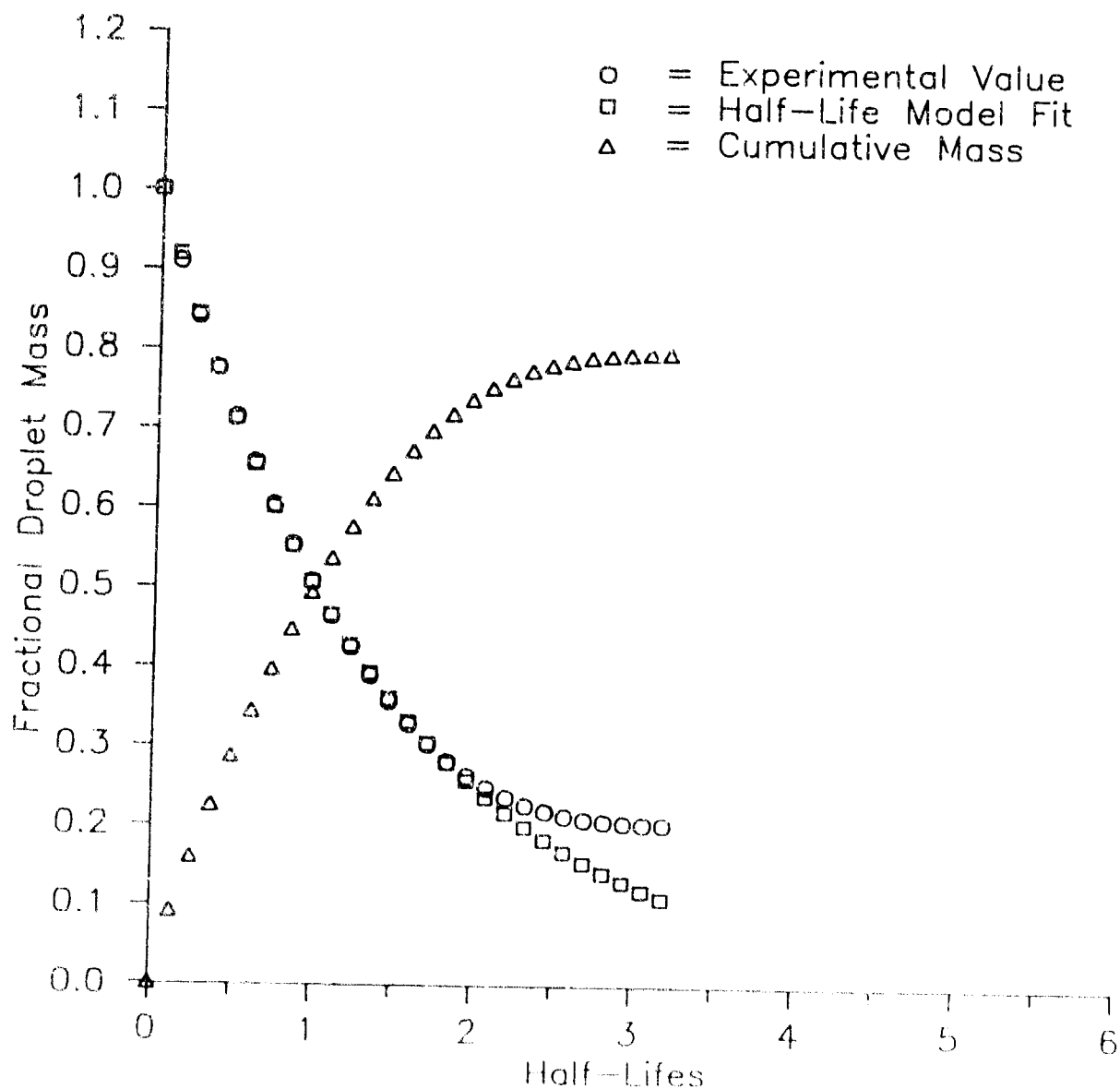


Figure 1-9. Fractional Droplet Mass Versus Droplet Half Life.



EVAPORATION EXPERIMENT NO. GLF10 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/TOP SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 52%

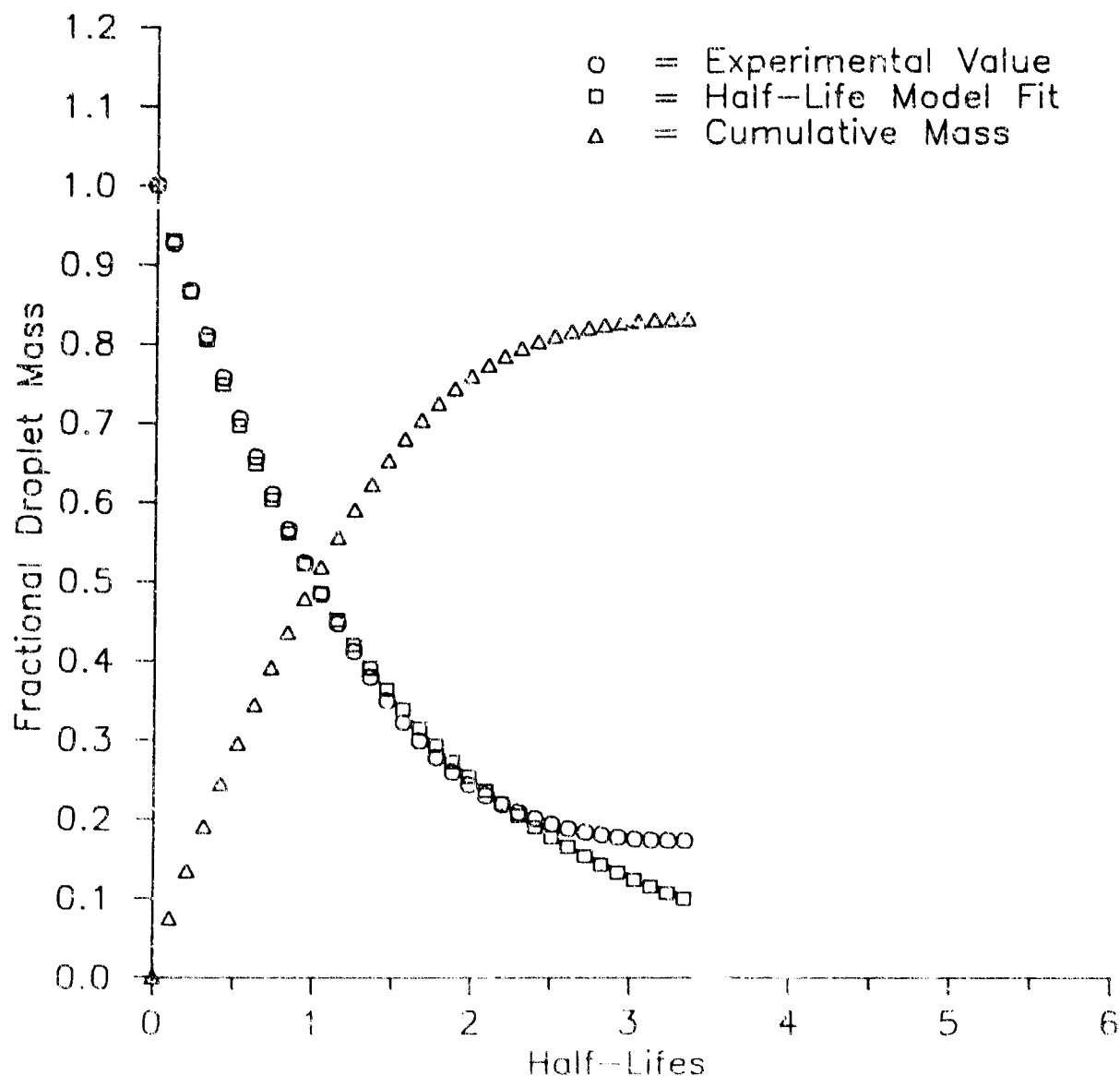


Figure I-10. Fractional Droplet Mass Versus Droplet Half-Life.

EVAPORATION EXPERIMENT NO. GLF11 SERIES ID 2♦♦4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/TOP SURFACE  
 WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 55%

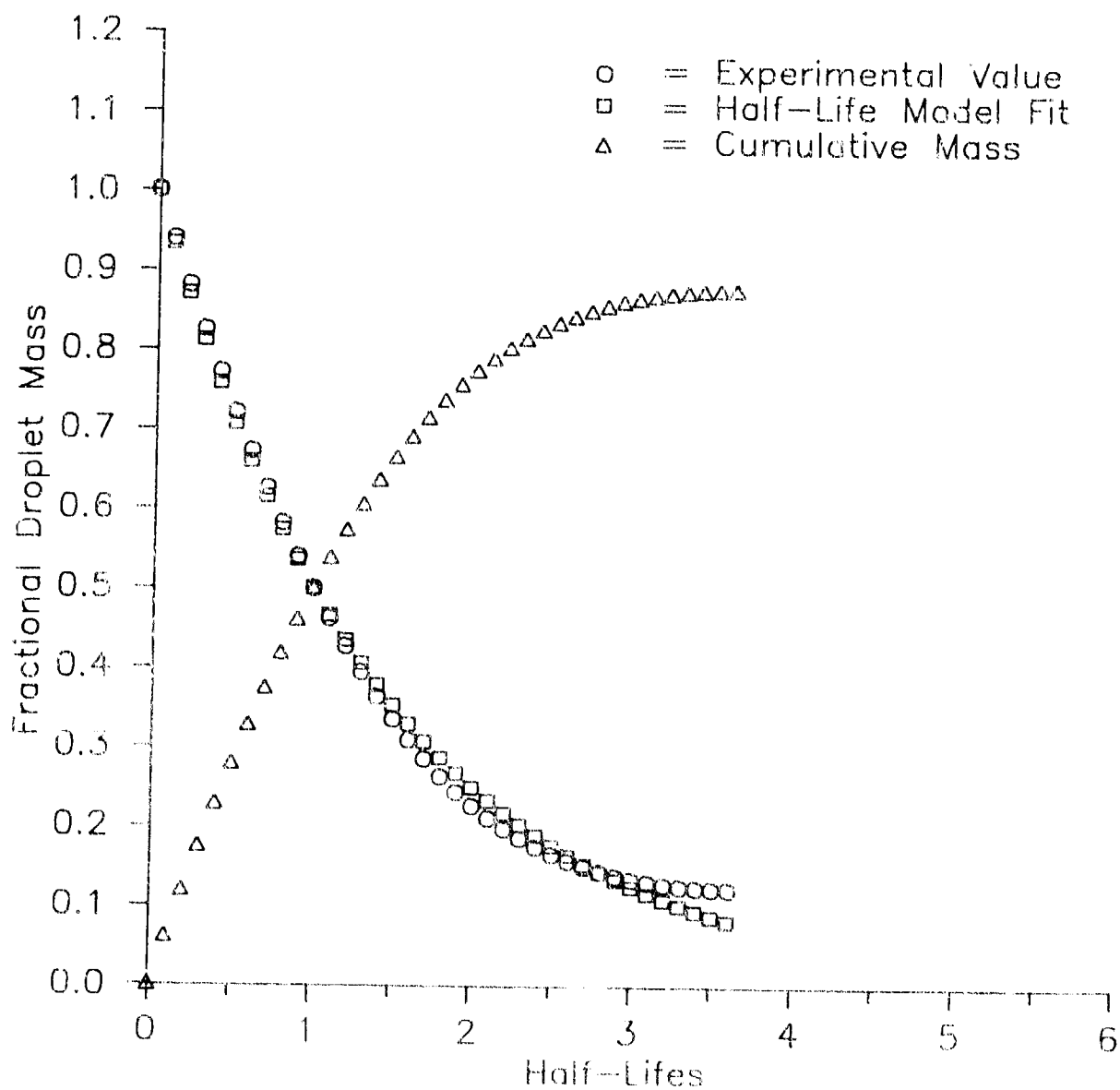


Figure I-11 Fractional Droplet Mass Versus Droplet Half-Life.

EVAPORATION EXPERIMENT NO. GLF12 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/TOP SURFACE  
 WINDSPEED 1' MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 40%

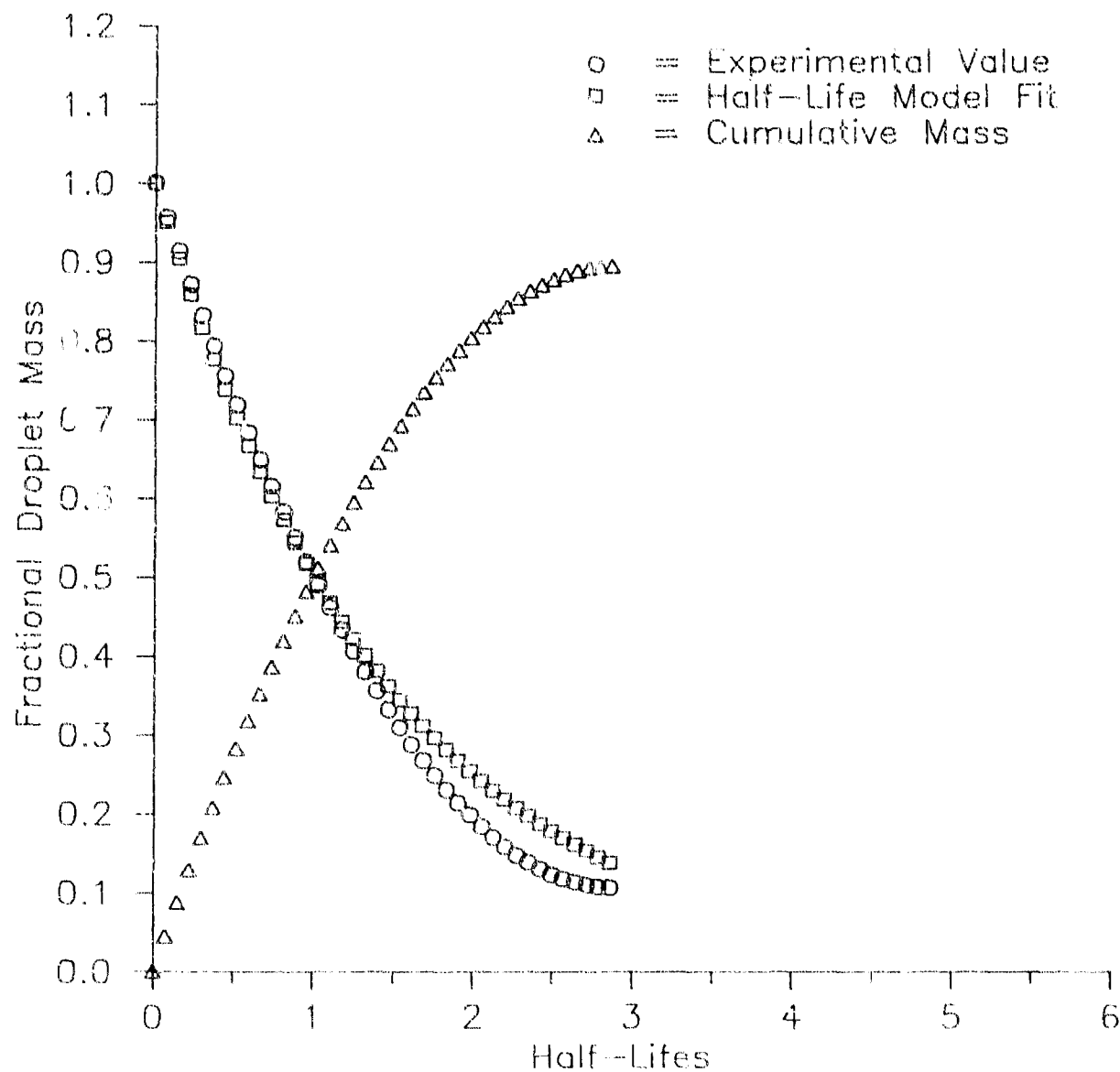


Figure I-12. Fractional Droplet Mass Versus Droplet Half-Life.

EVAPORATION EXPERIMENT NO. GLF13 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 50 G/SQ METER ON OAK LEAF/BOTTOM SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F, RELATIVE HUMIDITY 44%

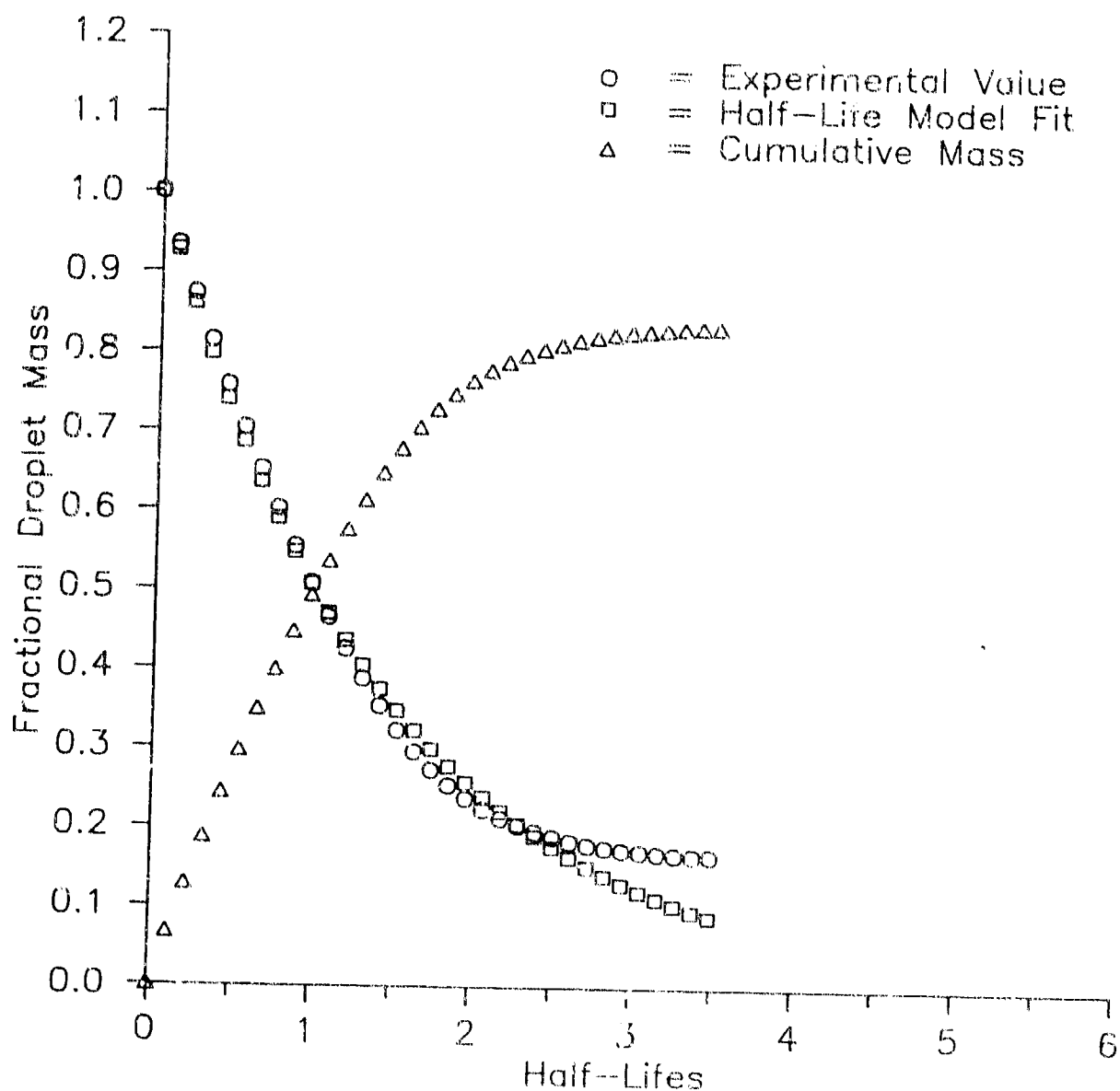


Figure I-13. Fractional Droplet Mass Versus Droplet Half-Life

EVAPORATION EXPERIMENT NO. GLF14 SERIES IC 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/BOTTOM SURFACE  
 WINDSPEED 2.8 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 43%

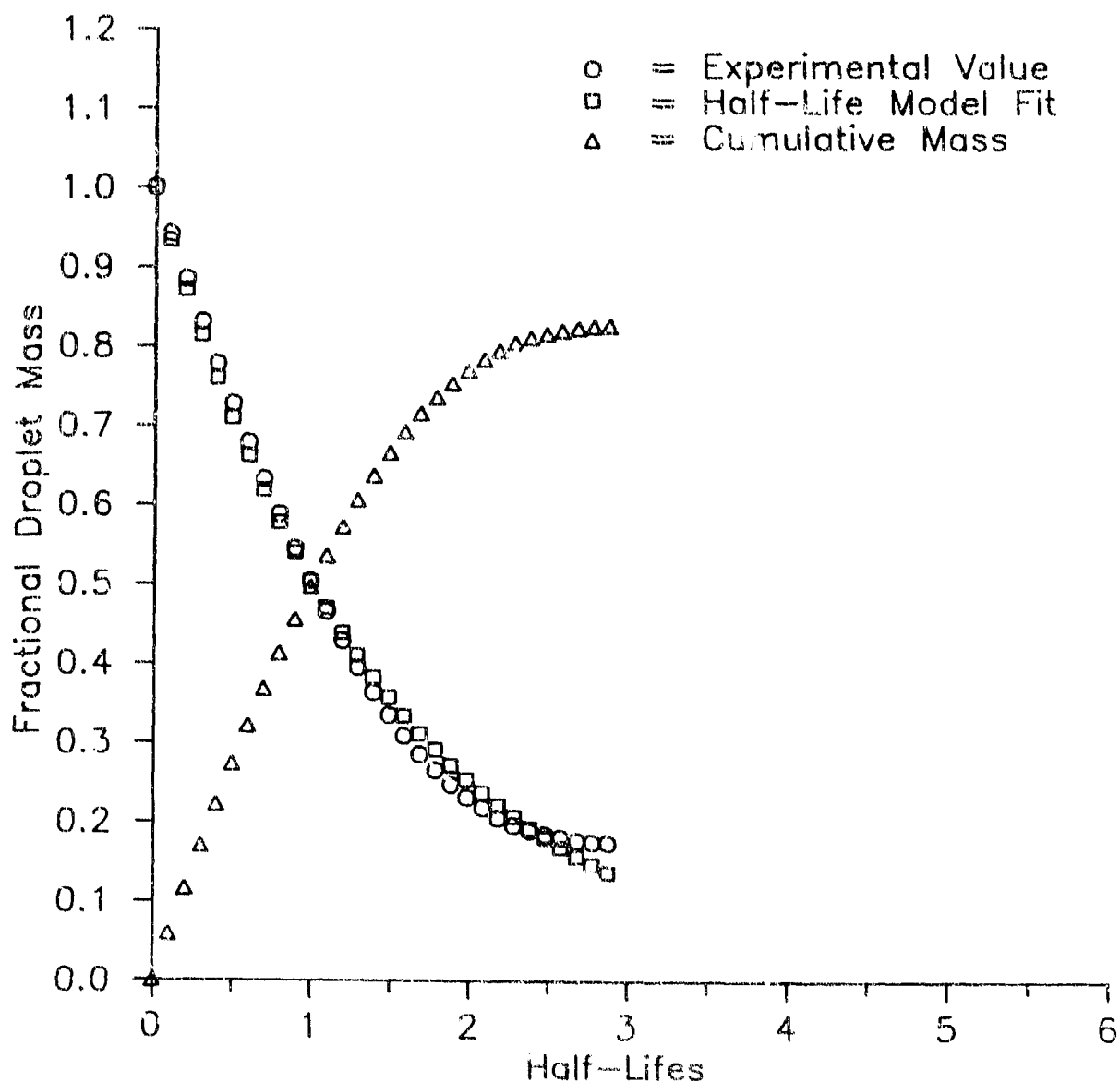


Figure I-14. Fractional Droplet Mass Versus Droplet Half-Life.

EVAPORATION EXPERIMENT NO. GLF15 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/BOTTOM SURFACE  
 WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

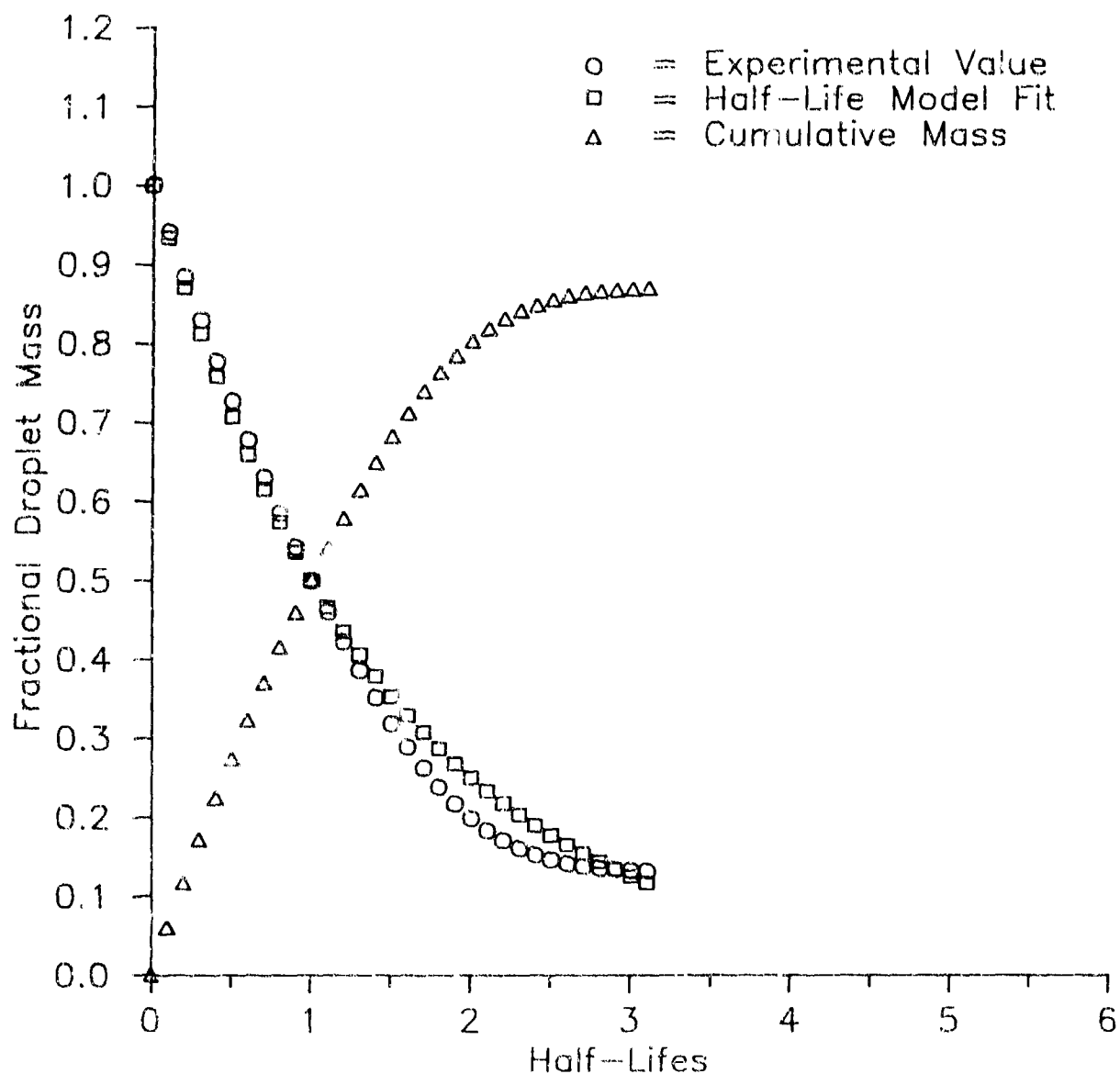


Figure 1-15. Fractional Droplet Mass Versus Droplet Half-Life.

EVAPORATION EXPERIMENT NO. GLF16 SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/BOTTOM SURFACE  
 WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

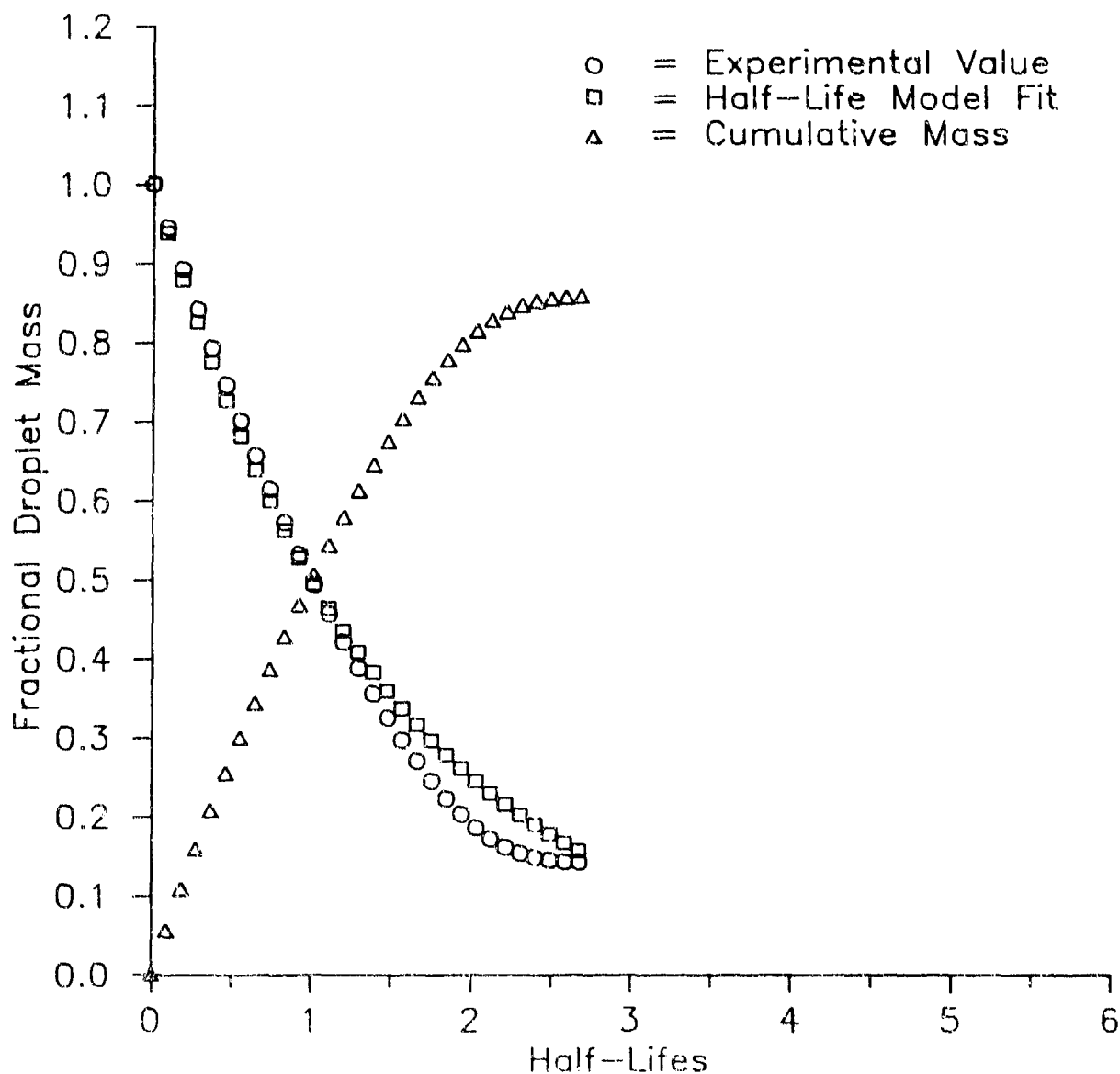


Figure I-16. Fractional Droplet Mass Versus Droplet Half-Life.

EVAPORATION EXPERIMENT NO. BLF1    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA.,    100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/TOP SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F.,    RELATIVE HUMIDITY 39%

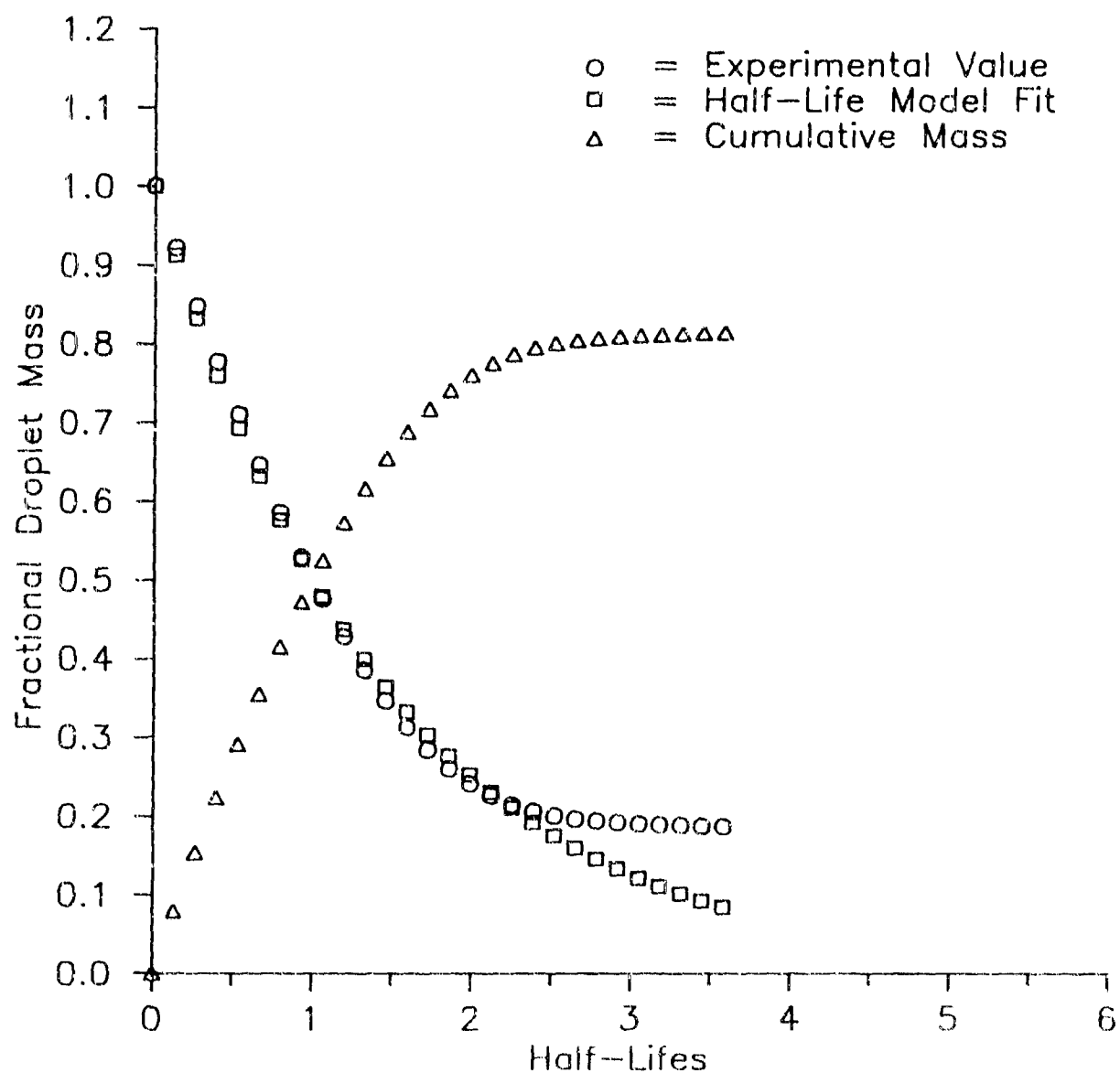


Figure 1-17. Fractional Droplet Mass Versus Droplet Half-Life.



EVAPORATION EXPERIMENT NO. BLF2    SERIES ID 2\*\*\* FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/TOP SURFACE  
 WINDSPEED 2.9 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 39%

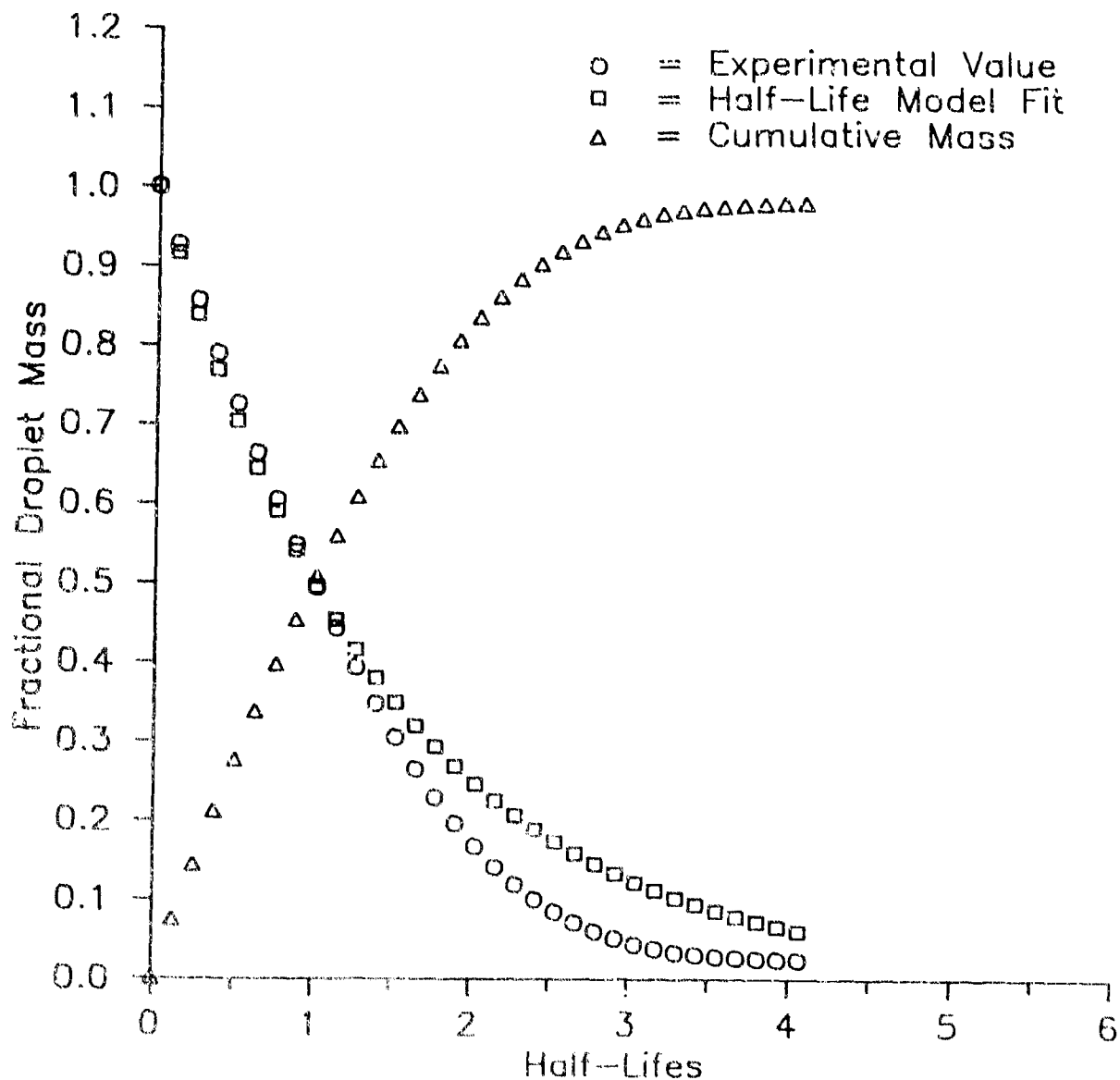


Figure 1-13. Fractional Droplet Mass Versus Droplet Half-Life.

EVAPORATION EXPERIMENT NO. BLF3    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/TOP SURFACE  
 WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

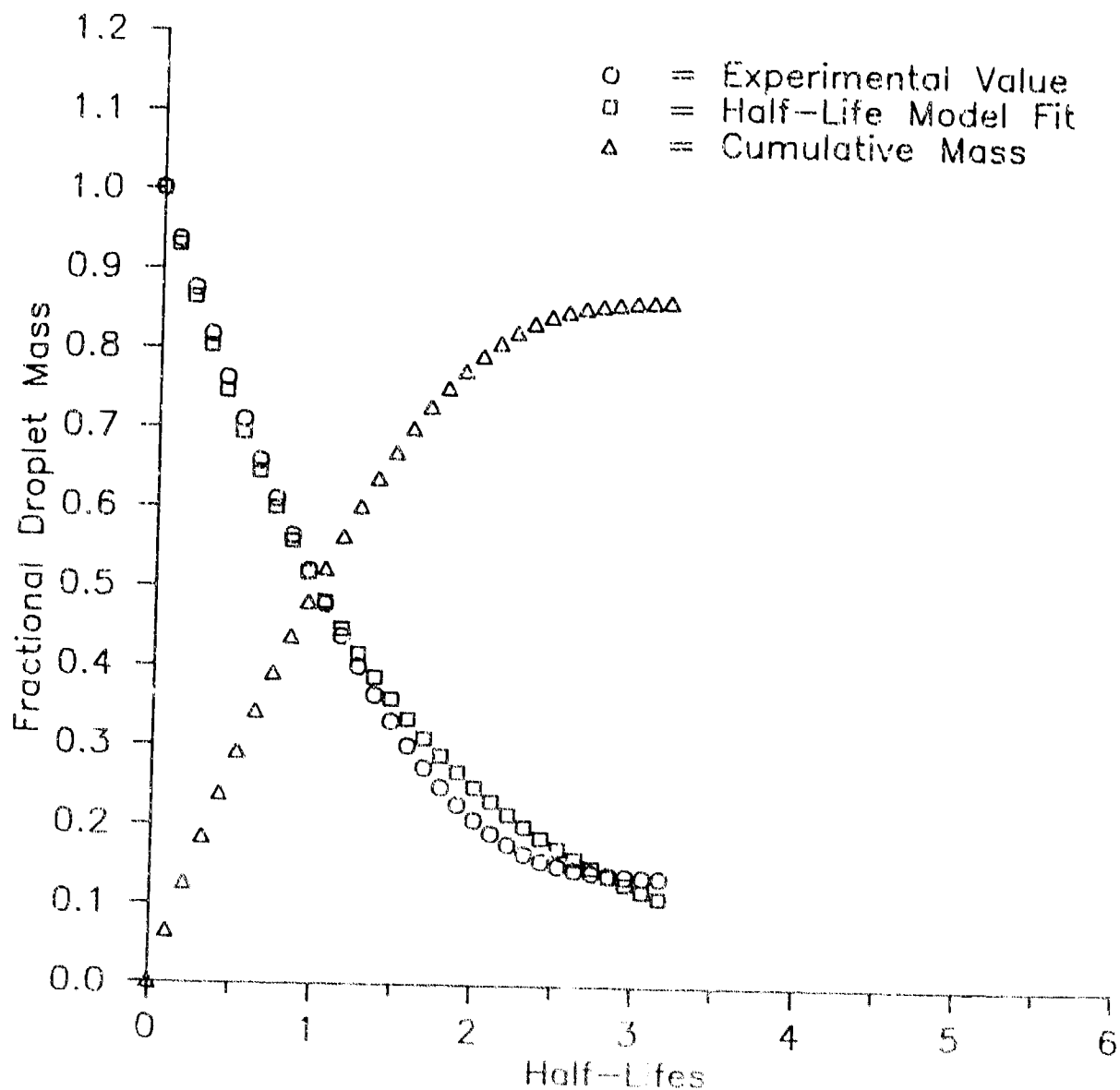


Figure I-19. Fractional Droplet Mass Versus Droplet Half-Life.

EVAPORATION EXPERIMENT NO. BLF4    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/TOP SURFACE  
 WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 29%

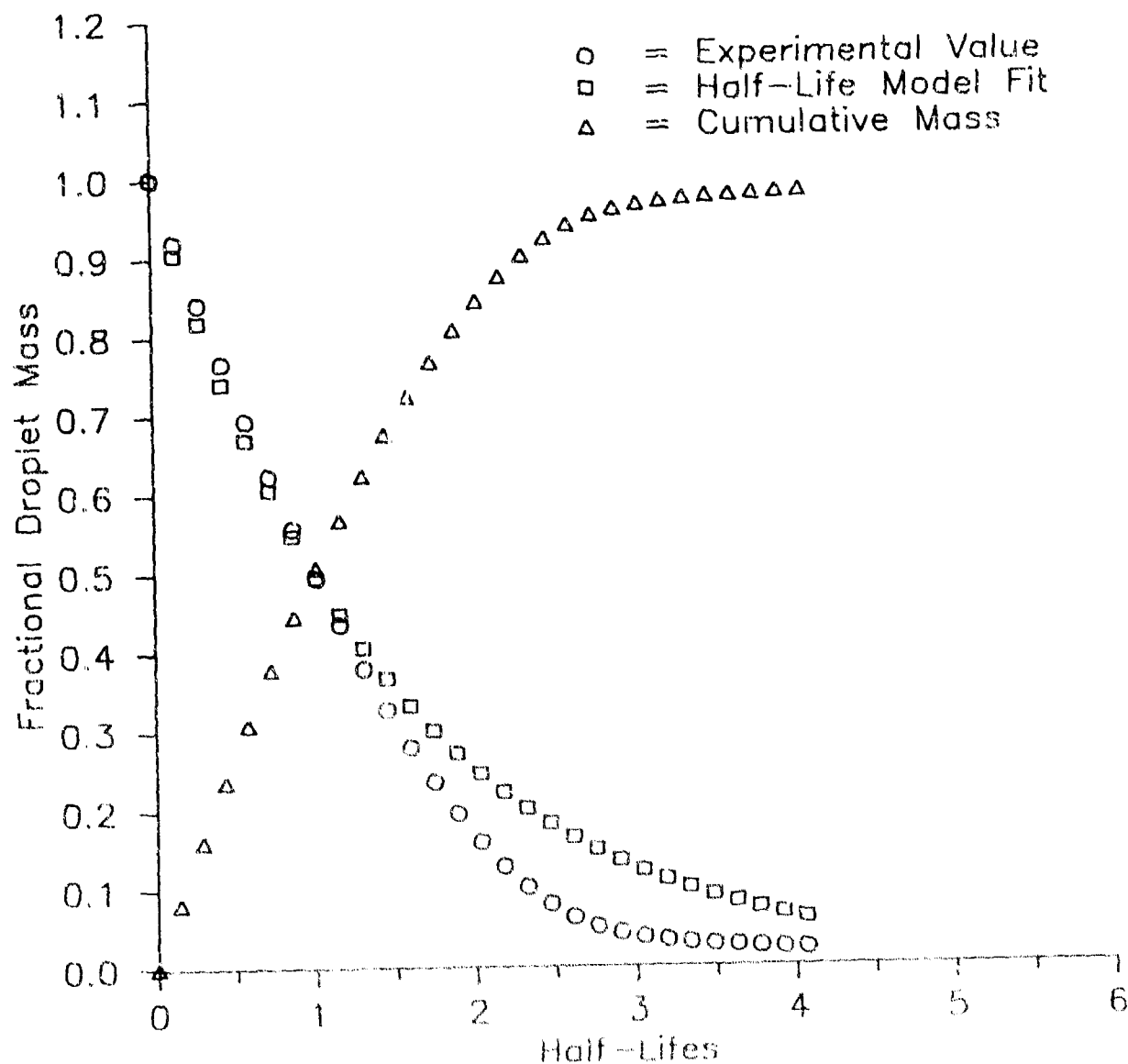


Figure 1-20. Fractional Droplet Mass Versus Droplet Half-Life.

EVAPORATION EXPERIMENT NO. BLF5    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 50 G/SQ METER ON OAK LEAF/BOTTOM SURFACE  
 WINDSPEED 3.0 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

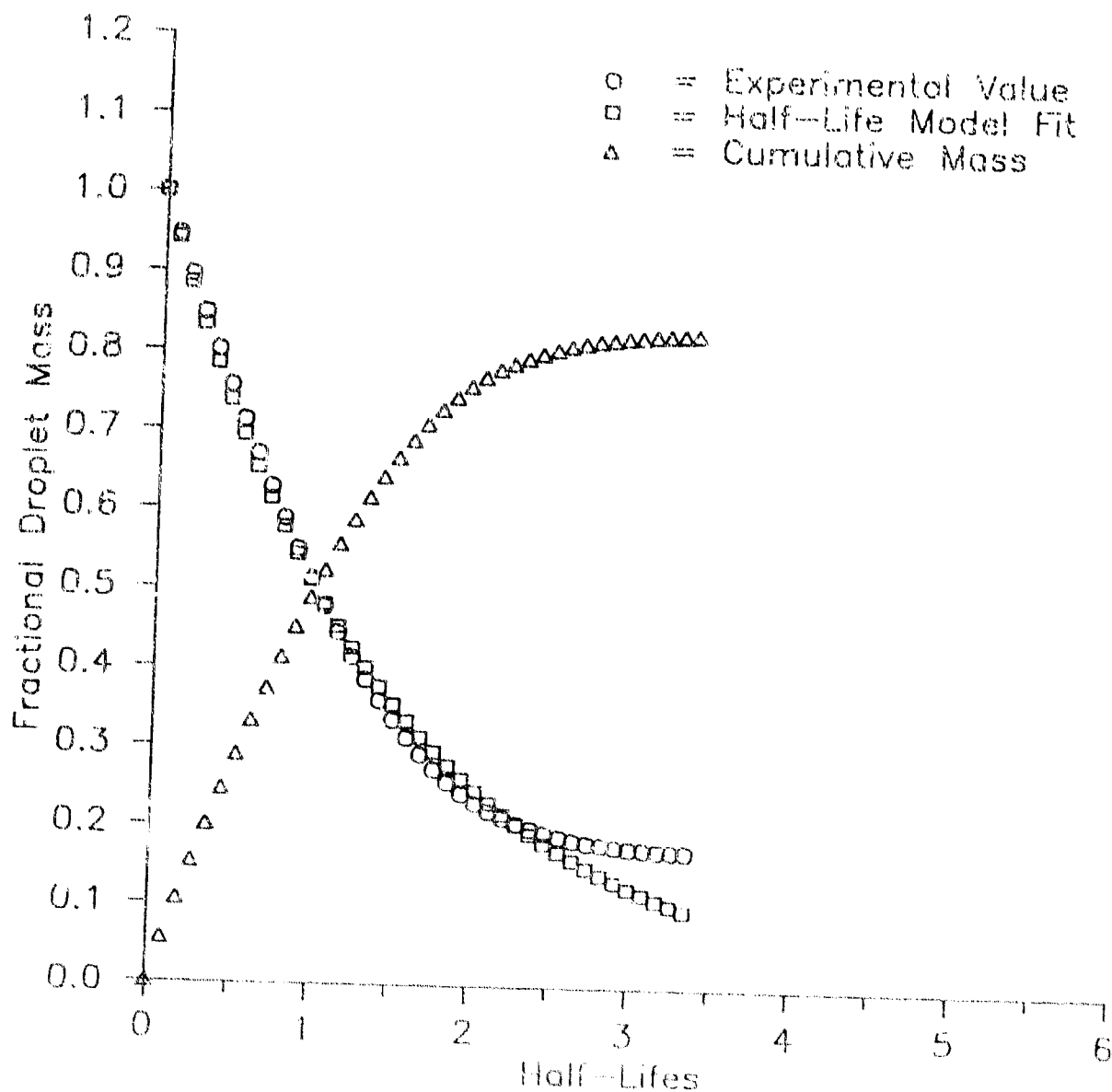


Figure I-21. Fractional Droplet Mass Versus Droplet Half-Life.

EVAPORATION EXPERIMENT NO. BLF6    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/BOTTOM SURFACE  
 WINDSPEED 2.9 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 37%

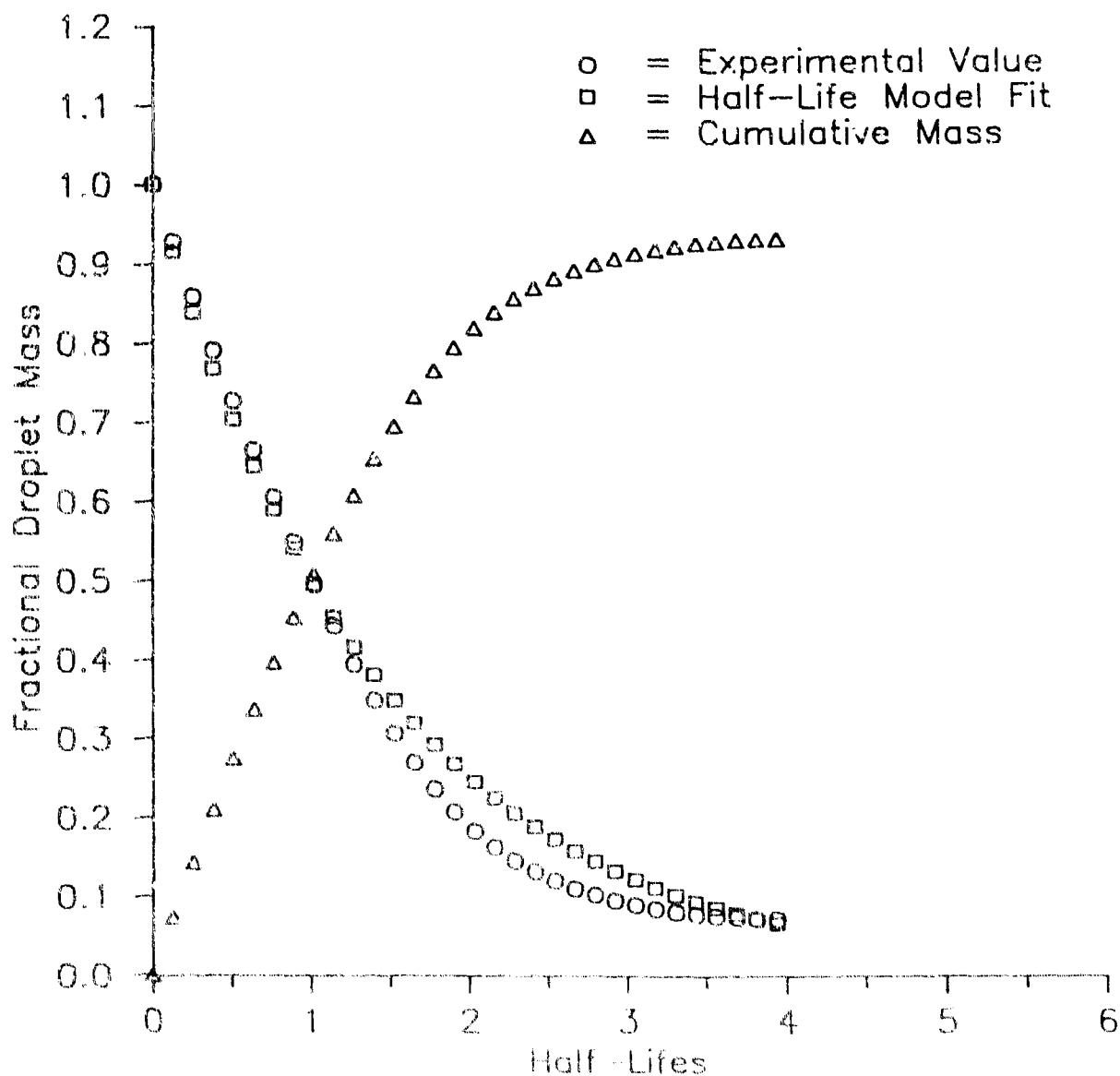


Figure 1-22. Fractional Droplet Mass Versus Droplet Half-Life.

EVAPORATION EXPERIMENT NO. BLF7    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/BOTTOM SURFACE  
 WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 38%

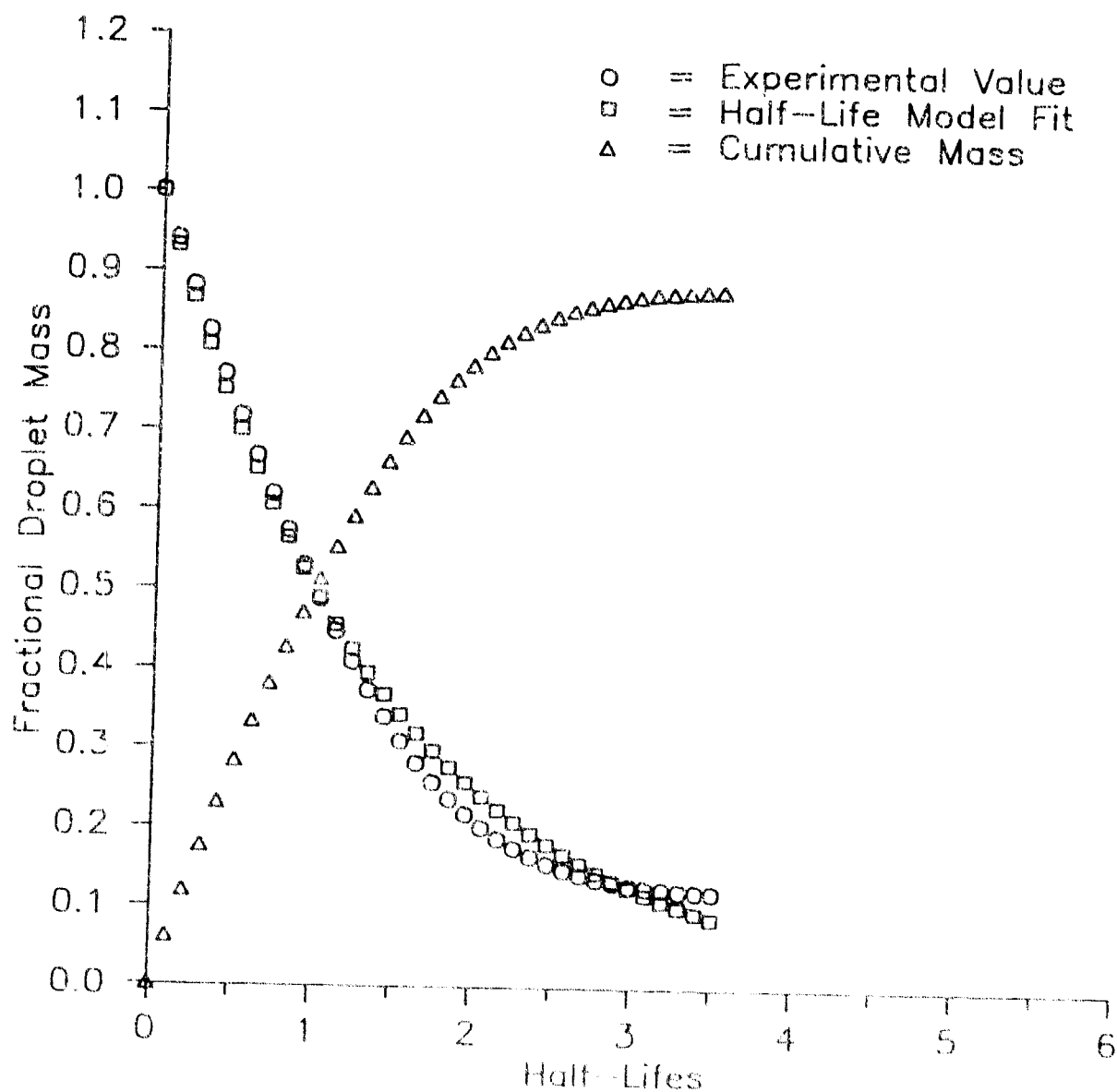


Figure 1-23. Fractional Droplet Mass Versus Droplet Half-Life.

EVAPORATION EXPERIMENT NO. BLF8    SERIES ID 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK LEAF/BOTTOM SURFACE  
 WINDSPEED 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 50%

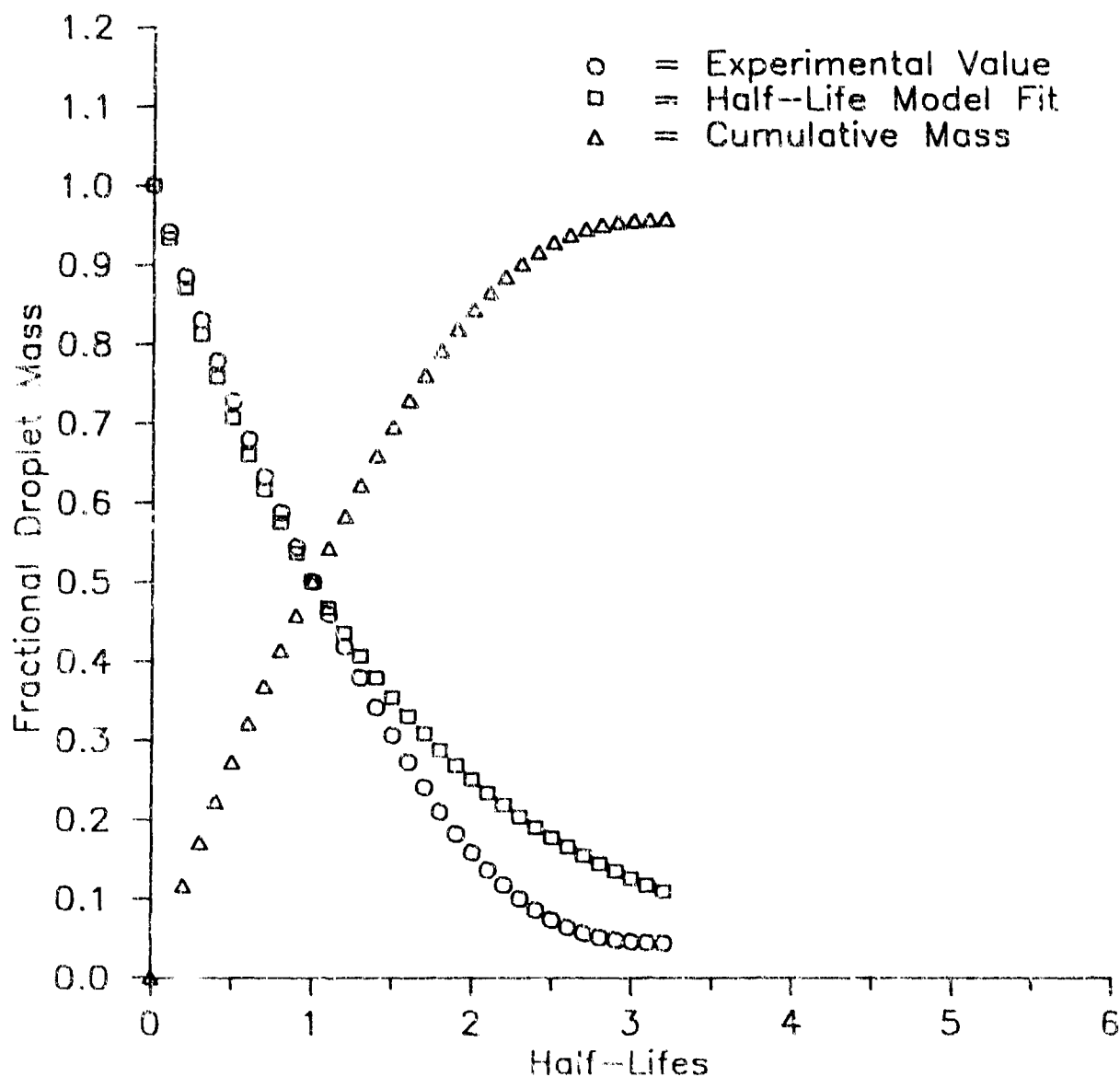


Figure I-24. Fractional Droplet Mass Versus Droplet Half-Life.

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APPENDIX J  
DATA ON SPREADING OF DEM DROPLETS DEPOSITED ON LEAF SURFACES

TABLE J-1. Maximum, Minimum and Average Spread Diameters of 2 mm (D1a.) DEM Droplets Deposited On Green Hickory Leaves.

| TEST<br>#1 | TEST<br>#2 | TEST<br>#3 | TEST<br>#4 | TEST<br>#5 | TEST<br>#6 | TEST<br>#7 | TEST<br>#8 |
|------------|------------|------------|------------|------------|------------|------------|------------|
| D1xD2      | D1xD2      | D1xD2      | D1xD2      | D1xD2      | D1xD2      | D1xD2      | D1xD2      |
| mm mm      | mm mm      | mm mm      | mm mm      | mm mm      | mm mm      | mm mm      | mm mm      |
| 6 6        | 5 5        | 35 2       | 8 4        | 4 4        | 5 4        | 9 4        | 4 4        |
| 8 5        | 5 4        | 14 4       | 7 5        | 4 4        | 4 4        | 5 4        | 5 4        |
| 8 4        | 5 4        | 6 4        | 7 5        | 4 4        | 6 4        | 4 4        | 4 4        |
| 6 4        | 6 6        | 5 4        | 6 5        | 5 4        | 5 4        | 4 4        | 5 4        |
| 5 5        | 5 5        | 6 4        | 8 6        | 4 4        | 5 4        | 4 4        | 4 4        |
| 6 6        | 6 6        | 5 4        | 6 5        | 4 4        | 5 4        | 6 4        | 4 4        |
| 4 4        | 6 5        | 6 3        | 6 5        | 5 4        | 5 4        | 5 4        | 6 4        |
| 4 4        | 6 5        | 6 4        | 5 5        | 4 4        | 5 4        | 4 4        | 5 4        |
| 5 4        | 7 6        | 7 4        | 6 6        | 4 4        | 5 4        | 4 4        | 5 4        |
| 4 4        | 8 5        | 4 4        | 7 6        | 5 4        | 4 4        | 4 4        | 5 5        |
| 8 5        | 7 6        | 12 4       | 6 5        | 4 4        | 4 4        | 4 4        | 5 4        |
| 6 5        | 7 7        | 6 4        | 6 5        | 4 4        | 4 4        | 4 4        | 6 4        |
| 8 6        | 7 6        | 12 9       | 10 5       | 5 4        | 4 4        | 4 4        | 4 4        |
| 8 6        | 7 6        | 7 6        | 7 7        | 4 4        | 4 4        | 4 4        | 4 4        |
| 6 4        | 9 6        | 7 4        | 6 5        | 5 4        | 5 4        | 5 4        | 5 4        |
| 5 5        | 7 5        | 6 5        | 7 6        | 4 4        | 6 5        | 4 4        | 4 4        |
| 5 5        | 7 6        | 7 5        | 7 5        | 4 4        | 5 4        | 4 4        | 4 4        |
| 7 6        | 7 5        | 6 4        | 5 4        | 4 4        | 5 4        | 5 4        | 5 4        |
| 6 5        | 8 6        | 6 3        | 8 7        | 5 4        | 4 4        | 4 4        | 5 4        |
| 7 5        | 7 5        | 7 5        | 6 6        | 4 4        | 4 4        | 4 4        | 3 3        |
| 8 6        | 5 5        | 6 5        | 9 6        | 5 3        | 5 4        | 5 4        | 5 4        |
| 8 4        | 11 5       | 6 5        | 5 5        | 4 4        | 4 4        | 8 4        | 4 4        |
| 5 5        | 11 5       | 5 4        | 12 6       | 4 4        | 4 4        | 4 4        | 4 4        |
| 8 5        | 6 6        | 6 4        | 7 6        | 4 4        | 7 4        | 4 4        | 4 4        |
| 5 5        | 7 5        | 6 6        | 8 8        | 4 4        | 4 4        | 5 3        | 4 4        |
| 7 5        | 7 6        | 6 6        | 7 6        | 5 4        | 7 4        | 4 4        | 4 4        |
| 8 4        | 8 5        | 6 5        | 9 8        | 5 4        | 4 4        | 4 4        | 4 4        |
| 7 4        | 7 5        | 5 4        | 6 6        | 4 4        | 4 4        | 5 4        | 5 4        |
| 6 6        | 6 6        | 8 6        | 6 6        | 4 4        | 4 4        | 5 5        | 4 4        |
| 6 6        | 8 5        | 6 4        | 10 6       | 4 4        | 4 4        | 4 4        | 4 4        |
| 7 6        | 7 5        | 6 6        | 10 6       | 4 4        | 4 4        | 5 4        | 4 3        |
| 6 5        | 6 5        | 8 4        | 8 7        | 4 4        | 5 4        | 5 4        | 5 4        |
| 5 5        | 6 5        | 5 4        | 8 6        | 5 3        | 4 4        | 5 4        | 4 4        |
| 6 6        | 6 6        | 5 4        | 6 6        | 4 4        | 4 4        | 4 4        | 4 4        |
| 6 5        | 6 6        | 7 5        | 7 5        | 4 4        | 4 4        | 6 4        | 4 4        |
| 5 5        | 9 6        | 5 4        | 10 5       | 4 4        | 4 4        | 4 4        | 5 5        |
| 6 5        | 10 5       | 6 4        | 8 7        | 5 4        | 5 4        | 4 4        | 4 4        |
| 6 6        | 8 7        | 7 5        | 6 5        | 4 4        | 4 4        | 4 4        | 5 4        |
| 5 5        | 5 5        | 9 4        | 7 5        | 5 4        | 4 4        | 4 4        | 6 4        |
| 5 4        | 7 5        | 6 6        | 7 6        | 4 4        | 5 4        | 5 3        | 5 5        |
| AVG        | AVG        | AVG        | AVG        | AVG        | AVG        | AVG        | AVG        |
| 5.59mm     | 6.16mm     | 5.94mm     | 6.49mm     | 4.12mm     | 4.31mm     | 4.30mm     | 4.28mm     |
| +/-        | +/-        | +/-        | +/-        | +/-        | +/-        | +/-        | +/-        |
| 0.81       | 0.87       | 40         | 1.03       | 0.22       | 0.43       | 0.55       | 0.47       |
| s.d.       | s.d.       | s.d.       | s.d.       | s.d.       | s.d.       | s.d.       | s.d.       |

TABLE J-2. Maximum, Minimum and Average Spread Diameters of 2 mm (Dia.) DEM Droplets Deposited on Green Oak Leaves.

| TEST<br>#9<br>D1xD2                  | TEST<br>#10<br>D1xD2                 | TEST<br>#11<br>D1xD2                 | TEST<br>#12<br>D1xD2                 | TEST<br>#13<br>D1xD2                 | TEST<br>#14<br>D1xD2                 | TEST<br>#15<br>D1xD2         | TEST<br>#16<br>D1xD2                 |
|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|------------------------------|--------------------------------------|
| mm mm                                | mm mm                                | mm mm                                | mm mm                                | mm mm                                | mm mm                                | mm mm                        | mm mm                                |
| 6 5                                  | 6 4                                  | 8 5                                  | 6 5                                  | 4 4                                  | 4 4                                  | - -                          | 5 4                                  |
| 6 4                                  | 7 4                                  | 5 5                                  | 5 3                                  | 4 5                                  | 5 4                                  | - -                          | 4 4                                  |
| 6 4                                  | 5 5                                  | 8 5                                  | 6                                    | 4 5                                  | 4 4                                  | - -                          | 5 4                                  |
| 6 5                                  | 6 4                                  | 8 5                                  | 9 5                                  | 4 4                                  | 4 4                                  | - -                          | 4 4                                  |
| 7 4                                  | 6 5                                  | 6 5                                  | 6 6                                  | 4 4                                  | 4 4                                  | - -                          | 4 4                                  |
| 5 5                                  | 4 4                                  | 5 5                                  | 7 5                                  | 4 4                                  | 4 4                                  | - -                          | 4 4                                  |
| 5 5                                  | 5 5                                  | 6 4                                  | 5 3                                  | 4 4                                  | 5 4                                  | - -                          | 4 4                                  |
| 5 5                                  | 5 4                                  | 5 5                                  | 6 4                                  | 4 5                                  | 5 4                                  | - -                          | 4 4                                  |
| 6 5                                  | 8 5                                  | 6 6                                  | 6 4                                  | 4 4                                  | 4 4                                  | - -                          | 4 4                                  |
| 8 5                                  | 5 4                                  | 6 5                                  | 6 4                                  | 4 4                                  | 5 4                                  | - -                          | 4 4                                  |
| 9 5                                  | 6 5                                  | 5 5                                  | 5 5                                  | 4 4                                  | 4 4                                  | - -                          | 5 4                                  |
| 6 6                                  | 6 5                                  | 6 6                                  | 5 4                                  | 4 4                                  | 4 3                                  | - -                          | 5 4                                  |
| 7 6                                  | 8 5                                  | 5 5                                  | 6 4                                  | 4 5                                  | 5 5                                  | - -                          | 4 4                                  |
| 9 5                                  | 6 6                                  | 6 5                                  | 7 5                                  | 4 4                                  | 5 4                                  | - -                          | 5 4                                  |
| 5 4                                  | 7 5                                  | 5 4                                  | 7 4                                  | 4 4                                  | 4 4                                  | - -                          | 4 4                                  |
| 10 5                                 | 6 5                                  | 6 5                                  | 6 6                                  | 4 4                                  | 5 4                                  | - -                          | 4 4                                  |
| 10 6                                 | 5 5                                  | 6 5                                  | 4 4                                  | 4 4                                  | 4 4                                  | - -                          | 4 4                                  |
| 6 5                                  | 5 5                                  | 8 5                                  | 4 4                                  | 5 4                                  | 5 4                                  | - -                          | 4 4                                  |
| 12 5                                 | 5 4                                  | 7 6                                  | 5 4                                  | 4 4                                  | 5 4                                  | - -                          | 4 4                                  |
| 6 5                                  | 6 6                                  | 7 5                                  | 9 3                                  | 4 4                                  | 4 4                                  | - -                          | 4 4                                  |
| 12 5                                 | 6 5                                  | 6 6                                  | 6 5                                  | 4 4                                  | 4 4                                  | - -                          | 4 4                                  |
| 9 7                                  | 5 5                                  | 8 6                                  | 6 4                                  | 5 4                                  | 5 3                                  | - -                          | 4 4                                  |
| 9 8                                  | 6 5                                  | 6 5                                  | 8 4                                  | 4 4                                  | 4 4                                  | - -                          | 4 4                                  |
| 7 6                                  | 6 5                                  | 9 5                                  | 4 4                                  | 4 4                                  | 5 3                                  | - -                          | 5 4                                  |
| 6 6                                  | 5 5                                  | 12 4                                 | 4 4                                  | 5 4                                  | 6 3                                  | - -                          | 4 4                                  |
| 6 6                                  | 8 6                                  | 7 6                                  | 6 5                                  | 4 4                                  | 5 4                                  | - -                          | 4 4                                  |
| 5 4                                  | 7 4                                  | 8 3                                  | 5 5                                  | 4 4                                  | 4 4                                  | - -                          | 5 3                                  |
| 7 4                                  | 9 4                                  | 7 4                                  | 8 6                                  | 5 4                                  | 5 4                                  | - -                          | 4 4                                  |
| 5 4                                  | 6 6                                  | 5 4                                  | 6 5                                  | 4 4                                  | 5 4                                  | - -                          | 4 4                                  |
| 5 5                                  | 7 5                                  | 5 5                                  | 5 4                                  | 4 4                                  | 4 4                                  | - -                          | 5 4                                  |
| 6 4                                  | 6 5                                  | 4 4                                  | 7 4                                  | 4 4                                  | 5 4                                  | - -                          | 5 4                                  |
| 6 6                                  | 7 4                                  | 7 5                                  | 5 4                                  | 5 4                                  | 6 3                                  | - -                          | 4 4                                  |
| 10 5                                 | 5 5                                  | 5 4                                  | 6 5                                  | 6 4                                  | 4 4                                  | - -                          | 4 4                                  |
| 6 5                                  | 6 5                                  | 5 4                                  | 7 5                                  | 5 4                                  | 5 3                                  | - -                          | 4 4                                  |
| 11 5                                 | 7 5                                  | 5 4                                  | 5 5                                  | 4 4                                  | 4 4                                  | - -                          | 4 4                                  |
| 6 6                                  | 7 5                                  | 5 4                                  | 4 4                                  | 4 4                                  | 5 4                                  | - -                          | 4 4                                  |
| 8 6                                  | 8 5                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | - -                          | 4 4                                  |
| 9 6                                  | 6 4                                  | 6 5                                  | 7 5                                  | 4 4                                  | 5 4                                  | - -                          | 4 4                                  |
| 8 5                                  | 7 5                                  | 6 6                                  | 6 6                                  | 5 4                                  | 4 4                                  | - -                          | 5 3                                  |
| 6 5                                  | 7 5                                  | 5 4                                  | 6 5                                  | 4 4                                  | 5 4                                  | - -                          | 4 4                                  |
| AVG<br>6.19mm<br>+/-<br>1.12<br>s.d. | AVG<br>5.53mm<br>+/-<br>0.65<br>s.d. | AVG<br>5.13mm<br>+/-<br>2.11<br>s.d. | AVG<br>5.18mm<br>+/-<br>0.85<br>s.d. | AVG<br>4.18mm<br>+/-<br>0.27<br>s.d. | AVG<br>4.22mm<br>+/-<br>0.30<br>s.d. | AVG<br>-<br>+/-<br>-<br>s.d. | AVG<br>4.11mm<br>+/-<br>0.21<br>s.d. |

TABLE J-3. Maximum, Minimum and Average Spread Diameters of 2 mm (Dia.) DEM Droplets Deposited on Red Oak Leaves.

| TEST<br>#1<br>D1xD2<br>mm mm         | TEST<br>#2<br>D1xD2<br>mm mm         | TEST<br>#3<br>D1xD2<br>mm mm         | TEST<br>#4<br>D1xD2<br>mm mm         | TEST<br>#5<br>D1xD2<br>mm mm         | TEST<br>#6<br>D1xD2<br>mm mm         | TEST<br>#7<br>D1xD2<br>mm mm         | TEST<br>#8<br>D1xD2<br>mm mm         |
|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|--------------------------------------|
| 4 5                                  | 5 5                                  | 5 4                                  | 5 5                                  | 6 4                                  | 4 4                                  | 5 4                                  | 5 4                                  |
| 6 3                                  | 4 4                                  | 4 4                                  | 5 4                                  | 4 4                                  | 4 4                                  | 5 4                                  | 4 4                                  |
| 4 4                                  | 5 5                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 5 4                                  | 5 5                                  |
| 5 4                                  | 5 4                                  | 6 4                                  | 5 5                                  | 4 4                                  | 4 4                                  | 4 4                                  | 5 4                                  |
| 4 4                                  | 5 5                                  | 6 4                                  | 4 4                                  | 3 3                                  | 4 4                                  | 4 4                                  | 4 4                                  |
| 4 4                                  | 4 4                                  | 5 4                                  | 5 5                                  | 3 3                                  | 4 4                                  | 5 4                                  | 5 4                                  |
| 4 4                                  | 5 5                                  | 5 4                                  | 5 4                                  | 4 4                                  | 4 4                                  | 5 4                                  | 5 4                                  |
| 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  |
| 5 4                                  | 5 4                                  | 4 4                                  | 5 5                                  | 4 4                                  | 4 4                                  | 5 4                                  | 4 3                                  |
| 5 4                                  | 5 5                                  | 4 4                                  | 5 5                                  | 4 4                                  | 5 4                                  | 4 4                                  | 7 4                                  |
| 5 4                                  | 5 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 5 4                                  |
| 5 5                                  | 5 5                                  | 5 4                                  | 5 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  |
| 5 4                                  | 5 5                                  | 5 4                                  | 4 4                                  | 4 3                                  | 4 4                                  | 4 4                                  | 4 4                                  |
| 4 4                                  | 5 5                                  | 5 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 5 4                                  | 4 4                                  |
| 5 4                                  | 5 5                                  | 4 4                                  | 5 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  |
| 5 5                                  | 5 5                                  | 4 4                                  | 5 4                                  | 5 4                                  | 4 4                                  | 5 4                                  | 5 5                                  |
| 4 4                                  | 5 5                                  | 5 3                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 3                                  |
| 4 4                                  | 5 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  |
| 5 4                                  | 5 5                                  | 5 4                                  | 4 4                                  | 4 3                                  | 4 4                                  | 6 4                                  | 4 4                                  |
| 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  |
| 4 4                                  | 5 5                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  |
| 5 4                                  | 5 4                                  | 5 5                                  | 7 3                                  | 4 4                                  | 4 4                                  | 5 3                                  | 4 4                                  |
| 4 4                                  | 5 4                                  | 5 5                                  | 6 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  |
| 5 5                                  | 5 5                                  | 5 4                                  | 6 5                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  |
| 5 5                                  | 4 4                                  | 4 4                                  | 5 5                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  |
| 5 4                                  | 4 4                                  | 4 4                                  | 6 5                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  |
| 6 4                                  | 5 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  |
| 5 4                                  | 4 4                                  | 6 3                                  | 5 4                                  | 4 4                                  | 5 4                                  | 5 4                                  | 4 4                                  |
| 6 5                                  | 4 4                                  | 6 3                                  | 5 5                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  |
| 6 5                                  | 4 4                                  | 4 4                                  | 5 4                                  | 4 4                                  | 5 4                                  | 4 4                                  | 4 4                                  |
| 5 4                                  | 5 5                                  | 4 4                                  | 4 4                                  | 4 4                                  | 5 4                                  | 6 4                                  | 4 4                                  |
| 5 4                                  | 5 4                                  | 4 4                                  | 4 4                                  | 4 4                                  | 5 3                                  | 4 4                                  | 4 4                                  |
| 5 4                                  | 6 5                                  | 4 4                                  | 5 5                                  | 5 4                                  | 4 4                                  | 5 4                                  | 5 4                                  |
| 5 4                                  | 6 5                                  | 5 4                                  | 5 5                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  |
| 5 4                                  | 4 4                                  | 4 4                                  | 7 5                                  | 4 4                                  | 4 4                                  | 5 4                                  | 4 4                                  |
| 5 4                                  | 4 4                                  | 4 4                                  | 5 5                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  |
| 5 4                                  | 5 4                                  | 4 4                                  | 7 5                                  | 4 4                                  | 4 4                                  | 4 4                                  | 4 4                                  |
| 6 5                                  | 4 4                                  | 4 4                                  | 5 5                                  | 4 4                                  | 4 4                                  | 4 3                                  | 4 4                                  |
|                                      |                                      |                                      |                                      |                                      |                                      |                                      |                                      |
| AVG<br>4.50mm<br>+/-<br>0.42<br>s.d. | AVG<br>4.59mm<br>+/-<br>0.46<br>s.d. | AVG<br>4.25mm<br>+/-<br>0.36<br>s.d. | AVG<br>4.65mm<br>+/-<br>0.59<br>s.d. | AVG<br>3.92mm<br>+/-<br>0.32<br>s.d. | AVG<br>4.04mm<br>+/-<br>0.14<br>s.d. | AVG<br>4.15mm<br>+/-<br>0.28<br>s.d. | AVG<br>4.13mm<br>+/-<br>0.38<br>s.d. |

APPENDIX K

FACTORIAL ANALYSIS AND HALF NORMAL PROBABILITY PLOTS  
OF STANDARDIZED ABSOLUTE CONTRASTS FOR TESTS ON OAK AND HICKORY LEAVES

TABLE K-1. THE DESIGN MATRIX FOR THE  $2^4$  FACTORIAL EXPERIMENT NO. 1.

| TEST | VARIABLES |   |   |   | CONTRAST CONFOUNDING |
|------|-----------|---|---|---|----------------------|
|      | 1         | 2 | 3 | 4 |                      |
| 1    | -         | - | - | - | MEAN                 |
| 2    | +         | - | - | - | 1                    |
| 3    | -         | + | - | - | 2                    |
| 4    | +         | + | - | - | 12                   |
| 5    | -         | - | + | - | 3                    |
| 6    | +         | - | + | - | 13                   |
| 7    | -         | + | + | - | 23                   |
| 8    | +         | + | + | - | 123                  |
| 9    | -         | - | - | + | 4                    |
| 10   | +         | - | - | + | 14                   |
| 11   | -         | + | - | + | 24                   |
| 12   | +         | + | - | + | 124                  |
| 13   | -         | - | + | + | 34                   |
| 14   | +         | - | + | + | 134                  |
| 15   | -         | + | + | + | 234                  |
| 16   | +         | + | + | + | 1234                 |

#### VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

TABLE K-2. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
HALF-LIFE OF DROPLET (2 MM DIA) CONTAMINATION DEPOSITED  
ON LEAFY SURFACE AT 60 DEG F AND 42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 246   | 218.7       | --             |
| 2    | 1        | 264   | 22.4        | 2002.5625      |
| 3    | 2        | 84    | -178.9      | 127985.063     |
| 4    | 12       | 98    | -4.9        | 95.0625        |
| 5    | 3        | 320   | 72.4        | 20952.5625     |
| 6    | 13       | 332   | -5.1        | 105.0625       |
| 7    | 23       | 148   | -22.9       | 2093.0625      |
| 8    | 123      | 156   | -2.4        | 22.5625        |
| 9    | 4        | 245   | 25.4        | 2575.5625      |
| 10   | 14       | 287   | 9.4         | 351.5625       |
| 11   | 24       | 100   | -9.9        | 390.0625       |
| 12   | 124      | 136   | -2.9        | 33.0625        |
| 13   | 34       | 367   | 6.4         | 162.5625       |
| 14   | 134      | 404   | -2.1        | 18.0625        |
| 15   | 234      | 150   | -17.9       | 1278.0625      |
| 16   | 1234     | 162   | -2.4        | 22.5625        |

TOTAL = 158087.438

#### VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

TABLE K-3. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
 HALF-LIFE OF DROPLET (2 MM DIA) CONTAMINATION DEPOSITED  
 ON LEAFY SURFACE AT 60 DEG F AND 42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 178.9         | 96.67 | 7.99    | 98.33       |
| 14   | 3        | 72.4          | 90    | 3.23    | 95          |
| 13   | 4        | 25.4          | 83.33 | 1.13    | 91.67       |
| 12   | 23       | 22.9          | 76.67 | 1.02    | 88.33       |
| 11   | 1        | 22.4          | 70    | 1       | 85          |
| 10   | 234      | 17.9          | 63.33 | .8      | 81.67       |
| 9    | 24       | 9.9           | 56.67 | .44     | 78.33       |
| 8    | 14       | 9.4           | 50    | .42     | 75          |
| 7    | 34       | 6.4           | 43.33 | .29     | 71.67       |
| 6    | 13       | 5.1           | 36.67 | .23     | 68.33       |
| 5    | 12       | 4.9           | 30    | .22     | 65          |
| 4    | 124      | 2.9           | 23.33 | .13     | 61.67       |
| 3    | 1234     | 2.4           | 16.67 | .11     | 58.33       |
| 2    | 123      | 2.4           | 10    | .11     | 55          |
| 1    | 134      | 2.1           | 3.33  | .09     | 51.67       |

PROB =  $((R(I) - .5) / R(\text{MAX})) * 100\%$  WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
 THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL =  $(\text{PROB} + 100\%) / 2$

#### VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |



# VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

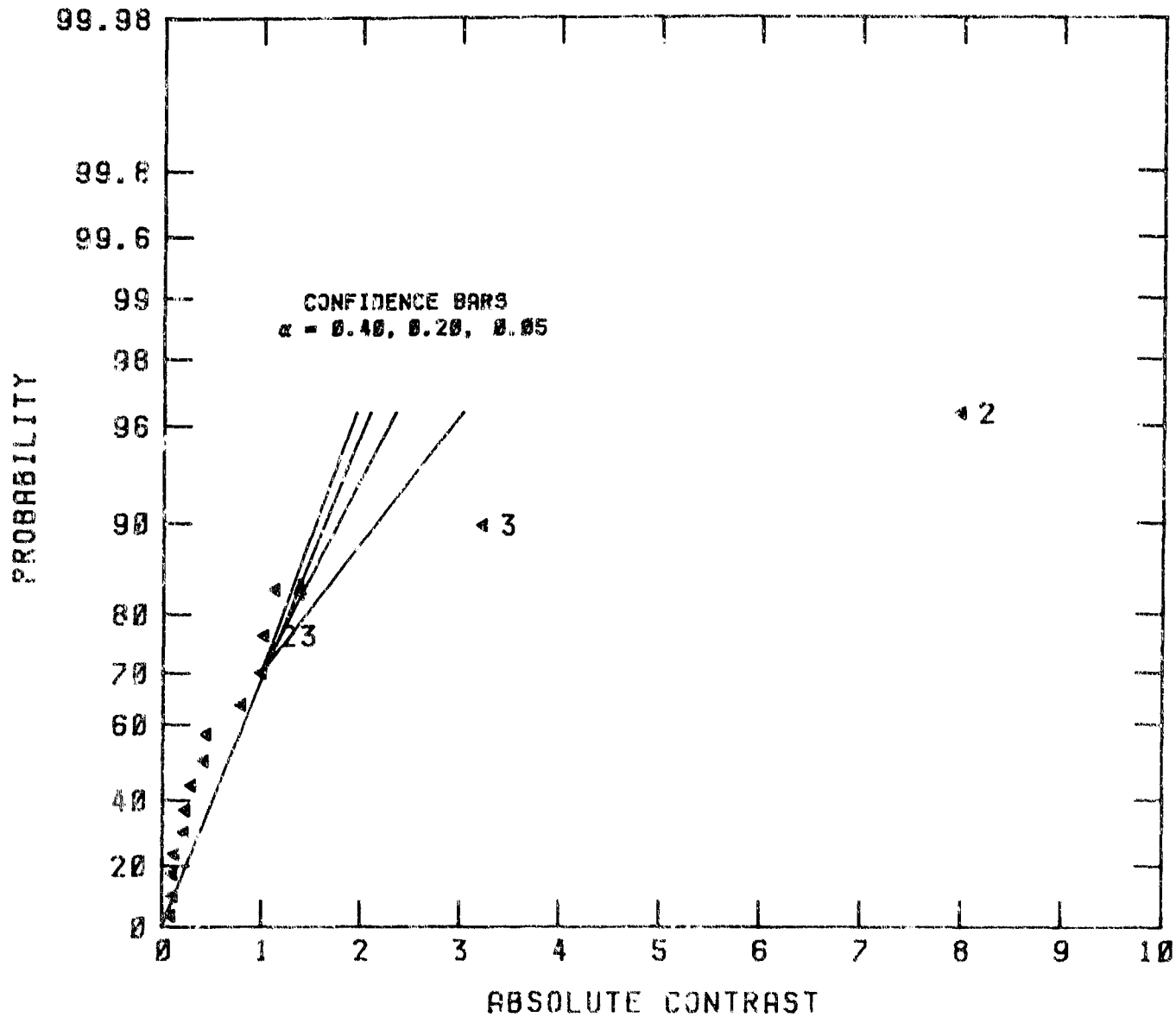


FIGURE K-1. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
HALF-LIFE OF 2 MM DIAMETER DROPS  
DEPOSITED ON LEAF SURFACE AT 80 DEG F AND 42% RH

TABLE K-4. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
AVERAGE EVAPORATION RATE (MMG/MIN) OVER HALF-LIFE OF  
DROPLET (2 MM DIA) DEPOSITED ON LEAF SURFACE AT 60  
DEG F AND 42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 13    | 17.3        | -              |
| 2    | 1        | 12    | -.2         | .25            |
| 3    | 2        | 33    | 14.8        | 870.25         |
| 4    | 12       | 33    | -.5         | 1              |
| 5    | 3        | 9     | -6.5        | 169            |
| 6    | 13       | 9     | .8          | 2.25           |
| 7    | 23       | 20    | -3.2        | 42.25          |
| 8    | 123      | 21    | .5          | 1              |
| 9    | 4        | 10    | -3          | 36             |
| 10   | 14       | 11    | -.2         | .25            |
| 11   | 24       | 28    | -1.2        | 6.25           |
| 12   | 124      | 21    | -1          | 4              |
| 13   | 34       | 7     | 1.5         | 9              |
| 14   | 134      | 8     | .3          | .25            |
| 15   | 234      | 19    | 1.3         | 6.25           |
| 16   | 1234     | 19    | .5          | 1              |

TOTAL = 1149

#### VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)/11 MPH | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

TABLE K-5. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
AVERAGE EVAPORATION RATE (MMG/MIN) OVER HALF-LIFE OF  
DROPIET (2 MM DIA) DEPOSITED ON LEAF SURFACE AT 60  
DEG F AND 42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 14.8          | 96.67 | 9.87    | 98.33       |
| 14   | 3        | 6.5           | 90    | 4.33    | 95          |
| 13   | 23       | 3.2           | 83.33 | 2.13    | 91.67       |
| 12   | 4        | 3             | 76.67 | 2       | 88.33       |
| 11   | 34       | 1.5           | 70    | 1       | 85          |
| 10   | 234      | 1.3           | 63.33 | .87     | 81.67       |
| 9    | 24       | 1.2           | 56.67 | .8      | 78.33       |
| 8    | 124      | 1             | 50    | .67     | 75          |
| 7    | 13       | .8            | 43.33 | .53     | 71.67       |
| 6    | 1234     | .5            | 36.67 | .33     | 68.33       |
| 5    | 123      | .5            | 30    | .33     | 65          |
| 4    | 12       | .5            | 23.33 | .33     | 61.67       |
| 3    | 134      | .3            | 16.67 | .2      | 58.33       |
| 2    | 14       | .2            | 10    | .13     | 55          |
| 1    | 1        | .2            | 3.33  | .13     | 51.67       |

PROB =  $((R(I) - .5) / R(\text{MAX})) * 100\%$  WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL =  $(\text{PROB} + 100\%) / 2$

#### VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

# VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

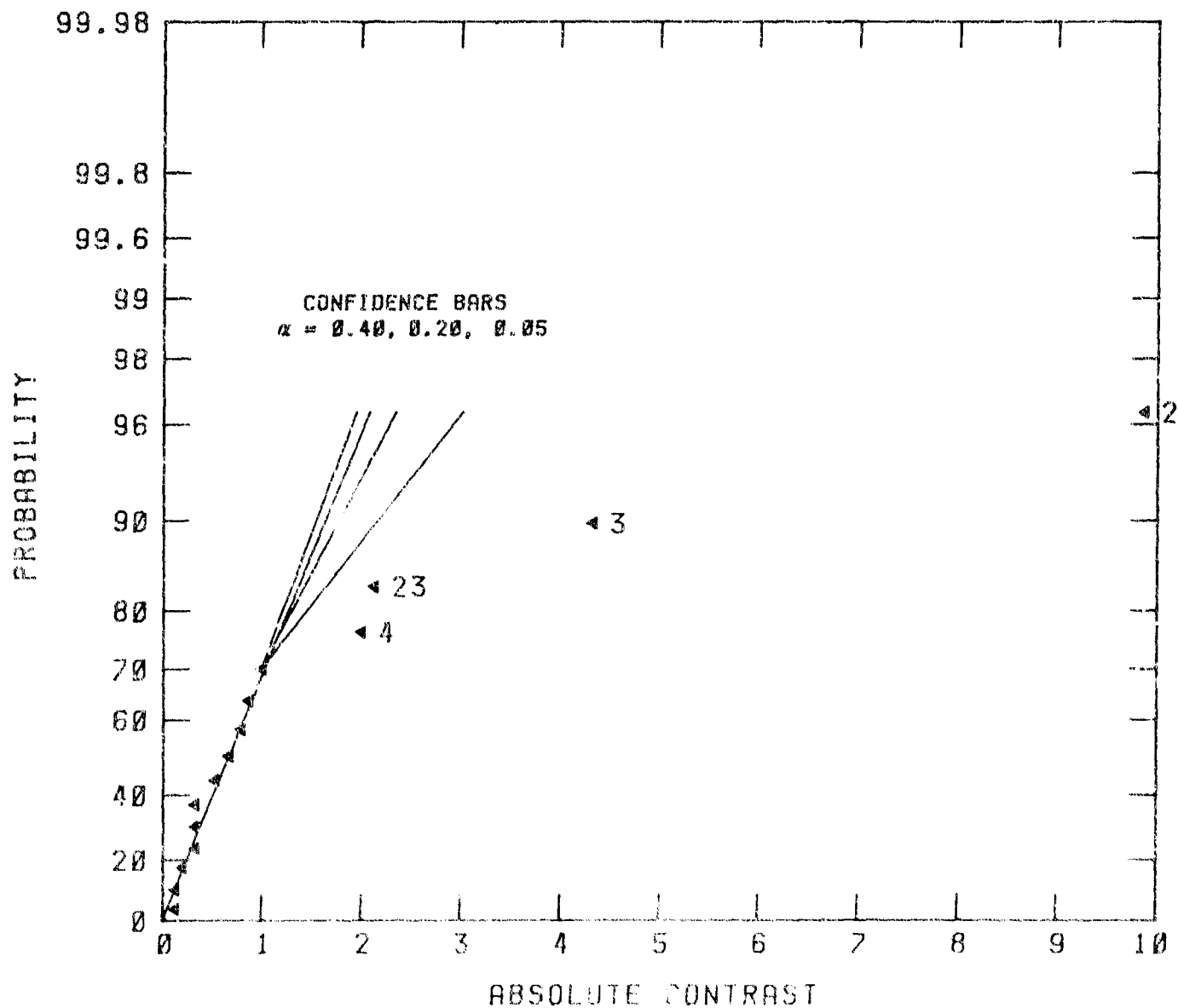


FIGURE K-2. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
 AVERAGE EVAPORATION RATE OVER HALF-LIFE OF 2 MM DIA DROPS  
 DEPOSITED ON LEAF SURFACE AT 60 DEG F AND 42% RH

TABLE K-6. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
TOTAL PERCENT OF DROPLET (2 MM DIA) CONTAMINATION RECOVERED  
AS VAPOR FROM LEAF SURFACE AT 60 DEG F AND 42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 76    | 84.1        | -              |
| 2    | 1        | 84    | 3.1         | 39.0625        |
| 3    | 2        | 84    | 7.9         | 248.0625       |
| 4    | 12       | 94    | -.1         | .0625          |
| 5    | 3        | 75    | -1.4        | 7.5625         |
| 6    | 13       | 77    | -2.4        | 22.5625        |
| 7    | 23       | 87    | -.1         | .0625          |
| 8    | 123      | 89    | -.1         | .0625          |
| 9    | 4        | 80    | 1.6         | 10.5625        |
| 10   | 14       | 83    | -2.4        | 22.5625        |
| 11   | 24       | 88    | -2.6        | 27.5625        |
| 12   | 124      | 89    | -.6         | 1.5625         |
| 13   | 34       | 83    | 1.1         | 5.0625         |
| 14   | 134      | 83    | 1.1         | 5.0625         |
| 15   | 234      | 87    | -1.6        | 10.5625        |
| 16   | 1234     | 86    | .4          | .5625          |

TOTAL = 400.9375

#### VARIABLE #'S AND IDENTITIES

|    |                  |            |            |
|----|------------------|------------|------------|
| 1: | LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: | WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: | LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: | LEAF TYPE        | (+)OAK     | (-)HICKORY |

TABLE K-7. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
TOTAL PERCENT OF DROPLET (2 MM DIA) CONTAMINATION RECOVERED  
AS VAPOR FROM LEAF SURFACE AT 60 DEG F AND 42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 7.9           | 96.67 | 3.29    | 98.33       |
| 14   | 1        | 3.1           | 90    | 1.29    | 95          |
| 13   | 24       | 2.6           | 83.33 | 1.08    | 91.67       |
| 12   | 14       | 2.4           | 76.67 | 1       | 88.33       |
| 11   | 13       | 2.4           | 70    | 1       | 85          |
| 10   | 234      | 1.6           | 63.33 | .67     | 81.67       |
| 9    | 4        | 1.6           | 56.67 | .67     | 78.33       |
| 8    | 3        | 1.4           | 50    | .58     | 75          |
| 7    | 134      | 1.1           | 43.33 | .46     | 71.67       |
| 6    | 34       | 1.1           | 36.67 | .46     | 68.33       |
| 5    | 124      | .6            | 30    | .25     | 65          |
| 4    | 1234     | .4            | 23.33 | .17     | 61.67       |
| 3    | 123      | .1            | 16.67 | .04     | 58.33       |
| 2    | 23       | .1            | 10    | .04     | 55          |
| 1    | 12       | .1            | 3.33  | .04     | 51.67       |

PROB = ((R(I)-.5)/R(MAX))\*100% WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL = (PROB+100%)/2

#### VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

# VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

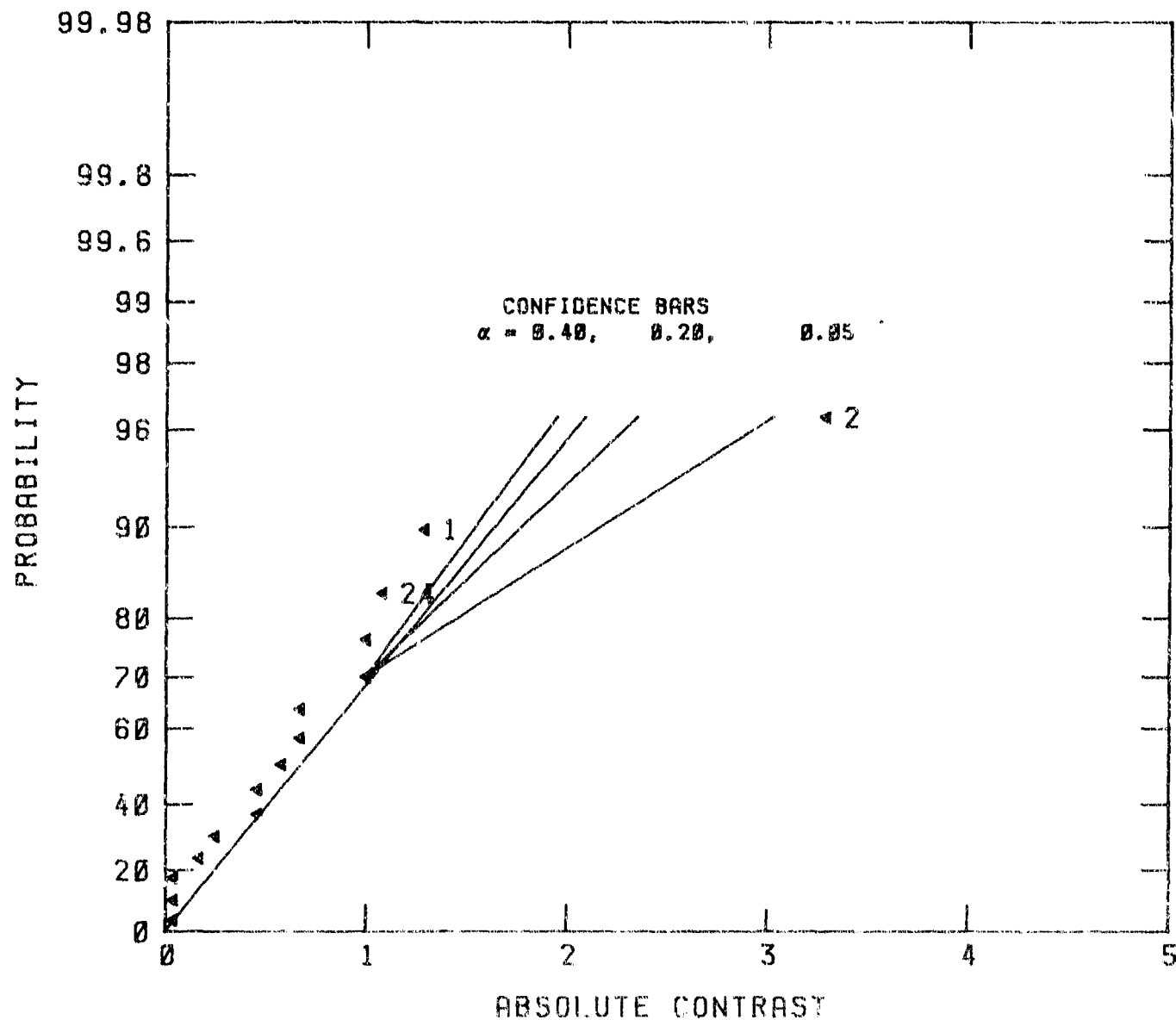


FIGURE K-3. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
TOTAL PERCENT OF CONTAMINATION RECOVERED AS VAPOR FROM  
2 MM DIA DROPS ON LEAF SURFACE AT 80 DEG F AND 42% RH

TABLE K-8. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
LIFE TIME OF DROPLET (2 MM DIA) CONTAMINATION ON LEAF  
SURFACE AT 60 DEG F AND 42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 870   | 698.8       | -              |
| 2    | 1        | 1020  | 31.3        | 3906.25        |
| 3    | 2        | 360   | -562.5      | 1265625        |
| 4    | 12       | 370   | -28.7       | 3306.25        |
| 5    | 3        | 870   | 120         | 57600.0001     |
| 6    | 13       | 900   | -61.2       | 15006.25       |
| 7    | 23       | 480   | -25         | 2500           |
| 8    | 123      | 480   | 43.8        | 7656.25002     |
| 9    | 4        | 780   | 60          | 14400          |
| 10   | 14       | 960   | -16.2       | 1056.25        |
| 11   | 24       | 360   | -70         | 19600          |
| 12   | 124      | 390   | 13.8        | 756.25         |
| 13   | 34       | 1280  | 92.5        | 34225          |
| 14   | 134      | 1160  | -28.7       | 3306.25        |
| 15   | 234      | 465   | -112.5      | 50625.0001     |
| 16   | 1234     | 435   | 16.3        | 1056.25        |

TOTAL = 1480625

VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |



TABLE K-9. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
LIFE TIME OF DROPLET (2 MM DIA) CONTAMINATION ON LEAF  
SURFACE AT 60 DEG F AND 42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 562.5         | 96.67 | 8.04    | 98.33       |
| 14   | 3        | 120           | 90    | 1.71    | 95          |
| 13   | 234      | 112.5         | 83.33 | 1.61    | 91.67       |
| 12   | 34       | 92.5          | 76.67 | 1.32    | 88.33       |
| 11   | 24       | 70            | 70    | 1       | 85          |
| 10   | 13       | 61.2          | 63.33 | .87     | 81.67       |
| 9    | 4        | 60            | 56.67 | .86     | 78.33       |
| 8    | 123      | 43.8          | 50    | .63     | 75          |
| 7    | 1        | 31.3          | 43.33 | .45     | 71.67       |
| 6    | 134      | 28.7          | 36.67 | .41     | 68.33       |
| 5    | 12       | 28.7          | 30    | .41     | 65          |
| 4    | 23       | 25            | 23.33 | .36     | 61.67       |
| 3    | 1234     | 16.3          | 16.67 | .23     | 58.33       |
| 2    | 14       | 16.2          | 10    | .23     | 55          |
| 1    | 124      | 13.8          | 3.33  | .2      | 51.67       |

PROB =  $((R(I) - .5) / R(\text{MAX})) * 100\%$  WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL =  $(\text{PROB} + 100\%) / 2$

#### VARIABLE #'S AND IDENTITIES

|    |                  |            |            |
|----|------------------|------------|------------|
| 1: | LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: | WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: | LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: | LEAF CONDITION   | (+)OAK     | (-)HICKORY |

# VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

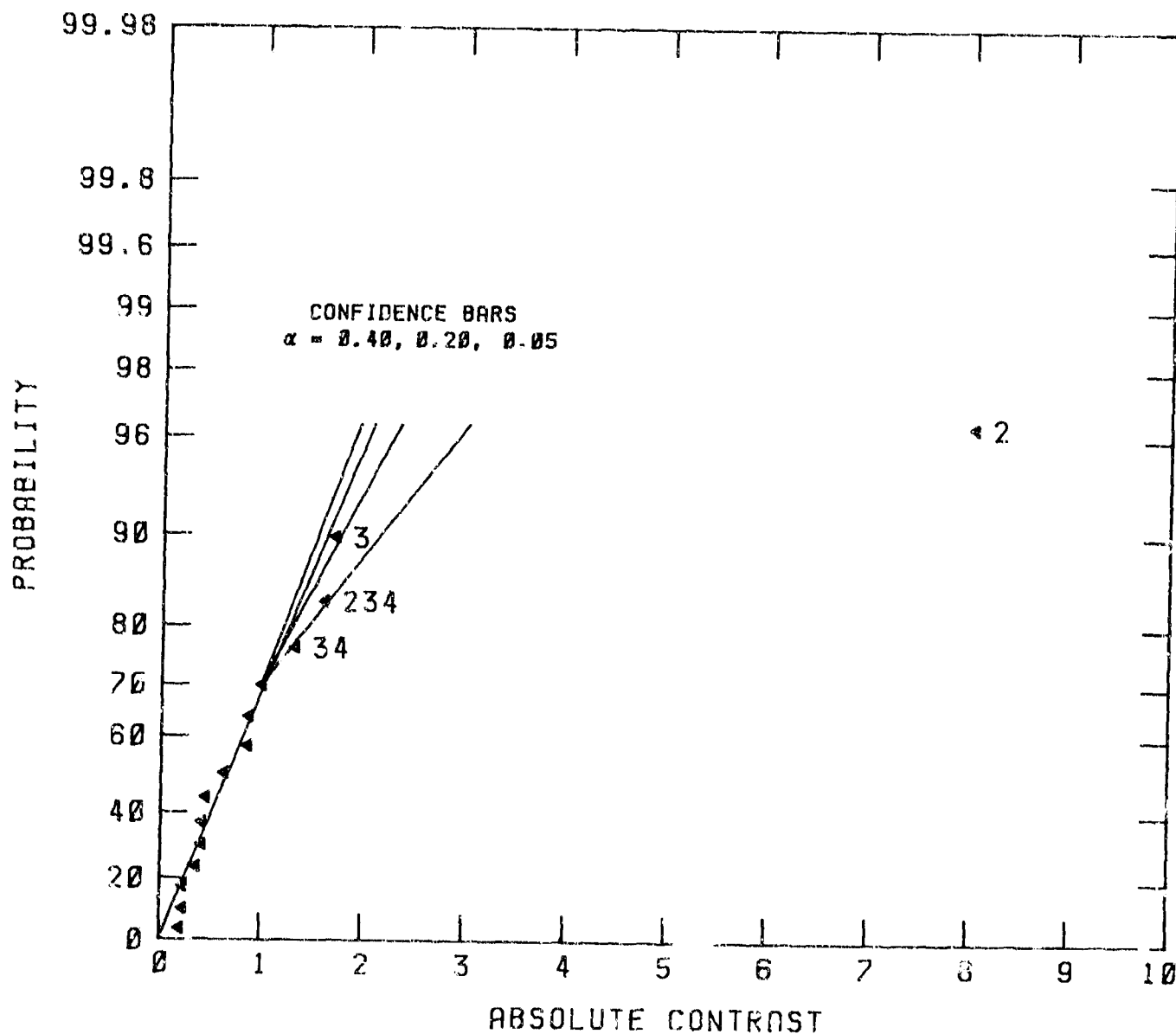


FIGURE K-4. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
 LIFE TIME OF 2 MM DIA DROPLETS DEPOSITED ON  
 LEAF SURFACE AT 80 DEG F AND 42% RH

TABLE K-10. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
AVERAGE EVAPORATION RATE (MMG/MIN) OVER LIFE TIME OF  
DROPLET (2 MM DIA) CONTAMINATION ON LEAF SURFACE AT  
60 DEG F AND 42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 5     | 9           | -              |
| 2    | 1        | 5     | 1           | 4              |
| 3    | 2        | 13    | 8           | 256            |
| 4    | 12       | 16    | .5          | 1              |
| 5    | 3        | 5     | -1.7        | 12.25          |
| 6    | 13       | 5     | -.2         | .25            |
| 7    | 23       | 11    | -1.2        | 6.25           |
| 8    | 123      | 12    | -.2         | .25            |
| 9    | 4        | 5     | 0           | 0              |
| 10   | 14       | 6     | 0           | 0              |
| 11   | 24       | 14    | 0           | 0              |
| 12   | 124      | 15    | -.5         | 1              |
| 13   | 34       | 4     | -.2         | .25            |
| 14   | 134      | 5     | .3          | .25            |
| 15   | 234      | 11    | .3          | .25            |
| 16   | 1234     | 12    | .3          | .25            |

TOTAL = 282

#### VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

TABLE K-11. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
AVERAGE EVAPORATION RATE (MMG/MIN) OVER LIFE TIME OF  
DROPLET (2 MM DIA) CONTAMINATION ON LEAF SURFACE AT  
60 DEG F AND 42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 8             | 96.67 | 16      | 98.33       |
| 14   | 3        | 1.7           | 90    | 3.4     | 95          |
| 13   | 23       | 1.2           | 83.33 | 2.4     | 91.67       |
| 12   | 1        | 1             | 76.67 | 2       | 88.33       |
| 11   | 124      | .5            | 70    | 1       | 85          |
| 10   | 12       | .5            | 63.33 | 1       | 81.67       |
| 9    | 1234     | .3            | 56.67 | .6      | 78.33       |
| 8    | 234      | .3            | 50    | .6      | 75          |
| 7    | 134      | .3            | 43.33 | .6      | 71.67       |
| 6    | 34       | .2            | 36.67 | .4      | 68.33       |
| 5    | 123      | .2            | 30    | .4      | 65          |
| 4    | 13       | .2            | 23.33 | .4      | 61.67       |
| 3    | 24       | 0             | 16.67 | 0       | 58.33       |
| 2    | 14       | 0             | 10    | 0       | 55          |
| 1    | 4        | 0             | 3.33  | 0       | 51.67       |

PROB =  $((R(I) - .5) / R(\text{MAX})) * 100\%$  WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL =  $(\text{PROB} + 100\%) / 2$

#### VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

# VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

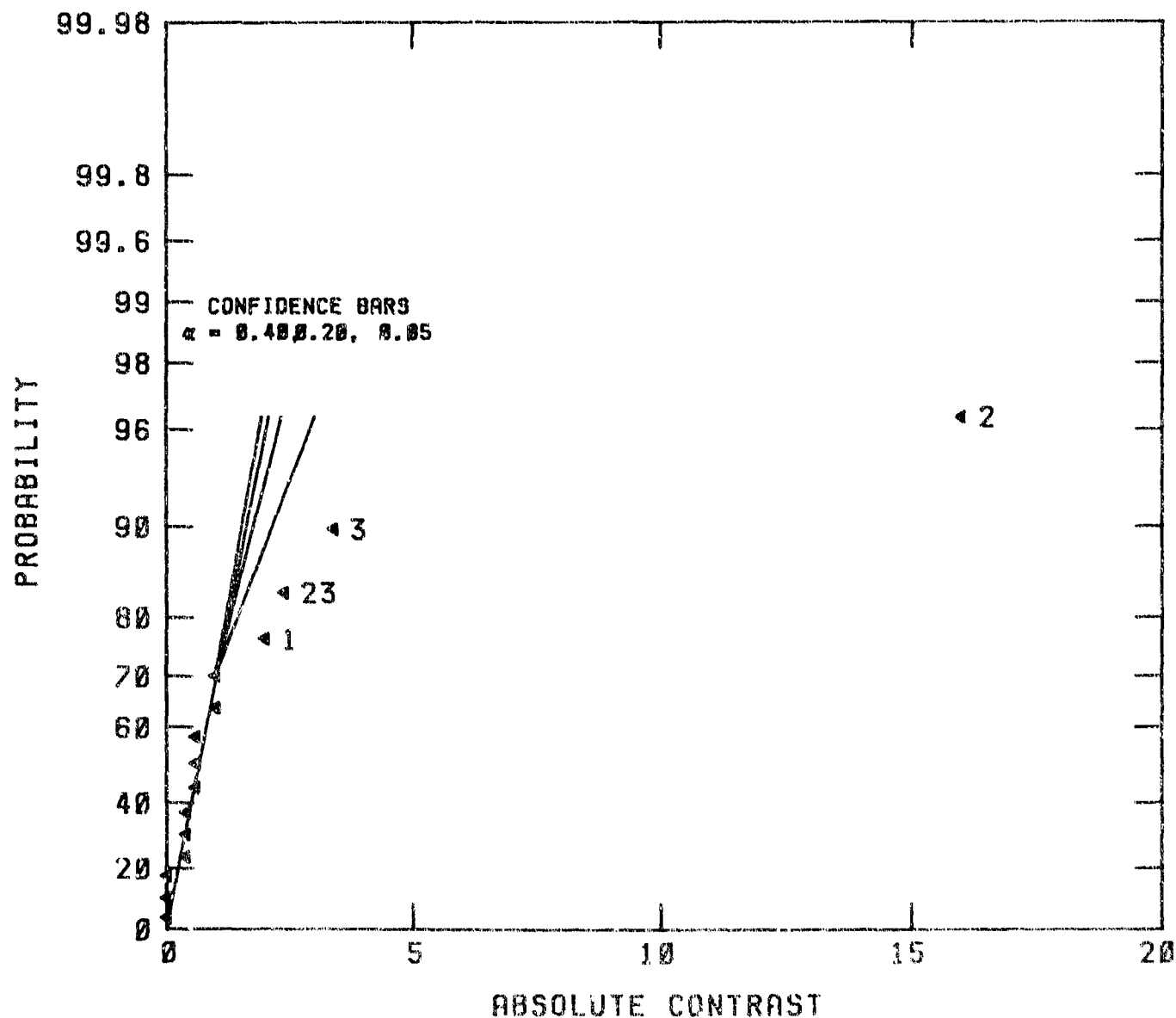


FIGURE K-5. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
 AVERAGE EVAPORATION RATE FOR 2 MM DIA DROPLETS  
 DEPOSITED ON LEAF SURFACE AT 60 DEG F AND 42% RH

TABLE K-12. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
PERCENT OF DROPLET (2 MM DIA) CONTAMINATION RECOVERED  
AS VAPOR AFTER 1 HR FROM LEAF SURFACE AT 60 DEG F AND  
42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 16    | 19.9        | -              |
| 2    | 1        | 14    | -3          | 36             |
| 3    | 2        | 39    | 14.5        | 641            |
| 4    | 12       | 33    | -1.2        | 6.25           |
| 5    | 3        | 12    | -7.2        | 210.25         |
| 6    | 13       | 11    | 2           | 16             |
| 7    | 23       | 23    | -3          | 36             |
| 8    | 123      | 22    | 1.3         | 6.25           |
| 9    | 4        | 16    | -2.7        | 30.25          |
| 10   | 14       | 13    | -.5         | 1              |
| 11   | 24       | 33    | -1.5        | 9              |
| 12   | 124      | 24    | -.2         | .25            |
| 13   | 34       | 10    | 1.3         | 6.25           |
| 14   | 134      | 9     | .5          | 1              |
| 15   | 234      | 22    | 2           | 16             |
| 16   | 1234     | 21    | .3          | .25            |

TOTAL = 1215.75

#### VARIABLE #'S AND IDENTITIES

|    |                  |            |            |
|----|------------------|------------|------------|
| 1: | LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: | WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: | LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: | LEAF TYPE        | (+)OAK     | (-)HICKORY |

TABLE K-13. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
PERCENT OF DROPLET (2 MM DIA) CONTAMINATION RECOVERED  
AS VAPOR AFTER 1 HR FROM LEAF SURFACE AT 60 DEG F AND  
42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 14.5          | 96.67 | 5.37    | 98.33       |
| 14   | 3        | 7.2           | 90    | 2.67    | 95          |
| 13   | 23       | 3             | 83.33 | 1.11    | 91.67       |
| 12   | 1        | 3             | 76.67 | 1.11    | 88.33       |
| 11   | 4        | 2.7           | 70    | 1       | 85          |
| 10   | 234      | 2             | 63.33 | .74     | 81.67       |
| 9    | 13       | 2             | 56.67 | .74     | 78.33       |
| 8    | 24       | 1.5           | 50    | .56     | 75          |
| 7    | 34       | 1.3           | 43.33 | .48     | 71.67       |
| 6    | 123      | 1.3           | 36.67 | .48     | 68.33       |
| 5    | 12       | 1.2           | 30    | .44     | 65          |
| 4    | 134      | .5            | 23.33 | .19     | 61.67       |
| 3    | 14       | .5            | 16.67 | .19     | 58.33       |
| 2    | 1234     | .3            | 10    | .11     | 55          |
| 1    | 124      | .2            | 3.33  | .07     | 51.67       |

PROB =  $((R(I) - .5) / R(\text{MAX})) * 100\%$  WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL =  $(\text{PROB} + 100\%) / 2$

#### VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

# VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

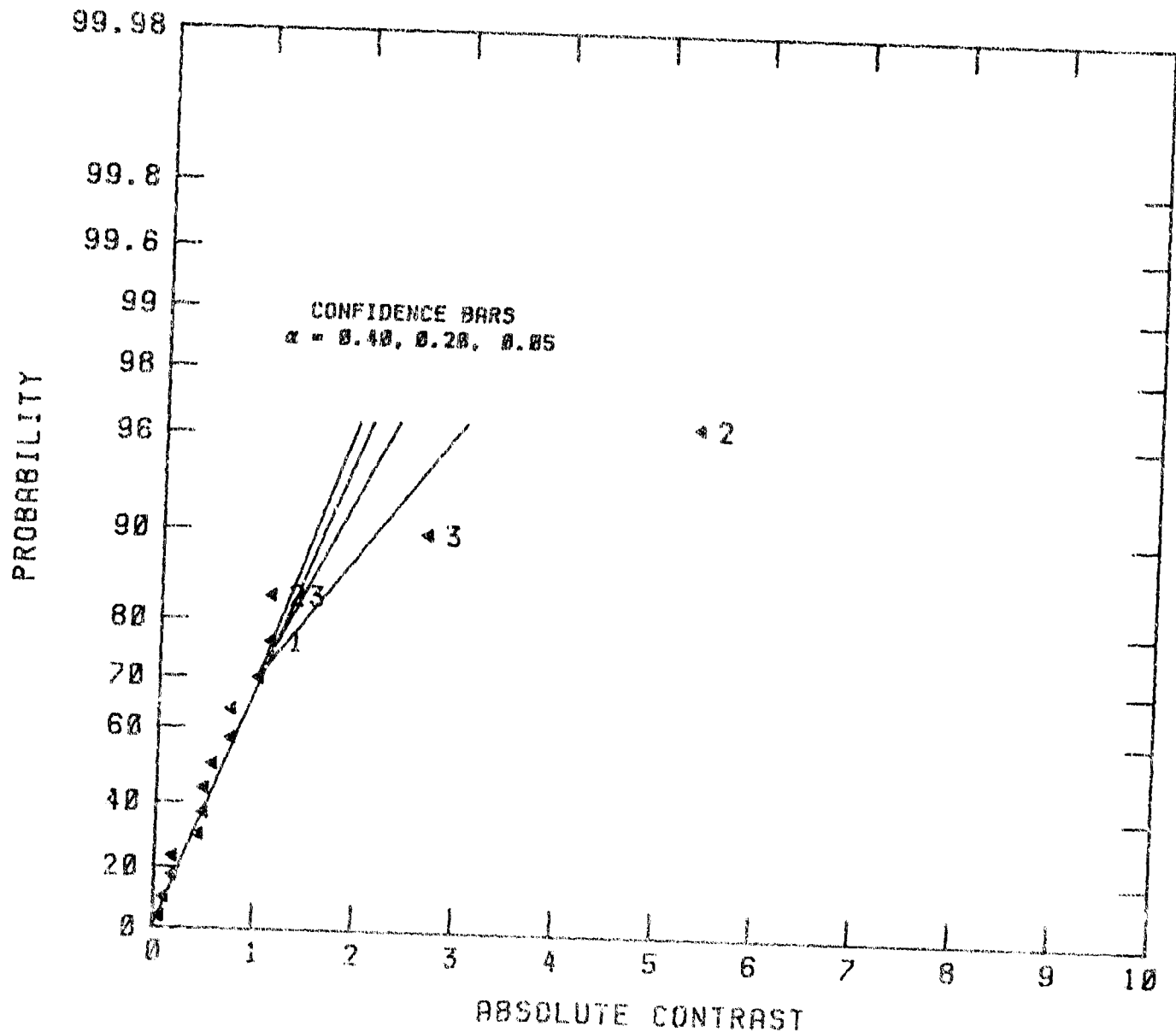


FIGURE K-6. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
 PERCENT OF CONTAMINATION RECOVERED AS VAPOR AFTER 1 HR  
 FROM 2 MM DIA DROPS ON LEAF SURFACE AT 80 DEG F AND 42% RH



TABLE K-14. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
PERCENT OF DROPLET (2 MM DIA) CONTAMINATION RECOVERED  
AS VAPOR AFTER 2 HR FROM LEAF SURFACE AT 60 DEG F AND  
42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 29    | 35.9        | -              |
| 2    | 1        | 27    | -4          | 64             |
| 3    | 2        | 63    | 24.8        | 2450.25        |
| 4    | 12       | 58    | -1.5        | 9              |
| 5    | 3        | 22    | -11.2       | 506.25         |
| 6    | 13       | 21    | 2           | 16             |
| 7    | 23       | 42    | -3.7        | 56.25          |
| 8    | 123      | 40    | 1           | 4              |
| 9    | 4        | 29    | -3.7        | 56.25          |
| 10   | 14       | 24    | -1.5        | 9              |
| 11   | 24       | 57    | -1.2        | 6.25           |
| 12   | 124      | 45    | -.5         | 1              |
| 13   | 34       | 19    | 1.8         | 12.25          |
| 14   | 134      | 17    | 1           | 4              |
| 15   | 234      | 42    | 2.8         | 30.25          |
| 16   | 1234     | 39    | .5          | 1              |

TOTAL = 3225.75

#### VARIABLE #'S AND IDENTITIES

|    |                  |            |            |
|----|------------------|------------|------------|
| 1: | LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: | WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: | LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: | LEAF TYPE        | (+)OAK     | (-)HICKORY |

TABLE K-15. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
PERCENT OF DROPLET (2 MM DIA) CONTAMINATION RECOVERED  
AS VAPOR AFTER 2 HR FROM LEAF SURFACE AT 60 DEG F AND  
42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 24.8          | 96.67 | 6.7     | 98.33       |
| 14   | 3        | 11.2          | 90    | 3.03    | 95          |
| 13   | 1        | 4             | 83.33 | 1.08    | 91.67       |
| 12   | 4        | 3.7           | 76.67 | 1       | 88.33       |
| 11   | 23       | 3.7           | 70    | 1       | 85          |
| 10   | 234      | 2.8           | 63.33 | .76     | 81.67       |
| 9    | 13       | 2             | 56.67 | .54     | 78.33       |
| 8    | 34       | 1.8           | 50    | .49     | 75          |
| 7    | 14       | 1.5           | 43.33 | .41     | 71.67       |
| 6    | 12       | 1.5           | 36.67 | .41     | 68.33       |
| 5    | 24       | 1.2           | 30    | .32     | 65          |
| 4    | 134      | 1             | 23.33 | .27     | 61.67       |
| 3    | 123      | 1             | 16.67 | .27     | 58.33       |
| 2    | 1234     | .5            | 10    | .14     | 55          |
| 1    | 124      | .5            | 3.33  | .14     | 51.67       |

PROB = ((R(I)-.5)/R(MAX))\*100% WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL = (PROB+100.)/2

#### VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

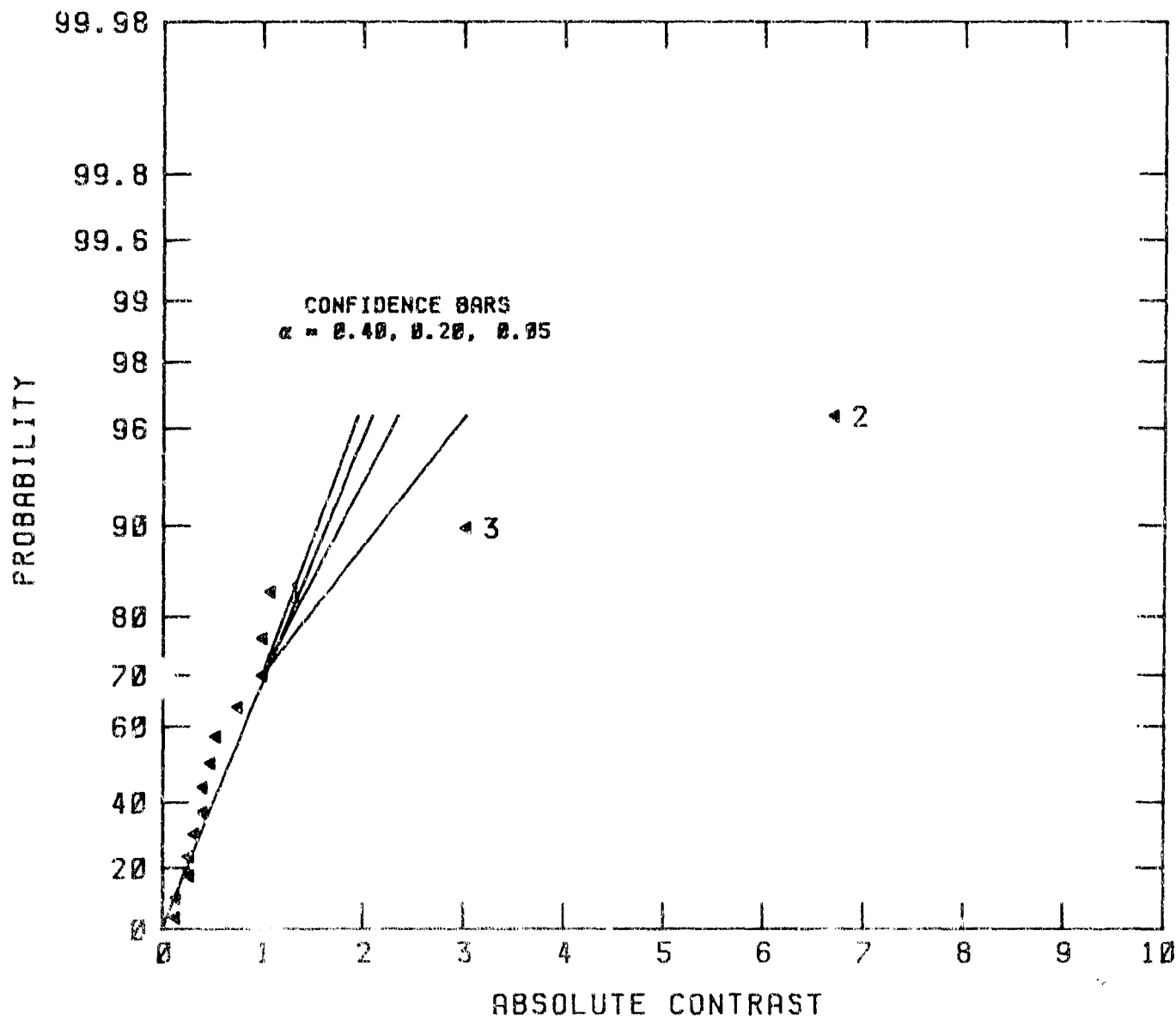


FIGURE K-7. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
 PERCENT OF CONTAMINATION RECOVERED AS VAPOR AFTER 2 HR  
 FROM 2 MM DIA DROPS ON LEAF SURFACE AT 80 DEG F AND 42% RH

TABLE K-16. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
PERCENT OF DROPLET (2 MM DIA) CONTAMINATION RECOVERED  
AS VAPOR AFTER 3 HR FROM LEAF SURFACE AT 60 DEG F AND  
42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 40    | 48.5        | -              |
| 2    | 1        | 37    | -4.2        | 72.25          |
| 3    | 2        | 76    | 31.3        | 3906.25        |
| 4    | 12       | 75    | -.5         | 1              |
| 5    | 3        | 32    | -12.5       | 625            |
| 6    | 13       | 30    | 1.3         | 6.25           |
| 7    | 23       | 58    | -2.7        | 30.25          |
| 8    | 123      | 56    | .5          | 1              |
| 9    | 4        | 40    | -4          | 64             |
| 10   | 14       | 34    | -2.2        | 20.25          |
| 11   | 24       | 74    | -.2         | .25            |
| 12   | 124      | 62    | -1          | 4              |
| 13   | 34       | 27    | .5          | 1              |
| 14   | 134      | 23    | 1.3         | 6.25           |
| 15   | 234      | 58    | 2.8         | 30.25          |
| 16   | 1234     | 54    | 1           | 4              |

TOTAL = 4772

#### VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

TABLE K-17. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
PERCENT OF DROPLET (2 MM DIA) CONTAMINATION RECOVERED  
AS VAPOR AFTER 3 HR FROM LEAF SURFACE AT 60 DEG F AND  
42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 31.3          | 96.57 | 11.18   | 98.33       |
| 14   | 3        | 12.5          | 90    | 4.46    | 95          |
| 13   | 1        | 4.2           | 33.33 | 1.5     | 91.67       |
| 12   | 4        | 4             | 76.67 | 1.43    | 88.33       |
| 11   | 234      | 2.8           | 70    | 1       | 85          |
| 10   | 23       | 2.7           | 63.33 | .96     | 81.67       |
| 9    | 14       | 2.2           | 56.67 | .79     | 78.33       |
| 8    | 134      | 1.3           | 50    | .46     | 75          |
| 7    | 13       | 1.3           | 43.33 | .46     | 71.67       |
| 6    | 1234     | 1             | 36.67 | .36     | 68.33       |
| 5    | 124      | 1             | 30    | .36     | 65          |
| 4    | 34       | .5            | 23.33 | .18     | 61.67       |
| 3    | 123      | .5            | 16.67 | .18     | 58.33       |
| 2    | 12       | .5            | 10    | .18     | 55          |
| 1    | 24       | .2            | 3.33  | .07     | 51.67       |

PROB = ((R(I)-.5)/R(MAX))\*100% WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL = (PROB+100%)/2

#### VARIABLE #'S AND IDENTITIES

|    |                  |            |            |
|----|------------------|------------|------------|
| 1: | LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: | WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: | LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: | LEAF TYPE        | (+)OAK     | (-)HICKORY |

# VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

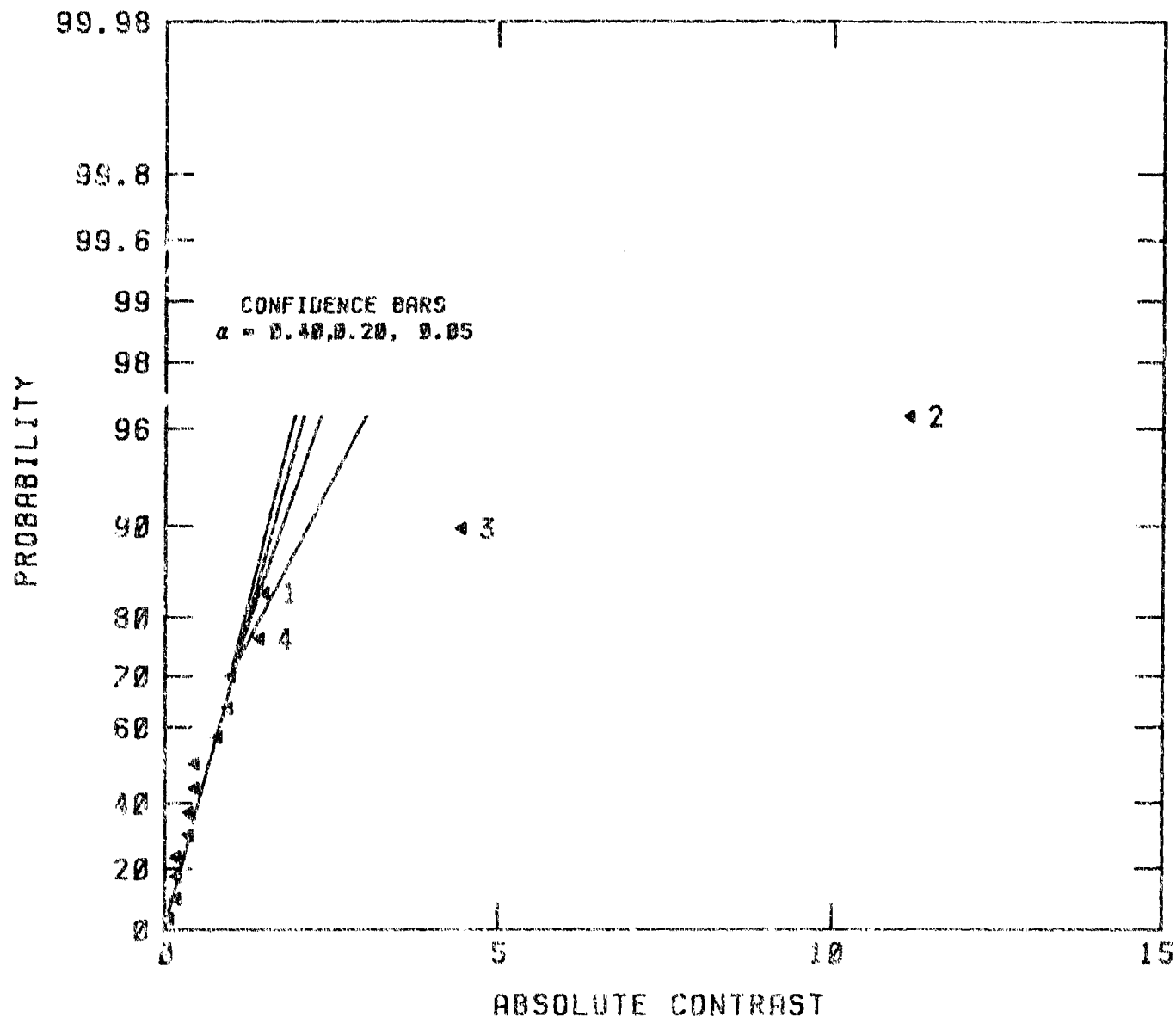


FIGURE K-8. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
 PERCENT OF CONTAMINATION RECOVERED AS VAPOR AFTER 3 HR  
 FROM 2 MM DIA DROPS ON LEAF SURFACE AT 80 DEG F AND 42% RH

TABLE K-18. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
PERCENT OF DROPLET (2 MM DIA) CONTAMINATION RECOVERED  
AS VAPOR AFTER 6 HR FROM LEAF SURFACE AT 60 DEG F AND  
42% RH

| TEST    | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|---------|----------|-------|-------------|----------------|
| 1       | MEAN     | 62    | 71.3        | -              |
| 2       | 1        | 61    | .1          | .0625          |
| 3       | 2        | 84    | 30.6        | 3751.5625      |
| 4       | 12       | 94    | 2.6         | 27.5625        |
| 5       | 3        | 54    | -7.6        | 232.5625       |
| 6       | 13       | 53    | -1.1        | 5.0625         |
| 7       | 23       | 84    | 3.4         | 45.5625        |
| 8       | 123      | 85    | -1.6        | 10.5625        |
| 9       | 4        | 64    | -1.6        | 10.5625        |
| 10      | 14       | 59    | -2.1        | 18.0625        |
| 11      | 24       | 88    | 1.4         | 7.5625         |
| 12      | 124      | 89    | -.6         | 1.5625         |
| 13      | 34       | 49    | -1.4        | 7.5625         |
| 14      | 134      | 46    | 1.1         | 5.0625         |
| 15      | 234      | 85    | 1.6         | 10.5625        |
| 16      | 1234     | 84    | .6          | 1.5625         |
| TOTAL = |          |       |             | 4135.4375      |

#### VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1. LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2. WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3. LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4. LEAF TYPE        | (+)OAK     | (-)HICKORY |

TABLE K-19. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
PERCENT OF DROPLET (2 MM DIA) CONTAMINATION RECOVERED  
AS VAPOR AFTER 6 HR FROM LEAF SURFACE AT 60 DEG F AND  
42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 30.6          | 96.67 | 14.57   | 98.33       |
| 14   | 3        | 7.6           | 90    | 3.62    | 95          |
| 13   | 23       | 3.4           | 83.33 | 1.62    | 91.67       |
| 12   | 12       | 2.6           | 76.67 | 1.24    | 88.33       |
| 11   | 14       | 2.1           | 70    | 1       | 85          |
| 10   | 234      | 1.6           | 63.33 | .76     | 81.67       |
| 9    | 4        | 1.6           | 56.67 | .76     | 78.33       |
| 8    | 123      | 1.6           | 50    | .76     | 75          |
| 7    | 34       | 1.4           | 43.33 | .67     | 71.67       |
| 6    | 24       | 1.4           | 36.67 | .67     | 68.33       |
| 5    | 134      | 1.1           | 30    | .52     | 65          |
| 4    | 13       | 1.1           | 23.33 | .52     | 61.67       |
| 3    | 1234     | .6            | 16.67 | .29     | 58.33       |
| 2    | 124      | .6            | 10    | .29     | 55          |
| 1    | 1        | .1            | 3.33  | .05     | 51.67       |

PROB = ((R(I)-.5)/R(MAX))\*100% WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL = (PROB+100%)/2

#### VARIABLE #'S AND IDENTITIES

|    |                  |            |            |
|----|------------------|------------|------------|
| 1: | LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: | WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: | LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: | LEAF TYPE        | (+)OAK     | (-)HICKORY |



# VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

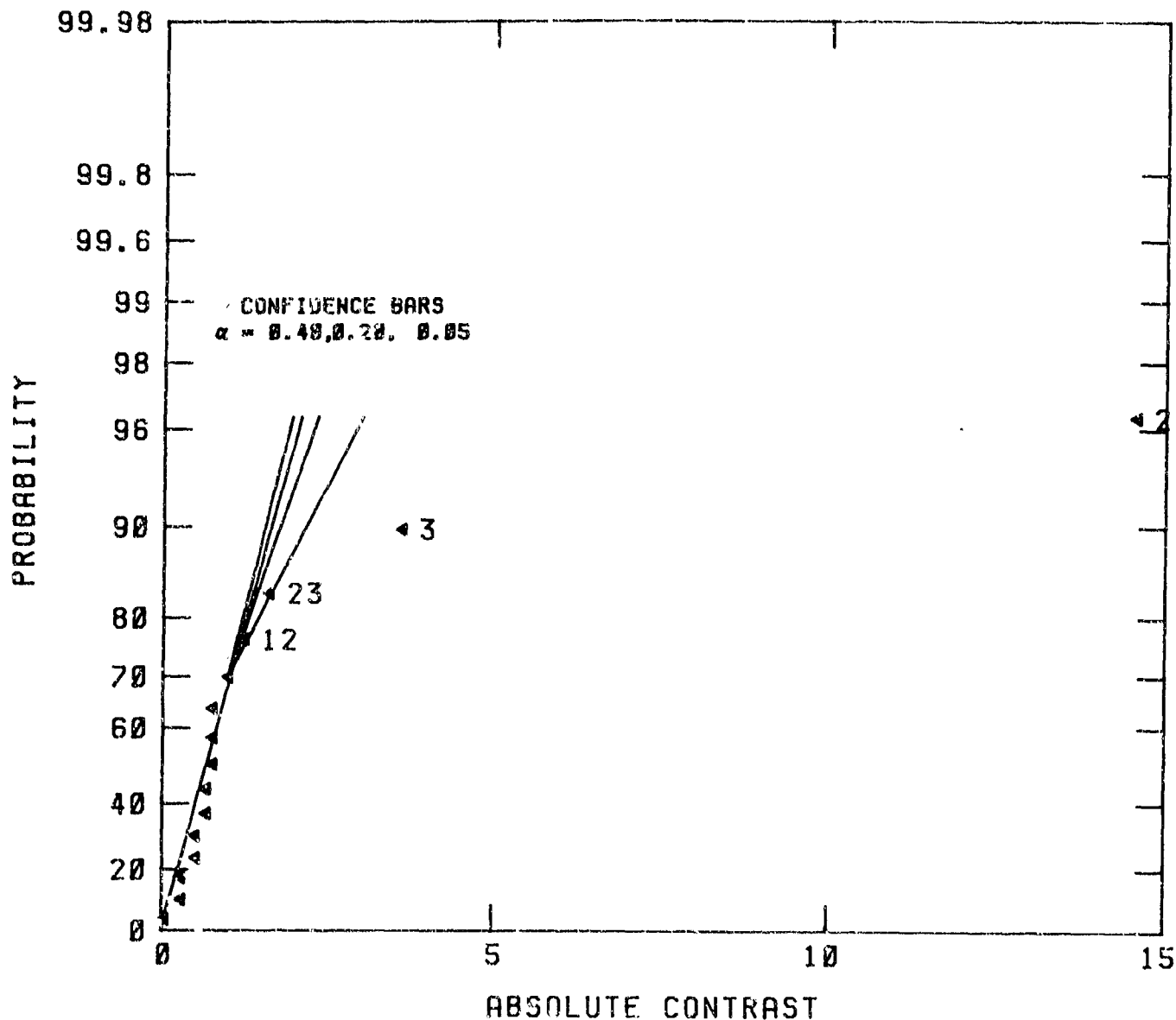


FIGURE K-9. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
 PERCENT OF CONTAMINATION RECOVERED AS VAPOR AFTER 8 HR  
 FROM 2 MM DIA DROPS ON LEAF SURFACE AT 80 DEG F AND 42% RH

TABLE K-20. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
AVERAGE EVAPORATION RATE (MMG/MIN) FOR DROPLET (2 MM  
DIA) DEPOSITED ON LEAF SURFACE FOR 1 HR AT 60 DEG F  
AND 42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 17    | 19.9        | -              |
| 2    | 1        | 15    | -.9         | 3.0625         |
| 3    | 2        | 36    | 14.9        | 885.0625       |
| 4    | 12       | 36    | -.4         | .5625          |
| 5    | 3        | 11    | -7.4        | 217.5625       |
| 6    | 13       | 11    | .9          | 3.0625         |
| 7    | 23       | 23    | -2.4        | 22.5625        |
| 8    | 123      | 23    | .4          | .5625          |
| 9    | 4        | 14    | -3.1        | 39.0625        |
| 10   | 14       | 14    | -.4         | .5625          |
| 11   | 24       | 31    | -1.1        | 5.0625         |
| 12   | 124      | 26    | -.9         | 3.0625         |
| 13   | 34       | 9     | 1.6         | 10.5625        |
| 14   | 134      | 9     | .4          | .5625          |
| 15   | 234      | 22    | 1.6         | 10.5625        |
| 16   | 1234     | 22    | .9          | 3.0625         |

TOTAL = 1204.9375

#### VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

TABLE K-21. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
AVERAGE EVAPORATION RATE (MMG/MIN) FOR DROPLET (2 MM  
DIA) DEPOSITED ON LEAF SURFACE FOR 1 HR AT 60 DEG F  
AND 42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 14.9          | 96.67 | 9.31    | 98.33       |
| 14   | 3        | 7.4           | 90    | 4.63    | 95          |
| 13   | 4        | 3.1           | 83.33 | 1.94    | 91.67       |
| 12   | 23       | 2.4           | 76.67 | 1.5     | 88.33       |
| 11   | 234      | 1.6           | 70    | 1       | 85          |
| 10   | 34       | 1.6           | 63.33 | 1       | 81.67       |
| 9    | 24       | 1.1           | 56.67 | .69     | 78.33       |
| 8    | 1234     | .9            | 50    | .56     | 75          |
| 7    | 124      | .9            | 43.33 | .56     | 71.67       |
| 6    | 13       | .9            | 36.67 | .56     | 68.33       |
| 5    | 1        | .9            | 30    | .56     | 65          |
| 4    | 134      | .4            | 23.33 | .25     | 61.67       |
| 3    | 14       | .4            | 16.67 | .25     | 58.33       |
| 2    | 123      | .4            | 10    | .25     | 55          |
| 1    | 12       | .4            | 3.33  | .25     | 51.67       |

PROB =  $((R(I) - .5) / R(\text{MAX})) * 100\%$  WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL =  $(\text{PROB} + 100\%) / 2$

#### VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

# VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

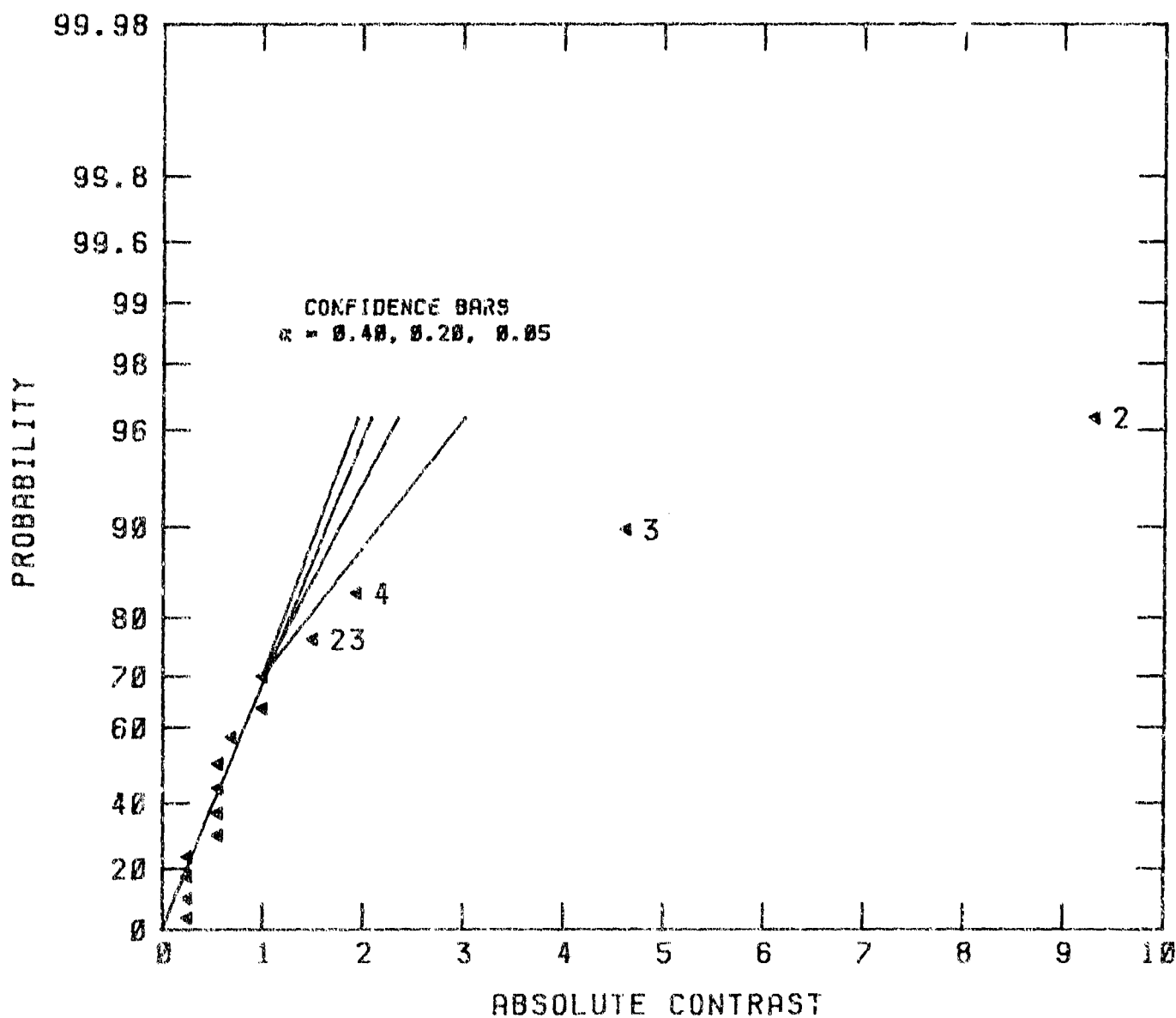


FIGURE K-10. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
 AVERAGE EVAPORATION RATE OF 2MM DIA DROPS DEPOSITED ON  
 LEAF SURFACE FOR 1 HR AT 60 DEG F AND 42% RH

TABLE K-22. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
AVERAGE EVAPORATION RATE (MMG/MIN) FOR DROPLET (2 MM  
DIA) DEPOSITED ON LEAF SURFACE FOR 2 HR AT 60 DEG F  
AND 42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 15    | 17.8        | -              |
| 2    | 1        | 14    | .1          | .0625          |
| 3    | 2        | 29    | 12.9        | 663.0625       |
| 4    | 12       | 31    | -.1         | .0625          |
| 5    | 3        | 10    | -5.6        | 126.5625       |
| 6    | 13       | 10    | .4          | .5625          |
| 7    | 23       | 21    | -1.4        | 7.5625         |
| 8    | 123      | 22    | .1          | .0625          |
| 9    | 4        | 12    | -2.4        | 22.5625        |
| 10   | 14       | 13    | -.4         | .5625          |
| 11   | 24       | 27    | -.6         | 1.5625         |
| 12   | 124      | 24    | -1.1        | 5.0625         |
| 13   | 34       | 8     | .9          | 3.0625         |
| 14   | 134      | 9     | .4          | .5625          |
| 15   | 234      | 20    | .6          | 1.5625         |
| 16   | 1234     | 20    | .6          | 1.5625         |

TOTAL = 834.4375

VARIABLE #'S AND IDENTITIES

|    |                  |            |            |
|----|------------------|------------|------------|
| 1: | LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: | WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: | LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: | LEAF TYPE        | (+)OAK     | (-)HICKORY |

TABLE K-23. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
AVERAGE EVAPORATION RATE (MMG/MIN) FOR DROPLET (2 MM  
DIA) DEPOSITED ON LEAF SURFACE FOR 2 HR AT 60 DEG F  
AND 42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 12.9          | 96.67 | 11.73   | 98.33       |
| 14   | 3        | 5.6           | 90    | 5.09    | 95          |
| 13   | 4        | 2.4           | 83.33 | 2.18    | 91.67       |
| 12   | 23       | 1.4           | 76.67 | 1.27    | 88.33       |
| 11   | 124      | 1.1           | 70    | 1       | 85          |
| 10   | 34       | .9            | 63.33 | .82     | 81.67       |
| 9    | 1234     | .6            | 56.67 | .55     | 78.33       |
| 8    | 234      | .6            | 50    | .55     | 75          |
| 7    | 24       | .6            | 43.33 | .55     | 71.67       |
| 6    | 134      | .4            | 36.67 | .36     | 68.33       |
| 5    | 14       | .4            | 30    | .36     | 65          |
| 4    | 13       | .4            | 23.33 | .36     | 61.67       |
| 3    | 123      | .1            | 16.67 | .09     | 58.33       |
| 2    | 12       | .1            | 10    | .09     | 55          |
| 1    | 1        | .1            | 3.33  | .09     | 51.67       |

PROB =  $((R(I) - .5) / R(\text{MAX})) * 100\%$  WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL =  $(\text{PROB} + 100\%) / 2$

#### VARIABLE #'S AND IDENTITIES

|    |                  |            |            |
|----|------------------|------------|------------|
| 1: | LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: | WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: | LEAF SURFACE     | (-)BOTTOM  | (-)TOP     |
| 4: | LEAF TYPE        | (+)OAK     | (-)HICKORY |

# VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

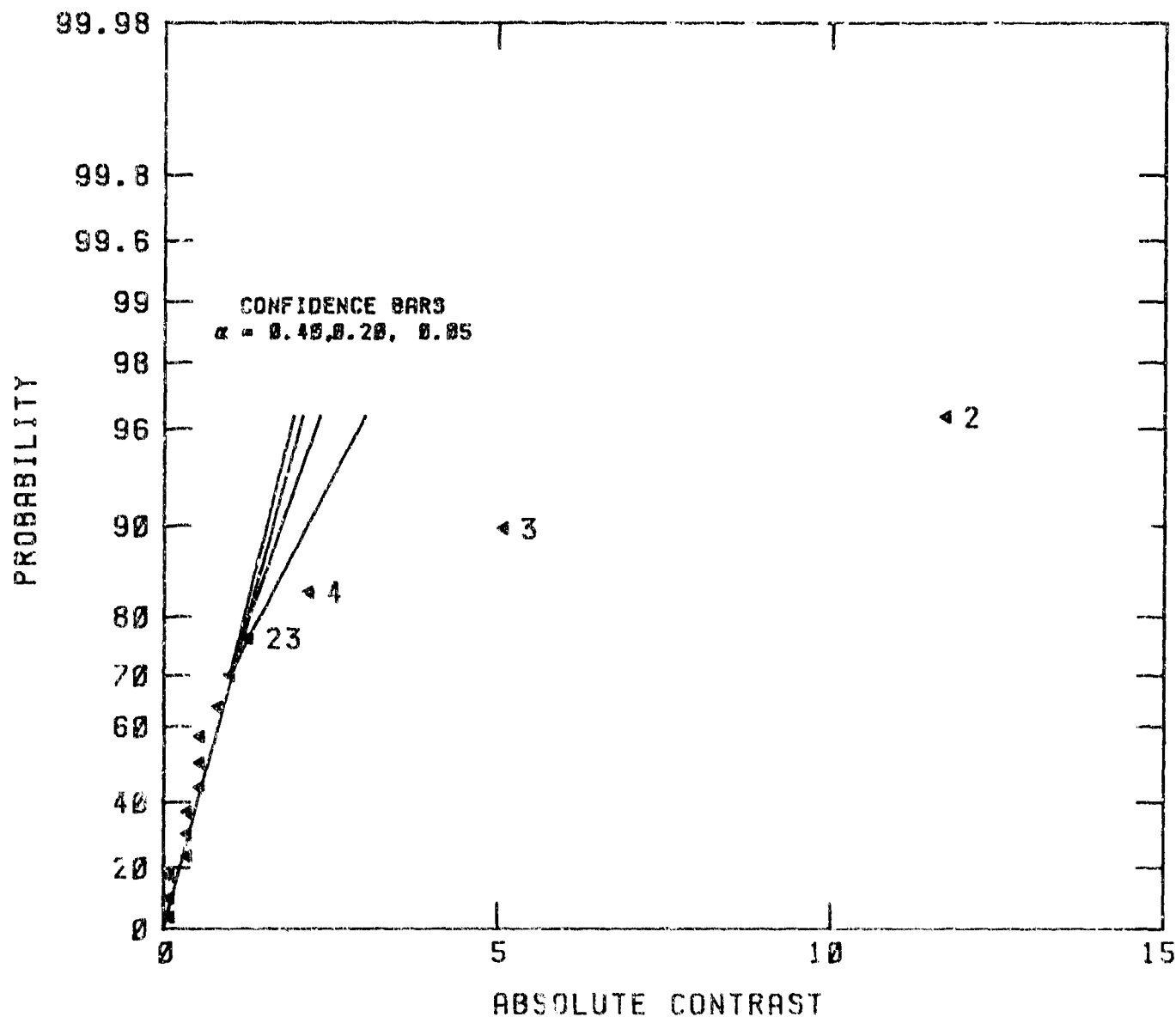


FIGURE K-11. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
 AVERAGE EVAPORATION RATE OF 2 MM DIA DROPS DEPOSITED ON  
 LEAF SURFACE FOR 2 HR AT 60 DEG F AND 42% RH

TABLE K-24. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
AVERAGE EVAPORATION RATE (MMG/MIN) FOR DROPLET (2 MM  
DIA) DEPOSITED ON LEAF SURFACE FOR 3 HR AT 60 DEG F  
AND 42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 14    | 16.2        | -              |
| 2    | 1        | 13    | .6          | 1.5625         |
| 3    | 2        | 23    | 10.6        | 451.5625       |
| 4    | 12       | 27    | .4          | .5625          |
| 5    | 3        | 10    | -3.9        | 60.0625        |
| 6    | 13       | 10    | -.1         | .0625          |
| 7    | 23       | 20    | -.6         | 1.5625         |
| 8    | 123      | 20    | -.4         | .5625          |
| 9    | 4        | 11    | -1.9        | 14.0625        |
| 10   | 14       | 12    | -.1         | .0625          |
| 11   | 24       | 23    | -.1         | .0625          |
| 12   | 124      | 22    | -.9         | 3.0625         |
| 13   | 34       | 8     | .4          | .5625          |
| 14   | 134      | 9     | .6          | 1.5625         |
| 15   | 234      | 18    | .1          | .0625          |
| 16   | 1234     | 19    | .9          | 3.0625         |

TOTAL = 538.4375

#### VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |



TABLE K-25. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
AVERAGE EVAPORATION RATE (MMG/MIN) FOR DROPLET (2 MM  
DIA) DEPOSITED ON LEAF SURFACE FOR 3 HR AT 60 DEG F  
AND 42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 10.6          | 96.67 | 11.78   | 98.33       |
| 14   | 3        | 3.9           | 90    | 4.33    | 95          |
| 13   | 4        | 1.9           | 83.33 | 2.11    | 91.67       |
| 12   | 1234     | .9            | 76.67 | 1       | 88.33       |
| 11   | 124      | .9            | 70    | 1       | 85          |
| 10   | 134      | .6            | 63.33 | .67     | 81.67       |
| 9    | 23       | .6            | 56.67 | .67     | 78.33       |
| 8    | 1        | .6            | 50    | .67     | 75          |
| 7    | 34       | .4            | 43.33 | .44     | 71.67       |
| 6    | 123      | .4            | 36.67 | .44     | 68.33       |
| 5    | 12       | .4            | 30    | .44     | 65          |
| 4    | 234      | .1            | 23.33 | .11     | 61.67       |
| 3    | 24       | .1            | 16.67 | .11     | 58.33       |
| 2    | 14       | .1            | 10    | .11     | 55          |
| 1    | 13       | .1            | 3.33  | .11     | 51.67       |

PROB =  $((R(I) - .5) / P(\text{MAX})) * 100\%$  WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL =  $(\text{PROB} + 100\%) / 2$

#### VARIABLE #'S AND IDENTITIES

|    |                  |            |            |
|----|------------------|------------|------------|
| 1: | LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: | WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: | LEAF SURFACE     | (+)BO TOM  | (-)TOP     |
| 4: | LEAF TYPE        | (+)OA      | (-)HICKORY |

# VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

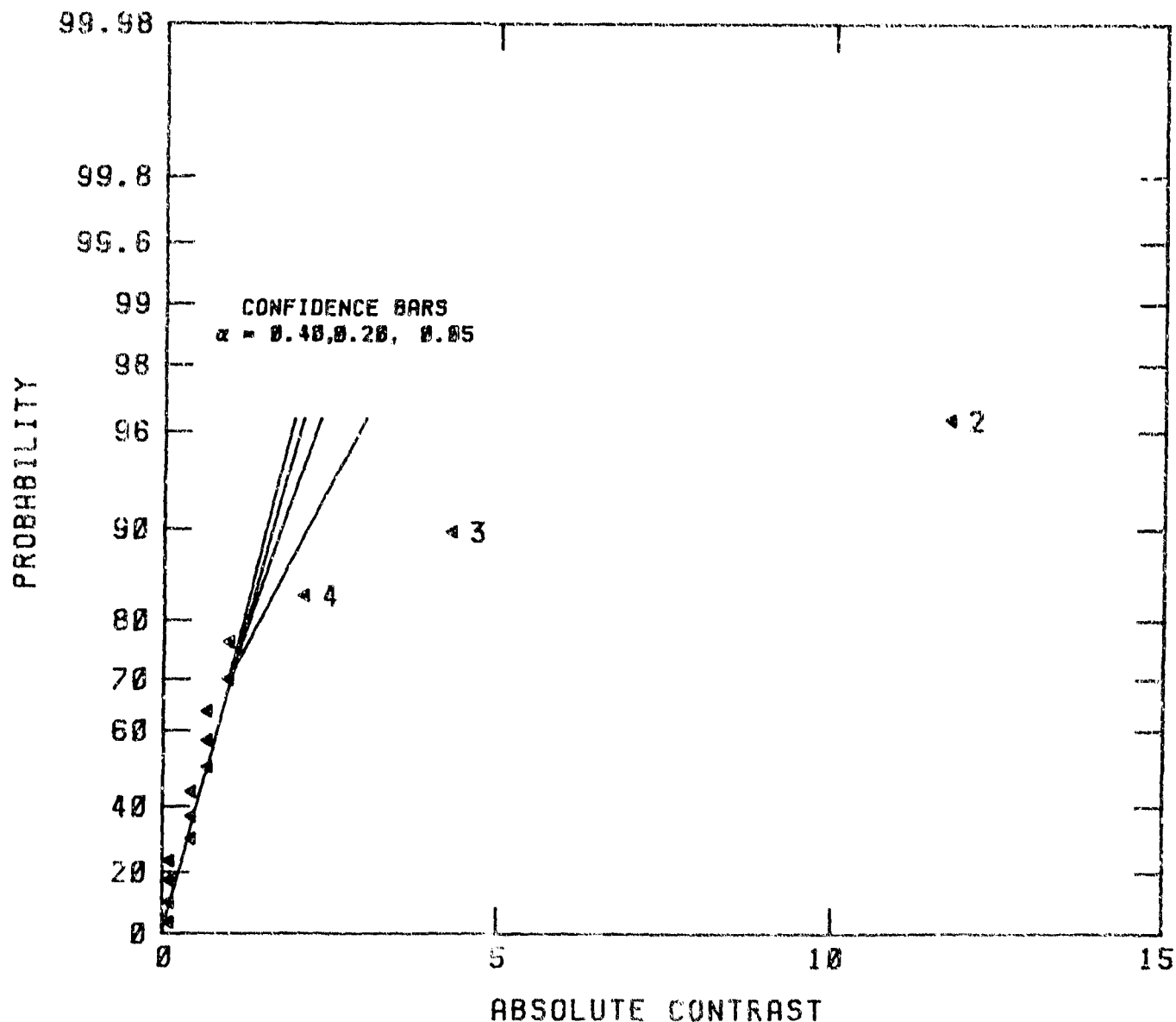


FIGURE K-12. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
 AVERAGE EVAPORATION RATE OF 2 MM DROPS DEPOSITED ON  
 LEAF SURFACE FOR 3 HR AT 60 DEG F AND 42% RH

TABLE K-26. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
AVERAGE EVAPORATION RATE (MMG/MIN) FOR DROPLET DEPOSITED  
ON LEAF SURFACE FOR 6 HR AT 60 DEG F AND 42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 11    | 11.9        | -              |
| 2    | 1        | 11    | 1.5         | 9              |
| 3    | 2        | 13    | 5.3         | 110.25         |
| 4    | 12       | 17    | .5          | 1              |
| 5    | 3        | 8     | -1.7        | 12.25          |
| 6    | 13       | 9     | -.5         | 1              |
| 7    | 23       | 14    | .8          | 2.25           |
| 8    | 123      | 15    | -.5         | 1              |
| 9    | 4        | 9     | -.7         | 2.25           |
| 10   | 14       | 11    | 0           | 0              |
| 11   | 24       | 14    | .3          | .25            |
| 12   | 124      | 16    | -.5         | 1              |
| 13   | 34       | 7     | -.2         | .25            |
| 14   | 134      | 8     | 0           | 0              |
| 15   | 234      | 13    | -.2         | .25            |
| 16   | 1234     | 14    | 5           | 1              |

TOTAL = 141.75

#### VARIABLE #'S AND IDENTITIES

|    |                  |            |           |
|----|------------------|------------|-----------|
| 1: | LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: | WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: | LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: | LEAF TYPE        | (+)OAK     | HICKORY   |

TABLE K-27. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
AVERAGE EVAPORATION RATE (MMG/MIN) FOR DROPLET DEPOSITED  
ON LEAF SURFACE FOR 6 HP AT 60 DEG F AND 42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 5.3           | 96.67 | 7.57    | 98.33       |
| 14   | 3        | 1.7           | 90    | 2.47    | 95          |
| 13   | 1        | 1.5           | 83.33 | 2.14    | 91.67       |
| 12   | 23       | .8            | 76.67 | 1.14    | 88.33       |
| 11   | 4        | .7            | 70    | 1       | 85          |
| 10   | 1234     | .5            | 63.33 | .71     | 81.67       |
| 9    | 124      | .5            | 56.67 | .71     | 78.33       |
| 8    | 123      | .5            | 50    | .71     | 75          |
| 7    | 13       | .5            | 43.33 | .71     | 71.67       |
| 6    | 12       | .5            | 36.67 | .71     | 68.33       |
| 5    | 24       | .3            | 30    | .43     | 65          |
| 4    | 234      | .2            | 23.33 | .29     | 61.67       |
| 3    | 34       | .2            | 16.67 | .29     | 58.33       |
| 2    | 134      | 0             | 10    | 0       | 55          |
| 1    | 14       | 0             | 3.33  | 0       | 51.67       |

PROB = ((R(I)-.5)/R(MAX))\*100% WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL = (PROB+100%)/2

#### VARIABLE #'S AND IDENTITIES

|    |                  |            |            |
|----|------------------|------------|------------|
| 1: | LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: | WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: | LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: | LEAF TYPE        | (+)OAK     | (-)HICKORY |

# VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

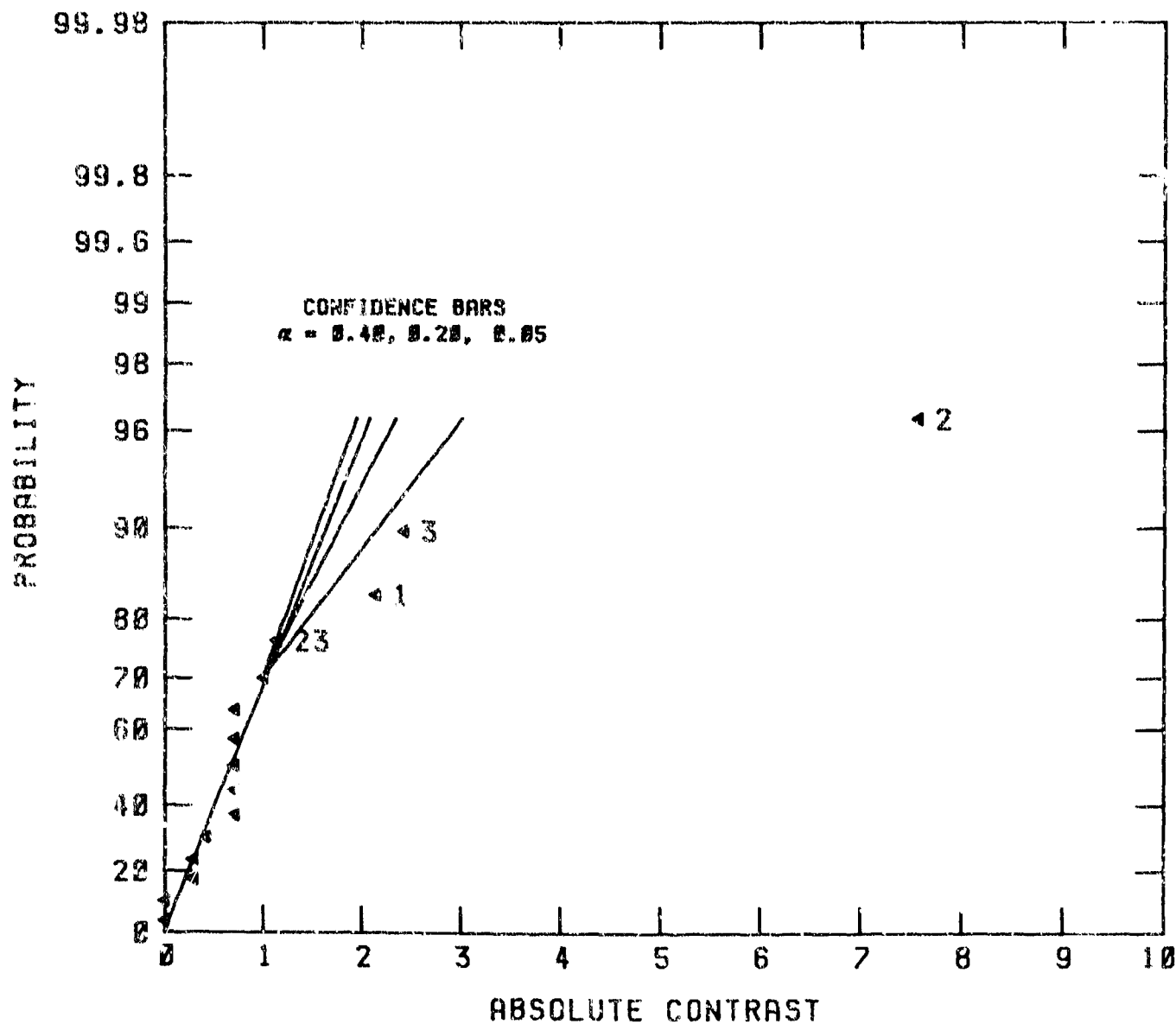


FIGURE K-13. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
 AVERAGE EVAPORATION RATE OF 2 MM DIA DROPS DEPOSITED ON  
 LEAF SURFACE FOR 8 HR AT 86 DEG F AND 42% RH

Blank

APPENDIX L

FACTORIAL ANALYSIS AND HALF NORMAL PROBABILITY PLOTS  
OF STANDARDIZED ABSOLUTE CONTRASTS FOR TESTS ON GREEN AND RED OAK LEAVES

TABLE L-1. THE DESIGN MATRIX FOR THE  $2^4$  FACTORIAL EXPERIMENT NO. 2.

| TEST | VARIABLES |   |   |   | CONTRAST CONFOUNDING |
|------|-----------|---|---|---|----------------------|
|      | 1         | 2 | 3 | 4 |                      |
| 1    | -         | - | - | - | MEAN                 |
| 2    | +         | - | - | - | 1                    |
| 3    | -         | + | - | - | 2                    |
| 4    | +         | + | - | - | 12                   |
| 5    | -         | - | + | - | 3                    |
| 6    | +         | - | + | - | 13                   |
| 7    | -         | + | + | - | 23                   |
| 8    | +         | + | + | - | 123                  |
| 9    | -         | - | - | + | 4                    |
| 10   | +         | - | - | + | 14                   |
| 11   | -         | + | - | + | 24                   |
| 12   | +         | + | - | + | 124                  |
| 13   | -         | - | + | + | 34                   |
| 14   | +         | - | + | + | 134                  |
| 15   | -         | + | + | + | 234                  |
| 16   | +         | + | + | + | 1234                 |

#### VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |



TABLE L-2. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
HALF-LIFE OF DROPLET (2 MM DIA) CONTAMINATION DEPOSITED  
ON OAK LEAF SURFACE AT 60 DEG F AND 42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 339   | 233.4       | -              |
| 2    | 1        | 315   | 9.6         | 370.5625       |
| 3    | 2        | 142   | -186.4      | 138942.5625    |
| 4    | 12       | 137   | 2.4         | 22.5625        |
| 5    | 3        | 341   | 41.6        | 6930.5625      |
| 6    | 13       | 315   | -2.6        | 27.5625        |
| 7    | 23       | 145   | -18.6       | 1387.5625      |
| 8    | 123      | 150   | -1.9        | 3.0625         |
| 9    | 4        | 245   | -4.1        | 68.0625        |
| 10   | 14       | 287   | 22.1        | 1958.0625      |
| 11   | 24       | 100   | -2.4        | 22.5625        |
| 12   | 124      | 136   | -10.1       | 410.0625       |
| 13   | 34       | 367   | 37.1        | 5513.0625      |
| 14   | 134      | 404   | -4.6        | 85.5625        |
| 15   | 234      | 150   | -22.1       | 1958.0625      |
| 16   | 1234     | 162   | -3.9        | 60.0625        |

TOTAL = 157759.938

VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

TABLE L-3. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
 HALF-LIFE OF DROPLET (2 MM DIA) CONTAMINATION DEPOSITED  
 ON OAK LEAF SURFACE AT 60 DEG F AND 42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 185.4         | 96.67 | 8.43    | 98.33       |
| 14   | 3        | 41.6          | 90    | 1.88    | 95          |
| 13   | 34       | 37.1          | 83.33 | 1.68    | 91.67       |
| 12   | 234      | 22.1          | 76.67 | 1       | 88.33       |
| 11   | 14       | 22.1          | 70    | 1       | 85          |
| 10   | 23       | 18.6          | 63.33 | .84     | 81.67       |
| 9    | 124      | 10.1          | 56.67 | .46     | 78.33       |
| 8    | 1        | 9.6           | 50    | .43     | 75          |
| 7    | 134      | 4.6           | 43.33 | .21     | 71.67       |
| 6    | 4        | 4.1           | 36.67 | .19     | 68.33       |
| 5    | 1234     | 3.9           | 30    | .18     | 65          |
| 4    | 13       | 2.6           | 23.33 | .12     | 61.67       |
| 3    | 24       | 2.4           | 16.67 | .11     | 58.33       |
| 2    | 12       | 2.4           | 10    | .11     | 55          |
| 1    | 123      | .9            | 3.33  | .04     | 51.67       |

PROB =  $((R(I) - .5) / R(\text{MAX})) * 100\%$  WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
 THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL =  $(\text{PROB} + 100\%) / 2$

#### VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

# VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

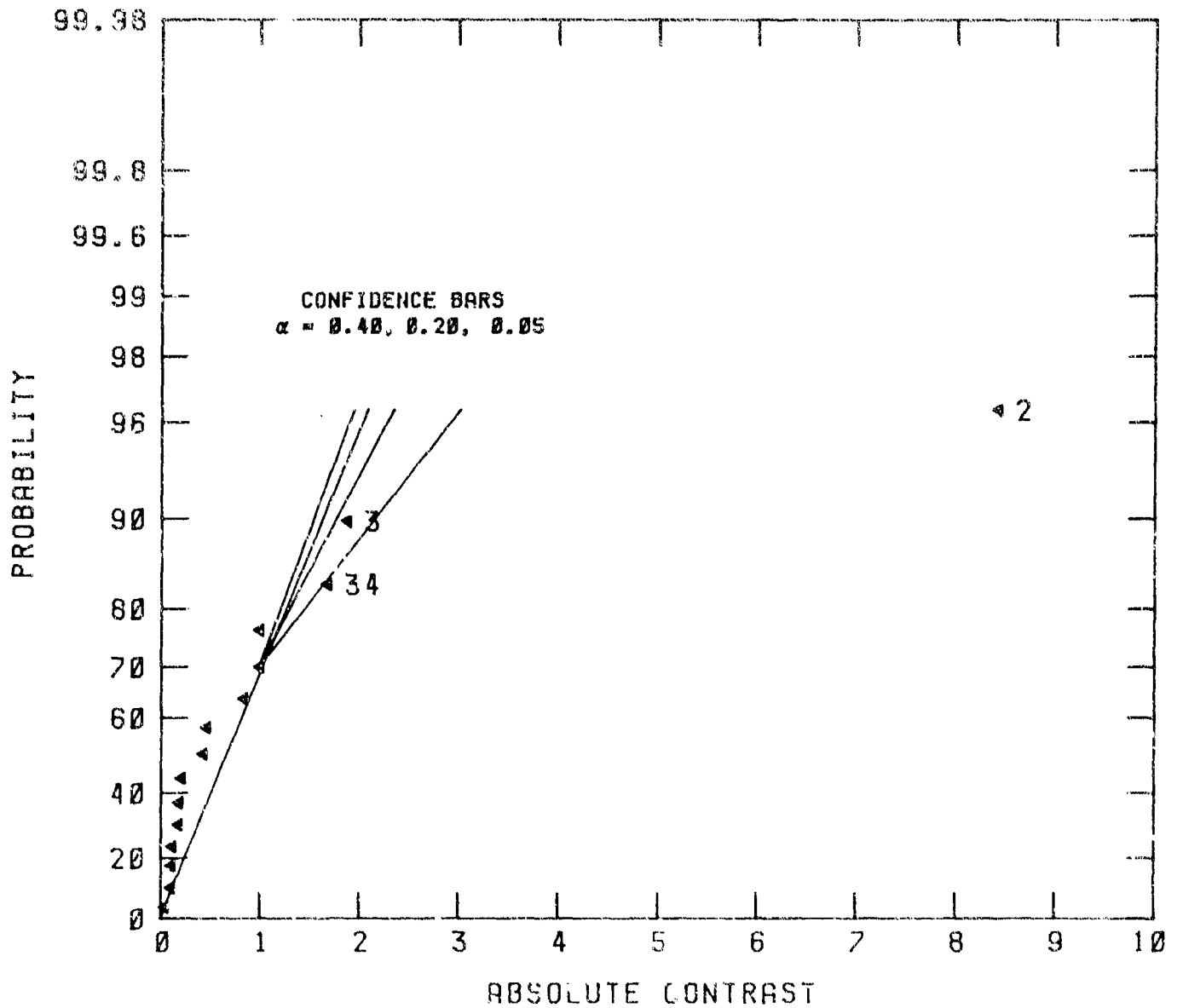


FIGURE L-1. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
HALF-LIFE OF 2 MM DIAMETER DROPS DEPOSITED ON  
OAK LEAF SURFACE AT 60 DEG F AND 42% RH

TABLE L-4. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
AVERAGE EVAPORATION RATE (MMG/MIN) OVER HALF-LIFE OF  
DROPLET (2 MM DIA) DEPOSITED ON OAK LEAF SURFACE AT  
60 DEG F AND 42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 9     | 15.8        | -              |
| 2    | 1        | 10    | .5          | 1              |
| 3    | 2        | 22    | 1.3         | 676            |
| 4    | 12       | 24    | -.5         | 1              |
| 5    | 3        | 9     | -3          | 36             |
| 6    | 13       | 10    | .5          | 1              |
| 7    | 23       | 20    | -1.5        | 9              |
| 8    | 123      | 22    | .5          | 1              |
| 9    | 4        | 10    | 0           | 0              |
| 10   | 14       | 11    | -1          | 4              |
| 11   | 24       | 28    | .5          | 1              |
| 12   | 124      | 24    | -1          | 4              |
| 13   | 34       | 7     | -2          | 16             |
| 14   | 134      | 8     | .5          | 1              |
| 15   | 234      | 19    | -.5         | 1              |
| 16   | 1234     | 19    | .5          | 1              |

TOTAL = 753

#### VARIABLE #'S AND IDENTITIES

|    |                  |            |           |
|----|------------------|------------|-----------|
| 1: | LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: | WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: | LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: | LEAF CONDITION   | (+)GREEN   | (-)RED    |

TABLE L-5. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
AVERAGE EVAPORATION RATE (MMG/MIN) OVER HALF-LIFE OF  
DROPLET (2 MM DIA) DEPOSITED ON OAK LEAF SURFACE AT  
60 DEG F AND 42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 13            | 96.67 | 13      | 96.33       |
| 14   | 3        | 3             | 90    | 3       | 95          |
| 13   | 34       | 2             | 83.33 | 2       | 91.67       |
| 12   | 23       | 1.5           | 76.67 | 1.5     | 88.33       |
| 11   | 124      | 1             | 70    | 1       | 85          |
| 10   | 14       | 1             | 63.33 | 1       | 81.67       |
| 9    | 1234     | .5            | 56.67 | .5      | 78.33       |
| 8    | 234      | .5            | 50    | .5      | 75          |
| 7    | 14       | .5            | 43.33 | .5      | 71.67       |
| 6    | 24       | .5            | 36.67 | .5      | 68.33       |
| 5    | 123      | .5            | 30    | .5      | 65          |
| 4    | 13       | .5            | 23.33 | .5      | 61.67       |
| 3    | 12       | .5            | 16.67 | .5      | 58.33       |
| 2    | 1        | .5            | 10    | .5      | 55          |
| 1    | 4        | 0             | 3.33  | 0       | 51.67       |

PROB = ((R(I)-.5)/R(MAX))\*100% WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL = (PROB+100%)/2

#### VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

# VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

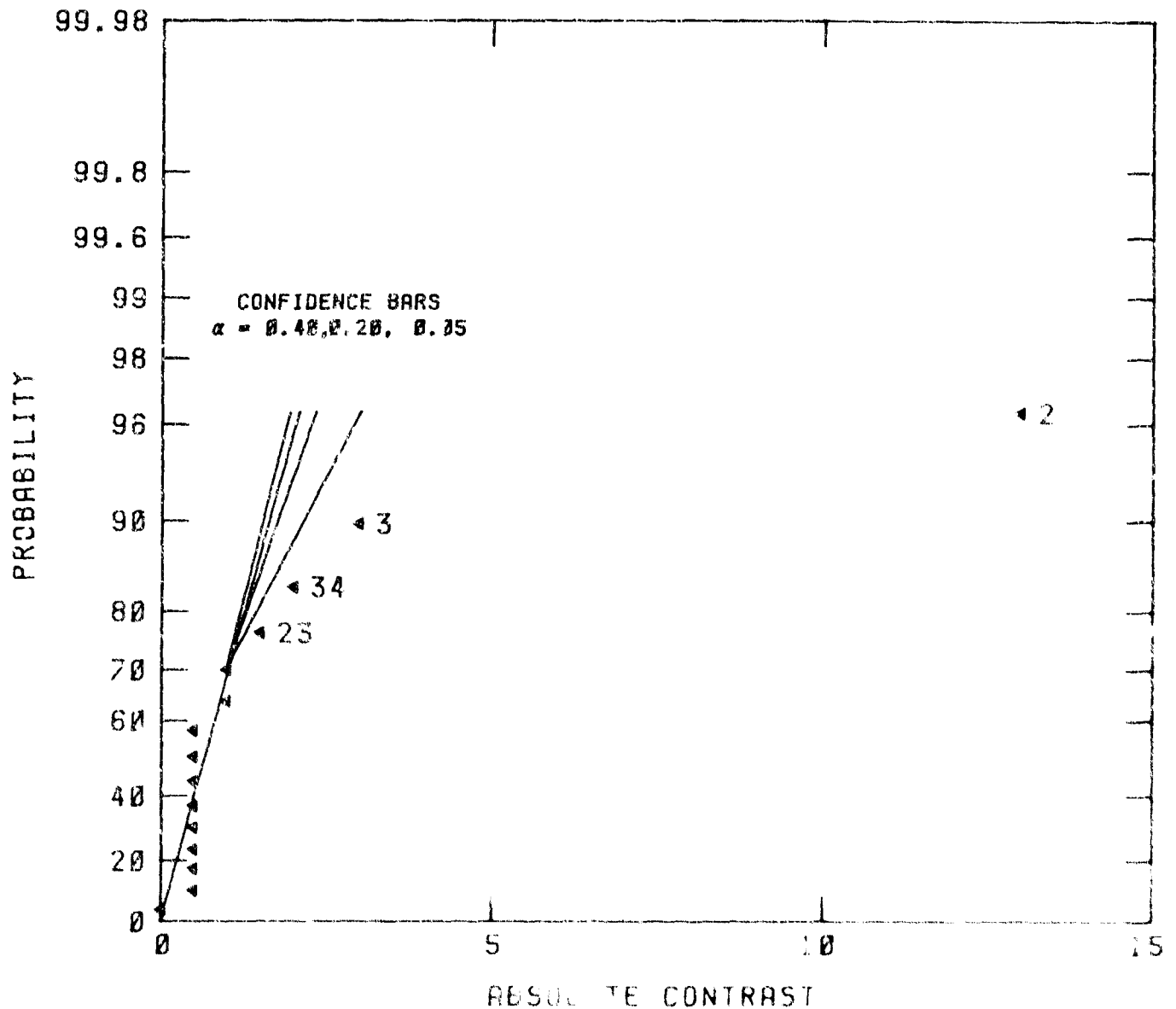


FIGURE L-2. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
 AVERAGE EVAPORATION RATE OVER HALF-LIFE OF 2 MM DIA DROPS  
 DEPOSITED ON OAK LEAF SURFACE AT 80 DEG F AND 42% RH

TABLE L-6. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
TOTAL PERCENT OF DROPLET (2 MM DIA) CONTAMINATION RECOVERED  
AS VAPOR FROM OAK LEAF SURFACE AT 60 DEG F AND 42%  
RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 81    | 27.6        | -              |
| 2    | 1        | 98    | 6.3         | 156.25         |
| 3    | 2        | 86    | 4.3         | 72.25          |
| 4    | 12       | 98    | -1.2        | 6.25           |
| 5    | 3        | 83    | -.5         | 1              |
| 6    | 13       | 93    | -2          | 16             |
| 7    | 23       | 88    | -.5         | 1              |
| 8    | 123      | 96    | .5          | 1              |
| 9    | 4        | 80    | -5.5        | 121            |
| 10   | 14       | 83    | -5.5        | 121            |
| 11   | 24       | 88    | 1           | 4              |
| 12   | 124      | 89    | .5          | 1              |
| 13   | 34       | 83    | .3          | .25            |
| 14   | 134      | 83    | .8          | 2.25           |
| 15   | 234      | 87    | -1.2        | 6.25           |
| 16   | 1234     | 86    | -.2         | .25            |

TOTAL = 509.75

#### VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

TABLE L-7. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
TOTAL PERCENT OF DROPLET (2 MM DIA) CONTAMINATION RECOVERED  
AS VAPOR FROM OAK LEAF SURFACE AT 60 DEG F AND 42%  
RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 1        | 6.3           | 96.67 | 3.15    | 98.33       |
| 14   | 14       | 5.5           | 90    | 2.75    | 95          |
| 13   | 4        | 5.5           | 83.33 | 2.75    | 91.67       |
| 12   | 2        | 4.3           | 76.67 | 2.15    | 88.33       |
| 11   | 13       | 2             | 70    | 1       | 85          |
| 10   | 234      | 1.2           | 63.33 | .6      | 81.67       |
| 9    | 12       | 1.2           | 56.67 | .6      | 78.33       |
| 8    | 24       | 1             | 50    | .5      | 75          |
| 7    | 134      | .8            | 43.33 | .4      | 71.67       |
| 6    | 124      | .5            | 36.67 | .25     | 68.33       |
| 5    | 123      | .5            | 30    | .25     | 65          |
| 4    | 23       | .5            | 23.33 | .25     | 61.67       |
| 3    | 3        | .5            | 16.67 | .25     | 58.33       |
| 2    | 34       | .3            | 10    | .15     | 55          |
| 1    | 1234     | .2            | 3.33  | .1      | 51.67       |

PROB = ((R(I)-.5)/R(MAX))\*100% WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL = (PROB+100%)/2

VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)PED    |



# VARIABLE $\theta$ 'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

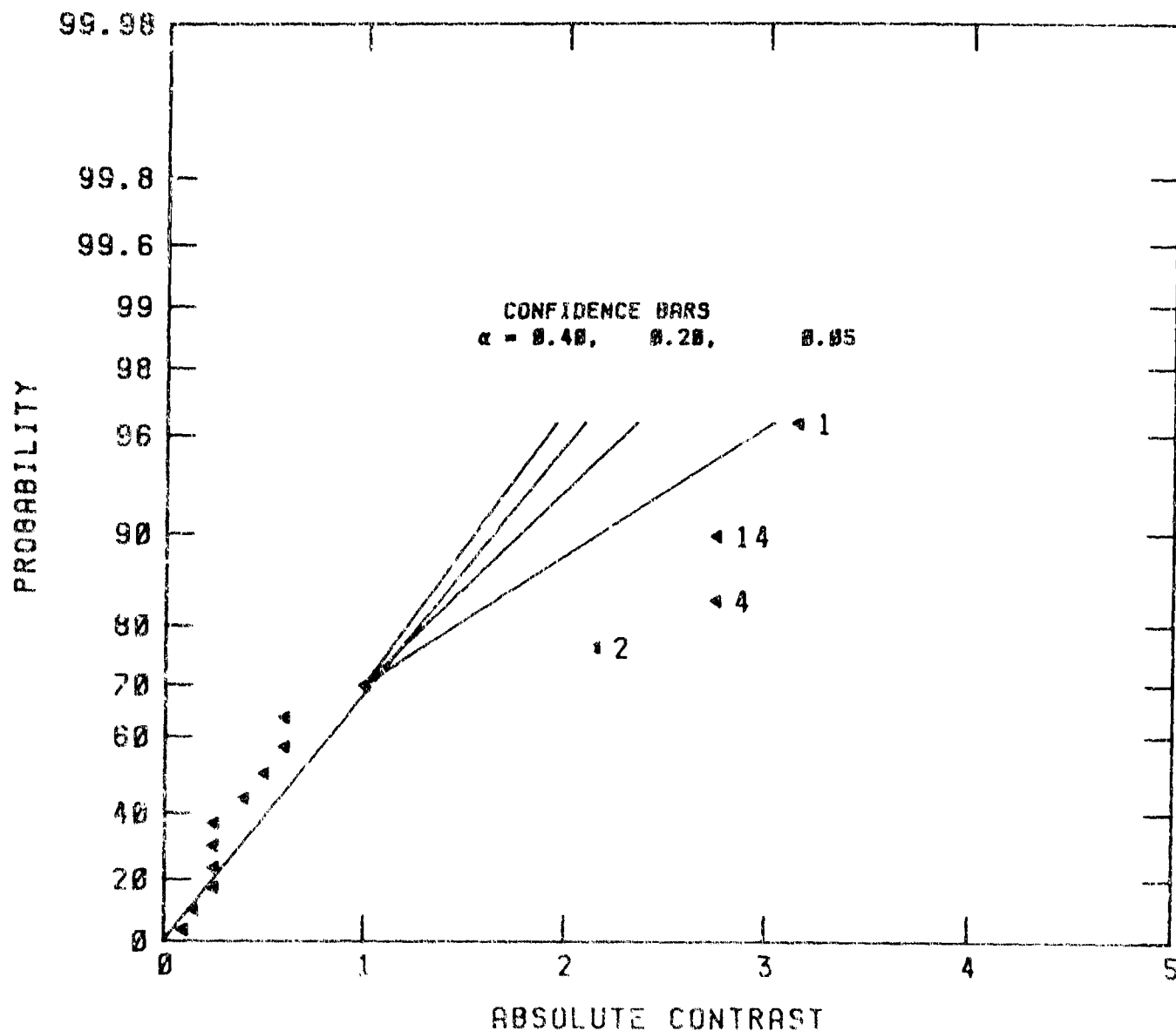


FIGURE L-3. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
TOTAL PERCENT OF CONTAMINATION RECOVERED AS VAPOR FROM  
2 MM DIA DROPS ON OAK LEAVES AT 80 DEG F AND 42% RH

TABLE 1-8. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
LIFE TIME OF DROPLET (2 MM DIA) CONTAMINATION ON OAK  
LEAF SURFACE AT 60 DEG F AND 42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 1215  | 794.1       | -              |
| 2    | 1        | 1280  | 38.1        | 5814.0625      |
| 3    | 2        | 450   | -675.6      | 1825876.56     |
| 4    | 12       | 560   | -18.1       | 1314.0625      |
| 5    | 3        | 1140  | 89.4        | 31951.5625     |
| 6    | 13       | 1240  | -58.1       | 13514.0625     |
| 7    | 23       | 510   | -56.9       | 12939.0625     |
| 8    | 123      | 480   | 8.1         | 264.0625       |
| 9    | 4        | 780   | -130.6      | 68251.5626     |
| 10   | 14       | 960   | -23.1       | 2139.0625      |
| 11   | 24       | 360   | 43.1        | 7439.06252     |
| 12   | 124      | 390   | 3.1         | 39.0625        |
| 13   | 34       | 1280  | 123.1       | 60639.0626     |
| 14   | 134      | 1160  | -31.9       | 4064.0625      |
| 15   | 234      | 465   | -80.6       | 26001.5625     |
| 16   | 1234     | 435   | 51.9        | 10764.0625     |

TOTAL = 2071010.94

#### VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

TABLE L-9. RANKED STANDARDIZED MAGNITUDE F EFFECTS  
 LIFE TIME OF DROPLET (2 MM DIA) CONTAMINATION ON OAK  
 LEAF SURFACE AT 60 DEG F AND 42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 675.6         | 96.67 | 8.38    | 98.33       |
| 14   | 4        | 130.6         | 90    | 1.62    | 95          |
| 13   | 34       | 123.1         | 83.33 | 1.53    | 91.67       |
| 12   | 3        | 89.4          | 76.67 | 1.11    | 88.33       |
| 11   | 234      | 80.6          | 70    | 1       | 85          |
| 10   | 13       | 58.1          | 63.33 | .72     | 81.67       |
| 9    | 23       | 56.9          | 56.67 | .71     | 78.33       |
| 8    | 1234     | 51.9          | 50    | .64     | 75          |
| 7    | 24       | 43.1          | 43.33 | .53     | 71.67       |
| 6    | 1        | 38.1          | 36.67 | .47     | 68.33       |
| 5    | 134      | 31.9          | 30    | .4      | 65          |
| 4    | 14       | 23.1          | 23.33 | .29     | 61.67       |
| 3    | 12       | 18.1          | 16.67 | .22     | 58.33       |
| 2    | 123      | 8.1           | 10    | .1      | 55          |
| 1    | 124      | 3.1           | 3.33  | .04     | 51.67       |

PROB = ((R(I)-.5)/R(MAX))\*100% WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
 THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL = (PROB+100%)/2

#### VARIABLE #'S AND IDENTITIES

|    |                  |            |           |
|----|------------------|------------|-----------|
| 1: | LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: | WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: | LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: | LEAF CONDITION   | (+)GREEN   | (-)RED    |

# VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

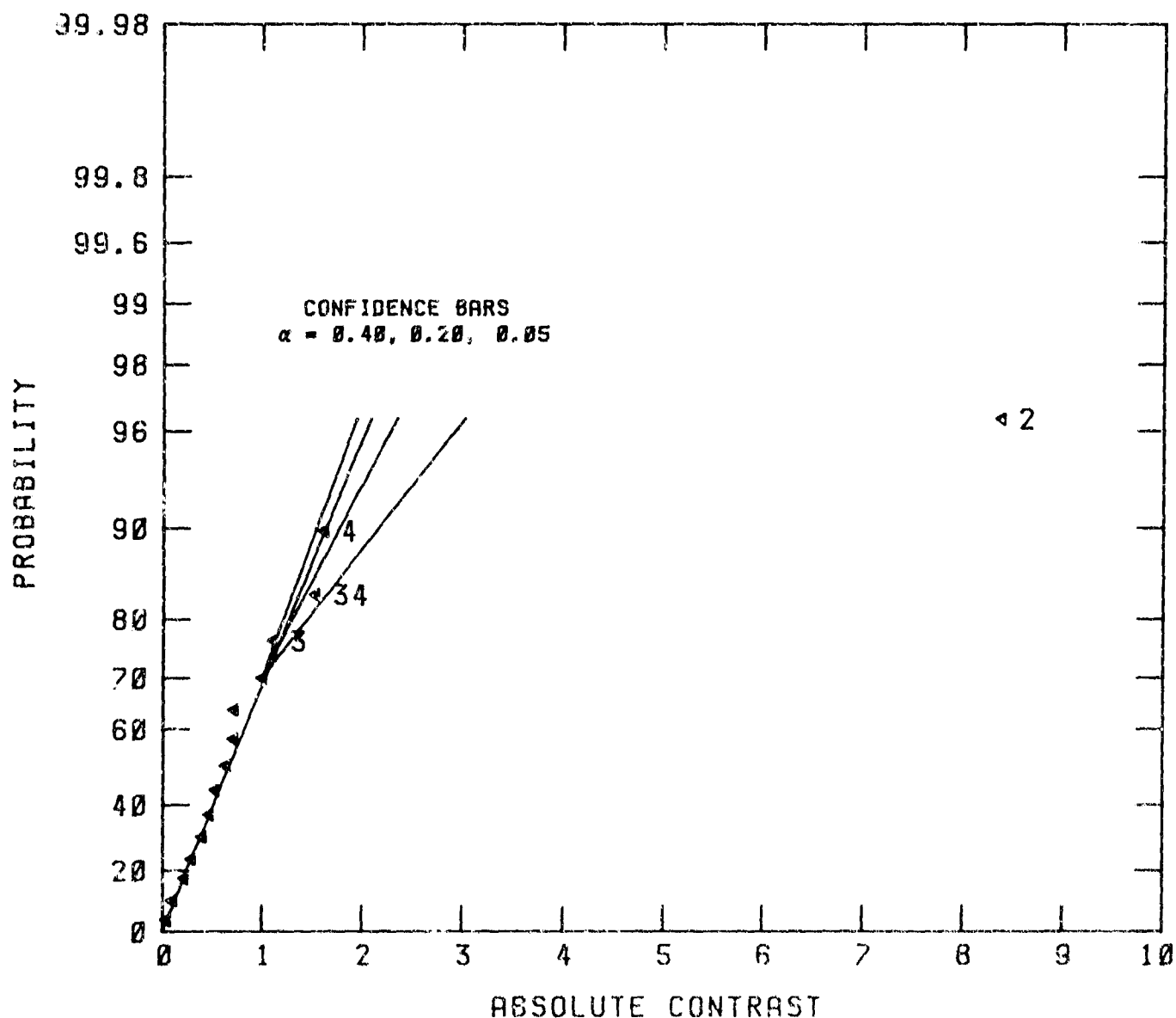


FIGURE L-4. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
LIFE TIME OF 2 MM DIA DROPLETS DEPOSITED ON  
OAK LEAF SURFACE AT 80 DEG F AND 42% RH

TABLE L-10. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
 AVERAGE EVAPORATION RATE (MMG/MIN) OVER LIFE TIME OF  
 DROPLET (2 MM DIA) CONTAMINATION ON OAK LEAF SURFACE  
 AT 60 DEG F AND 42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 4     | 8.6         | -              |
| 2    | +        | 5     | 1.1         | 5.0625         |
| 3    | -        | 12    | 7.6         | 232.5625       |
| 4    | 12       | 12    | .1          | .0625          |
| 5    | 3        | 4     | -1.1        | 5.0625         |
| 6    | 13       | 5     | .4          | .5625          |
| 7    | 23       | 10    | -.6         | 1.5625         |
| 8    | 123      | 13    | .4          | .5625          |
| 9    | 4        | 5     | .9          | 3.0625         |
| 10   | 14       | 6     | -.1         | .0625          |
| 11   | 24       | 14    | .4          | .5625          |
| 12   | 124      | 15    | -.1         | .0625          |
| 13   | 34       | 4     | -.9         | 3.0625         |
| 14   | 134      | 5     | -.4         | .5625          |
| 15   | 234      | 11    | -.4         | .5625          |
| 16   | 1234     | 12    | -.4         | .5625          |

TOTAL = 253.9375

#### VARIABLE #'S AND IDENTITIES

|    |                  |            |           |
|----|------------------|------------|-----------|
| 1: | LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: | WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: | LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: | LEAF CONDITION   | (+)GREEN   | (-)RED    |

TABLE L-11. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
AVERAGE EVAPORATION RATE (MMC/MIN) OVER LIFE TIME OF  
DROPLET (2 MM DIA) CONTAMINATION ON OAK LEAF SURFACE  
AT 60 DEG F AND 42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 7.6           | 96.67 | 8.44    | 98.33       |
| 14   | 3        | 1.1           | 90    | 1.22    | 95          |
| 13   | 1        | 1.1           | 83.33 | 1.22    | 91.67       |
| 12   | 34       | .9            | 76.67 | 1       | 88.33       |
| 11   | 4        | .9            | 70    | 1       | 85          |
| 10   | 23       | .6            | 63.33 | .67     | 81.67       |
| 9    | 1234     | .4            | 56.67 | .44     | 78.33       |
| 8    | 234      | .4            | 50    | .44     | 75          |
| 7    | 134      | .4            | 43.33 | .44     | 71.67       |
| 6    | 24       | .4            | 36.67 | .44     | 68.33       |
| 5    | 123      | .4            | 30    | .44     | 65          |
| 4    | 13       | .4            | 23.33 | .44     | 61.67       |
| 3    | 124      | .1            | 16.67 | .11     | 58.33       |
| 2    | 14       | .1            | 10    | .11     | 55          |
| 1    | 12       | .1            | 3.33  | .11     | 51.67       |

PROB = ((R(I)-.5)/R(MAX))\*100% WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL = (PROB+100%)/2

#### VARIABLE #'S AND IDENTITIES

|    |                  |            |           |
|----|------------------|------------|-----------|
| 1: | LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: | WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: | LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: | LEAF CONDITION   | (+)GREEN   | (-)RED    |

# VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

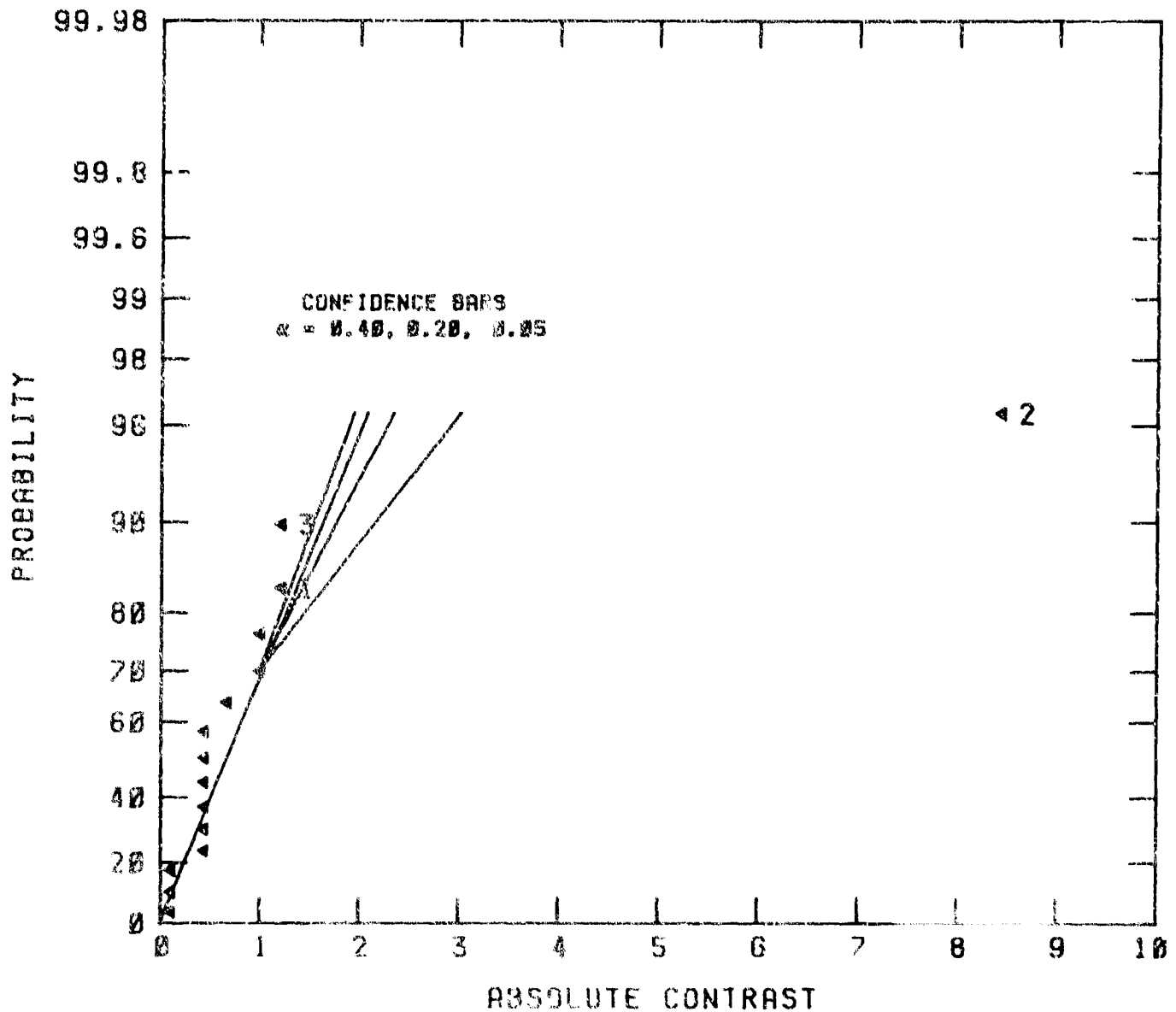


FIGURE L-5. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
 AVERAGE EVAPORATION RATE FOR 2 MM DIA DROPLETS  
 DEPOSITED ON OAK LEAVES AT 80 DEG F AND 42% RH

TABLE L-12. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
PERCENT OF DROPLET (2 MM DIA) CONTAMINATION RECOVERED  
AS VAPOR AFTER 1 HR FROM OAK LEAF SURFACE AT 60 DEG  
W AND 42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 10    | 17.7        | -              |
| 2    | 1        | 11    | -1.6        | 10.5625        |
| 3    | 2        | 14    | 12.9        | 663.0625       |
| 4    | 12       | 24    | -1.1        | 5.0625         |
| 5    | 3        | 10    | -3.4        | 45.5625        |
| 6    | 13       | 11    | 1.1         | 5.0625         |
| 7    | 23       | 23    | -1.9        | 3.0625         |
| 8    | 123      | 22    | .6          | 1.5625         |
| 9    | 4        | 16    | 1.6         | 10.5625        |
| 10   | 14       | 13    | -1.9        | 14.0625        |
| 11   | 24       | 33    | .1          | .0625          |
| 12   | 124      | 24    | -1.4        | .5625          |
| 13   | 34       | 10    | -2.6        | 27.5625        |
| 14   | 134      | 9     | 1.4         | 7.5625         |
| 15   | 234      | 22    | -1.1        | .0625          |
| 16   | 1234     | 21    | .9          | 3.0625         |

TOTAL = 757.4375

#### VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (*) 10 CG  | (-) 100 CG |
| 2: WIND SPEED       | (*) 11 MPH | (-) 1 MPH  |
| 3: LEAF SURFACE     | (*) BOTTOM | (-) TOP    |
| 4: LEAF CONDITION   | (*) GREEN  | (-) RED    |



TABLE L-13. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
PERCENT OF DROPLET (2 MM DIA) CONTAMINATION RECOVERED  
AS VAPOR AFTER 1 HR FROM OAK LEAF SURFACE AT 60 DEG  
F AND 42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 12.9          | 96.67 | 8.06    | 98.33       |
| 14   | 3        | 3.4           | 90    | 2.13    | 95          |
| 13   | 34       | 2.6           | 83.33 | 1.62    | 91.67       |
| 12   | 14       | 1.9           | 76.67 | 1.19    | 88.33       |
| 11   | 4        | 1.6           | 70    | 1       | 85          |
| 10   | 1        | 1.6           | 63.33 | 1       | 81.67       |
| 9    | 134      | 1.4           | 56.67 | .88     | 78.33       |
| 8    | 13       | 1.1           | 50    | .69     | 75          |
| 7    | 12       | 1.1           | 43.33 | .69     | 71.67       |
| 6    | 1234     | .9            | 36.67 | .56     | 68.33       |
| 5    | 23       | .9            | 30    | .56     | 65          |
| 4    | 123      | .6            | 23.33 | .38     | 61.67       |
| 3    | 124      | .4            | 16.67 | .25     | 58.33       |
| 2    | 234      | .1            | 10    | .06     | 55          |
| 1    | 24       | .1            | 3.33  | .06     | 51.67       |

PROB =  $((R(I) - .5) / R(\text{MAX})) * 100\%$  WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL =  $(\text{PROB} * 100\%) / 2$

#### VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

# VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

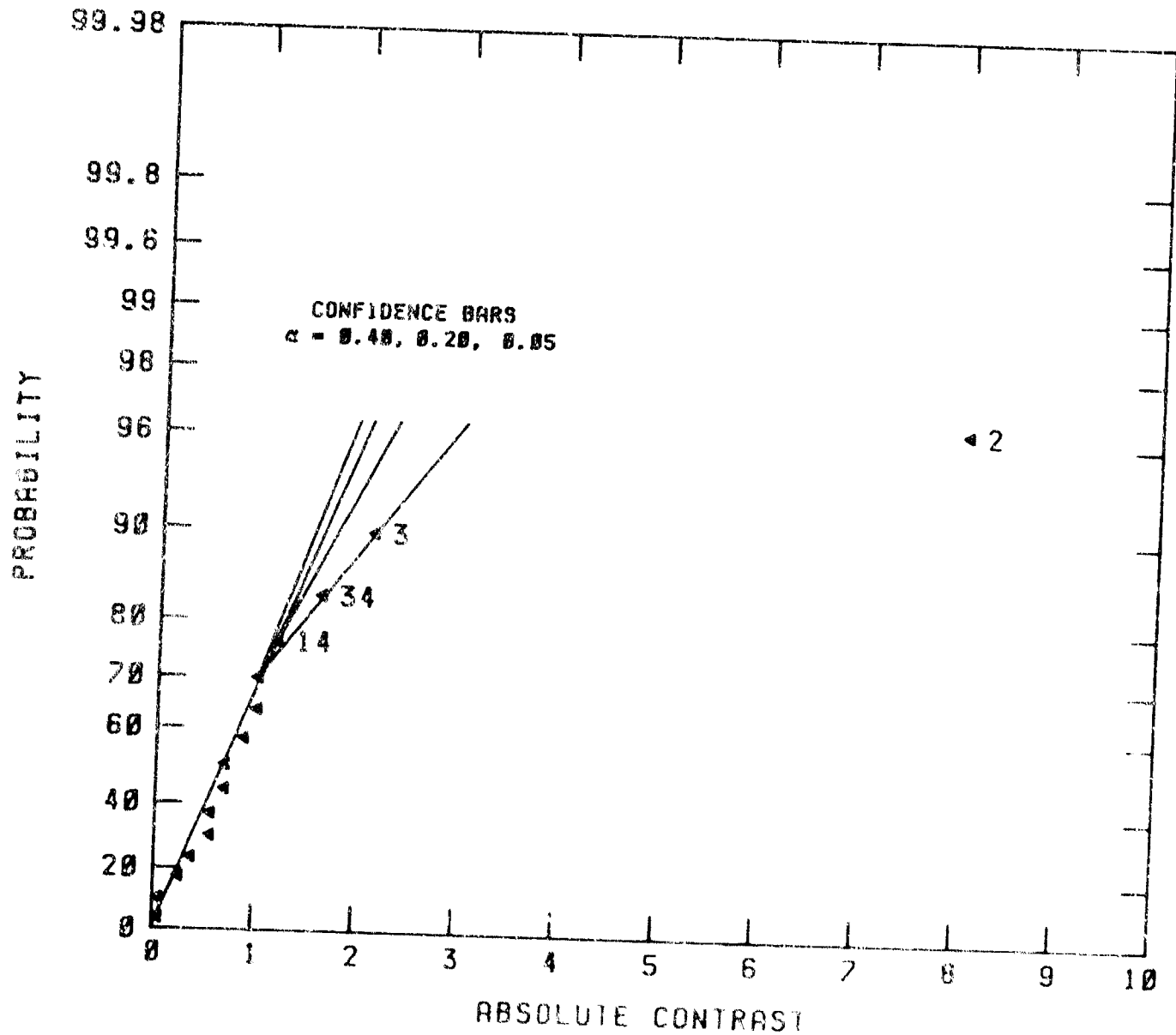


FIGURE L-6. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
 PERCENT OF CONTAMINATION RECOVERED AS VAPOR AFTER 1 HR  
 FROM 2 MM DIA DROPS ON OAK LEAVES AT 80 DEG F AND 42% RH

TABLE L-14. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
PERCENT OF DROPLET (2 MM DIA) CONTAMINATION RECOVERED  
AS VAPOR AFTER 2 HR FROM OAK LEAF SURFACE AT 60 DEG  
F AND 42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 20    | 32.9        | -              |
| 2    | 1        | 21    | -2.7        | 30.25          |
| 3    | 2        | 44    | 23          | 2116           |
| 4    | 12       | 44    | -1.5        | 9              |
| 5    | 3        | 20    | -5.2        | 110.25         |
| 6    | 13       | 21    | 1.3         | 6.25           |
| 7    | 23       | 43    | -1          | 4              |
| 8    | 123      | 41    | .5          | 1              |
| 9    | 4        | 29    | 2.3         | 20.25          |
| 10   | 14       | 24    | -2.7        | 30.25          |
| 11   | 24       | 57    | .5          | 1              |
| 12   | 124      | 45    | -1.5        | 1              |
| 13   | 34       | 19    | -4.2        | 72.25          |
| 14   | 134      | 17    | 1.8         | 12.25          |
| 15   | 34       | 42    | 0           | 0              |
| 16   | 1234     | 39    | 1           | 4              |

TOTAL = 2417.75

#### VARIABLE #'S AND IDENTITIES

|    |                  |            |           |
|----|------------------|------------|-----------|
| 1: | LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: | WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: | LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: | LEAF CONDITION   | (+)GREEN   | (-)RED    |

TABLE L-15. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
PERCENT OF DROPLET (2 MM DIA) CONTAMINATION RECOVERED  
AS VAPOR AFTER 2 HR FROM OAK LEAF SURFACE AT 60 DEG  
F AND 42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 23            | 96.67 | 8.52    | 98.33       |
| 14   | 3        | 5.2           | 90    | 1.93    | 95          |
| 13   | 34       | 4.2           | 83.33 | 1.56    | 91.67       |
| 12   | 14       | 2.7           | 76.67 | 1       | 88.33       |
| 11   | 1        | 2.7           | 70    | 1       | 85          |
| 10   | 4        | 2.3           | 63.33 | .85     | 81.67       |
| 9    | 134      | 1.8           | 56.67 | .67     | 78.33       |
| 8    | 12       | 1.5           | 50    | .56     | 75          |
| 7    | 13       | 1.3           | 43.33 | .48     | 71.67       |
| 6    | 1234     | 1             | 36.67 | .37     | 68.33       |
| 5    | 23       | 1             | 30    | .37     | 65          |
| 4    | 124      | .5            | 23.33 | .19     | 61.67       |
| 3    | 24       | .5            | 16.67 | .19     | 58.33       |
| 2    | 123      | .5            | 10    | .19     | 55          |
| 1    | 234      | 0             | 3.33  | 0       | 51.67       |

PROB = ((R(I)-.5)/R(MAX))\*100% WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL = (PRCB+100%)/2

#### VARIABLE #'S AND IDENTITIES

|    |                  |            |           |
|----|------------------|------------|-----------|
| 1: | LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: | WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: | LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: | LEAF CONDITION   | (+)GREEN   | (-)RED    |

# VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

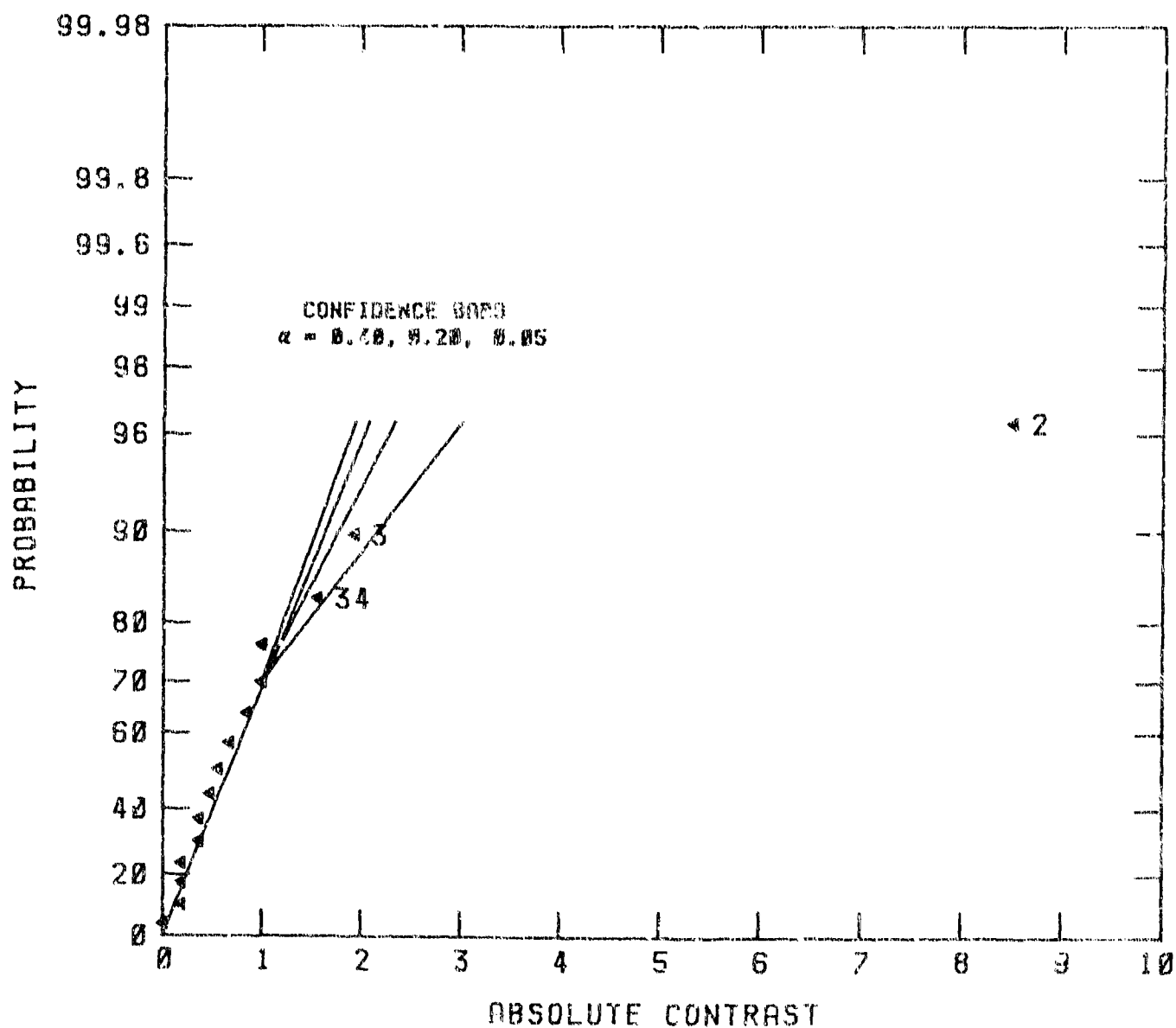


FIGURE L-7. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
 PERCENT OF CONTAMINATION RECOVERED AS VAPOR AFTER 2 HR  
 FROM 2 MM DIA DROPS ON OAK LEAVES AT 80 DEG F AND 62% RH

TABLE L-16. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
PERCENT OF DROPLET (2 MM DIA) CONTAMINATION RECOVERED  
AS VAPOR AFTER 3 HR FROM OAK LEAF SURFACE AT 60 DEG  
F AND 42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 29    | 45.6        | -              |
| 2    | 1        | 31    | -2.7        | 30.25          |
| 3    | 2        | 60    | 30.5        | 3721           |
| 4    | 12       | 62    | -1          | 4              |
| 5    | 3        | 29    | -6.7        | 182.25         |
| 6    | 13       | 30    | .8          | 2.25           |
| 7    | 23       | 59    | -5.5        | 1              |
| 8    | 123      | 58    | .5          | 1              |
| 9    | 4        | 40    | 1.8         | 12.25          |
| 10   | 14       | 34    | -3.7        | 56.25          |
| 11   | 24       | 74    | .5          | 1              |
| 12   | 124      | 62    | -5.5        | 1              |
| 13   | 34       | 27    | -5.2        | 110.25         |
| 14   | 134      | 23    | 1.8         | 12.25          |
| 15   | 234      | 58    | .5          | 1              |
| 16   | 1234     | 54    | 1           | 4              |

TOTAL = 4139.75

#### VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF COND OR     | (+)GREEN   | (-)RED    |

TABLE L-17. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
PERCENT OF DROPLET (2 MM DIA) CONTAMINATION RECOVERED  
AS VAPOR AFTER 3 HR FROM OAK LEAF SURFACE AT 60 DEG  
F AND 42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 30.5          | 96.67 | 11.3    | 98.33       |
| 14   | 3        | 6.7           | 90    | 2.48    | 95          |
| 13   | 34       | 5.2           | 33.33 | 1.93    | 91.67       |
| 12   | 14       | 3.7           | 76.67 | 1.37    | 88.33       |
| 11   | 1        | 2.7           | 70    | 1       | 85          |
| 10   | 134      | 1.8           | 63.33 | .67     | 81.67       |
| 9    | 4        | 1.8           | 56.67 | .67     | 78.33       |
| 8    | 1234     | 1             | 50    | .37     | 75          |
| 7    | 12       | 1             | 43.33 | .37     | 71.67       |
| 6    | 13       | .8            | 36.67 | .3      | 68.33       |
| 5    | 234      | .5            | 30    | .19     | 65          |
| 4    | 124      | .5            | 23.33 | .19     | 61.67       |
| 3    | 24       | .5            | 16.67 | .19     | 58.33       |
| 2    | 123      | .5            | 10    | .19     | 55          |
| 1    | 23       | .5            | 3.33  | .19     | 51.67       |

PROB =  $((R(I) - .5) / R(\text{MAX})) * 100\%$  WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL =  $(\text{PROB} + 100\%) / 2$

#### VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

# VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

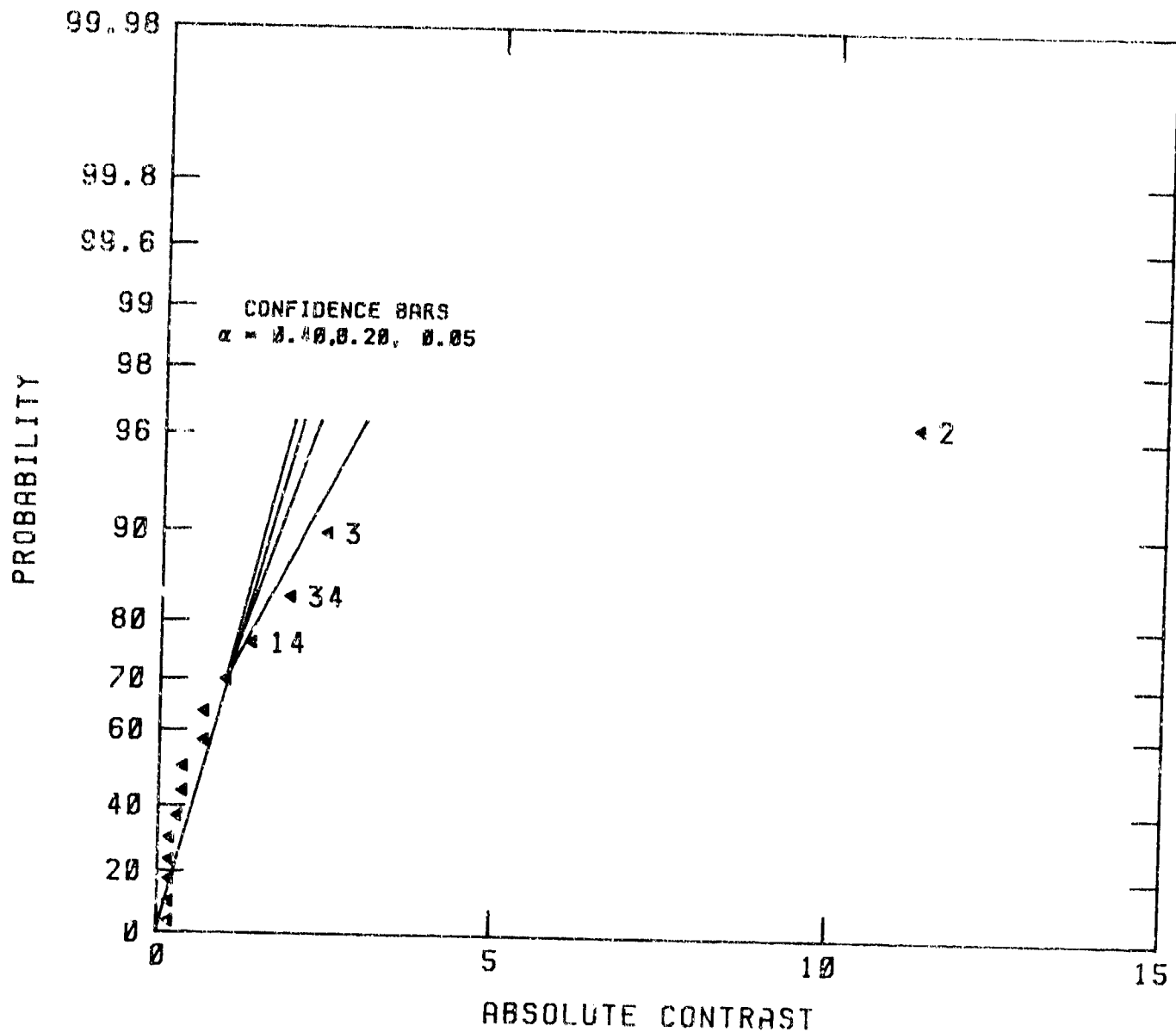


FIGURE L-8. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
 PERCENT OF CONTAMINATION RECOVERED AS VAPOR AFTER 3 HR  
 FROM 2 MM DIA DROPS ON OAK LEAVES AT 80 DEG F AND 42% RH



TABLE L-18. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
PERCENT OF DROPLET (2 MM DIA) CONTAMINATION RECOVERED  
AS VAPOR AFTER 6 HR FROM OAK LEAF SURFACE AT 60 DEG  
F AND 42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 54    | 71.1        | -              |
| 2    | 1        | 56    | 1.9         | 14.0625        |
| 3    | 2        | 85    | 33.1        | 4389.0625      |
| 4    | 12       | 94    | 2.4         | 22.5625        |
| 5    | 3        | 52    | -5.1        | 105.0625       |
| 6    | 13       | 56    | .1          | .0625          |
| 7    | 23       | 84    | 2.4         | 22.5625        |
| 8    | 123      | 92    | -.9         | 3.0625         |
| 9    | 4        | 64    | -1.1        | 5.0625         |
| 10   | 14       | 59    | -3.9        | 60.0625        |
| 11   | 24       | 88    | -1.1        | 5.0625         |
| 12   | 124      | 89    | -.4         | .5625          |
| 13   | 34       | 49    | -3.9        | 60.0625        |
| 14   | 134      | 46    | -.1         | .0625          |
| 15   | 234      | 85    | 2.6         | 27.5625        |
| 16   | 1234     | 84    | -.1         | .0625          |

TOTAL = 4714.9375

VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

TABLE L-15. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
PERCENT OF DROPLET (2 MM DIA) CONTAMINATION RECOVERED  
AS VAPOR AFTER 6 HR FROM OAK LEAF SURFACE AT 60 DEG  
F AND 42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 33.1          | 96.67 | 12.73   | 98.33       |
| 14   | 3        | 5.1           | 90    | 1.96    | 95          |
| 13   | 34       | 3.9           | 83.33 | 1.5     | 91.67       |
| 12   | 14       | 3.9           | 76.67 | 1.5     | 88.33       |
| 11   | 234      | 2.6           | 70    | 1       | 85          |
| 10   | 23       | 2.4           | 63.33 | .92     | 81.67       |
| 9    | 12       | 2.4           | 56.67 | .92     | 78.33       |
| 8    | 1        | 1.9           | 50    | .73     | 75          |
| 7    | 24       | 1.1           | 43.33 | .42     | 71.67       |
| 6    | 4        | 1.1           | 36.67 | .42     | 68.33       |
| 5    | 123      | .9            | 30    | .35     | 65          |
| 4    | 124      | .4            | 23.33 | .15     | 61.67       |
| 3    | 1234     | .1            | 16.67 | .04     | 58.33       |
| 2    | 134      | .1            | 10    | .04     | 55          |
| 1    | 13       | .1            | 3.33  | .04     | 51.67       |

PROB =  $((R(I) - .5) / R(\text{MAX})) * 100\%$  WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL =  $(\text{PROB} + 100\%) / 2$

#### VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

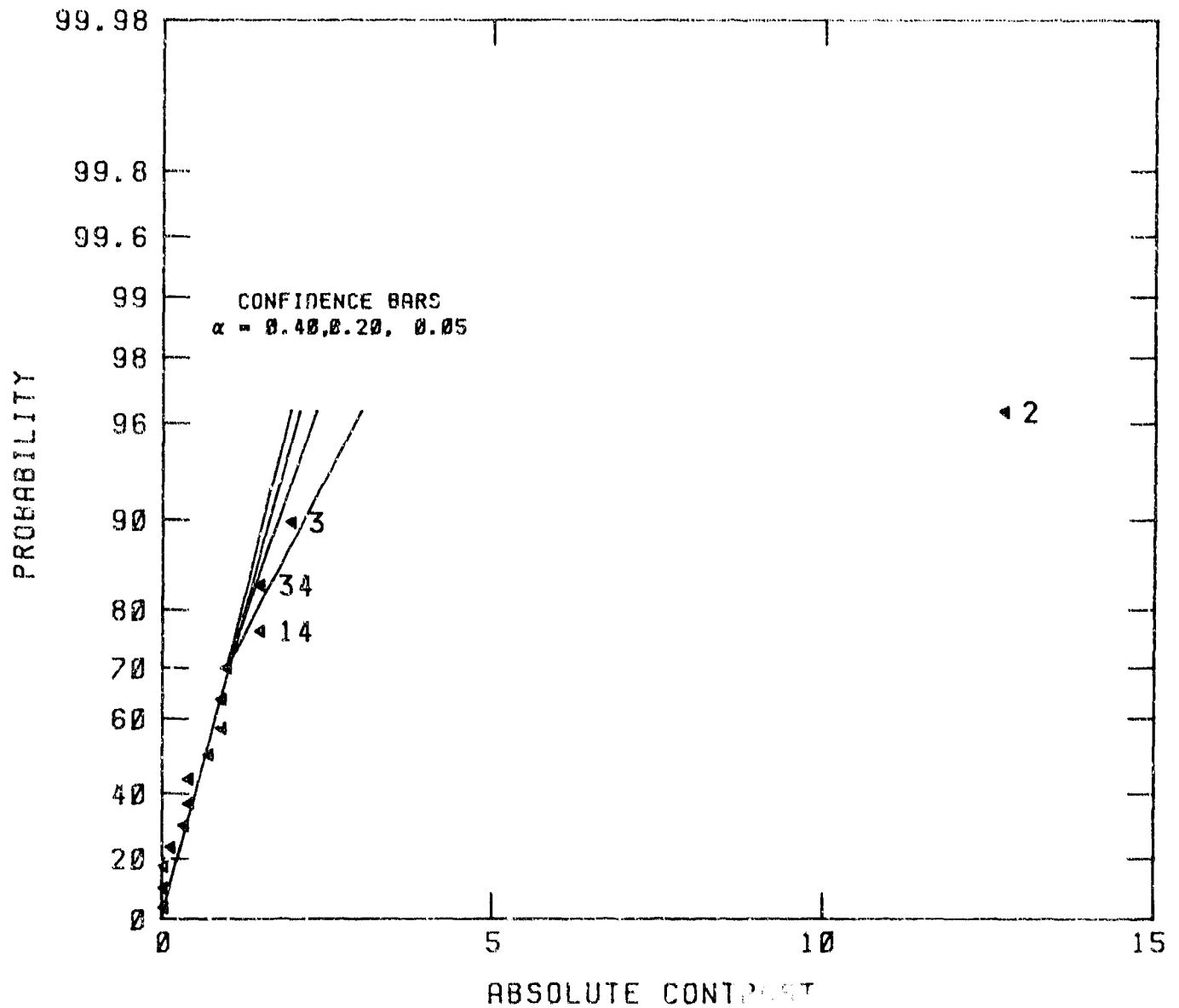


FIGURE L-9. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
 PERCENT OF CONTAMINATION RECOVERED AS VAPOR AFTER 8 HR  
 FROM 2 MM DIA DROPS ON OAK LEAVES AT 60 DEG F AND 42% RH

TABLE L-20. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
AVERAGE EVAPORATION RATE (MMG/MIN) FOR DROPLET (2 MM  
DIA) DEPOSITED ON OAK LEAF SURFACE FOR 1 HR AT 60 DEG  
F AND 42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 11    | 18.1        | -              |
| 2    | 1        | 12    | -.1         | .0625          |
| 3    | 2        | 25    | 13.4        | 715.5625       |
| 4    | 12       | 26    | -.4         | .5625          |
| 5    | 3        | 11    | -3.6        | 52.5625        |
| 6    | 13       | 11    | .6          | 1.5625         |
| 7    | 23       | 22    | -.9         | 3.0625         |
| 8    | 123      | 24    | .9          | 3.0625         |
| 9    | 4        | 14    | .6          | 1.5625         |
| 10   | 14       | 14    | -1.1        | 5.0625         |
| 11   | 24       | 31    | .4          | .5625          |
| 12   | 124      | 26    | -.9         | 3.0625         |
| 13   | 34       | 9     | -2.1        | 18.0625        |
| 14   | 134      | 9     | .6          | 1.5625         |
| 15   | 234      | 22    | .1          | .0625          |
| 16   | 1234     | 22    | .4          | .5625          |

TOTAL = 806.9375

#### VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

TABLE L-21. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
AVERAGE EVAPORATION RATE (MMG/MIN) FOR DROPLET (2 MM  
DIA) DEPOSITED ON OAK LEAF SURFACE FOR 1 HR AT 60 DEG  
F AND 42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 13.4          | 96.67 | 14.89   | 98.33       |
| 14   | 3        | 3.6           | 90    | 4       | 95          |
| 13   | 34       | 2.1           | 83.33 | 2.33    | 91.67       |
| 12   | 14       | 1.1           | 76.67 | 1.22    | 88.33       |
| 11   | 124      | .9            | 70    | 1       | 85          |
| 10   | 123      | .9            | 63.33 | 1       | 81.67       |
| 9    | 23       | .9            | 56.67 | 1       | 78.33       |
| 8    | 134      | .6            | 50    | .67     | 75          |
| 7    | 4        | .6            | 43.33 | .67     | 71.67       |
| 6    | 13       | .6            | 36.67 | .67     | 68.33       |
| 5    | 1234     | .4            | 30    | .44     | 65          |
| 4    | 24       | .4            | 23.33 | .44     | 61.67       |
| 3    | 12       | .4            | 16.67 | .44     | 58.33       |
| 2    | 234      | .1            | 10    | .11     | 55          |
| 1    | 1        | .1            | 3.33  | .11     | 51.67       |

PROB =  $((R(I) - .5) / R(\text{MAX})) * 100\%$  WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL =  $(\text{PROB} + 100\%) / 2$

#### VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

# VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

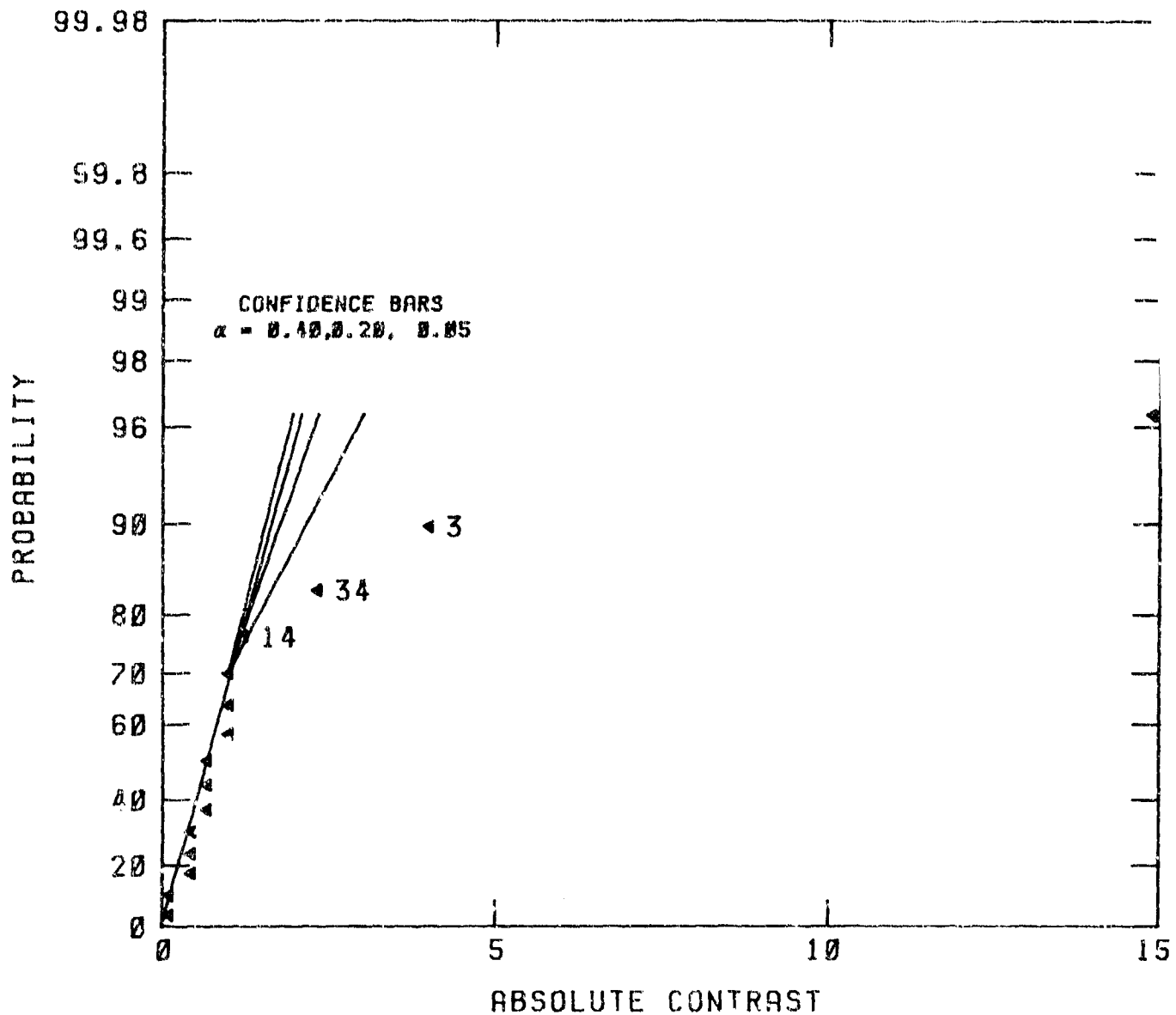


FIGURE L-10. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
 AVERAGE EVAPORATION RATE OF 2MM DIA DROPS DEPOSITED ON  
 OAK LEAVES FOR 1 HR AT 60 DEG F AND 42% RH

TABLE L-22. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
 AVERAGE EVAPORATION RATE (MMG/MIN) FOR DROPLET (2 MM  
 DIA) DEPOSITED ON OAK LEAF SURFACE FOR 2 HR AT 60 DEG  
 F AND 42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 10    | 16.7        | -              |
| 2    | 1        | 11    | .6          | 1.5625         |
| 3    | 2        | 23    | 12.4        | 612.5625       |
| 4    | 12       | 25    | -.4         | .5625          |
| 5    | 3        | 10    | -2.9        | 33.0625        |
| 6    | 13       | 11    | .4          | .5625          |
| 7    | 23       | 21    | -.9         | 3.0625         |
| 8    | 123      | 23    | .4          | .5625          |
| 9    | 4        | 12    | -.1         | .0625          |
| 10   | 14       | 13    | -.9         | 3.0625         |
| 11   | 24       | 27    | -.1         | .0625          |
| 12   | 124      | 24    | -.9         | 3.0625         |
| 13   | 34       | 8     | -1.9        | 14.0625        |
| 14   | 134      | 9     | .4          | .5625          |
| 15   | 234      | 20    | .1          | .0625          |
| 16   | 1234     | 20    | .4          | .5625          |

TOTAL = 673.4375

#### VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

TABLE L-23. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
AVERAGE EVAPORATION RATE (MMG/MIN) FOR DROPLET (2 MM  
DIA) DEPOSITED ON OAK LEAF SURFACE FOR 2 HR AT 60 DEG  
F AND 42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 12.4          | 96.67 | 13.78   | 98.33       |
| 14   | 3        | 2.9           | 90    | 3.22    | 95          |
| 13   | 34       | 1.9           | 83.33 | 2.11    | 91.67       |
| 12   | 124      | .9            | 76.67 | 1       | 88.33       |
| 11   | 14       | .9            | 70    | 1       | 85          |
| 10   | 23       | .9            | 63.33 | 1       | 81.67       |
| 9    | 1        | .6            | 56.67 | .67     | 78.33       |
| 8    | 1234     | .4            | 50    | .44     | 75          |
| 7    | 134      | .4            | 43.33 | .44     | 71.67       |
| 6    | 123      | .4            | 36.67 | .44     | 68.33       |
| 5    | 13       | .4            | 30    | .44     | 65          |
| 4    | 12       | .4            | 23.33 | .44     | 61.67       |
| 3    | 234      | .1            | 16.67 | .11     | 58.33       |
| 2    | 24       | .1            | 10    | .11     | 55          |
| 1    | 4        | .1            | 3.33  | .11     | 51.67       |

PROB =  $((R(I) - .5) / R(\text{MAX})) * 100\%$  WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL =  $(\text{PROB} + 100\%) / 2$

#### VARIABLE #'S AND IDENTITIES

|    |                  |            |           |
|----|------------------|------------|-----------|
| 1: | LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: | WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: | LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: | LEAF CONDITION   | (+)GREEN   | (-)RED    |



VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

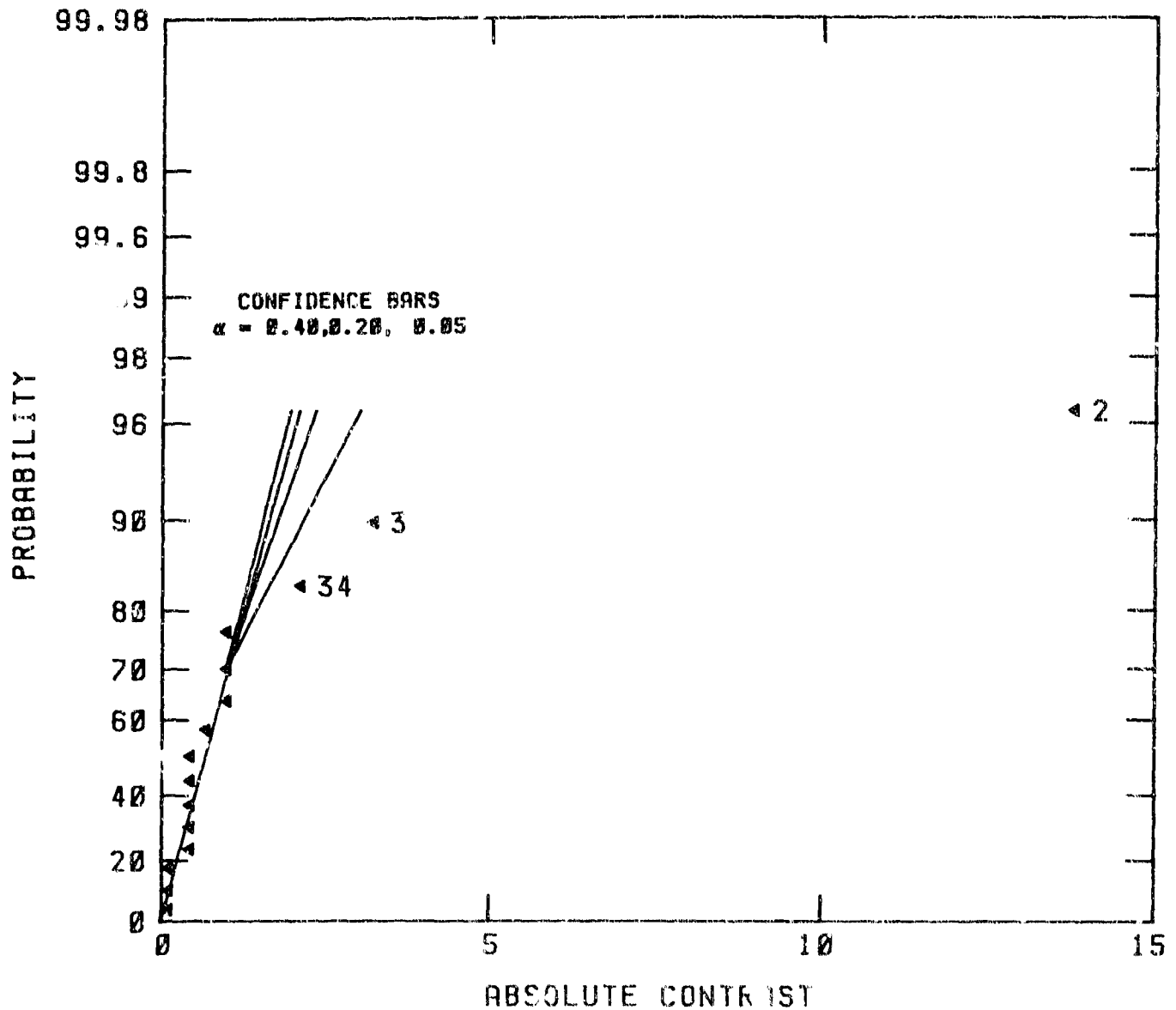


FIGURE L-11. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
 AVERAGE EVAPORATION RATE OF 2 MM DIA DROPS DEPOSITED  
 ON OAK LEAVES FOR 2 HR AT 80 DEG F AND 42% RH

TABLE L-24. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
AVERAGE EVAPORATION RATE (MMG/MIN) FOR DROPLET (2 MM  
DIA) DEPOSITED FOR 3 HR ON OAK LEAF SURFACE AT 60 DEG  
F AND 42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 10    | 15.5        | -              |
| 2    | 1        | 11    | 1           | 4              |
| 3    | 2        | 21    | 10.5        | 441            |
| 4    | 12       | 23    | 0           | 0              |
| 5    | 3        | 10    | -2.2        | 20.25          |
| 6    | 13       | 11    | .3          | .25            |
| 7    | 23       | 13    | -.7         | 2.25           |
| 8    | 123      | 21    | .3          | .25            |
| 9    | 4        | 11    | -.5         | 1              |
| 10   | 14       | 12    | -.5         | 1              |
| 11   | 24       | 23    | 0           | 0              |
| 12   | 124      | 22    | -.5         | 1              |
| 13   | 34       | 8     | -1.2        | 6.25           |
| 14   | 134      | 9     | .3          | .25            |
| 15   | 234      | 18    | .3          | .25            |
| 16   | 1234     | 19    | .3          | .25            |

TOTAL = 478

#### VARIABLE #'S AND IDENTITIES

|    |                  |            |           |
|----|------------------|------------|-----------|
| 1: | LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: | WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: | LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: | LEAF CONDITION   | (+)GREEN   | (-)RED    |

TABLE 1-25. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
AVERAGE EVAPORATION RATE (MMG/MIN) FOR DROPLET (2 MM  
DIA) DEPOSITED FOR 3 HR ON OAK LEAF SURFACE AT 60 DEG  
F AND 42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 10.5          | 96.67 | 15      | 98.33       |
| 14   | 3        | 2.2           | 90    | 3.14    | 95          |
| 13   | 34       | 1.2           | 83.33 | 1.71    | 91.67       |
| 12   | 1        | 1             | 76.67 | 1.43    | 88.33       |
| 11   | 23       | .7            | 70    | 1       | 85          |
| 10   | 124      | .5            | 63.33 | .71     | 81.67       |
| 9    | 14       | .5            | 56.67 | .71     | 78.33       |
| 8    | 4        | .5            | 50    | .71     | 75          |
| 7    | 1234     | .3            | 43.33 | .43     | 71.67       |
| 6    | 234      | .3            | 36.67 | .43     | 68.33       |
| 5    | 134      | .3            | 30    | .43     | 65          |
| 4    | 123      | .3            | 23.33 | .43     | 61.67       |
| 3    | 13       | .3            | 16.67 | .43     | 58.33       |
| 2    | 24       | 0             | 10    | 0       | 55          |
| 1    | 12       | 0             | 3.33  | 0       | 51.67       |

PROB =  $((R(I) - .5) / R(\text{MAX})) * 100\%$  WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL =  $(\text{PROB} + 100\%) / 2$

#### VARIABLE #'S AND IDENTITIES

|    |                  |            |           |
|----|------------------|------------|-----------|
| 1: | LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: | WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: | LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: | LEAF CONDITION   | (+)GREEN   | (-)RED    |

# VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

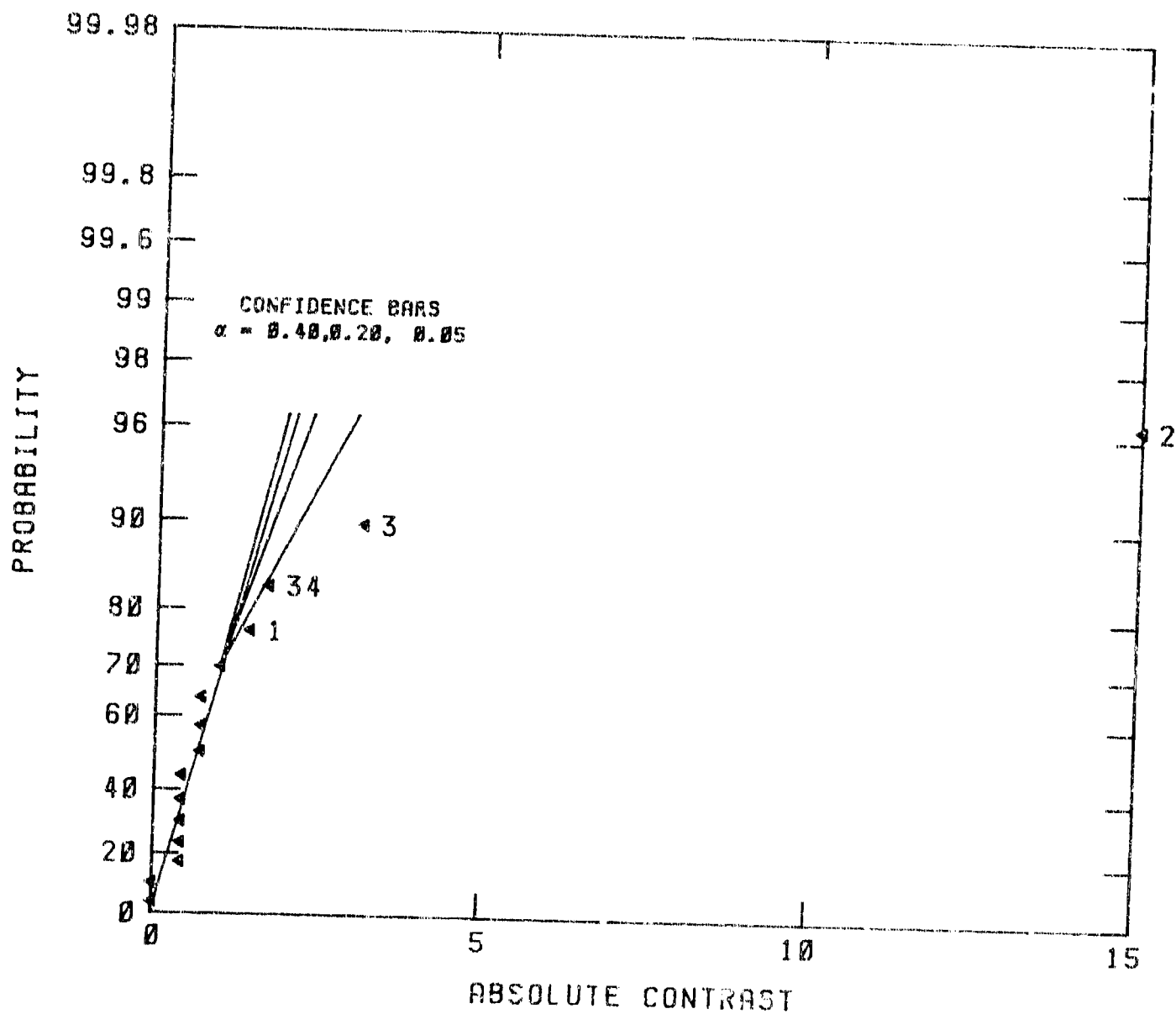


FIGURE L-12. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
 AVERAGE EVAPORATION RATE OF 2 MM DIA DROPS DEPOSITED  
 ON OAK LEAVES FOR 3 HR AT 80 DEG F AND 42% RH

TABLE L-26. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
AVERAGE EVAPORATION RATE (MMG/MIN) FOR DROPLET (2 MM  
DIA) DEPOSITED FOR 6 HR ON OAK LEAF SURFACE AT 60 DEG  
F AND 42% RH

| TEST | CONTRAST | YIELD | AVG EFFECTS | SUM OF SQUARES |
|------|----------|-------|-------------|----------------|
| 1    | MEAN     | 9     | 12.1        | -              |
| 2    | 1        | 10    | 1.8         | 12.25          |
| 3    | 2        | 15    | 6           | 144            |
| 4    | 12       | 18    | .5          | 1              |
| 5    | 3        | 9     | -1.2        | 6.25           |
| 6    | 13       | 10    | -.2         | .25            |
| 7    | 23       | 14    | 0           | 0              |
| 8    | 123      | 17    | 0           | 0              |
| 9    | 4        | 9     | -1.2        | 6.25           |
| 10   | 14       | 11    | -.2         | .25            |
| 11   | 24       | 14    | -.5         | 1              |
| 12   | 124      | 16    | -.5         | 1              |
| 13   | 34       | 7     | -.7         | 2.25           |
| 14   | 134      | 8     | -.2         | .25            |
| 15   | 234      | 13    | .5          | 1              |
| 16   | 1234     | 14    | 0           | 0              |

TOTAL = 175.75

VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

TABLE L-27. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
AVERAGE EVAPORATION RATE (MMG/MIN) FOR DROPLET (2 MM  
DIA) DEPOSITED FOR 6 HR ON OAK LEAF SURFACE AT 60 DEG  
F AND 42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 2        | 6             | 96.67 | 8.57    | 98.33       |
| 14   | 1        | 1.8           | 90    | 2.57    | 95          |
| 13   | 4        | 1.2           | 83.33 | 1.71    | 91.67       |
| 12   | 3        | 1.2           | 76.67 | 1.71    | 88.33       |
| 11   | 34       | .7            | 70    | 1       | 85          |
| 10   | 234      | .5            | 63.33 | .71     | 81.67       |
| 9    | 124      | .5            | 56.67 | .71     | 78.33       |
| 8    | 24       | .5            | 50    | .71     | 75          |
| 7    | 12       | .5            | 43.33 | .71     | 71.67       |
| 6    | 134      | .2            | 36.67 | .29     | 68.33       |
| 5    | 14       | .2            | 30    | .29     | 65          |
| 4    | 13       | .2            | 23.33 | .29     | 61.67       |
| 3    | 1234     | 0             | 16.67 | 0       | 58.33       |
| 2    | 123      | 0             | 10    | 0       | 55          |
| 1    | 23       | 0             | 3.33  | 0       | 51.67       |

PROB =  $((R(I) - .5) / R(\text{MAX})) * 100\%$  WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL =  $(\text{PROB} + 100\%) / 2$

#### VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

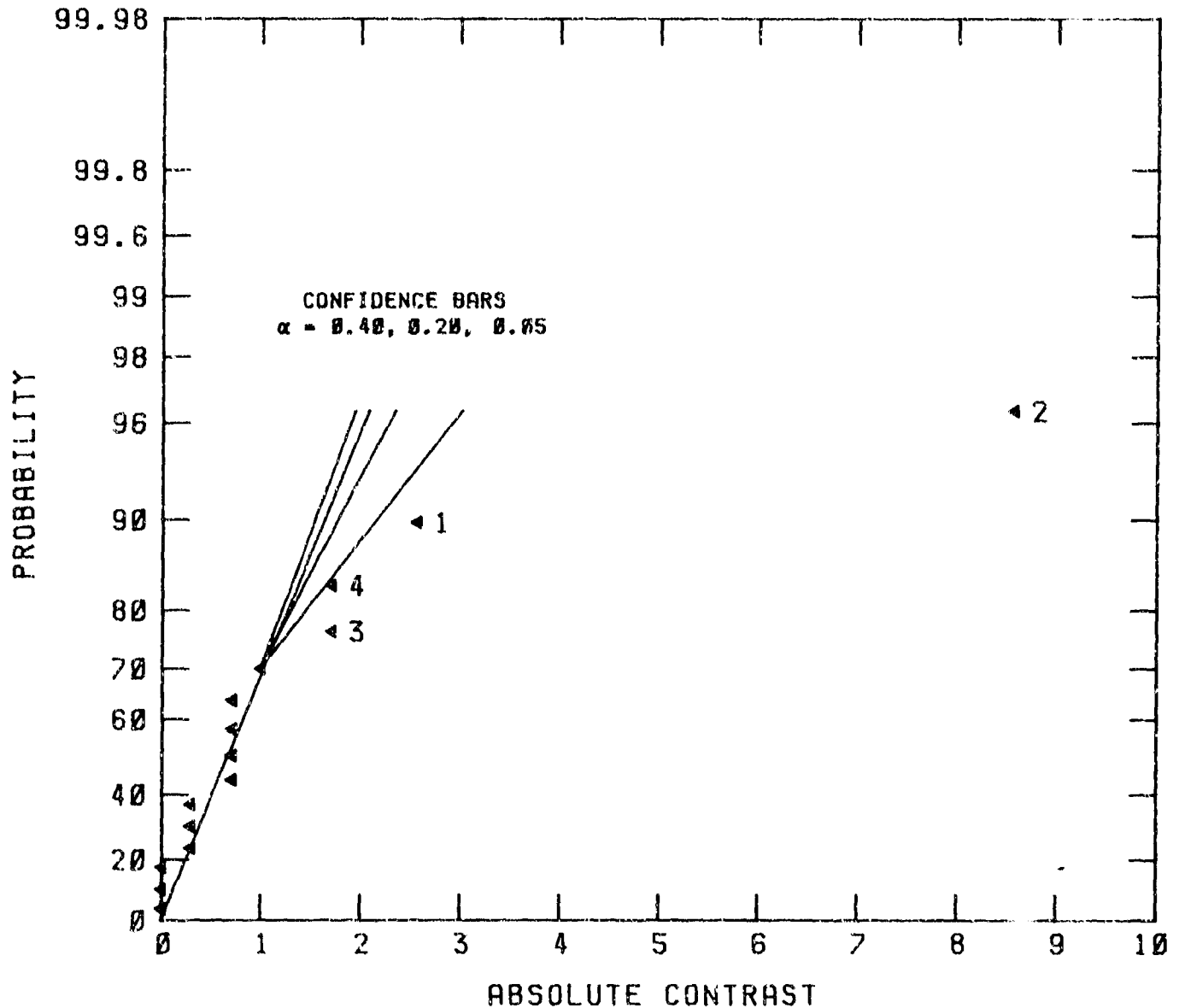


FIGURE L-13. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
 AVERAGE EVAPORATION RATE OF 2 MM DIA DROPS DEPOSITED  
 ON OAK LEAVES FOR 6 HR AT 80 DEG F AND 42% RH

Blank



APPENDIX M

ANOVA TABLES OF  $2^4$  FACTORIAL EXPERIMENTS  
ON DROPLET EVAPORATION CHARACTERISTICS

TABLE M-1. ANOVA Table of 2<sup>4</sup> Experiment No. 1 - Half-Life Droplet Contamination Deposited on Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|--------------------|----------------|--------------------|-------------|-------------------|
| 1 Liquid Viscosity | 2,002.562      | 1                  | 2,002.562   | 7.285 **          |
| 2 Wind Speed       | 127,985.063    | 1                  | 127,985.063 | 465.633 ****      |
| 3 Leaf Surface     | 20,952.562     | 1                  | 20,952.562  | 76.229 ****       |
| 4 Leaf Type        | 2,575.562      | 1                  | 2,575.562   | 9.370 **          |
| 1x2                | 95.0625        | 1                  | 95.0625     | 0.346             |
| 1x3                | 105.0625       | 1                  | 105.0625    | 0.382             |
| 1x4                | 351.5625       | 1                  | 351.5625    | 1.279             |
| 2x3                | 2,093.0625     | 1                  | 2,093.0625  | 7.615 **          |
| 2x4                | 390.0625       | 1                  | 390.0625    | 1.419             |
| 3x4                | 162.5625       | 1                  | 162.5625    | 0.591             |
| 1x2x3              | 22.5625        | 1                  |             |                   |
| 1x2x4              | 33.0625        | 1                  |             |                   |
| 1x3x4              | 18.0625        | 1                  |             |                   |
| 2x3x4              | 1,278.0625     | 1                  |             |                   |
| 1x2x3x4            | 22.5625        | 1                  |             |                   |
|                    | 1,374.3125     | 5                  | 274.8625    |                   |

Total Sum of Squares = 158,087.438

Critical Values:

\*\*\*\*  $F_{1,5,0.999} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*  $F_{1,5,0.90} = 4.06$

$F_{1,5,0.75} = 1.69$

TABLE M-2. ANOVA Table of  $2^4$  Experiment No. 2 - Half-Li e Droplet Contamination Deposited on Oak Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square  | Mean Square Ratio |
|--------------------|----------------|--------------------|--------------|-------------------|
| 1 Liquid Viscosity | 370.5625       | 1                  | 370.5625     | 0.736             |
| 2 Wind Speed       | 138,942.5625   | 1                  | 138,942.5625 | 276.029 ****      |
| 3 Leaf Surface     | 6,930.5625     | 1                  | 6,930.5625   | 13.769 **         |
| 4 Leaf Condition   | 68.0625        | 1                  | 68.0625      | 0.135             |
| 1x2                | 22.5625        | 1                  | 22.5625      | 0.045             |
| 1x3                | 27.5625        | 1                  | 27.5625      | 0.055             |
| 1x4                | 1,958.0625     | 1                  | 1,958.0625   | 3.890             |
| 2x3                | 1,387.5625     | 1                  | 1,387.5625   | 2.757             |
| 2x4                | 22.5625        | 1                  | 22.5625      | 0.045             |
| 3x4                | 5,513.0625     | 1                  | 5,513.0625   | 10.952 **         |
| 1x2x3              | 3.0625         | 1                  |              |                   |
| 1x2x4              | 410.0625       | 1                  |              |                   |
| 1x3x4              | 85.5625        | 1                  |              |                   |
| 2x3x4              | 1,958.0625     | 1                  |              |                   |
| 1x2x3x4            | 62.0625        | 1                  |              |                   |
|                    | 2,516.8125     | 5                  | 503.3625     |                   |

Total Sum of Squares = 158,087.438

Critical Values:

|      |                 |   |       |
|------|-----------------|---|-------|
| **** | $F_{1,5,0.999}$ | = | 47.18 |
| ***  | $F_{1,5,0.99}$  | = | 16.26 |
| **   | $F_{1,5,0.95}$  | = | 6.61  |
| *    | $F_{1,5,0.90}$  | = | 4.06  |
|      | $F_{1,5,0.75}$  | = | 1.69  |

TABLE M-3. ANOVA Table of  $2^4$  Experiment No. 1 - Average Evaporation Rate Over Half-life of Droplet Deposited on Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|--------------------|----------------|--------------------|-------------|-------------------|
| 1 Liquid Viscosity | 0.25           | 1                  | 0.25        | 0.10              |
| 2 Wind Speed       | 870.25         | 1                  | 870.25      | 348.10 ****       |
| 3 Leaf Surface     | 169.00         | 1                  | 169.00      | 67.60 ****        |
| 4 Leaf Type        | 36.00          | 1                  | 36.00       | 14.40 **          |
| 1x2                | 1.00           | 1                  | 1.00        | 0.40              |
| 1x3                | 2.25           | 1                  | 2.25        | 0.90              |
| 1x4                | 0.25           | 1                  | 0.25        | 0.10              |
| 2x3                | 42.25          | 1                  | 42.25       | 16.90 ***         |
| 2x4                | 6.25           | 1                  | 6.25        | 2.50              |
| 3x4                | 9.00           | 1                  | 9.00        | 3.60              |
| 1x2x3              | 1.000          | 1                  |             |                   |
| 1x2x4              | 4.000          | 1                  |             |                   |
| 1x3x4              | 0.250          | 1                  |             |                   |
| 2x3x4              | 6.250          | 1                  |             |                   |
| 1x2x3x4            | 1.000          | 1                  |             |                   |
|                    | 15.5           | 5                  | 2.5         |                   |

Total Sum of Squares = 1149

Critical Values:

\*\*\*\*  $F_{1,5,0.999} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*  $F_{1,5,0.90} = 4.06$

$F_{1,5,0.75} = 1.69$

TABLE M-4. ANOVA Table of  $2^4$  Experiment No. 2 - Average Evaporation Rate Over Half-life of Droplet Deposited on Oak Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|--------------------|----------------|--------------------|-------------|-------------------|
| 1 Liquid Viscosity | 1.00           | 1                  | 1.00        | 0.625             |
| 2 Wind Speed       | 676.00         | 1                  | 676.00      | 422.5 ****        |
| 3 Leaf Surface     | 36.00          | 1                  | 36.00       | 22.50 ***         |
| 4 Leaf Condition   | 1.00           | 1                  | 1.00        | 0.625             |
| 1x2                | 1.00           | 1                  | 1.00        | 0.625             |
| 1x3                | 1.00           | 1                  | 1.00        | 0.625             |
| 1x4                | 4.00           | 1                  | 4.00        | 2.5               |
| 2x3                | 9.00           | 1                  | 9.00        | 5.625 *           |
| 2x4                | 1.00           | 1                  | 1.00        | 0.625             |
| 3x4                | 16.00          | 1                  | 16.00       | 10.0 **           |
| <hr/>              |                |                    |             |                   |
| 1x2x3              | 1.00           | 1                  |             |                   |
| 1x2x4              | 4.00           | 1                  |             |                   |
| 1x3x4              | 1.00           | 1                  |             |                   |
| 2x3x4              | 1.00           | 1                  |             |                   |
| 1x2x3x4            | 1.00           | 1                  |             |                   |
|                    | <hr/>          | <hr/>              |             |                   |
|                    | 8.0            | 5                  | 1.6         |                   |

Total Sum of Squares = 754

Critical Values:

\*\*\*\*  $F_{1,5,0.999} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*  $F_{1,5,0.90} = 4.06$

$F_{1,5,0.75} = 1.69$

TABLE M-5. ANOVA Table of 2<sup>4</sup> Experiment No. 1 - Total Percent of Droplet Contamination Recovered as Vapor From Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|--------------------|----------------|--------------------|-------------|-------------------|
| 1 Liquid Viscosity | 39.0625        | 1                  | 39.0625     | 10.965 **         |
| 2 Wind Speed       | 248.0625       | 1                  | 248.0625    | 69.632 ****       |
| 3 Leaf Surface     | 7.5625         | 1                  | 7.5625      | 2.123             |
| 4 Leaf Type        | 10.5625        | 1                  | 10.5625     | 2.965             |
| 1x2                | 0.0625         | 1                  | 0.0625      | 0.018             |
| 1x3                | 22.5625        | 1                  | 22.5625     | 6.333 *           |
| 1x4                | 22.5625        | 1                  | 22.5625     | 6.333 *           |
| 2x3                | 0.0625         | 1                  | 0.0625      | 0.018             |
| 2x4                | 27.5625        | 1                  | 27.5625     | 7.737 **          |
| 3x4                | 5.0625         | 1                  | 5.0625      | 1.421             |
| <hr/>              |                |                    |             |                   |
| 1x2x3              | 0.0625         | 1                  |             |                   |
| 1x2x4              | 1.5625         | 1                  |             |                   |
| 1x3x4              | 5.0625         | 1                  |             |                   |
| 2x3x4              | 10.5625        | 1                  |             |                   |
| 1x2x3x4            | 0.5625         | 1                  |             |                   |
|                    | <hr/>          | <hr/>              |             |                   |
|                    | 17.8125        | 5                  | 3.5625      |                   |

Total Sum of Squares = 400.9375

Critical Values:

$$**** F_{1,5,0.999} = 47.18$$

$$*** F_{1,5,0.99} = 16.26$$

$$** F_{1,5,0.95} = 6.61$$

$$* F_{1,5,0.90} = 4.06$$

$$F_{1,5,0.75} = 1.69$$

TABLE M-6. ANOVA Table of  $2^4$  Experiment No. 2 - Total Percent of Droplet Contamination Recovered as Vapor From Oak Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|--------------------|----------------|--------------------|-------------|-------------------|
| 1 Liquid Viscosity | 156.25         | 1                  | 156.25      | 72.764 ****       |
| 2 Wind Speed       | 72.25          | 1                  | 72.25       | 33.604 ***        |
| 3 Leaf Surface     | 1.0            | 1                  | 1.0         | 0.465             |
| 4 Leaf Condition   | 121.0          | 1                  | 121.0       | 56.279 ****       |
| 1x2                | 6.25           | 1                  | 6.25        | 2.907             |
| 1x3                | 16.0           | 1                  | 16.0        | 7.442 **          |
| 1x4                | 121.0          | 1                  | 121.0       | 56.279 ****       |
| 2x3                | 1.0            | 1                  | 1.0         | 0.465             |
| 2x4                | 4.0            | 1                  | 4.0         | 1.860             |
| 3x4                | 0.25           | 1                  | 0.25        | 0.116             |
| <hr/>              |                |                    |             |                   |
| 1x2x3              | 1.0            | 1                  |             |                   |
| 1x2x4              | 1.0            | 1                  |             |                   |
| 1x3x4              | 2.25           | 1                  |             |                   |
| 2x3x4              | 6.25           | 1                  |             |                   |
| 1x2x3x4            | 0.25           | 1                  |             |                   |
|                    | 10.750         | 5                  | 2.15        |                   |

Total Sum of Squares = 509.75

Critical Values:

\*\*\*\*  $F_{1,5,0.999} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.51$

\*  $F_{1,5,0.90} = 4.0$

$F_{1,5,0.75} = 1.69$

TABLE M-7. ANOVA Table of  $2^4$  Experiment No. 1 - Life Time of Droplet Contamination on Leaf Surface.

| Source  |                  | Sum of Squares | Degrees of Freedom | Mean Square  | Mean Square Ratio |
|---------|------------------|----------------|--------------------|--------------|-------------------|
| 1       | Liquid Viscosity | 3,906.25       | 1                  | 3,906.25     | 0.30              |
| 2       | Wind Speed       | 1,265,625.00   | 1                  | 1,265,625.00 | 99.812 ***        |
| 3       | Leaf Surface     | 57,600.00      | 1                  | 57,600.00    | 4.543 *           |
| 4       | Leaf Type        | 14,400.00      | 1                  | 14,400.00    | 1.136             |
| 1x2     |                  | 3,306.25       | 1                  | 3,306.25     | 0.261             |
| 1x3     |                  | 15,006.25      | 1                  | 15,006.25    | 1.183             |
| 1x4     |                  | 1,056.25       | 1                  | 1,056.25     | 0.083             |
| 2x3     |                  | 2,500.00       | 1                  | 2,500.00     | 0.197             |
| 2x4     |                  | 19,600.00      | 1                  | 19,600.00    | 1.546             |
| 3x4     |                  | 34,225.00      | 1                  | 34,225.00    | 2.699             |
| <hr/>   |                  |                |                    |              |                   |
| 1x2x3   |                  | 7556.25        | 1                  |              |                   |
| 1x2x4   |                  | 756.25         | 1                  |              |                   |
| 1x3x4   |                  | 3306.25        | 1                  |              |                   |
| 2x3x4   |                  | 50,625.00      | 1                  |              |                   |
| 1x2x3x4 |                  | 1,056.25       | 1                  |              |                   |
|         |                  | <hr/>          |                    |              |                   |
|         |                  | 63,400.0       | 5                  | 12,680.0     |                   |

Total Sum of Squares = 1,480,625

Critical Values:

\*\*\*\*  $F_{1,5,0.999} = 47.16$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*  $F_{1,5,0.90} = 4.06$

$F_{1,5,0.75} = 1.69$



TABLE M-8. ANOVA Table of  $2^4$  Experiment No. 2 - Life Time of Droplet Contamination on Oak Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square  | Mean Square Ratio |
|--------------------|----------------|--------------------|--------------|-------------------|
| 1 Liquid Viscosity | 5,814.0625     | 1                  | 5,814.0625   | 0.707             |
| 2 Wind Speed       | 1,825,876.56   | 1                  | 1,825,876.56 | 221.949 ****      |
| 3 Leaf Surface     | 31,951.5625    | 1                  | 31,951.5625  | 3.884             |
| 4 Leaf Condition   | 68,251.5625    | 1                  | 68,251.5625  | 8.296 **          |
| 1x2                | 1,314.0625     | 1                  | 1,314.0625   | 0.160             |
| 1x3                | 13,514.0625    | 1                  | 13,514.0625  | 1.643             |
| 1x4                | 2,139.0625     | 1                  | 2,139.0625   | 0.260             |
| 2x3                | 12,939.0625    | 1                  | 12,939.0625  | 1.573             |
| 2x4                | 7,439.0625     | 1                  | 7,439.0625   | 0.904             |
| 3x4                | 60,639.0625    | 1                  | 60,639.0625  | 7.371 **          |
| 1x2x3              | 264.0625       | 1                  |              |                   |
| 1x2x4              | 39.0625        | 1                  |              |                   |
| 1x3x4              | 4064.0625      | 1                  |              |                   |
| 2x3x4              | 26,001.5625    | 1                  |              |                   |
| 1x2x3x4            | 10,764.0625    | 1                  |              |                   |
|                    | 41,132.8125    | 5                  | 8,256.5625   |                   |

Total Sum of Squares = 2,071,010.94

Critical Values:

\*\*\*\*  $F_{1,5,0.999} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*  $F_{1,5,0.90} = 4.06$

$F_{1,5,0.75} = 1.69$

TABLE M-9. ANOVA Table of 2<sup>4</sup> Experiment No. 1 - Average Evaporation Rate Over Life Time of Droplet Contamination on Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|--------------------|----------------|--------------------|-------------|-------------------|
| 1 Liquid Viscosity | 4.0            | 1                  | 4.0         | 10.0 **           |
| 2 Wind Speed       | 256.0          | 1                  | 256.0       | 640.0 ****        |
| 3 Leaf Surface     | 12.25          | 1                  | 12.25       | 30.625 ***        |
| 4 Leaf Type        | 0.0            | 1                  | 0.0         | 0.0               |
| 1x2                | 1.0            | 1                  | 1.0         | 0.4               |
| 1x3                | 0.25           | 1                  | 0.25        | 0.625             |
| 1x4                | 0.0            | 1                  | 0.0         | 0.0               |
| 2x3                | 6.25           | 1                  | 6.25        | 15.625 **         |
| 2x4                | 0.0            | 1                  | 0.0         | 0.0               |
| 3x4                | 0.25           | 1                  | 0.25        | 0.625             |
| 1x2x3              | 0.25           | 1                  |             |                   |
| 1x2x4              | 1.00           | 1                  |             |                   |
| 1x3x4              | 0.25           | 1                  |             |                   |
| 2x3x4              | 0.25           | 1                  |             |                   |
| 1x2x3x4            | 0.25           | 1                  |             |                   |
|                    | 2.0            | 5                  | 0.4         |                   |

Total Sum of Squares = 282

Critical Values:

\*\*\*\*  $F_{1,5,0.999} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*  $F_{1,5,0.90} = 4.06$

$F_{1,5,0.75} = 1.69$

TABLE M-10. ANOVA Table of  $2^4$  Experiment No. 2 - Average Evaporation Rate Over Life Time of Droplet Contamination on Oak Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|--------------------|----------------|--------------------|-------------|-------------------|
| 1 Liquid Viscosity | 5.0625         | 1                  | 5.0625      | 10.946 **         |
| 2 Wind Speed       | 232.5625       | 1                  | 232.5625    | 502.838 ****      |
| 3 Leaf Surface     | 5.0526         | 1                  | 5.0526      | 10.946 ***        |
| 4 Leaf Condition   | 3.0625         | 1                  | 3.0625      | 6.622 **          |
| 1x2                | 0.0625         | 1                  | 0.0625      | 0.135             |
| 1x3                | 0.5625         | 1                  | 0.5625      | 1.216             |
| 1x4                | 0.0625         | 1                  | 0.0625      | 0.135             |
| 2x3                | 1.5625         | 1                  | 1.5625      | 3.378             |
| 2x4                | 0.5625         | 1                  | 0.5625      | 1.216             |
| 3x4                | 3.0625         | 1                  | 3.0625      | 6.622 **          |
| 1x2x3              | 0.5625         | 1                  |             |                   |
| 1x2x4              | 0.0625         | 1                  |             |                   |
| 1x3x4              | 0.5625         | 1                  |             |                   |
| 2x3x4              | 0.5625         | 1                  |             |                   |
| 1x2x3x4            | 0.5625         | 1                  |             |                   |
|                    | 2.315          | 5                  | 0.4625      |                   |

Total Sum of Squares = 253.9375

Critical Values:

\*\*\*\*  $F_{1,5,0.999} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*  $F_{1,5,0.90} = 4.06$

$F_{1,5,0.75} = 1.69$

TABLE M-11. ANOVA Table of 2<sup>4</sup> Experiment No. 1 - Percent Of Droplet Contamination Recovered as Vapor After 1 Hr from Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|--------------------|----------------|--------------------|-------------|-------------------|
| 1 Liquid Viscosity | 36.0           | 1                  | 36.0        | 7.579 **          |
| 2 Wind Speed       | 841.0          | 1                  | 841.0       | 177.053 ****      |
| 3 Leaf Surface     | 210.25         | 1                  | 210.25      | 44.263 ***        |
| 4 Leaf Type        | 30.25          | 1                  | 30.25       | 6.368 *           |
| 1x2                | 6.25           | 1                  | 6.25        | 1.316             |
| 1x3                | 16.0           | 1                  | 16.0        | 3.368             |
| 1x4                | 1.0            | 1                  | 1.0         | 0.210             |
| 2x3                | 36.0           | 1                  | 36.0        | 7.579 **          |
| 2x4                | 9.0            | 1                  | 9.0         | 1.895             |
| 3x4                | 6.25           | 1                  | 6.25        | 1.316             |
| <hr/>              |                |                    |             |                   |
| 1x2x3              | 6.25           | 1                  |             |                   |
| 1x2x4              | 0.25           | 1                  |             |                   |
| 1x3x4              | 1.0            | 1                  |             |                   |
| 2x3x4              | 16.0           | 1                  |             |                   |
| 1x2x3x4            | 0.25           | 1                  |             |                   |
|                    | <hr/>          | <hr/>              |             |                   |
|                    | 23.75          | 5                  | 4.75        |                   |

Total Sum of Squares = 1215.75

Critical Values:

\*\*\*\*  $F_{1,5,0.999} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*  $F_{1,5,0.90} = 4.06$

$F_{1,5,0.75} = 1.69$

TABLE M-12. ANOVA Table of 2<sup>4</sup> Experiment No. 2 - Percent Of Droplet Contamination Recovered as Vapor After 1 Hr from Oak Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|--------------------|----------------|--------------------|-------------|-------------------|
| 1 Liquid Viscosity | 10.5625        | 1                  | 10.5625     | 4.122 *           |
| 2 Wind Speed       | 663.0625       | 1                  | 663.0625    | 258.756 ****      |
| 3 Leaf Surface     | 45.5625        | 1                  | 45.5625     | 17.780 ***        |
| 4 Leaf Condition   | 10.5625        | 1                  | 10.5625     | 4.122 *           |
| 1x2                | 5.0625         | 1                  | 5.0625      | 1.976             |
| 1x3                | 5.0625         | 1                  | 5.0625      | 1.976             |
| 1x4                | 14.0625        | 1                  | 14.0625     | 5.487 *           |
| 2x3                | 3.0625         | 1                  | 3.0625      | 1.195             |
| 2x4                | 0.0625         | 1                  | 0.0625      | 0.024             |
| 3x4                | 27.5625        | 1                  | 27.5625     | 10.756 **         |
| 1x2x3              | 1.5625         | 1                  |             |                   |
| 1x2x4              | 0.5625         | 1                  |             |                   |
| 1x3x4              | 7.5625         | 1                  |             |                   |
| 2x3x4              | 0.0625         | 1                  |             |                   |
| 1x2x3x4            | 3.0625         | 1                  |             |                   |
|                    | 12.8125        | 5                  | 2.5625      |                   |

Total Sum of Squares = 797.4375

Critical Values:

\*\*\*\*  $F_{1,5,0.999} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*  $F_{1,5,0.90} = 4.06$

$F_{1,5,0.75} = 1.69$

TABLE M-13. ANOVA Table of  $2^4$  Experiment No. 1 - Percent Of Droplet Contamination Recovered as Vapor After 2 Hr from Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|--------------------|----------------|--------------------|-------------|-------------------|
| 1 Liquid Viscosity | 64.0           | 1                  | 64.0        | 7.950 **          |
| 2 Wind Speed       | 2450.25        | 1                  | 2450.25     | 304.379 ****      |
| 3 Leaf Surface     | 506.25         | 1                  | 506.25      | 62.888 ****       |
| 4 Leaf Type        | 56.25          | 1                  | 56.25       | 6.988 **          |
| 1x2                | 9.0            | 1                  | 9.0         | 1.118             |
| 1x3                | 16.0           | 1                  | 16.0        | 1.988             |
| 1x4                | 9.0            | 1                  | 9.0         | 1.118             |
| 2x3                | 56.25          | 1                  | 56.25       | 6.988 **          |
| 2x4                | 5.25           | 1                  | 6.25        | 0.776             |
| 3x4                | 12.25          | 1                  | 12.25       | 1.522             |
| <hr/>              |                |                    |             |                   |
| 1x2x3              | 4.0            | 1                  |             |                   |
| 1x2x4              | 1.0            | 1                  |             |                   |
| 1x3x4              | 4.0            | 1                  |             |                   |
| 2x3x4              | 30.25          | 1                  |             |                   |
| 1x2x3x4            | 1.0            | 1                  |             |                   |
|                    | <hr/>          | <hr/>              |             |                   |
|                    | 40.25          | 5                  | 8.05        |                   |

Total Sum of Squares = 3225.75

Critical Values:

\*\*\*\*  $F_{1,5,0.999} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*  $F_{1,5,0.90} = 4.06$

$F_{1,5,0.75} = 1.69$

TABLE M-14. ANOVA Table of 2<sup>4</sup> Experiment No. 2 - Percent Of Droplet Contamination Recovered as Vapor After 2 Hr from Oak Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|--------------------|----------------|--------------------|-------------|-------------------|
| 1 Liquid Viscosity | 30.25          | 1                  | 30.25       | 8.288 **          |
| 2 Wind Speed       | 2116.0         | 1                  | 2116.0      | 579.726 ****      |
| 3 Leaf Surface     | 110.25         | 1                  | 110.25      | 30.205 ***        |
| 4 Leaf Condition   | 20.25          | 1                  | 20.25       | 5.548 *           |
| 1x2                | 9.0            | 1                  | 9.0         | 2.466             |
| 1x3                | 6.25           | 1                  | 6.25        | 1.712             |
| 1x4                | 30.25          | 1                  | 30.25       | 8.288 **          |
| 2x3                | 4.0            | 1                  | 4.0         | 1.096             |
| 2x4                | 1.0            | 1                  | 1.0         | 0.274             |
| 3x4                | 72.75          | 1                  | 72.75       | 19.794 ***        |
| 1x2x3              | 1.0            | 1                  |             |                   |
| 1x2x4              | 1.0            | 1                  |             |                   |
| 1x3x4              | 12.25          | 1                  |             |                   |
| 2x3x4              | 0.0            | 1                  |             |                   |
| 1x2x3x4            | 4.0            | 1                  |             |                   |
|                    | 18.25          | 5                  | 3.65        |                   |

Total Sum of Squares = 2417.755

Critical Values:

\*\*\*\*  $F_{1,5,0.999} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*  $F_{1,5,0.90} = 4.06$

$F_{1,5,0.75} = 1.69$

TABLE M-15. ANOVA Table of  $2^4$  Experiment No. 1 - Percent Of Droplet Contamination Recovered as Vapor After 3 Hr from Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|--------------------|----------------|--------------------|-------------|-------------------|
| 1 Liquid Viscosity | 72.25          | 1                  | 72.25       | 7.940 **          |
| 2 Wind Speed       | 3906.25        | 1                  | 3906.25     | 429.258 ****      |
| 3 Leaf Surface     | 625.0          | 1                  | 625.0       | 68.681 ****       |
| 4 Leaf Type        | 64.0           | 1                  | 64.0        | 7.032 **          |
| 1x2                | 1.0            | 1                  | 1.0         | 0.110             |
| 1x3                | 6.25           | 1                  | 6.25        | 0.687             |
| 1x4                | 20.25          | 1                  | 20.25       | 2.225             |
| 2x3                | 30.25          | 1                  | 30.25       | 3.324             |
| 2x4                | 0.25           | 1                  | 0.25        | 0.027             |
| 3x4                | 1.0            | 1                  | 1.0         | 0.110             |
| 1x2x3              | 1.0            | 1                  |             |                   |
| 1x2x4              | 4.0            | 1                  |             |                   |
| 1x3x4              | 6.25           | 1                  |             |                   |
| 2x3x4              | 30.25          | 1                  |             |                   |
| 1x2x3x4            | 4.0            | 1                  |             |                   |
|                    | 45.50          | 5                  | 9.1         |                   |

Total Sum of Squares = 4772.0

Critical Values:

\*\*\*\*  $F_{1,5,0.999} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*  $F_{1,5,0.90} = 4.06$

$F_{1,5,0.75} = 1.69$



TABLE M-16. ANOVA Table of  $2^4$  Experiment No. 2 - Percent Of Droplet Contamination Recovered as Vapor After 3 Hr from Oak Leaf Surface.

| Source  |                  | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|---------|------------------|----------------|--------------------|-------------|-------------------|
| 1       | Liquid Viscosity | 30.25          | 1                  | 30.25       | 7.857 **          |
| 2       | Wind Speed       | 3721.0         | 1                  | 3721.0      | 966.493 ****      |
| 3       | Leaf Surface     | 182.25         | 1                  | 182.25      | 47.338 ****       |
| 4       | Leaf Condition   | 12.25          | 1                  | 12.25       | 3.182             |
| 1x2     |                  | 4.0            | 1                  | 4.0         | 1.039             |
| 1x3     |                  | 2.25           | 1                  | 2.25        | 0.584             |
| 1x4     |                  | 56.25          | 1                  | 56.25       | 14.610 **         |
| 2x3     |                  | 1.0            | 1                  | 1.0         | 0.260             |
| 2x4     |                  | 1.0            | 1                  | 1.0         | 0.260             |
| 3x4     |                  | 110.25         | 1                  | 110.25      | 28.636 ***        |
| <hr/>   |                  |                |                    |             |                   |
| 1x2x3   |                  | 1.0            | 1                  |             |                   |
| 1x2x4   |                  | 1.0            | 1                  |             |                   |
| 1x3x4   |                  | 12.25          | 1                  |             |                   |
| 2x3x4   |                  | 1.0            | 1                  |             |                   |
| 1x2x3x4 |                  | 4.0            | 1                  |             |                   |
|         |                  | <hr/>          | <hr/>              |             |                   |
|         |                  | 19.25          | 5                  | 3.85        |                   |

Total Sum of Squares = 4129.755

Critical Values:

\*\*\*\*  $F_{1,5,0.999} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*\*  $F_{1,5,0.90} = 4.06$

\*  $F_{1,5,0.75} = 1.69$

TABLE M-17. ANOVA Table of 2<sup>4</sup> Experiment No. 1 - Percent Of Droplet Contamination Recovered as Vapor After 6 Hr from Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|--------------------|----------------|--------------------|-------------|-------------------|
| 1 Liquid Viscosity | 0.0625         | 1                  | 0.0625      | 0.062             |
| 2 Wind Speed       | 3751.5625      | 1                  | 3751.5625   | 639.925 ****      |
| 3 Leaf Surface     | 232.5625       | 1                  | 232.5625    | 39.670 ***        |
| 4 Leaf Type        | 10.5625        | 1                  | 10.5625     | 1.802             |
| 1x2                | 27.5625        | 1                  | 27.5625     | 4.701 *           |
| 1x3                | 5.0625         | 1                  | 5.0625      | 0.864             |
| 1x4                | 18.0625        | 1                  | 18.0625     | 3.081             |
| 2x3                | 45.5625        | 1                  | 45.5625     | 7.771 **          |
| 2x4                | 7.5625         | 1                  | 7.5625      | 1.290             |
| 3x4                | 7.5625         | 1                  | 7.5625      | 1.290             |
| <hr/>              |                |                    |             |                   |
| 1x2x3              | 10.5625        | 1                  |             |                   |
| 1x2x4              | 1.5625         | 1                  |             |                   |
| 1x3x4              | 5.0625         | 1                  |             |                   |
| 2x3x4              | 10.5625        | 1                  |             |                   |
| 1x2x3x4            | 1.5625         | 1                  |             |                   |
|                    | <hr/>          | <hr/>              |             |                   |
|                    | 29.3125        | 5                  | 5.8625      |                   |

Total Sum of Squares = 4135.4375

Critical Values:

\*\*\*\*  $F_{1,5,0.999} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*  $F_{1,5,0.90} = 4.06$

$F_{1,5,0.75} = 1.69$

TABLE M-18. ANOVA Table of 2<sup>4</sup> Experiment No. 2 - Percent Of Droplet Contamination Recovered as Vapor After 6 Hr from Oak Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|--------------------|----------------|--------------------|-------------|-------------------|
| 1 Liquid Viscosity | 14.0625        | 1                  | 14.0625     | 2.246             |
| 2 Wind Speed       | 4389.0625      | 1                  | 4389.0625   | 700.848 ****      |
| 3 Leaf Surface     | 105.0625       | 1                  | 105.0625    | 16.776 ***        |
| 4 Leaf Condition   | 5.0625         | 1                  | 5.0625      | 0.808             |
| 1x2                | 22.5625        | 1                  | 22.5625     | 3.603             |
| 1x3                | 0.0625         | 1                  | 0.0625      | 0.010             |
| 1x4                | 60.0625        | 1                  | 60.0625     | 9.591 **          |
| 2x3                | 22.5625        | 1                  | 22.5625     | 3.603             |
| 2x4                | 5.0625         | 1                  | 5.0625      | 0.808             |
| 3x4                | 60.0625        | 1                  | 60.0625     | 9.591 **          |
| <hr/>              |                |                    |             |                   |
| 1x2x3              | 3.0625         | 1                  |             |                   |
| 1x2x4              | 0.5625         | 1                  |             |                   |
| 1x3x4              | 0.0625         | 1                  |             |                   |
| 2x3x4              | 27.5625        | 1                  |             |                   |
| 1x2x3x4            | 0.0625         | 1                  |             |                   |
|                    | <hr/>          | <hr/>              |             |                   |
|                    | 31.3125        | 5                  | 6.2625      |                   |

Total Sum of Squares = 4714.9375

Critical Values:

\*\*\*\*  $F_{1,5,0.999} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*  $F_{1,5,0.90} = 4.06$

$F_{1,5,0.75} = 1.69$

TABLE M-19. ANOVA Table of 2<sup>4</sup> Experiment No. 1 - Average Evaporation Rate After 1 Hr For 2.2 mm (Dia.) Droplet Deposited on Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|--------------------|----------------|--------------------|-------------|-------------------|
| 1 Liquid Viscosity | 3.0625         | 1                  | 3.0625      | 0.860             |
| 2 Wind Speed       | 885.0625       | 1                  | 885.0625    | 248.439 ****      |
| 3 Leaf Surface     | 217.5625       | 1                  | 217.5625    | 61.070 ****       |
| 4 Leaf Type        | 39.0625        | 1                  | 39.0625     | 10.965 **         |
| 1x2                | 0.5625         | 1                  | 0.5625      | 0.158             |
| 1x3                | 3.0625         | 1                  | 3.0625      | 0.860             |
| 1x4                | 0.5625         | 1                  | 0.5625      | 0.158             |
| 2x3                | 22.5625        | 1                  | 22.5625     | 6.333 *           |
| 2x4                | 5.0525         | 1                  | 5.0525      | 1.421             |
| 3x4                | 10.5625        | 1                  | 10.5625     | 2.965             |
| 1x2x3              | 0.5625         | 1                  |             |                   |
| 1x2x4              | 3.0625         | 1                  |             |                   |
| 1x3x4              | 0.5625         | 1                  |             |                   |
| 2x3x4              | 10.5625        | 1                  |             |                   |
| 1x2x3x4            | 3.0625         | 1                  |             |                   |
|                    | 17.8125        | 5                  | 3.5625      |                   |

Total Sum of Squares = 1204.9375

Critical Values

\*\*\*\*  $F_{1,5,0.995} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*  $F_{1,5,0.90} = 4.06$

$F_{1,5,0.75} = 1.69$

TABLE M-20. ANOVA Table of  $2^4$  Experiment No. 2 - Average Evaporation Rate After 1 Hr For 2.2 mm (Dia.) Droplet Deposited on Oak Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|--------------------|----------------|--------------------|-------------|-------------------|
| 1 Liquid Viscosity | 0.0625         | 1                  | 0.0625      | 0.038             |
| 2 Wind Speed       | 715.5625       | 1                  | 715.5625    | 430.414 ****      |
| 3 Leaf Surface     | 52.5625        | 1                  | 52.5625     | 31.616 ***        |
| 4 Leaf Condition   | 1.5625         | 1                  | 1.5625      | 0.940             |
| 1x2                | 0.5625         | 1                  | 0.5625      | 0.338             |
| 1x3                | 1.5625         | 1                  | 1.5625      | 0.940             |
| 1x4                | 5.0625         | 1                  | 5.0625      | 3.045             |
| 2x3                | 3.0625         | 1                  | 3.0625      | 1.842             |
| 2x4                | 0.5625         | 1                  | 0.5625      | 0.338             |
| 3x4                | 18.0625        | 1                  | 18.0625     | 10.865 **         |
| 1x2x3              | 3.0625         | 1                  |             |                   |
| 1x2x4              | 3.0625         | 1                  |             |                   |
| 1x3x4              | 1.5625         | 1                  |             |                   |
| 2x3x4              | 0.0625         | 1                  |             |                   |
| 1x2x3x4            | 0.5625         | 1                  |             |                   |
|                    | 8.3125         | 5                  | 1.6625      |                   |

Total Sum of Squares = 806.9375

Critical Values:

\*\*\*  $F_{1,5,0.999} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*  $F_{1,5,0.90} = 4.06$

$F_{1,5,0.75} = 1.69$

TABLE M-21. ANOVA Table of 2<sup>4</sup> Experiment No. 1 - Average Evaporation Rate After 2 Hr For 2.2 mm (Dia.) Droplet Deposited on Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|--------------------|----------------|--------------------|-------------|-------------------|
| 1 Liquid Viscosity | 0.0625         | 1                  | 0.0625      | 0.035             |
| 2 Wind Speed       | 663.0625       | 1                  | 663.0625    | 376.206 ****      |
| 3 Leaf Surface     | 126.5625       | 1                  | 126.5625    | 71.805 ****       |
| 4 Leaf Type        | 22.5625        | 1                  | 22.5625     | 12.801 **         |
| 1x2                | 0.0625         | 1                  | 0.0625      | 0.035             |
| 1x3                | 0.5625         | 1                  | 0.5625      | 0.319             |
| 1x4                | 0.5625         | 1                  | 0.5625      | 0.319             |
| 2x3                | 7.5625         | 1                  | 7.5625      | 4.291 *           |
| 2x4                | 1.5625         | 1                  | 1.5625      | 0.886             |
| 3x4                | 3.0625         | 1                  | 3.0625      | 1.738             |
| 1x2x3              | 0.0625         | 1                  |             |                   |
| 1x2x4              | 5.0625         | 1                  |             |                   |
| 1x3x4              | 0.5625         | 1                  |             |                   |
| 2x3x4              | 1.5625         | 1                  |             |                   |
| 1x2x3x4            | 1.5625         | 1                  |             |                   |
|                    | 8.8125         | 5                  | 1.7625      |                   |

Total Sum of Squares = 834.4375

Critical Values:

\*\*\*\*  $F_{1,5,0.999} = 47.18$   
 \*\*\*  $F_{1,5,0.99} = 16.26$   
 \*\*  $F_{1,5,0.95} = 6.61$   
 \*  $F_{1,5,0.90} = 4.06$   
 $F_{1,5,0.75} = 1.69$

TABLE M-22. ANOVA Table of 2<sup>4</sup> Experiment No. 2 - Average Evaporation Rate After 2 Hr For 2.2 mm (Dia.) Droplet Deposited on Oak Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|--------------------|----------------|--------------------|-------------|-------------------|
| 1 Liquid Viscosity | 1.5625         | 1                  | 1.5625      | 1.623             |
| 2 Wind Speed       | 612.5625       | 1                  | 612.5625    | 636.429 ****      |
| 3 Leaf Surface     | 33.0625        | 1                  | 33.0625     | 34.351 ***        |
| 4 Leaf Condition   | 0.0625         | 1                  | 0.0625      | 0.065             |
| 1x2                | 0.5625         | 1                  | 0.5625      | 0.584             |
| 1x3                | 0.5625         | 1                  | 0.5625      | 0.584             |
| 1x4                | 3.0625         | 1                  | 3.0625      | 3.182             |
| 2x3                | 3.0625         | 1                  | 3.0625      | 3.182             |
| 2x4                | 0.0625         | 1                  | 0.0625      | 0.065             |
| 3x4                | 14.0625        | 1                  | 14.0625     | 14.610 **         |
| 1x2x3              | 0.5625         | 1                  |             |                   |
| 1x2x4              | 3.0625         | 1                  |             |                   |
| 1x3x4              | 0.5625         | 1                  |             |                   |
| 2x3x4              | 0.0625         | 1                  |             |                   |
| 1x2x3x4            | 0.5625         | 1                  |             |                   |
|                    | 4.8125         | 5                  | 0.9625      |                   |

Total Sum of Squares = 673.4375

Critical Values:

\*\*\*\*  $F_{1,5,0.999} = 47.18$   
 \*\*\*  $F_{1,5,0.99} = 16.26$   
 \*\*  $F_{1,5,0.95} = 6.61$   
 \*  $F_{1,5,0.90} = 4.96$   
 $F_{1,5,0.75} = 1.69$

TABLE M-23. ANOVA Table of  $2^4$  Experiment No. 1 - Average Evaporation Rate After 3 Hr For 2.2 mm (Dia.) Droplet Deposited on Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|--------------------|----------------|--------------------|-------------|-------------------|
| 1 Liquid Viscosity | 1.5625         | 1                  | 1.5625      | 0.940             |
| 2 Wind Speed       | 451.5625       | 1                  | 451.5625    | 271.616 ****      |
| 3 Leaf Surface     | 60.0625        | 1                  | 60.0625     | 36.128 ***        |
| 4 Leaf Type        | 14.0625        | 1                  | 14.0625     | 8.459 **          |
| 1x2                | 0.5625         | 1                  | 0.5625      | 0.338             |
| 1x3                | 0.0625         | 1                  | 0.0625      | 0.038             |
| 1x4                | 0.0625         | 1                  | 0.0625      | 0.038             |
| 2x3                | 1.5625         | 1                  | 1.5625      | 0.940             |
| 2x4                | 0.0625         | 1                  | 0.0625      | 0.038             |
| 3x4                | 0.5625         | 1                  | 0.5625      | 1.338             |
| 1x2x3              | 0.5625         | 1                  |             |                   |
| 1x2x4              | 3.0625         | 1                  |             |                   |
| 1x3x4              | 1.5625         | 1                  |             |                   |
| 2x3x4              | 0.0625         | 1                  |             |                   |
| 1x2x3x4            | 3.0625         | 1                  |             |                   |
|                    | 8.3125         | 5                  | 1.6625      |                   |

Total Sum of Squares = 538.4375

Critical Values:

\*\*\*\*  $F_{1,5,0.999} = 47.18$   
 \*\*\*  $F_{1,5,0.99} = 16.26$   
 \*\*  $F_{1,5,0.95} = 6.61$   
 \*  $F_{1,5,0.90} = 4.06$   
 $F_{1,5,0.75} = 1.59$



TABLE M-24. ANOVA Table of 2<sup>4</sup> Experiment No. 2 - Average Evaporation Rate After 3 Hr For 2.2 mm (Dia.) Droplet Deposited on Oak Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|--------------------|----------------|--------------------|-------------|-------------------|
| 1 Liquid Viscosity | 4.0            | 1                  | 4.0         | 10.0 **           |
| 2 Wind Speed       | 441.0          | 1                  | 441.0       | 1102.5 ****       |
| 3 Leaf Surface     | 20.25          | 1                  | 20.25       | 50.625 ****       |
| 4 Leaf Condition   | 1.0            | 1                  | 1.0         | 2.5               |
| 1x2                | 0.0            | 1                  | 0.0         | 0.0               |
| 1x3                | 0.25           | 1                  | 0.25        | 0.625             |
| 1x4                | 1.0            | 1                  | 1.0         | 2.5               |
| 2x3                | 2.25           | 1                  | 2.25        | 5.625 *           |
| 2x4                | 0.0            | 1                  | 0.0         | 0.0               |
| 3x4                | 6.25           | 1                  | 6.25        | 15.625 **         |
| 1x2x3              | 0.25           | 1                  |             |                   |
| 1x2x4              | 1.0            | 1                  |             |                   |
| 1x3x4              | 0.25           | 1                  |             |                   |
| 2x3x4              | 0.25           | 1                  |             |                   |
| 1x2x3x4            | 0.25           | 1                  |             |                   |
|                    | 2.0            | 5                  | 0.40        |                   |

Total Sum of Squares = 478.0

Critical Values:

\*\*\*\*  $F_{1,5,0.999} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*  $F_{1,5,0.90} = 4.06$

$F_{1,5,0.75} = 1.69$

TABLE M-25. ANOVA Table of 2<sup>4</sup> Experiment No. 1 - Average Evaporation Rate  
After 6 Hr For 2.2 mm (Dia.) Droplet Deposited on Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|--------------------|----------------|--------------------|-------------|-------------------|
| 1 Liquid Viscosity | 9.0            | 1                  | 9.0         | 13.846 **         |
| 2 Wind Speed       | 110.25         | 1                  | 110.25      | 169.615 ****      |
| 3 Leaf Surface     | 12.25          | 1                  | 12.25       | 18.846 ***        |
| 4 Leaf Type        | 2.25           | 1                  | 2.25        | 3.462             |
| 1x2                | 1.0            | 1                  | 1.0         | 1.538             |
| 1x3                | 1.0            | 1                  | 1.0         | 1.538             |
| 1x4                | 0.0            | 1                  | 0.0         | 0.000             |
| 2x3                | 2.25           | 1                  | 2.25        | 3.462             |
| 2x4                | 0.25           | 1                  | 0.25        | 0.385             |
| 3x4                | 0.25           | 1                  | 0.25        | 0.385             |
| <hr/>              |                |                    |             |                   |
| 1x2x3              | 1.0            | 1                  |             |                   |
| 1x2x4              | 1.0            | 1                  |             |                   |
| 1x3x4              | 0.0            | 1                  |             |                   |
| 2x3x4              | 0.25           | 1                  |             |                   |
| 1x2x3x4            | 1.0            | 1                  |             |                   |
|                    | <hr/>          | <hr/>              |             |                   |
|                    | 3.25           | 5                  | 0.65        |                   |

Total Sum of Squares = 141.75

Critical Values:

\*\*\*\*  $F_{1,5,0.999} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*  $F_{1,5,0.90} = 4.06$

$F_{1,5,0.75} = 1.69$

TABLE M-26. ANOVA Table of  $2^4$  Experiment No. 2 - Average Evaporation Rate After 6 Hr For 2.2 mm (Dia.) Droplet Deposited on Oak Leaf Surface.

| Source  |                  | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|---------|------------------|----------------|--------------------|-------------|-------------------|
| 1       | Liquid Viscosity | 12.25          | 1                  | 12.25       | 27.222 ***        |
| 2       | Wind Speed       | 144.0          | 1                  | 144.0       | 320.0 *****       |
| 3       | Leaf Surface     | 6.25           | 1                  | 6.25        | 13.895 **         |
| 4       | Leaf Condition   | 6.25           | 1                  | 6.25        | 13.889 **         |
| 1x2     |                  | 1.0            | 1                  | 1.0         | 2.222             |
| 1x3     |                  | 0.25           | 1                  | 0.25        | 0.556             |
| 1x4     |                  | 0.25           | 1                  | 0.25        | 0.556             |
| 2x3     |                  | 0.0            | 1                  | 0.0         | 0.0               |
| 2x4     |                  | 1.0            | 1                  | 1.0         | 2.222             |
| 3x4     |                  | 2.25           | 1                  | 2.25        | 5.0 *             |
| <hr/>   |                  |                |                    |             |                   |
| 1x2x3   |                  | 0.0            | 1                  |             |                   |
| 1x2x4   |                  | 1.0            | 1                  |             |                   |
| 1x3x4   |                  | 0.25           | 1                  |             |                   |
| 2x3x4   |                  | 1.0            | 1                  |             |                   |
| 1x2x3x4 |                  | 0.0            | 1                  |             |                   |
|         |                  | <hr/>          | <hr/>              |             |                   |
|         |                  | 2.25           | 5                  | 0.45        |                   |

Total Sum of Squares = 175.75

Critical Values:

\*\*\*\*\*  $F_{1,5,0.999}$  = 47.18

\*\*\*  $F_{1,5,0.99}$  = 16.26

\*\*  $F_{1,5,0.95}$  = 6.61

\*  $F_{1,5,0.90}$  = 4.06

$F_{1,5,0.75}$  = 1.69

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APPENDIX N

FACTORIAL ANALYSIS AND HALF NORMAL PROBABILITY PLOTS  
OF DROPLET SPREAD FACTOR RESULTS

TABLE N-1. THE DESIGN MATRIX FOR THE FACTORIAL EXPERIMENT  
AVERAGE SPREAD FACTOR OF DROPLET (2 MM DIA) DEPOSITED  
ON LEAF SURFACE AT 60 DEG F AND 42% RH

| TEST | VARIABLES |   |   |   | CONTRAST CONFOUNDING |
|------|-----------|---|---|---|----------------------|
|      | 1         | 2 | 3 | 4 |                      |
| 1    | -         |   | - | - | MEAN                 |
| 2    | +         | - | - | - | 1                    |
| 3    | -         | + | - | - | 2                    |
| 4    | +         | + | - | - | 12                   |
| 5    | -         | - | + | - | 3                    |
| 6    | +         | - |   | - | 13                   |
| 7    | -         | + |   | - | 23                   |
| 8    | +         | + | + | - | 123                  |
| 9    | -         | - | - | + | 4                    |
| 10   | +         | - | - | + | 14                   |
| 11   | -         | + | - |   | 24                   |
| 12   | +         | + | - | + | 124                  |
| 13   | -         | - | + | + | 34                   |
| 14   | +         | - | + | + | 134                  |
| 15   | -         | + | + | + | 234                  |
| 16   | +         | + | + | + | 1234                 |

#### VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)CAK     | (-)HICKORY |

TABLE N-2. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
AVERAGE SPREAD FACTOR OF DROPLET (2 MM DIA) DEPOSITED  
ON LEAF SURFACE AT 60 DEG F AND 42% RH

| TEST | CONTRAST | YIELD * | AVG EFFECTS | SUM OF SQUARES |
|------|----------|---------|-------------|----------------|
| 1    | MEAN     | 247     | 222.6       | -              |
| 2    | 1        | 267     | -8          | 256            |
| 3    | 2        | 272     | -4.7        | 90.25          |
| 4    | 12       | 280     | 2           | 16             |
| 5    | 3        | 189     | -68.5       | 18769          |
| 6    | 13       | 191     | .8          | 2.25           |
| 7    | 23       | 191     | 3           | 36             |
| 8    | 123      | 185     | -4.7        | 90.25          |
| 9    | 4        | 290     | -10.2       | 420.25         |
| 10   | 14       | 239     | -14         | 784            |
| 11   | 24       | 236     | -13.2       | 702.25         |
| 12   | 124      | 224     | 7           | 196            |
| 13   | 34       | 194     | 9           | 324            |
| 14   | 134      | 183     | 8.8         | 306.25         |
| 15   | 234      | 194     | 13.5        | 729            |
| 16   | 1234     | 180     | -5.7        | 132.25         |

TOTAL = 22853.75

VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

\* SPREAD FACTOR X 100

TABLE N-3. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
AVERAGE SPREAD FACTOR OF DROPLET (2 MM DIA) DEPOSITED  
ON LEAF SURFACE AT 60 DEG ° AND 42% RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HALF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 3        | 68.5          | 96.67 | 6.72    | 98.33       |
| 14   | 14       | 14            | 90    | 1.37    | 95          |
| 13   | 234      | 13.5          | 83.33 | 1.32    | 91.67       |
| 12   | 24       | 13.2          | 76.67 | 1.29    | 88.33       |
| 11   | 4        | 10.2          | 70    | 1       | 85          |
| 10   | 34       | 9             | 63.33 | .88     | 81.67       |
| 9    | 134      | 8.8           | 56.67 | .86     | 78.33       |
| 8    | 1        | 8             | 50    | .78     | 75          |
| 7    | 124      | 7             | 43.33 | .69     | 71.67       |
| 6    | 1234     | 5.7           | 36.67 | .56     | 68.33       |
| 5    | 123      | 4.7           | 30    | .46     | 65          |
| 4    | 2        | 4.7           | 23.33 | .46     | 61.67       |
| 3    | 23       | 3             | 16.67 | .2      | 58.33       |
| 2    | 12       | 2             | 10    | .2      | 55          |
| 1    | 13       | .8            | 3.33  | .08     | 51.67       |

PROB =  $((R(I) - .5) / R(\text{MAX})) * 100\%$  WHERE R(I) IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

HALF NORMAL =  $(\text{PROB} + 100\%) / 2$

#### VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |



# VARIABLE #'S AND IDENTITIES

|                     |            |            |
|---------------------|------------|------------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP  |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH   |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP     |
| 4: LEAF TYPE        | (+)OAK     | (-)HICKORY |

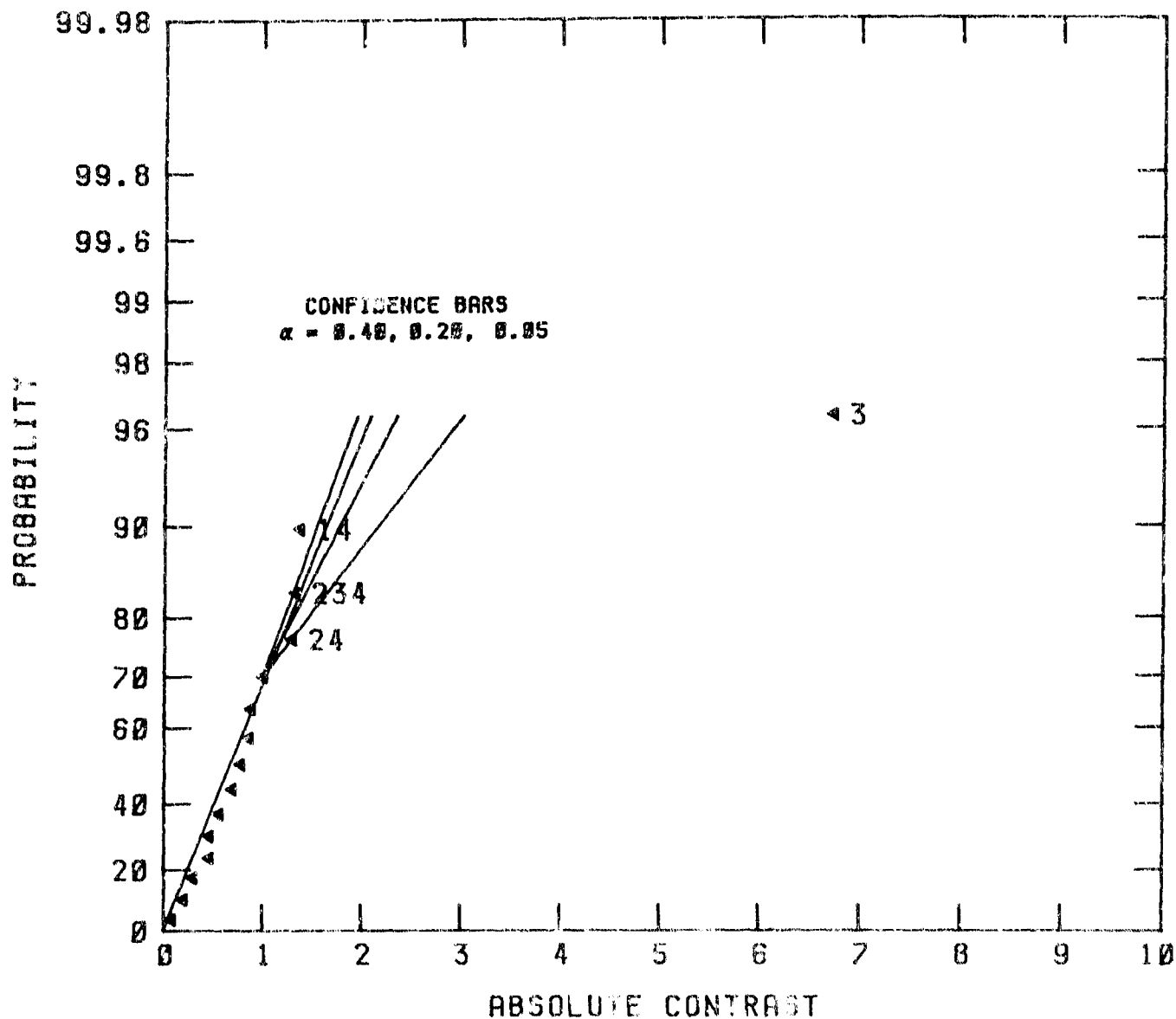


FIGURE N-1. HALF NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
 SPREAD FACTOR OF 2 MM DIAMETER DROPS DEPOSITED ON  
 LEAF SURFACE AT 80 DEG F AND 42% RH

TABLE N-4. THE DESIGN MATRIX FOR THE FACTORIAL EXPERIMENT  
AVERAGE SPREAD FACTOR OF DROPLET (2 MM DIA) DEPOSITED  
ON OAK LEAF SURFACE AT 60 DEG F AND 42% RH

| TEST | VARIABLES |   |   |   | CONTRAST CONFOUNDING |
|------|-----------|---|---|---|----------------------|
|      | 1         | 2 | 3 | 4 |                      |
| 1    | -         | - | - | - | MEAN                 |
| 2    | +         | - | - | - | 1                    |
| 3    | -         | + | - | - | 2                    |
| 4    | +         | + | - | - | 12                   |
| 5    | -         | - | + | - | 3                    |
| 6    | +         | - | + | - | 13                   |
| 7    | -         | + | + | - | 23                   |
| 8    | +         | + | + | - | 123                  |
| 9    | -         | - | - | + | 4                    |
| 10   | +         | - | - | + | 14                   |
| 11   | -         | + | - | + | 24                   |
| 12   | +         | + | - | + | 124                  |
| 13   | -         | - | + | + | 34                   |
| 14   | +         | - | + | + | 134                  |
| 15   | -         | + | + | + | 234                  |
| 16   | +         | + | + | + | 1234                 |

VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)10 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDLITION  | (+)GREEN   | (-)RED    |

TABLE 4-5. ESTIMATES OF AVERAGE EFFECTS AND SUM OF SQUARES  
AVERAGE SPREAD FACTOR OF DROPLET (2 MM DIA) DEPOSITED  
ON OAK LEAF SURFACE AT 60 DEG F AND 42% RH

| TEST | CONTRAST | YIELD * | AVG EFFECTS | SUM OF SQUARES |
|------|----------|---------|-------------|----------------|
| 1    | MEAN     | 197     | 202.4       | -              |
| 2    | 1        | 199     | -10.5       | 441            |
| 3    | 2        | 186     | -9          | 324            |
| 4    | 12       | 199     | 4.8         | 90.25          |
| 5    | 3        | 177     | -37.7       | 5700.25        |
| 6    | 13       | 176     | 1.5         | 9              |
| 7    | 23       | 187     | 11          | 484            |
| 8    | 123      | 177     | -7.7        | 240.25         |
| 9    | 4        | 290     | 30.3        | 3660.25        |
| 10   | 14       | 239     | -11.5       | 529            |
| 11   | 24       | 236     | -9          | 324            |
| 12   | 124      | 224     | 4.3         | 72.25          |
| 13   | 34       | 154     | -21.7       | 1892.25        |
| 14   | 134      | 183     | 3           | 256            |
| 15   | 234      | 194     | 5.5         | 121            |
| 16   | 1234     | 180     | -2.7        | 30.25          |

TOTAL = 14173.75

#### VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

\* SPREAD FACTOR X 100

TABLE N-6. RANKED STANDARDIZED MAGNITUDE OF EFFECTS  
AVERAGE SPREAD FACTOR OF DROPLET (2 MM DIA) DEPOSITED  
ON OAK LEAF SURFACE AT 50 DEG F AND 423 RH

| RANK | CONTRAST | MAG OF EFFECT | PROB  | STD MAG | HAIF NORMAL |
|------|----------|---------------|-------|---------|-------------|
| 15   | 3        | 37.7          | 96.67 | 3.43    | 98.33       |
| 14   | 4        | 30.3          | 90    | 2.75    | 95          |
| 13   | 34       | 21.7          | 83.33 | 1.97    | 91.67       |
| 12   | 14       | 11.5          | 76.67 | 1.05    | 88.33       |
| 11   | 23       | 11            | 70    | 1       | 85          |
| 10   | 1        | 10.5          | 63.33 | .95     | 81.67       |
| 9    | 24       | 9             | 56.67 | .82     | 78.33       |
| 8    | 2        | 9             | 50    | .82     | 75          |
| 7    | 134      | 8             | 43.33 | .73     | 71.67       |
| 6    | 123      | 7.7           | 36.67 | .7      | 68.33       |
| 5    | 234      | 5.5           | 30    | .5      | 65          |
| 4    | 12       | 4.8           | 23.33 | .44     | 61.67       |
| 3    | 124      | 4.3           | 16.67 | .39     | 58.33       |
| 2    | 1234     | 2.7           | 10    | .25     | 55          |
| 1    | 13       | 1.5           | 3.33  | .14     | 51.67       |

$PROB = ((R(I) - .5) / R(MAX)) * 100\%$  WHERE  $R(I)$  IS THE RANK.

STANDARDIZED MAGNITUDE = ABSOLUTE VALUE / U WHERE U IS DEFINED AS  
THE MAGNITUDE OF THE CONTRAST NEAREST 68.3 PERCENTILE.

$HAIF\ NORMAL = (PROB + 100\%) / 2$

#### VARIABLE #'S AND IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)3 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

# VARIABLES & IDENTITIES

|                     |            |           |
|---------------------|------------|-----------|
| 1: LIQUID VISCOSITY | (+)1000 CP | (-)100 CP |
| 2: WIND SPEED       | (+)11 MPH  | (-)5 MPH  |
| 3: LEAF SURFACE     | (+)BOTTOM  | (-)TOP    |
| 4: LEAF CONDITION   | (+)GREEN   | (-)RED    |

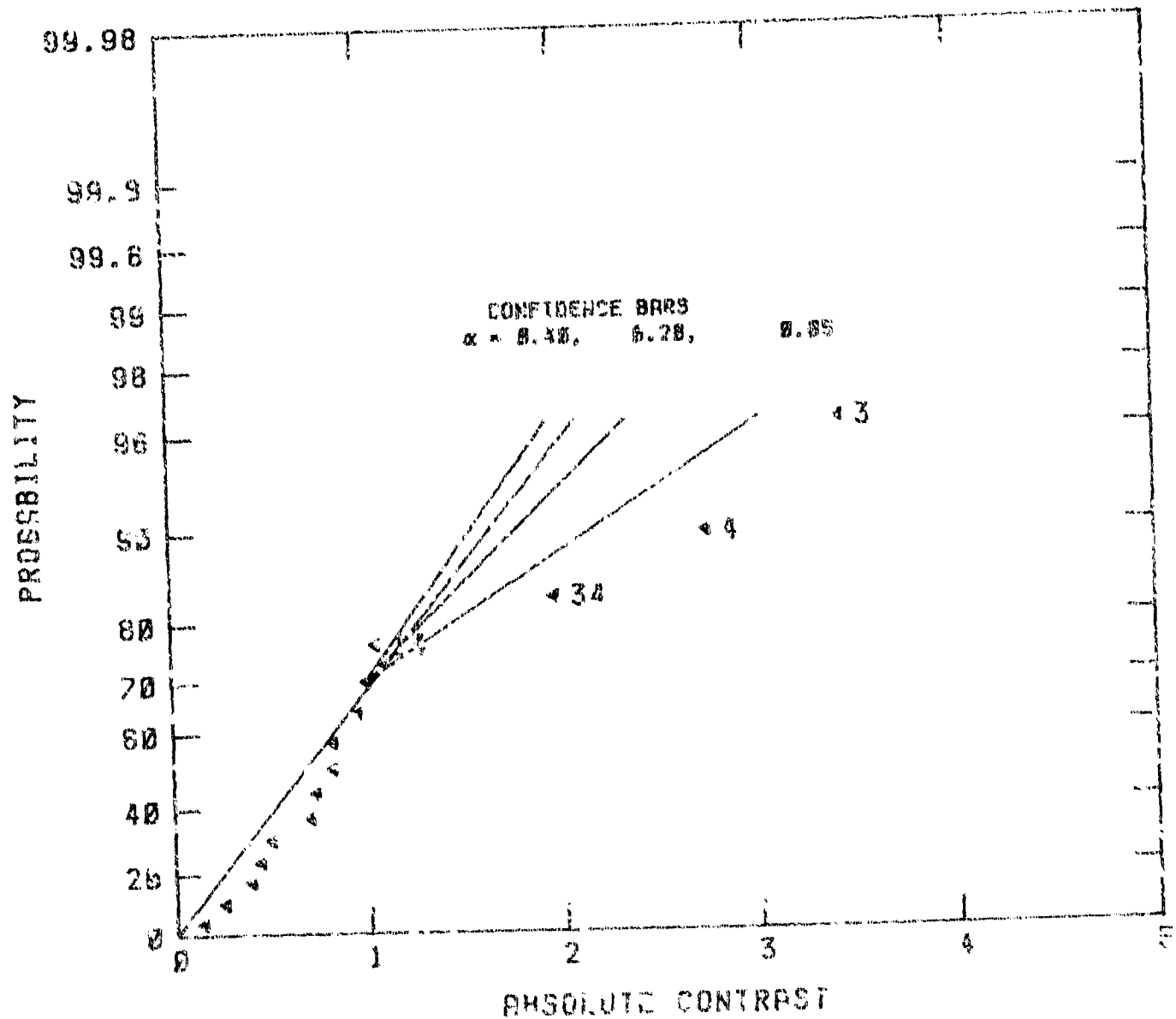


FIGURE N-7. HALF-NORMAL PROBABILITY PLOT OF FACTORIAL EXPERIMENT  
 SPREAD FACTOR OF 2 MM DIAMETER DROPS DEPOSITED ON  
 ONE LEAF SURFACE AT 65 DEG F AND 42X EN

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APPENDIX O

ANOVA TABLES OF  $2^4$  FACTORIAL EXPERIMENTS  
ON DROPLET SPREAD FACTOR RESULTS

TABLE 0-1. ANOVA Table of  $2^4$  Experiment No. 1 - Average Spread Factor of Droplet (2 mm Dia.) Deposited on Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|--------------------|----------------|--------------------|-------------|-------------------|
| 1 Liquid Viscosity | 256.0          | 1                  | 256.0       | 0.880             |
| 2 Wind Speed       | 90.25          | 1                  | 90.25       | 0.310             |
| 3 Leaf Surface     | 18,769.0       | 1                  | 18,769.0    | 64.554 ****       |
| 4 Leaf Type        | 420.25         | 1                  | 420.25      | 1.445             |
| 1x2                | 16.0           | 1                  | 16.0        | 0.055             |
| 1x3                | 2.25           | 1                  | 2.25        | 0.008             |
| 1x4                | 784.0          | 1                  | 784.0       | 2.696             |
| 2x3                | 36.0           | 1                  | 36.0        | 0.124             |
| 2x4                | 702.25         | 1                  | 702.25      | 2.415             |
| 3x4                | 324.0          | 1                  | 324.0       | 1.114             |
| 1x2x3              | 90.25          | 1                  |             |                   |
| 1x2x4              | 196.0          | 1                  |             |                   |
| 1x3x4              | 306.25         | 1                  |             |                   |
| 2x3x4              | 729.0          | 1                  |             |                   |
| 1x2x3x4            | 132.25         | 1                  |             |                   |
|                    | 1,453.75       | 5                  | 290.75      |                   |

Total Sum of Squares = 22853.75

Critical Values:

\*\*\*\*  $F_{1,5,0.999} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*  $F_{1,5,0.90} = 4.06$

$F_{1,5,0.75} = 1.69$



TABLE O-2. ANOVA Table of 2<sup>4</sup> Experiment No. 2 - Average Spread Factor of Droplet (2 mm Dia.) Deposited on Oak Leaf Surface.

| Source             | Sum of Squares | Degrees of Freedom | Mean Square | Mean Square Ratio |
|--------------------|----------------|--------------------|-------------|-------------------|
| 1 Liquid Viscosity | 441.0          | 1                  | 441.0       | 1.517             |
| 2 Wind Speed       | 324.0          | 1                  | 324.0       | 1.114             |
| 3 Leaf Surface     | 5,700.25       | 1                  | 5,700.25    | 19.605 ***        |
| 4 Leaf Condition   | 3,660.25       | 1                  | 3,660.25    | 12.590 **         |
| 1x2                | 90.25          | 1                  | 90.25       | 0.310             |
| 1x3                | 9.0            | 1                  | 9.0         | 0.031             |
| 1x4                | 529.0          | 1                  | 529.0       | 1.819             |
| 2x3                | 484.0          | 1                  | 484.0       | 1.665             |
| 2x4                | 324.25         | 1                  | 324.25      | 1.114             |
| 3x4                | 1892.25        | 1                  | 1892.25     | 6.508 *           |
| <hr/>              |                |                    |             |                   |
| 1x2x3              | 240.25         | 1                  |             |                   |
| 1x2x4              | 72.25          | 1                  |             |                   |
| 1x3x4              | 256.0          | 1                  |             |                   |
| 2x3x4              | 121.0          | 1                  |             |                   |
| 1x2x3x4            | 30.25          | 1                  |             |                   |
|                    | <hr/>          |                    |             |                   |
|                    | 719.75         | 5                  | 143.95      |                   |

Total Sum of Squares = 14173.75

Critical Values:

\*\*\*\*  $F_{1,5,0.999} = 47.18$

\*\*\*  $F_{1,5,0.99} = 16.26$

\*\*  $F_{1,5,0.95} = 6.61$

\*  $F_{1,5,0.90} = 4.06$

$F_{1,5,0.75} = 1.69$

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APPENDIX P

REGRESSION MODELS FOR PREDICTING HALF-LIFE  
OF DROPLETS DEPOSITED ON LEAF FOLIAGE

Table P-1. Model 1 Fit of Half-Life of DEM Droplet Deposited on Leaf Surface

| SOURCE   | DF | SS         | MS        |
|----------|----|------------|-----------|
| REGRESS. | 2  | 148937.625 | 74468.812 |
| RESIDUAL | 13 | 9149.812   | 703.832   |
| TOTAL    | 15 | 158087.437 |           |

F(2,13) = 105.805 P = <.001

MULTIPLE CORRELATION = .9706

R-SQUARED = .9421 ( .9332)

STANDARD ERROR = 26.530

| VARIABLE | COEFFICIENT | T       | S.E.   | P     | SR    |
|----------|-------------|---------|--------|-------|-------|
| B        | -89.4375    | -13.485 | 6.6325 | <.001 | .8096 |
| C        | 36.1875     | 5.456   | 6.6325 | <.001 | .1325 |
| CONSTANT | 218.6875    |         |        |       |       |

| CASE # | ACTUAL  | PREDICTED | RESIDUAL |
|--------|---------|-----------|----------|
| 1      | 246.000 | 271.938   | -25.938  |
| 2      | 264.000 | 271.938   | -7.938   |
| 3      | 84.000  | 93.063    | -9.063   |
| 4      | 98.000  | 93.063    | 4.937    |
| 5      | 320.000 | 344.313   | -24.313  |
| 6      | 332.000 | 344.313   | -12.313  |
| 7      | 148.000 | 165.438   | -17.438  |
| 8      | 156.000 | 165.438   | -9.438   |
| 9      | 245.000 | 271.938   | -26.938  |
| 10     | 287.000 | 271.938   | 15.063   |
| 11     | 100.000 | 93.063    | 6.937    |
| 12     | 136.000 | 93.063    | 42.937   |
| 13     | 367.000 | 344.313   | 22.688   |
| 14     | 404.000 | 344.313   | 59.688   |
| 15     | 150.000 | 165.438   | -15.438  |
| 16     | 162.000 | 165.438   | -3.438   |

RESIDUALS SUM = -4.76837158E-07

SERIAL CORRELATION, RESIDUALS = .2738

DURBIN-WATSON STATISTIC = 1.3782

Table P-2. Model 1B Fit of Half-Life of DEM Droplet Deposited on Leaf Surface.

| SOURCE   | DF | SS         | MS        |
|----------|----|------------|-----------|
| REGRESS. | 5  | 155608.812 | 31121.762 |
| RESIDUAL | 10 | 2478.624   | 247.862   |
| TOTAL    | 15 | 158087.437 |           |

$F(5,10) = 125.561$   $P = <.001$

MULTIPLE CORRELATION = .9921

R-SQUARED = .9843 ( .9765)

STANDARD ERROR = 15.744

| VARIABLE | COEFFICIENT | T       | S.E.   | P     | SR    |
|----------|-------------|---------|--------|-------|-------|
| B        | -89.4375    | -22.723 | 3.9359 | <.001 | .8096 |
| C        | 36.1875     | 9.194   | 3.9359 | <.001 | .1325 |
| A        | 11.1875     | 2.842   | 3.9359 | .0169 | .0127 |
| D        | 12.6875     | 3.224   | 3.9359 | .009  | .0163 |
| BC       | -11.4375    | -2.906  | 3.9359 | .0152 | .0132 |
| CONSTANT | 218.6875    |         |        |       |       |

| CASE # | ACTUAL  | PREDICTED | RESIDUAL |
|--------|---------|-----------|----------|
| 1      | 246.000 | 236.625   | 9.375    |
| 2      | 264.000 | 259.000   | 5.000    |
| 3      | 84.000  | 80.625    | 3.375    |
| 4      | 98.000  | 103.000   | -5.000   |
| 5      | 320.000 | 321.875   | -11.875  |
| 6      | 332.000 | 354.250   | -22.250  |
| 7      | 148.000 | 130.125   | 17.875   |
| 8      | 156.000 | 152.500   | 3.500    |
| 9      | 245.000 | 262.000   | -17.000  |
| 10     | 287.000 | 284.375   | 2.625    |
| 11     | 100.000 | 106.000   | -6.000   |
| 12     | 136.000 | 128.375   | 7.625    |
| 13     | 367.000 | 357.250   | 9.750    |
| 14     | 404.000 | 379.625   | 24.375   |
| 15     | 150.000 | 155.500   | -5.500   |
| 16     | 162.000 | 177.875   | -15.875  |

RESIDUALS SUM = -4.76837158E-07

SERIAL CORRELATION, RESIDUALS = .0606

DURBIN-WATSON STATISTIC = 1.7540

Table P-3. Model 2 Fit of Half-Life of DEM Droplet Deposited on Leaf Surface.

| SOURCE   | DF | SS         | MS        |
|----------|----|------------|-----------|
| REGRESS. | 3  | 151386.187 | 50462.062 |
| RESIDUAL | 12 | 6373.749   | 531.146   |
| TOTAL    | 15 | 157759.937 |           |

$F(3,12) = 95.006$   $P = <.001$

MULTIPLE CORRELATION = .9796

R-SQUARED = .9596 ( .9495)

STANDARD ERROR = 23.047

| VARIABLE | COEFFICIENT | T       | S.E.   | P     | SR    |
|----------|-------------|---------|--------|-------|-------|
| B        | -93.1875    | -16.174 | 5.7617 | <.001 | .8807 |
| C        | 20.8125     | 3.512   | 5.7617 | .003  | .0439 |
| CD       | 18.5625     | 3.222   | 5.7617 | .007  | .0349 |
| CONSTANT | 233.4375    |         |        |       |       |

| CASE # | ACTUAL  | PREDICTED | RESIDUAL |
|--------|---------|-----------|----------|
| 1      | 339.000 | 324.375   | 14.625   |
| 2      | 315.000 | 324.375   | -9.375   |
| 3      | 142.000 | 138.000   | 4.000    |
| 4      | 137.000 | 138.000   | -1.000   |
| 5      | 341.000 | 328.875   | 12.125   |
| 6      | 315.000 | 328.875   | -13.875  |
| 7      | 145.000 | 142.500   | 2.500    |
| 8      | 150.000 | 142.500   | 7.500    |
| 9      | 245.000 | 287.250   | -42.250  |
| 10     | 287.000 | 287.250   | -.250    |
| 11     | 100.000 | 100.875   | -.875    |
| 12     | 136.000 | 100.875   | 35.125   |
| 13     | 367.000 | 366.000   | 1.000    |
| 14     | 404.000 | 366.000   | 38.000   |
| 15     | 150.000 | 179.625   | -29.625  |
| 16     | 162.000 | 179.625   | -17.625  |

RESIDUALS SUM = -3.57627869E-07

SERIAL CORRELATION, RESIDUALS = -.2049

DURBIN-WATSON STATISTIC = 2.3075

Table P-4. Comparison of Predictions of Three Regression Models.

| Expected Droplet<br>Half-life<br>(min) | Predicted Droplet Half-Life |           |           |
|--|-----------------------------|-----------|-----------|
|  | Model 1                     | Model 2   | Model 3   |
| 60                                     | 69 (+9)                     | 62 (+2)   | 67 (+7)   |
| 120                                    | 126 (+6)                    | 122 (+2)  | 125 (+5)  |
| 180                                    | 182 (+2)                    | 181 (+1)  | 182 (+2)  |
| 240                                    | 239 (-1)                    | 240 ( 0 ) | 240 ( 0 ) |
| 300                                    | 295 (-5)                    | 299 (-1)  | 297 (-3)  |
| 360                                    | 352 (-8)                    | 358 (-2)  | 355 (-5)  |
| 420                                    | 408 (-12)                   | 417 (-3)  | 412 (-8)  |
| 480                                    | 465 (-15)                   | 476 (-4)  | 470 (-10) |

Model 1:  $t_{\frac{1}{2}} = 218.6875 - 89.4375B + 36.1875C$

Model 1b:  $t_{\frac{1}{2}} = 218.6875 - 89.4375B + 36.1875C + 11.1875A + 12.4375D - 11.4375BC$

Model 2:  $t_{\frac{1}{2}} = 233.4375 - 93.1875B + 20.8125C + 18.5625CE$

Parameters:

- A: Liquid Viscosity ( 100 cp = -1 & 1000 cp = +1)
- B: Wind Speed ( 3 mph = -1 & 11 mph = +1)
- C: Leaf Surface (Top = -1 & Bottom = +1)
- D: Leaf Type (Shagbark Hickory = -1 & Northern Red Oak = +1)
- E: Leaf Condition/Age (Red, October = -1 & Green, September = +1)

EVAPORATION EXPERIMENTS NO. 1 AND 2 SERIES 2\*\*4 FACTORIAL EXPERIMENT  
 DIETHYLMALONATE DROPS 2 MM DIA., 100 AND 1000 CP LIQUID VISCOSITY  
 NOMINAL CONTAMINATION DENSITY 30 G/SQ METER ON OAK AND HICKORY LEAVES  
 WINDSPEED 3 AND 11 MPH, AIR TEMPERATURE 60 DEG F., RELATIVE HUMIDITY 42%

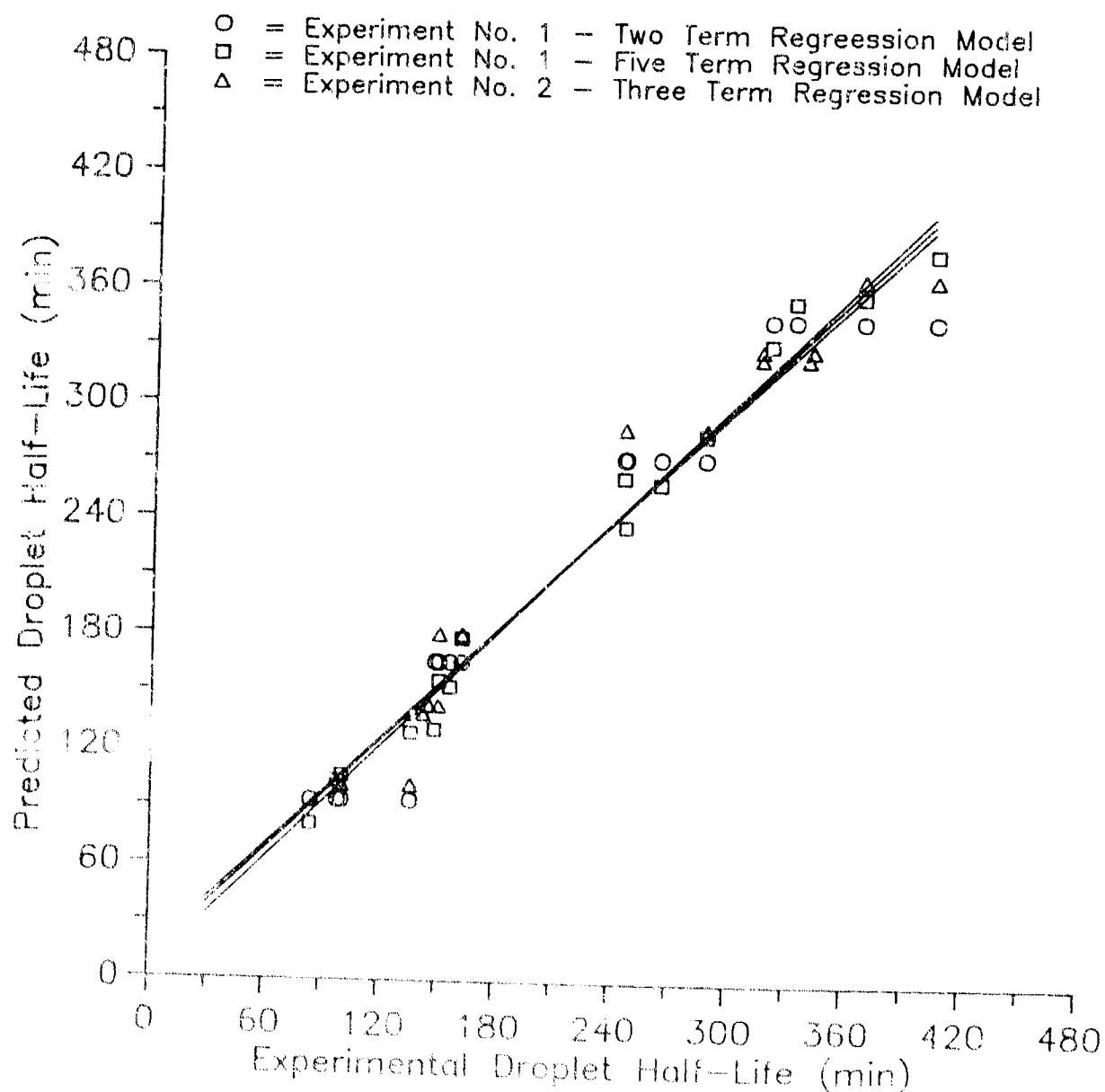


Figure P-1. Experimental versus Predicted Droplet Half -Life.